

Mechanics of Structures 2 Project Report

Analysis of Strap Handle in Public Transport

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0. Introduction

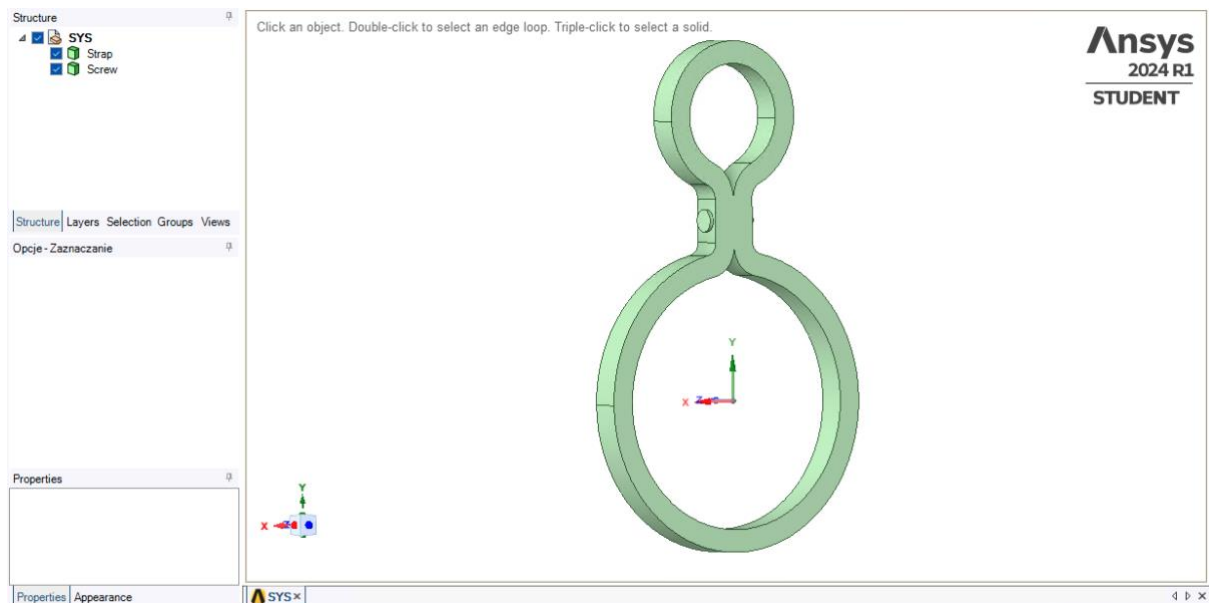
Objective of this report, is to analyze the structural behaviour of a strap handle used in public transport under the applied load of a person hanging from it.

The project will draw inspiration from available data, particularly referencing materials and suggested loading conditions as provided by Faigle's IGOSTRAP handle design and their official webpage descriptions.

Hence, vertical load of 1500N, and bolt pretension of 2650N will be applied to strap made of polyurethane, and bolt made of stainless steel.

1. The geometry, geometrical simplifications and materials.

Geometry will be simplified to more circular shape adjusted with a bolt to obtain a form of asymmetrical number eight. Such change should retain real-world case's properties.



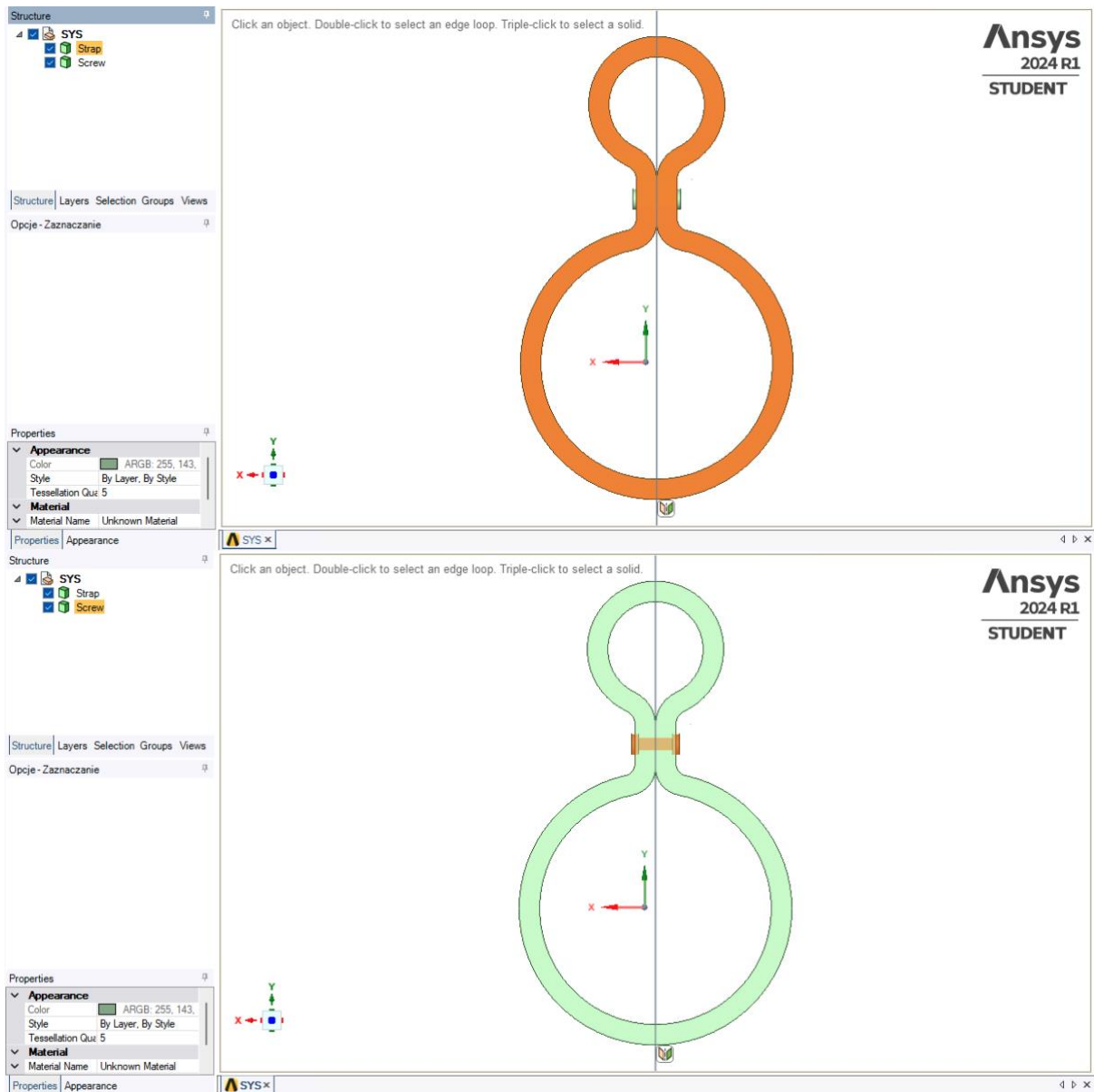


Fig. 1. Strap and bolt model made in SpaceClaim.

