

Ch9. Further Analysis of finite deformation

9.1 Deformation of a surface element

* area expansion & surface normal direction



$$N dS = \frac{1}{2} dX^{(1)} \times dX^{(2)} \leftrightarrow N_R dS = \frac{1}{2} e_{RST} dX_S^{(1)} dX_T^{(2)}$$

$$n ds = \frac{1}{2} dx^{(1)} \times dx^{(2)} \leftrightarrow n_i ds = \frac{1}{2} e_{ijk} dx_j^{(1)} dx_k^{(2)} \\ = \frac{1}{2} e_{ijk} \frac{\partial x_j}{\partial X_S} \frac{\partial x_k}{\partial X_T} dX_S^{(1)} dX_T^{(2)} + o(dx^3)$$

$$n_i \frac{\partial x_i}{\partial X_R} ds = \frac{1}{2} e_{ijk} \frac{\partial x_i}{\partial X_R} \frac{\partial x_j}{\partial X_S} \frac{\partial x_k}{\partial X_T} dX_S^{(1)} dX_T^{(2)} + o(dx^3)$$

$$= \frac{1}{2} e_{RST} \det F dX_S^{(1)} dX_T^{(2)} + o(dx^3)$$

$$= \det F N_R dS + o(dx^3)$$

$$dX^{(1)}, dX^{(2)} \rightarrow 0, \quad n_i \frac{\partial x_i}{\partial X_R} \frac{ds}{dS} = \det F N_R \rightarrow N_R N_R = 1 = (\det F)^{-2} n_i \frac{\partial x_i}{\partial X_R} n_j \frac{\partial x_j}{\partial X_R} \left(\frac{ds}{dS}\right)^2$$

$$\rightarrow \left(\frac{ds}{dS}\right)^2 = \frac{(\det F)^2}{n_i B_{ij} n_j} \quad \text{or} \quad N \det F = n \cdot F \left(\frac{ds}{dS}\right) \quad \& \quad \left(\frac{ds}{dS}\right)^2 = \frac{(\det F)^2}{n \cdot B \cdot n}$$

Similarly, $N \det F^{-1} = n \cdot F^{-1} \frac{dS}{ds} \quad \text{and} \quad \left(\frac{dS}{ds}\right)^2 = \frac{(\det F^{-1})^2}{n \cdot C^{-1} \cdot n}$ 10/30 2421

9.2 Decomposition of a deformation

Recall polar decomposition theorem

$$F = R \cdot U = V \cdot R \quad (R: \text{orthogonal}, \quad U \& V: \text{positive-definite, symmetric})$$

$$\text{Also, } \det F > 0 \quad (\text{since } \det F = \frac{\rho}{\rho_0}) \rightarrow R: \text{proper rotation (no inversion)}$$

$$U = R^T V R \leftrightarrow V = R U R^T$$

Components of F: all constant.

First, Consider the homogeneous deformation $x = F X$

Consider the two successive homogeneous deformation ($X \rightarrow \hat{x} \rightarrow x$)

$$\hat{x} = \underbrace{U}_{\text{Deformation}} \cdot X, \quad x = \underbrace{R}_{\text{Rotation}} \cdot \hat{x} \rightarrow x = R \cdot \hat{x} = R U X = F X$$

\therefore Any homogeneous deformation F can be decomposed into

① a deformation which correspond to the symmetric tensor, U followed by the rotation R . (늘리고, 돌리기)

② the same rotation R followed by a deformation, which correspond to the symmetric tensor V . (돌리고, 늘리기)

Next, if not homogeneous, $d\mathbf{x} = \mathbf{F} d\mathbf{X}$

$\mathbf{F}, \mathbf{R}, \mathbf{U}, \mathbf{V}$: function of position

local decomposition and rotation

\mathbf{R} : rotation tensor

\mathbf{U} : right stretch tensor

\mathbf{V} : left stretch tensor

$$\left. \begin{array}{l} \mathbf{U} \\ \mathbf{V} \end{array} \right\} \begin{array}{l} \mathbf{C} = \mathbf{F}^T \mathbf{F} = \mathbf{U}^2 \\ \mathbf{B} = \mathbf{F} \mathbf{F}^T = \mathbf{V}^2 \end{array}$$

