

ASSIGNMENT 3

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Problem 1

From previous assignment we found out that, Characteristic impedance is $\sqrt{\frac{R+j\omega L}{G+j\omega C}}$. Here it is given that

$\frac{L}{R} = \frac{C}{G}$ which means $z_0 = \sqrt{\frac{R}{G}} \Omega$.

Propagation constant is $\gamma = \sqrt{(R+j\omega L)(G+j\omega C)} = \sqrt{RG} + j\omega\sqrt{LC} = \alpha + j\beta$

Phase velocity is $V_p = \frac{\omega}{\beta} = 1/\sqrt{LC}$

Observations

- The characteristic impedance of the line is purely resistive.
- z_0 does not depend on the frequency of operation.
- α is frequency independent.
- β is linear function of ω .
- Phase velocity is same at all frequency which means the line is **Distortion less**.

Problem 2

Given lossless transmission line with a load Z_L

$$\begin{aligned} Z_{in}(x) &= z_0 \frac{1 + \Gamma_L e^{-2\gamma x}}{1 - \Gamma_L e^{-2\gamma x}} \\ \Gamma_L &= \frac{Z_L - z_0}{Z_L + z_0} \\ Z_{in}(-l/4) &= z_0 \frac{1 + \Gamma_L e^{2j\frac{2\pi}{\lambda} \frac{\lambda}{4}}}{1 - \Gamma_L e^{2j\frac{2\pi}{\lambda} \frac{\lambda}{4}}} \\ \Rightarrow Z_{in} &= z_0 \frac{1 - \frac{Z_L - z_0}{Z_L + z_0}}{1 + \frac{Z_L - z_0}{Z_L + z_0}} \\ \Rightarrow Z_{in} &= \frac{z_0^2}{Z_L} \end{aligned}$$

Problem 3

First we calculate Z_{in} .

$$Z_{in}(-l) = z_0 \frac{1 + \Gamma_L e^{2\gamma l}}{1 - \Gamma_L e^{2\gamma l}}$$

$$\Rightarrow \boxed{V_{in} = V_s \frac{Z_{in}}{z_0 + Z_{in}} = V_s \frac{1 + \Gamma_L e^{2\gamma l}}{2}} \quad (1)$$

$$V_o = V(0) \quad (2)$$

$$V_{in} = V(-l) \quad (3)$$

$$\Rightarrow \frac{V_o}{V_{in}} = \frac{V_o^+ (1 + \Gamma_L)}{V_o^+ e^{-\gamma l} (1 + \Gamma_L e^{2\gamma l})} = \frac{1 + \Gamma_L}{e^{-\gamma l} + e^{\gamma l} \Gamma_L} \quad (4)$$

$$\Rightarrow \boxed{V_o = V_s \frac{1 + \Gamma_L}{2} e^{\gamma l}} \quad (5)$$

For maximising V_o ,

$$\frac{\partial V_o}{\partial Z_L} = 0 \quad (6)$$

$$\frac{\partial \left(V_s \frac{Z_L}{Z_L + z_o} e^{\gamma l} \right)}{\partial Z_L} = 0 \quad (7)$$

$$\Rightarrow \frac{1}{(Z_L + z_o)^2} = 0 \quad (8)$$

$$\Rightarrow \boxed{Z_L \rightarrow \infty} \quad (9)$$

$$\frac{\partial^2 V_o}{\partial Z_L^2} @ Z_L \rightarrow \infty < 0 \Rightarrow \text{It is local maxima.} \quad (10)$$

Thus the keeping a open circuit near load will maximise the

$$\boxed{V_o = V_s e^{\gamma l}}$$

and corresponding

$$\boxed{V_{in} = V_s \frac{1 + e^{2\gamma l}}{2}}$$