Dimensions:

Strap

Big outer diameter = 80mm

Small outer diameter = 40mm

Distance between inner and outer circles = 6mm

Distance between big and small circle = 15mm

Thickness = 8mm

Bolt M3,5, nut diameter = 6mm

According to the Faigle's IGOSTRAP design [1], the strap is made of PAS-PU 90A-H [2], and the bolt is made of stainless steel.

| Properties of Outline Row 3: PAS-PU 90A-H | | | | | |
|---|---------------------------|------------|--------------------|---|---|
| | A | B | C | D | E |
| 1 | Property | Value | Unit | | |
| 2 | Material Field Variables | Table | | | |
| 3 | Density | 1,15 | g cm ⁻³ | | |
| 4 | Isotropic Elasticity | | | | |
| 5 | Derive from | Young... | | | |
| 6 | Young's Modulus | 6 | MPa | | |
| 7 | Poisson's Ratio | 0,43 | | | |
| 8 | Bulk Modulus | 1,4286E+07 | Pa | | |
| 9 | Shear Modulus | 2,0979E+06 | Pa | | |
| 10 | Tensile Yield Strength | 50 | MPa | | |
| 11 | Tensile Ultimate Strength | 100 | MPa | | |

| Properties of Outline Row 4: Stainless Steel | | | | | |
|--|---|------------|--------------------|---|---|
| | A | B | C | D | E |
| 1 | Property | Value | Unit | | |
| 2 | Material Field Variables | Table | | | |
| 3 | Density | 7750 | kg m ⁻³ | | |
| 4 | Isotropic Secant Coefficient of Thermal Expansion | | | | |
| 5 | Coefficient of Thermal Expansion | 1,7E-05 | C ⁻¹ | | |
| 6 | Isotropic Elasticity | | | | |
| 7 | Derive from | Youn... | | | |
| 8 | Young's Modulus | 1,93E+11 | Pa | | |
| 9 | Poisson's Ratio | 0,31 | | | |
| 10 | Bulk Modulus | 1,693E+11 | Pa | | |
| 11 | Shear Modulus | 7,3664E+10 | Pa | | |
| 12 | Tensile Yield Strength | 2,07E+08 | Pa | | |
| 13 | Compressive Yield Strength | 2,07E+08 | Pa | | |
| 14 | Tensile Ultimate Strength | 5,86E+08 | Pa | | |
| 15 | Compressive Ultimate Strength | 0 | Pa | | |

Fig. 2. Material details.

2. The boundary conditions

Fixed support will be applied to bottom face of the top part of the model, where it would hang on the pipe.

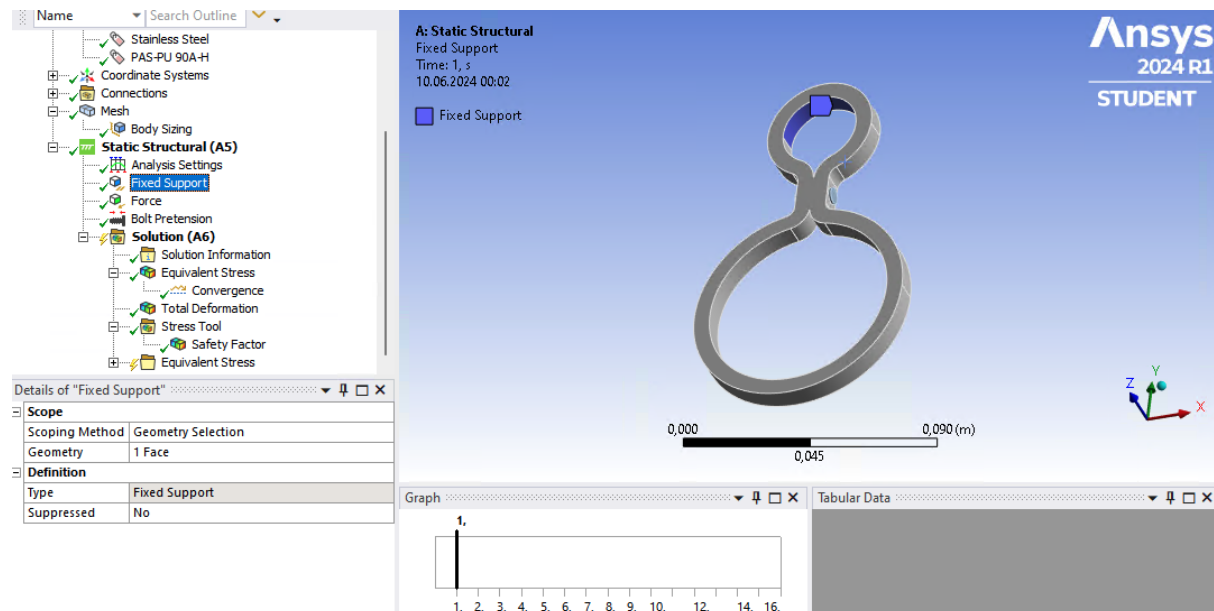


Fig. 3. Fixed support applied to the strap's face.

IGOSTRAP is designed to withstand loads of up to 150kg.

Hence, load of 1500N will be applied at the bottom face of the part.

Load was applied linearly, at each step increasing by 100N up to 1500N, to better identify significant deformations or stress concentrations.

