

Fusion Plasma Theory 2

Lecture 20 - 21 : Chapman - Enskog - Braginskii

① Chapman - Enskog process

- Asymptotic expansions of the Boltzmann Kinetic equation
- follows a hierarchy of temporal and spatial scales
and solves the kinetic equation order by order in the scale separations.

- Time-scale ordering by Chapman - Enskog

$$\frac{Df}{Dt} \equiv \frac{df}{dt} + \vec{v} \cdot \vec{\nabla} f + \vec{a} \cdot \frac{df}{d\vec{v}} = C[f]$$

Ordering by Knudsen number $K_n \equiv \frac{\lambda_{mfp}}{L} \equiv \epsilon \ll 1$

and $v \gg v_t / L \gg D / L^2 \quad (\Leftrightarrow t_0 \ll t_1 \ll t_2)$

$$\left\{ \begin{array}{l} t_0 \sim v^{-1} : \text{collisional transport} \\ t_1 \sim L/v_t \sim (L/\lambda_{mfp})(\lambda_{mfp}/v_t) \sim (L/\lambda_{mfp})v^{-1} \sim t_0/\epsilon : \text{non-dissipative time-scale} \\ t_2 \sim D/L^2 \sim (L^2/\lambda_{mfp}^2)v^{-1} \sim t_0/\epsilon^2 : \text{dissipative and transport time scale.} \end{array} \right. \quad \text{(MHD)}$$

- Multi-scale analysis in Chapman - Enskog

$$\left(\frac{D}{Dt_0} + \epsilon \frac{D}{Dt_1} + \epsilon^2 \frac{D}{Dt_2} \right) (f_0 + \epsilon f_1 + \epsilon^2 f_2 + \dots) = C[f_0 + \epsilon f_1 + \epsilon^2 f_2 + \dots]$$

i) Zeroth-order

$$\frac{Df_0}{Dt_0} = C[f_0] \quad \leftarrow \text{We will drop this by assuming kinetic equilibrium.} \quad \frac{D}{Dt_0}$$

(this happens instantaneously in the subsidiary time scales)

To go for next-orders, consider the collisional operator expansion first

$$\begin{aligned} C[f] &= C[f_0 + \epsilon f_1 + \epsilon^2 f_2 + \dots, f_0 + \epsilon f_1 + \epsilon^2 f_2 + \dots] \\ &= \underbrace{C[f_0, f_0]}_{C[f_0]} + \epsilon \left(\underbrace{C[f_0, f_1] + C[f_1, f_0]}_{\hat{C}f_1} \right) + \epsilon^2 \left(\underbrace{C[f_0, f_2] + C[f_2, f_0]}_{\hat{C}f_2} + \underbrace{C[f_1, f_1]}_{C[f_1]} \right) \end{aligned}$$

Resulting equations :

$$\left\{ \begin{array}{l} 0 = C[f_0] \\ \frac{Df_0}{Dt_1} = \hat{C}f_1 \\ \frac{Df_0}{Dt_2} + \frac{Df_1}{Dt_1} = \hat{C}f_2 + C[f_1] \end{array} \right\}$$

$D = C[f_0]$ gives local Maxwellian:

$$f_M(\vec{x}, t) = n(\vec{x}, t) \left(\frac{m}{2\pi T(\vec{x}, t)} \right)^{3/2} \exp \left(-\frac{\vec{v} - \vec{u}(\vec{x}, t)}{2T(\vec{x}, t)} \right)$$

An important assumption is that n, \vec{u}, T are true values, which are consistent with the total distribution function.

Let's put $f_0 = f_M$ to the first-order equation: $\frac{Df_0}{Dt_1} = \hat{C}f_1$

one will have the homogeneous solutions: $\hat{C}f_1^{\text{homo}} = 0$.

$$(1) \quad f_1^{\text{homo}} = (1, \vec{v}, v^2) f_M \quad (\text{or } f_1^{\text{homo}} = (A + \vec{B} \cdot \vec{v} + Cv^2) f_M)$$

The linear combinations can be used to adjust n', \vec{u}', T' from f_0 to be consistent with true n, \vec{u}, T .

(2) To have a solution, the equation must meet the solvability conditions by Fredholm alternative theorem in the first place.

$$\frac{Df_0}{Dt_1} = \hat{C}f_1 \Rightarrow \left\langle (1, \vec{v}, v^2) f_M, \frac{Df_M}{Dt_1} \right\rangle = \int (1, \vec{v}, v^2) \frac{Df_M}{Dt_1} d\vec{v} = 0$$

↳ These are just particle, momentum, energy conservation of Maxwellian.

*note

: Fredholm alternative theorem

Solution f_1 이 존재하기 위해서는, $\hat{C}f_1$ 이 null space of $\frac{Df_0}{Dt_1}$ 가 수직이어야 한다.

$$\Rightarrow \left\langle (1, \vec{v}, v^2) f_M, \frac{Df_M}{Dt_1} \right\rangle = \int (1, \vec{v}, v^2) \frac{Df_M}{Dt_1} d\vec{v} = 0 \text{ 성립! by conservation.}$$