(square root of eigenvalue)

Because \mathbf{U}, \mathbf{V} are symmetric & positive definite, we can recover \mathbf{U} from ①, \mathbf{V} from ②

$$\therefore \mathbf{U} \leftrightarrow \mathbf{C} \quad (\mathbf{C} = \mathbf{U}^2)$$

$$\mathbf{V} \leftrightarrow \mathbf{B} \quad (\mathbf{B} = \mathbf{V}^2)$$

↑
direct physical meaning

↑
easier to calculate

$$\mathbf{F} = \mathbf{I} + \mathbf{E} + \mathbf{\Delta}$$

infinitesimal strain tensor
($= \frac{\mathbf{F} + \mathbf{F}^T}{2} - \mathbf{I}$)

infinitesimal rotation tensor
($= \frac{\mathbf{F} - \mathbf{F}^T}{2}$)

$$\mathbf{U}^2 = \mathbf{F}^T \mathbf{F} = (\mathbf{I} + \mathbf{E} - \mathbf{\Delta})(\mathbf{I} + \mathbf{E} + \mathbf{\Delta}) \simeq \mathbf{I} + 2\mathbf{E}$$

$$\rightarrow \boxed{\mathbf{U} \simeq \mathbf{I} + \mathbf{E}} \quad \text{Similarly, } \boxed{\mathbf{V} \simeq \mathbf{I} + \mathbf{E}}$$

$$\therefore \mathbf{U} - \mathbf{I} = \mathbf{V} - \mathbf{I} = \mathbf{E} \quad (\text{small deformation rotation})$$

$$\text{Also, } \mathbf{U}^{-1} = \mathbf{I} - \mathbf{E}$$

$$\mathbf{R} = \mathbf{F} \mathbf{U}^{-1} \simeq (\mathbf{I} + \mathbf{E} + \mathbf{\Delta}) \cdot (\mathbf{I} - \mathbf{E}) \simeq \mathbf{I} + \mathbf{\Delta} \quad \therefore \boxed{\mathbf{R} - \mathbf{I} \simeq \mathbf{\Delta}}$$

9.3 Principal stretch & principal axes of deformation

Recall : line element, $\lambda \tilde{\mathbf{a}} = \mathbf{F} \cdot \tilde{\mathbf{A}}$ (unit vector),
stretch

$$\mathbf{F} \rightarrow \mathbf{U}, \quad \lambda \mathbf{a} = \mathbf{U} \cdot \mathbf{A}$$

$$\text{If } \mathbf{a} = \mathbf{A} \text{ (no rotation during } \mathbf{U}), \quad \underline{(\mathbf{U} - \lambda \mathbf{I}) \mathbf{A} = \mathbf{0}}$$

λ : principal value of \mathbf{U} (λ : real and positive)

\mathbf{A} : principal direction of \mathbf{U} .

(Since \mathbf{U} is symmetric,)

$\lambda_1 \geq \lambda_2 \geq \lambda_3$: principal stretches

$\mathbf{A}_1, \mathbf{A}_2, \mathbf{A}_3$: principal axes (mutually orthogonal)

if chosen to be coord. axes.

$$\rightarrow (\mathbf{U}_{RS}) = \begin{pmatrix} \lambda_1 & & \\ & \lambda_2 & \\ & & \lambda_3 \end{pmatrix}$$

- If the principal axes of U are chosen to be the coord axes,

$$(U_{RS}) = \begin{pmatrix} \lambda_1 & & \\ & \lambda_2 & \\ & & \lambda_3 \end{pmatrix}$$

$F = R U$: consists of these 3 extension followed by the rotation R . ($U \cdot A = \lambda A$)

$F = U R$: rotation R followed by 3 extension represented by U . ($F \cdot A = \lambda R \cdot A$)

$R A$ should be the principal axes of U . $U(R A) = \lambda(R A)$

$\therefore \lambda_1, \lambda_2, \lambda_3$: principal stretches of U , and also the principal values of U ,
and the corresponding principal directions are $R \cdot A_1, R \cdot A_2, R \cdot A_3$.