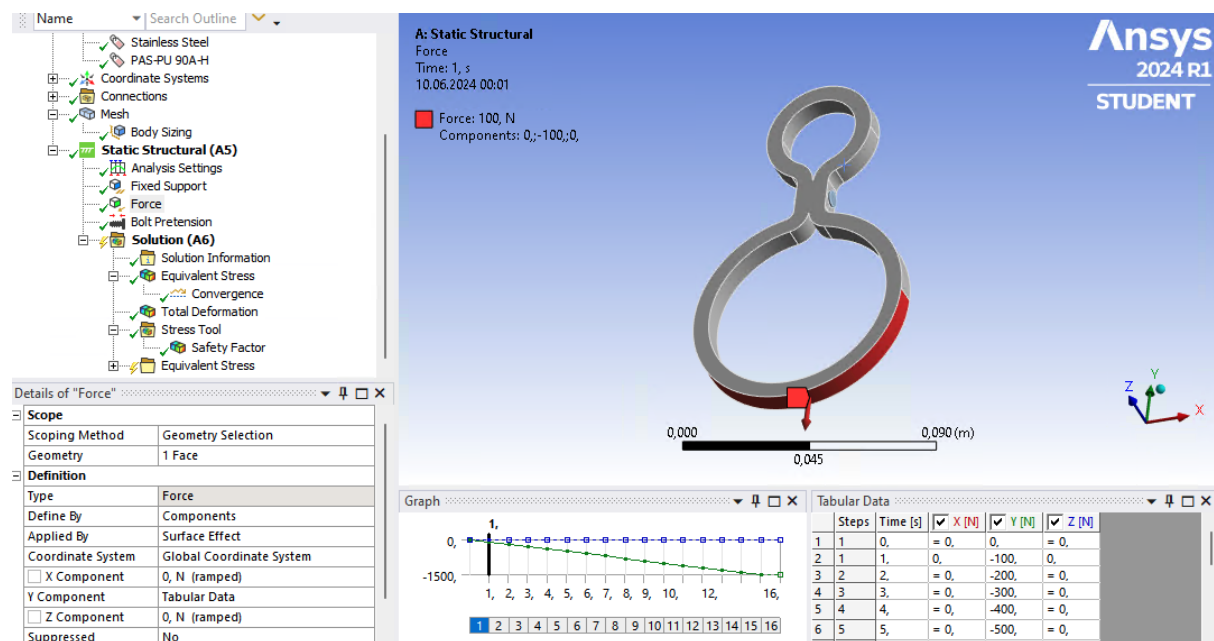


Fig. 4. Force of 1500N applied to the strap's bottom face.

Bolt pretension of 2650N will be applied, according to minimized values from TSF's table of preloads [3].

After first step, the load get Locked.

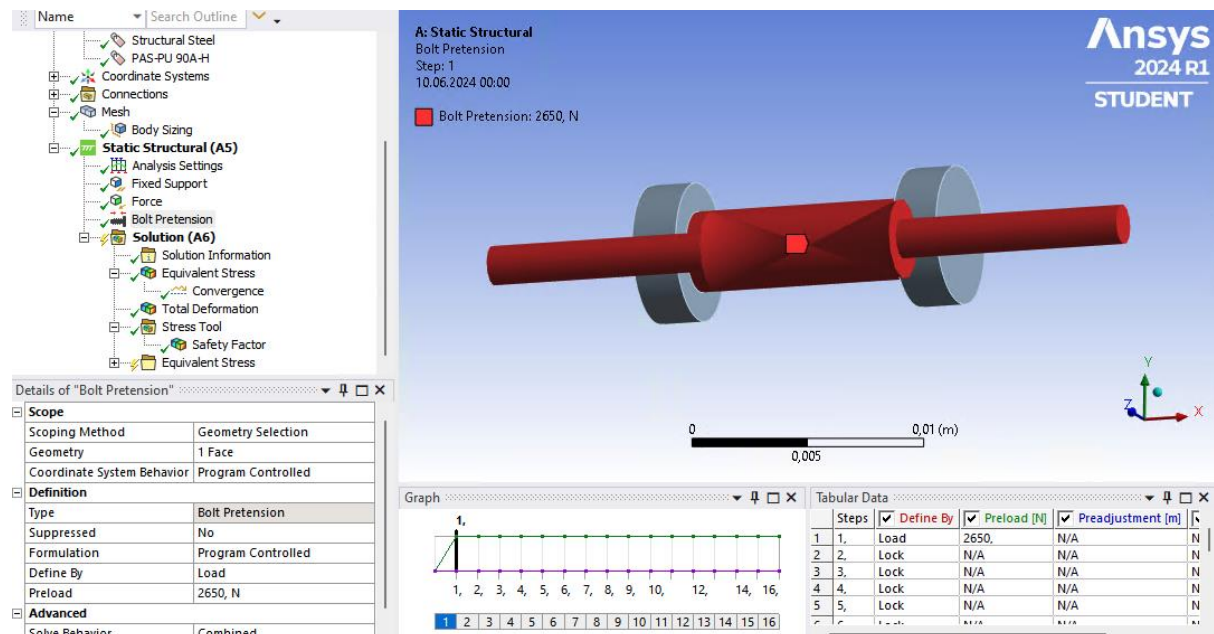
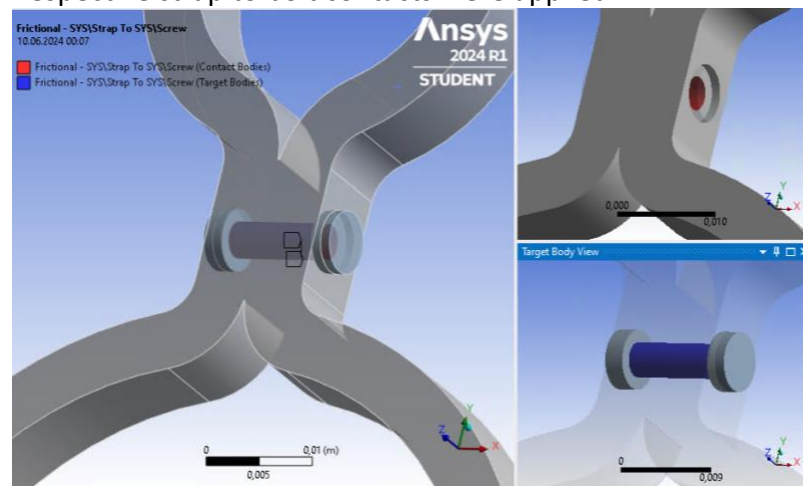


Fig. 5. Bolt pretension of 2650N applied to bolt.

Respective strap to bolt contacts were applied.



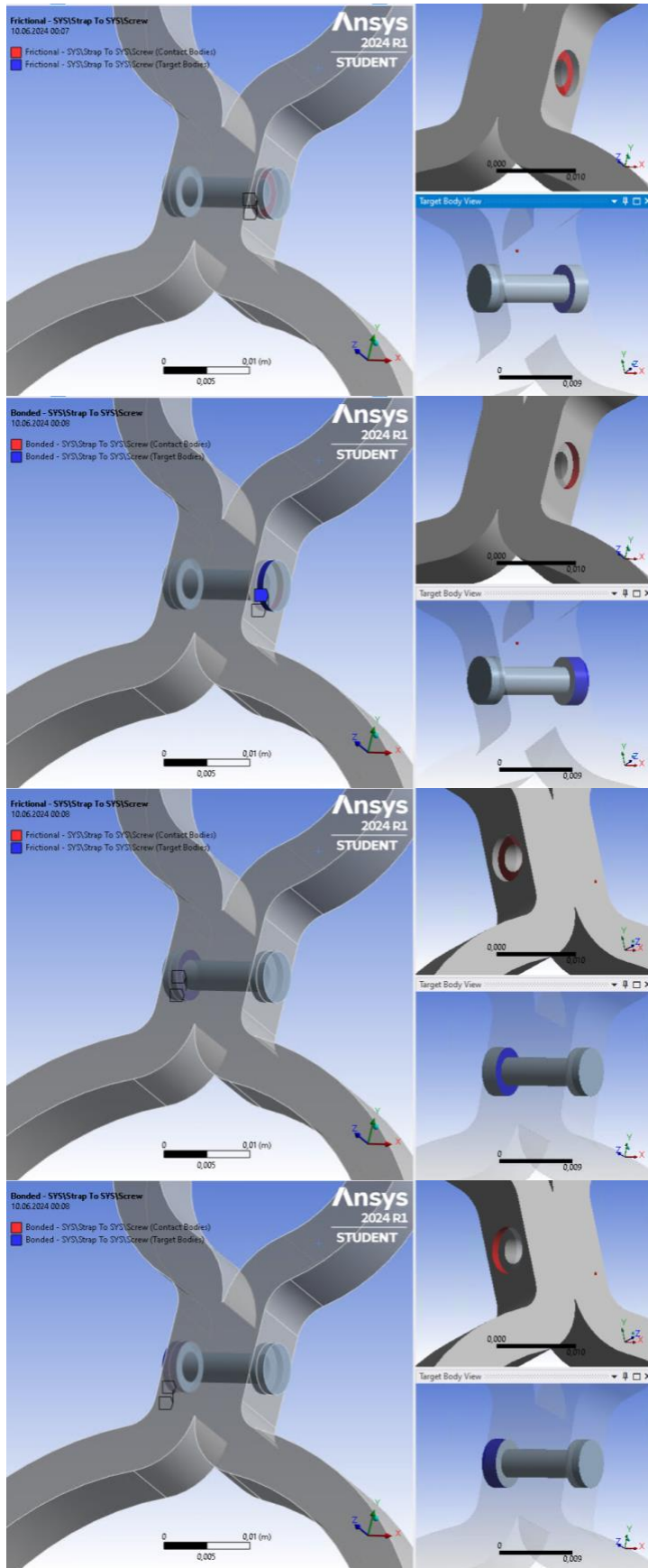


Fig. 6. Applied strap to bolt contacts.

2. The mesh

After applying Body Sizing element size to 4e-03mm to strap, automatically made mesh seemed sufficient, denser near bolt part, more widely distributed on outer parts.

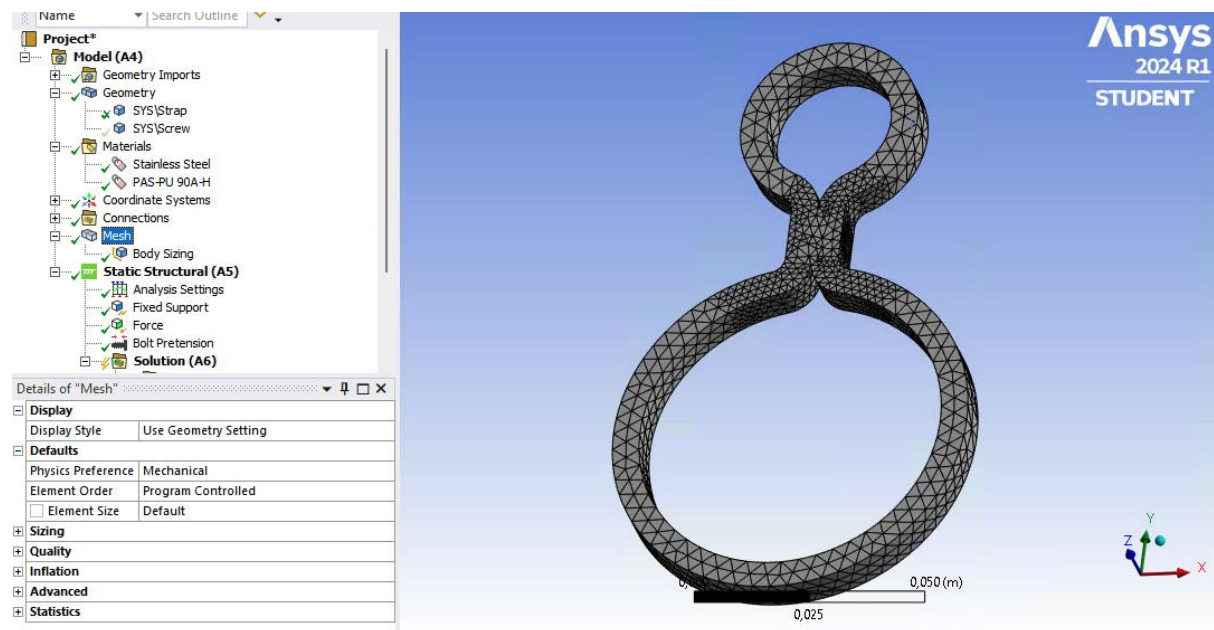


Fig. 7. Strap's mesh.