(U 와 U 의 principal stretch λ_i
but principal axes는 A_1, A_2, A_3 or $R A_1, R A_2, R A_3$ 로 변경)

$$C = F^T F = U^2, \quad \gamma = \frac{1}{2}(C - I) \leftarrow A_i = \lambda_i^2, \frac{\lambda_i^2 - 1}{2}$$

$$B = F F^T = U^2, \quad \eta = \frac{1}{2}(I - B^{-1}) \leftarrow R \cdot A_i = \lambda_i^2, \frac{1 - \lambda_i^2}{2}$$

Given F , easier to calculate C & B than U & V .

- Alternative way of interpretation

$$\text{From } U \cdot A = \lambda A, \quad \|A\| U^T U \|A\| = \lambda^2 \rightarrow A_R A_S C_{RS} = \lambda^2$$

Given direction A , we can calculate λ , extension ratio.

Q. When is the extremal value of λ^2 or $A_R C_{RS} A_S$ under the constraint of $A_R A_R = 1$?

$$\frac{d}{dA_R} \{ A_R A_S C_{RS} - \mu^2 (A_R A_R - 1) \} = 0 \quad (\text{라그랑주 승수법})$$

$$\text{Using } C_{RS} = C_{SR}, \quad (C_{RR} - \mu^2 \delta_{RR}) A_R = 0$$

\therefore The directions of A for which λ^2 is extremal are the principal direction of C .

The corresponding values of λ^2 are the principal values of C .

Similar analysis for B : $U A = \lambda A \rightarrow R U A = \lambda R A$

$N \cdot (R A) = \lambda(R A)$, also principal values of B .

9.4 Strain invariants

$\lambda_1, \lambda_2, \lambda_3$: invariants (i.e., independent of the reference frame)

↳ principal values of IU and IV.

$\lambda_1^2, \lambda_2^2, \lambda_3^2$: principal values of C and B.

IR (principal axes of C) = (principal axes of B)

$$\text{or } IU^2 = C, IU = \sqrt{C}, IR = IFM^{-1} = FC^{-\frac{1}{2}}$$

$$C = M^T D M \rightarrow C^{-\frac{1}{2}} = M^T D^{-\frac{1}{2}} M \quad (11/1 \text{ 과제})$$

9.5 Alternative Stress measures

T_{ij} : stress in the current config

In some cases, more convenient to describe in the reference config.

$$\begin{cases} N \det F = n F \frac{dS}{dS'} \\ n \det F^{-1} = N \cdot F^{-1} \frac{dS'}{dS} \end{cases}$$

reference config surface normal $e_R \xrightarrow{\text{deform}} n_R$ in current config.

$$\underline{n_R = (\det F) \frac{dS'}{dS} e_R F^{-1}}$$

The force on this deformed surface : $\Pi_R dS'$ (7.4)

$$\Pi_R = \Pi_{Ri} e_i \rightarrow \Pi_R dS' = n_R \cdot \Pi dS \rightarrow [\Pi_{Rj} e_j dS' = (\det F) \frac{dS'}{dS} e_R \cdot F^{-1} \cdot \Pi dS] e_i$$

$$\rightarrow \Pi_{Ri} = (\det F) F^{-1}_{Rj} T_{ji}, \text{ or, } \boxed{\Pi = (\det F) F^{-1} \cdot \Pi \leftrightarrow \Pi = (\det F)^{-1} F \cdot \Pi}$$

Π : (nominal stress tensor
(first Piola-Kirchhoff stress tensor))

$$\#^{(N)} = N \cdot \Pi \quad (\text{cf. } \#^{(n)} = n \cdot \Pi)$$

$$\underline{\text{Equation of motion}} : \frac{d\Pi_{Ri}}{dx_R} + \rho_0 b_i = \rho_0 f_i \quad (\text{cf. } \frac{d}{dx_i} T_{ij} + \rho b_j = \rho f_j)$$

Torque equation : should have references to x → NOT useful.

$$\Pi_{Ri} \neq \Pi_{iR}$$

The second Piola-Kirchhoff tensor $IP \rightarrow P_{RS}$

$$P = \Pi \cdot (F^{-1})^T = (\det F) F^{-1} \cdot \Pi \cdot (F^{-1})^T \rightarrow \text{Symmetric but no direct interpretation.}$$

$$\rightarrow \Pi = P \cdot F^T, \quad \Pi = (\det F)^{-1} F P F^T$$