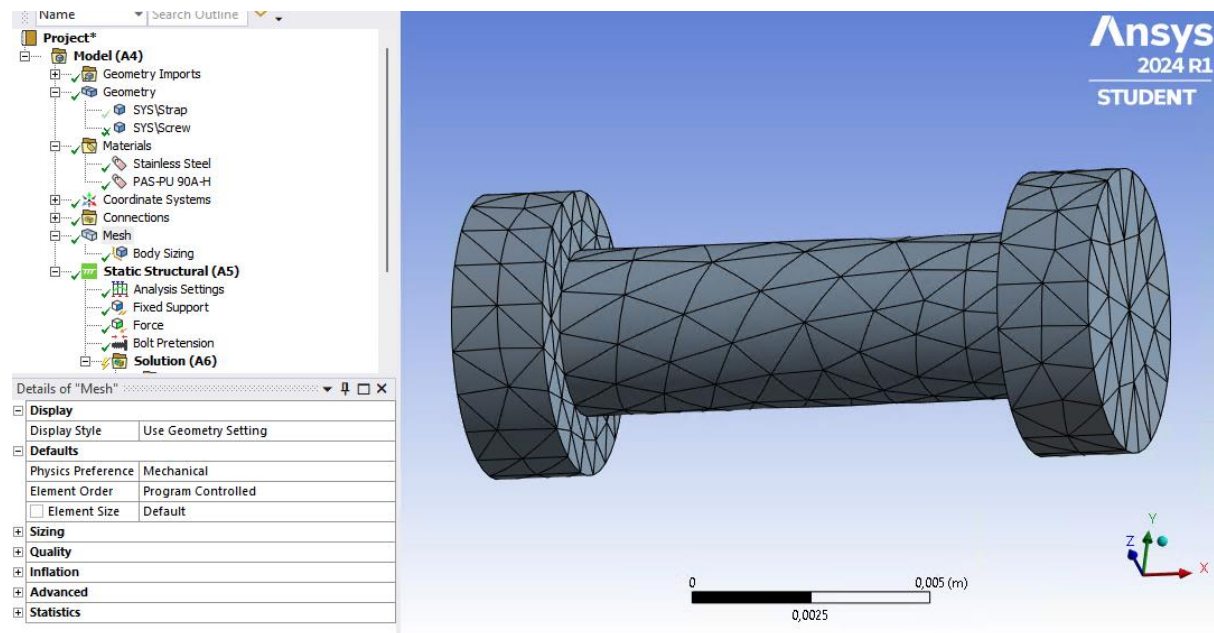


Fig. 8. Bolt's mesh.

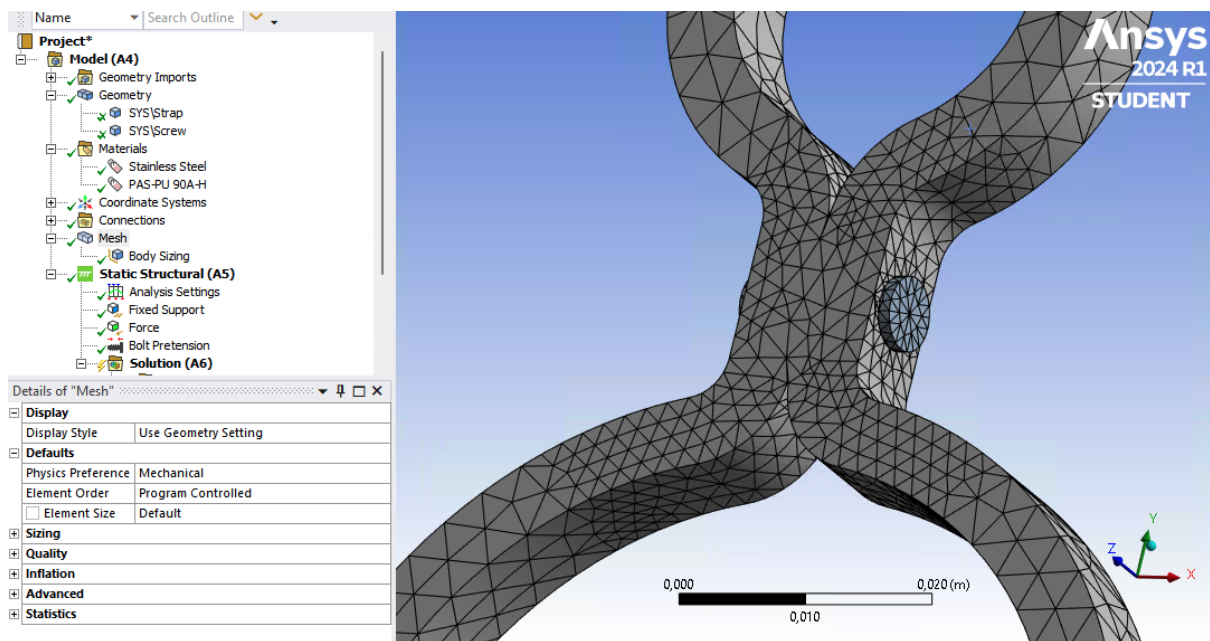


Fig. 9. Mesh on both bodies.

| | |
|---|----------------------------|
| Sizing | |
| Use Adaptive Sizing | Yes |
| Resolution | Default (2) |
| Mesh Defeaturing | Yes |
| <input type="checkbox"/> Defeature Size | Default |
| Transition | Fast |
| Span Angle Center | Coarse |
| Initial Size Seed | Assembly |
| Bounding Box Diagonal | 0,15799 m |
| Average Surface Area | 2,8932e-004 m ² |
| Minimum Edge Length | 1,e-004 m |
| Quality | |
| Check Mesh Quality | Yes, Errors |
| Error Limits | Aggressive Mechanical |
| <input type="checkbox"/> Target Element Quality | Default (5,e-002) |
| Smoothing | Medium |
| Mesh Metric | None |
| Statistics | |
| <input type="checkbox"/> Nodes | 6911 |
| <input type="checkbox"/> Elements | 3503 |
| Show Detailed Statistics | No |

Fig. 10. Mesh details.

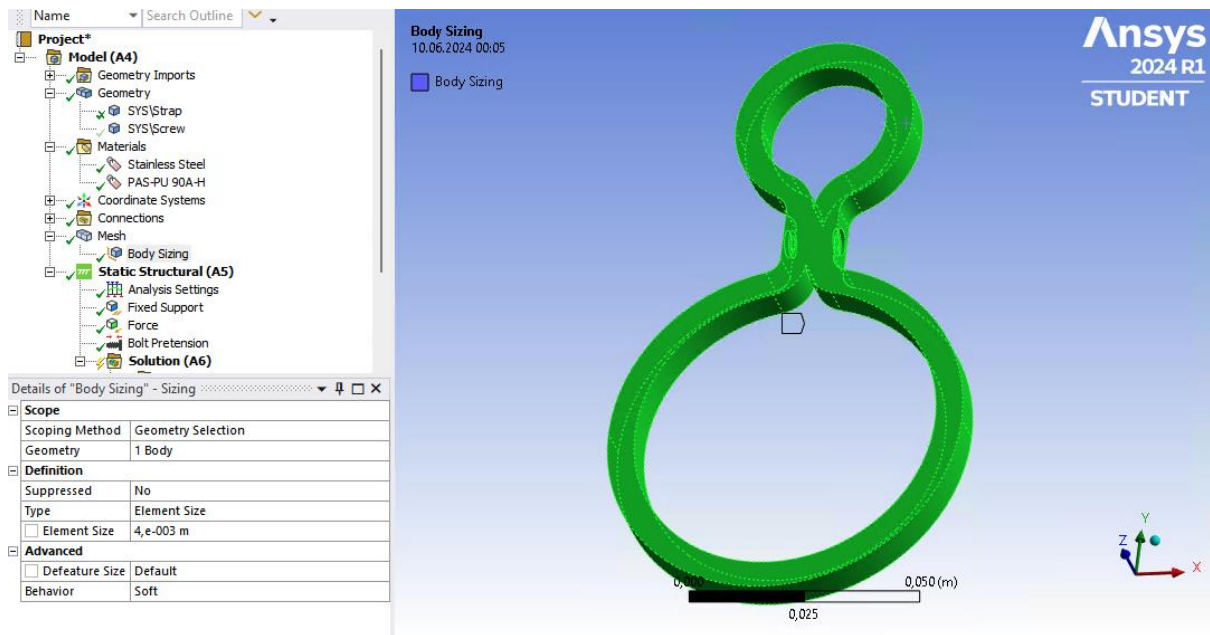


Fig. 11. Strap's mesh element size.

4. Deformation

Total deformation solution was performed. Analysis settings were set to 16 steps.

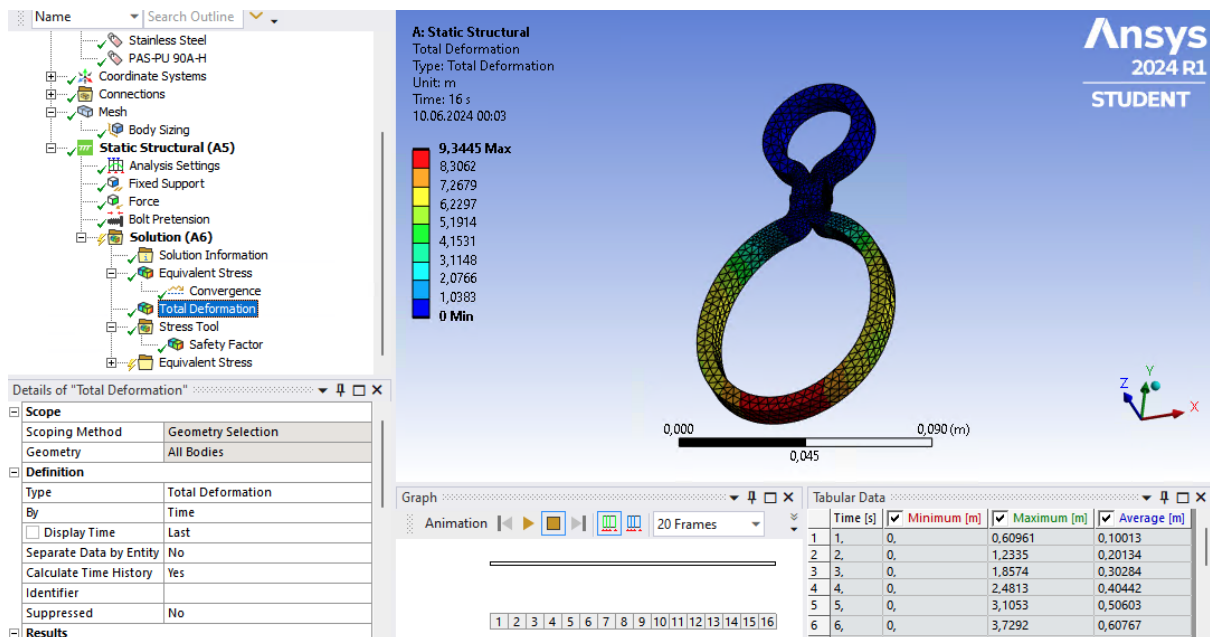


Fig. 12. Total deformation.

Obtained table:

| Step | Maximum [m] |
|------|-------------|
| 1 | 0,60961 |
| 2 | 1,2335 |
| 3 | 1,8574 |
| 4 | 2,4813 |
| 5 | 3,1053 |
| 6 | 3,7292 |
| 7 | 4,3531 |
| 8 | 4,977 |
| 9 | 5,6009 |
| 10 | 6,2249 |
| 11 | 6,8488 |
| 12 | 7,4727 |
| 13 | 8,0967 |
| 14 | 8,7206 |
| 15 | 9,3445 |
| 16 | 9,3445 |

Obtained plot:

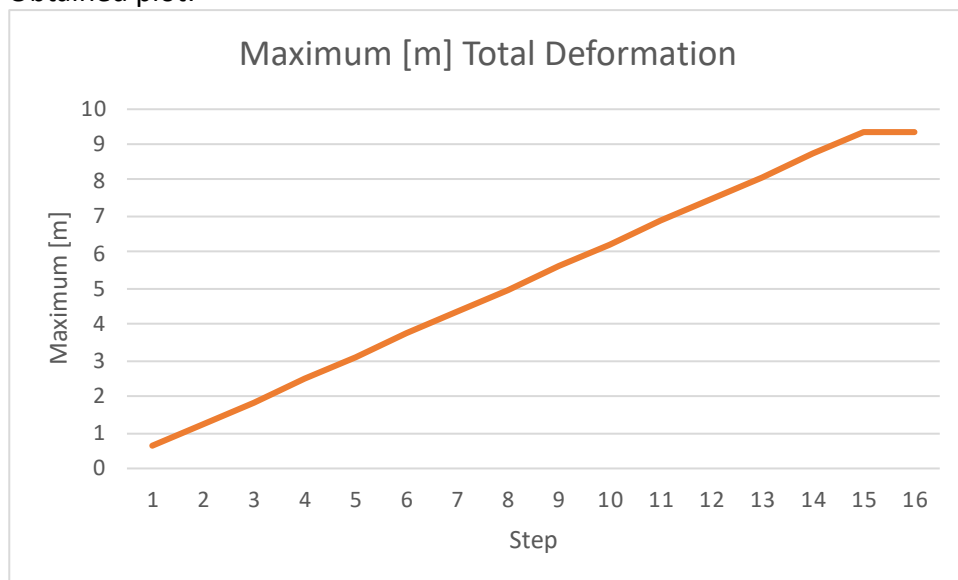


Fig. 13. Maximum [m] Total Deformation.

Maximum total deformation seems to be linear along all steps.

5. Stress

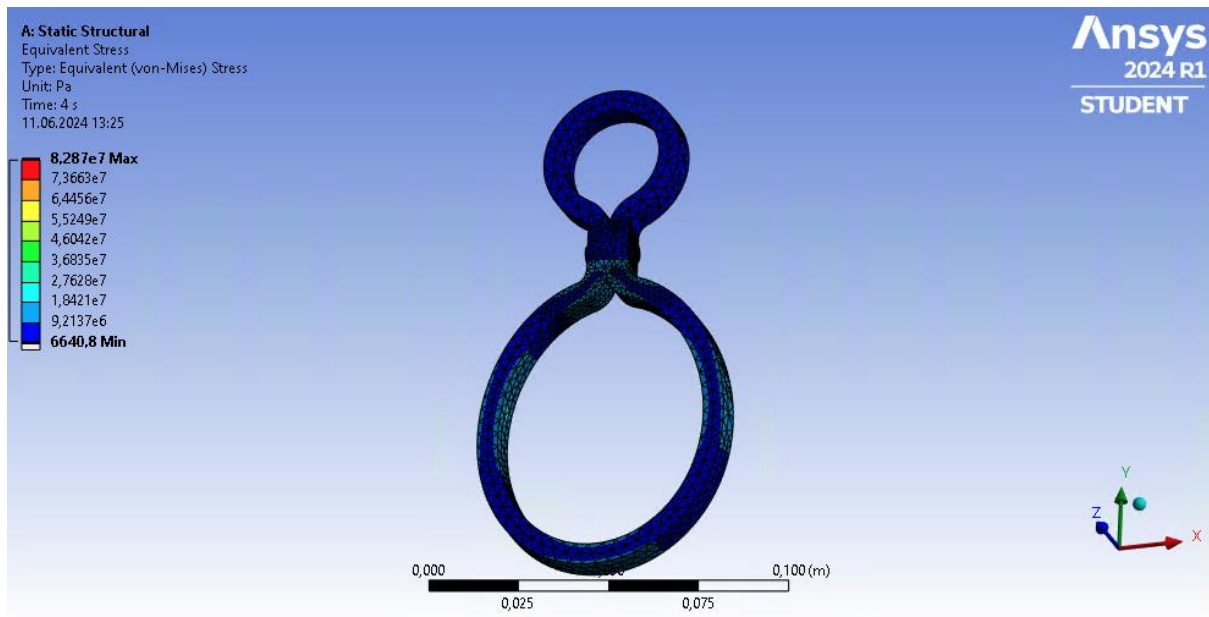


Fig. 14. Equivalent stress.

Obtained table:

| Step | Minimum [Pa] | Maximum [Pa] |
|------|--------------|--------------|
| 1 | 6154,3 | 5,5247e+006 |
| 2 | 13477 | 1,1049e+007 |
| 3 | 15945 | 1,6574e+007 |
| 4 | 18868 | 2,2099e+007 |
| 5 | 22740 | 2,7623e+007 |
| 6 | 27161 | 3,3148e+007 |
| 7 | 31902 | 3,8673e+007 |
| 8 | 36839 | 4,4197e+007 |
| 9 | 41905 | 4,9722e+007 |
| 10 | 47055 | 5,5247e+007 |
| 11 | 52267 | 6,0771e+007 |
| 12 | 57522 | 6,6296e+007 |
| 13 | 62812 | 7,1821e+007 |
| 14 | 68126 | 7,7345e+007 |
| 15 | 73461 | 8,287e+007 |
| 16 | 73461 | 8,287e+007 |

Obtained plot:

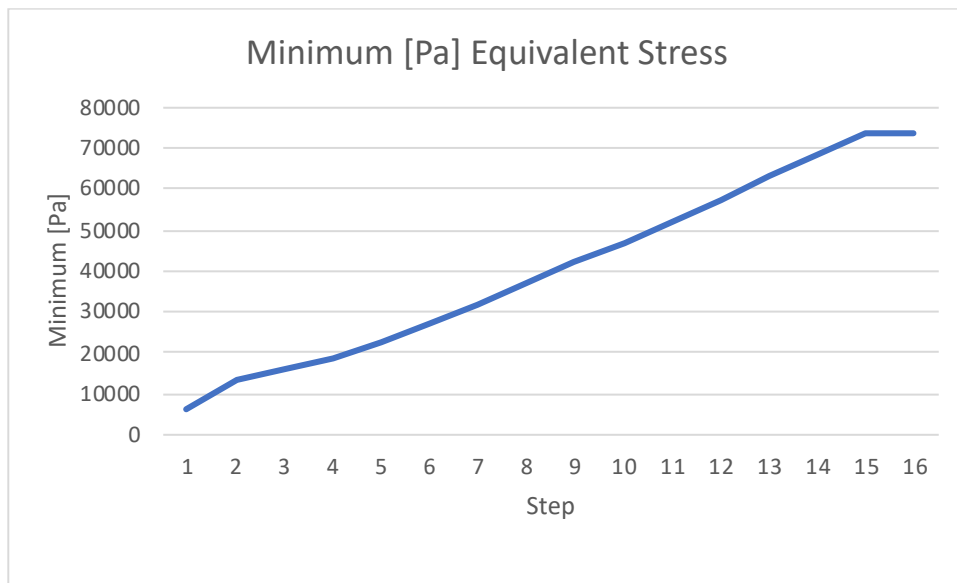


Fig. 15. Minimum [Pa] Equivalent Stress.

Minimum equivalent stress seems to have rapid increase at steps 1-2, stabilizing to linear at further steps.

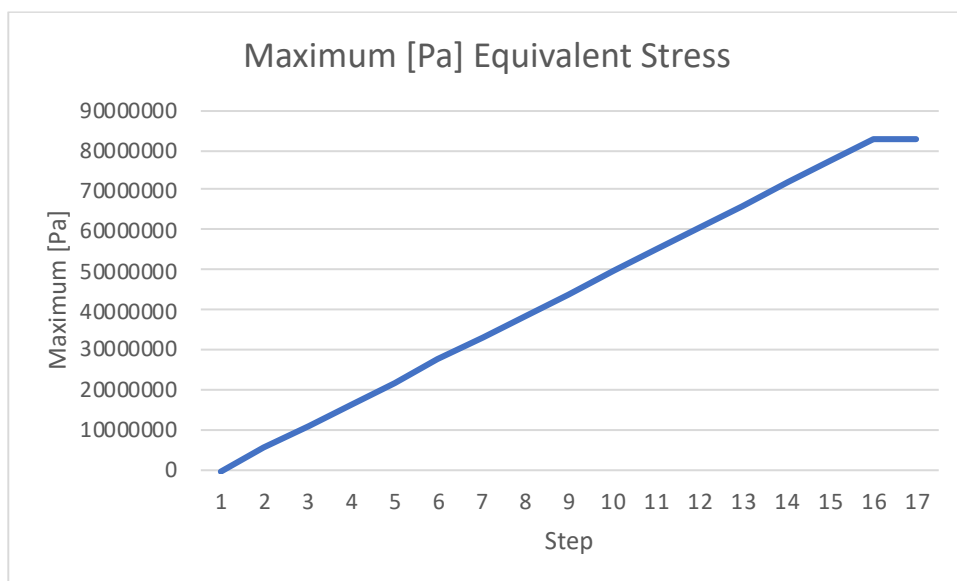


Fig. 16. Maximum [Pa] Equivalent Stress.

Maximum equivalent stress seems to be linear at all steps.

6. Safety factor

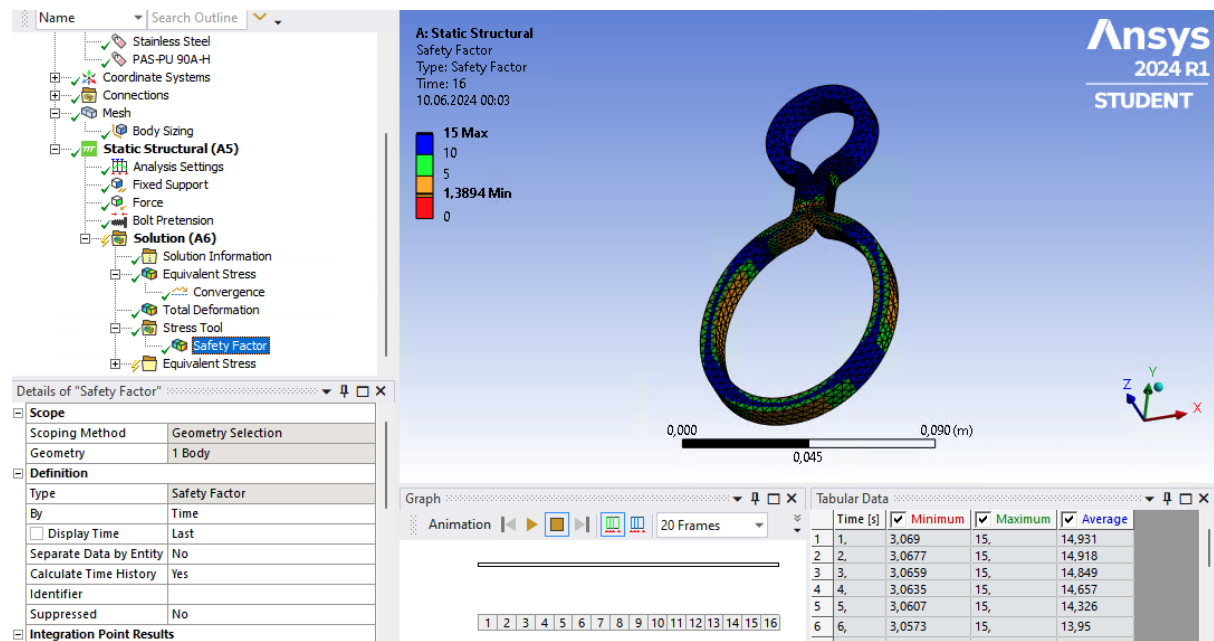


Fig. 17. Safety factor.

Obtained table:

| Step | Minimum |
|------|---------|
| 1 | 3,069 |
| 2 | 3,0677 |
| 3 | 3,0659 |
| 4 | 3,0635 |
| 5 | 3,0607 |
| 6 | 3,0573 |
| 7 | 2,9652 |
| 8 | 2,597 |
| 9 | 2,3102 |
| 10 | 2,0804 |
| 11 | 1,8922 |
| 12 | 1,7352 |
| 13 | 1,6023 |
| 14 | 1,4883 |
| 15 | 1,3894 |
| 16 | 1,3894 |

Obtained plot:

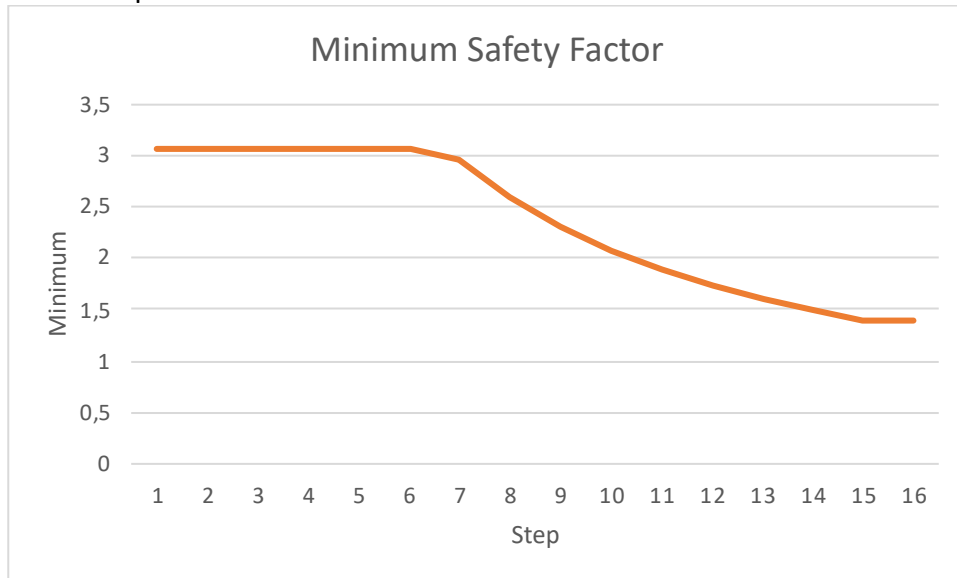


Fig. 18. Minimum Safety Factor.

Safety factor seems to drop at 7th step from being constant before that.

Safety factor of 1,39 was obtained at 1500N load.

7. Conclusions

The total deformation of the strap handle under a load of 1500N is within acceptable limits, ensuring it can safely support the weight of a user.

The equivalent stress remains below the material's yield strength, max stress being $8,3e+07$, material's tensile ultimate strength $100\text{MPa}=1e+08$, indicating that the handle will not fail under the specified loading conditions.

With a safety factor of 1.39, the handle is confirmed to be safe for use in public transport applications.

Further analysis could include fatigue testing to assess the handle's long-term performance.

8. References

[1] Faigle's IGOSTRAP description <https://www.faigle.com/en/local-public-transport-and-rail/hanging-straps/igostrap>

[2] Faigle's IGOSTRAP material <https://www.faigle.com/en/semi-finished-products-and-finished-parts/material-finder?material=pas-pu-90a-h>

[3] TSF Table of preloads and tightening approximate values
<https://www.tsftsh.com/docs/documentation/Precargas%20Web.pdf>

Static structural analysis was performed with ANSYS.

Plots were performed with Excel.