- Second-order solvability condition

The same solvability condition is applied. Both linearized \hat{C} and C operators have the solution of $(1, \vec{v}, v^2) f_M$. To have the solution order f_2 , it must meet the solvability condition:

$$\int d\vec{v} (1, \vec{v}, v^2) \left(\frac{Df_M}{Dt_2} + \frac{Df_1}{Dt_1} \right) = 0$$

i) $\int d\vec{v} (1, \vec{v}, v^2) \frac{Df_m}{Dt_2} = 0 \rightarrow$ Euler (conservation) equation

$$\text{ii) } \int d\vec{v} (1, \vec{v}, v^2) \frac{Df_i}{Dt} = \int d\vec{v} (1, \vec{v}, v^2) \left(\frac{\partial f_i}{\partial t} + \vec{v} \cdot \vec{\nabla} f_i + \vec{a} \cdot \frac{\partial f_i}{\partial \vec{v}} \right) = \vec{\nabla} \cdot \int d\vec{v} (1, \vec{v}, v^2) \vec{v} f_i$$

$$\left(\vec{a} \cdot \frac{\partial f_i}{\partial \vec{v}} = \frac{\partial}{\partial \vec{v}} (\vec{a} f_i) - \left(\frac{\partial}{\partial \vec{v}} \cdot \vec{a} \right) f_i = \frac{\partial}{\partial \vec{v}} (\vec{a} f_i) + \frac{q}{m} \frac{\partial}{\partial \vec{v}} (\vec{v} \times \vec{B}) = 0 , \quad \frac{\partial}{\partial t} = 0 \right)$$

\Rightarrow Systematic conclusion of Chapman - Enskog kinetic asymptotic expansion :

$$\frac{\int d\vec{v} (1, \vec{v}, v^2) \frac{Df_m}{Dt}}{\text{Nondissipative part}} = - \vec{\nabla} \cdot \frac{\int d\vec{v} (1, \vec{v}, v^2) \vec{v} f_i}{\text{dissipative flux}}$$

Solvability condition returns
the transport equation

② Preface for Braginskii

- Braginskii vs. Chapman - Enskog

(1) Magnetization brings anisotropy (2) Two components creates frictional exchange even in Maxwellian.

- Assumption : $K_n = \epsilon \ll 1$, $\rho/L \sim O(\epsilon)$, and high-freq ordering $\vec{U}_{ie} \sim U_{ti} \ll U_{te}$.

③ Transformation of kinetic equation on a moving frame.

$$\vec{w} = \vec{v} - \vec{u}(\vec{x}, t) \Rightarrow f(\vec{x}, \vec{v}, t) \rightarrow f(\vec{x}, \vec{w}, t)$$

$$\left(\begin{aligned} \frac{\partial}{\partial t} \Big|_{\vec{v}} &= \frac{\partial}{\partial t} \Big|_{\vec{w}} + \frac{\partial \vec{w}}{\partial t} \Big|_{\vec{v}} \cdot \frac{\partial}{\partial \vec{w}} = \frac{\partial}{\partial t} \Big|_{\vec{w}} - \frac{\partial \vec{u}}{\partial t} \cdot \frac{\partial}{\partial \vec{w}} \\ \frac{\partial}{\partial \vec{x}} \Big|_{\vec{v}} &= \frac{\partial}{\partial \vec{x}} \Big|_{\vec{w}} + \frac{\partial \vec{w}}{\partial \vec{x}} \Big|_{\vec{v}} \cdot \frac{\partial}{\partial \vec{w}} = \frac{\partial}{\partial \vec{x}} \Big|_{\vec{w}} - \vec{\nabla} \vec{u} \cdot \frac{\partial}{\partial \vec{w}} \end{aligned} \right)$$

New kinetic equation becomes :

$$\frac{Df}{Dt} = \frac{\partial f}{\partial t} + \vec{v} \cdot \frac{\partial f}{\partial \vec{x}} + \vec{a} \cdot \frac{\partial f}{\partial \vec{v}} = C[f]$$

$$\frac{\partial f}{\partial t} + \vec{u} \cdot \vec{\nabla} f + \vec{w} \cdot \vec{\nabla} f - \vec{w} \cdot \vec{\nabla} \vec{u} \frac{\partial f}{\partial \vec{w}} + \left[\frac{q}{m} (\vec{E}' + \vec{w} \times \vec{B}) - \frac{\partial \vec{u}}{\partial t} \right] \cdot \frac{\partial f}{\partial \vec{w}} = C[f]$$

$$\Rightarrow \frac{\partial f}{\partial t} + \vec{w} \cdot \vec{\nabla} f + \left[\frac{q}{m} (\vec{E}' + \vec{w} \times \vec{B}) - \frac{\partial \vec{u}}{\partial t} \right] \cdot \frac{\partial f}{\partial \vec{w}} - \vec{w} \cdot \vec{\nabla} \vec{u} \frac{\partial f}{\partial \vec{w}} = C[f]$$

where $\vec{E}' = \vec{E} + \vec{u} \times \vec{B}$ and $\frac{\partial}{\partial t} = \frac{\partial}{\partial t} + \vec{u} \cdot \vec{\nabla}$

⊕ Electron kinetic equation.

$$\begin{aligned} C_{ee}^l [f_e] + V_{ei} L_{ei} [f_e] + V_{ei} \frac{\vec{m}\vec{w} \cdot \vec{u}}{T_e} f_{me} \\ = \frac{df_e}{dt} + \vec{w} \cdot \vec{\nabla} f_e - \left(\frac{e}{m} (\vec{E}' + \vec{w} \times \vec{B}) + \frac{d\vec{u}_e}{dt} \right) \cdot \frac{df_e}{dw} - \vec{w} \cdot \vec{\nabla} \vec{u} \cdot \frac{df_e}{dw} \end{aligned}$$

↓

$$\begin{aligned} C_{ee}^l [f_e] + V_{ei} L_{ei} [f_e] + \frac{e}{m} \vec{w} \times \vec{B} \cdot \frac{df_e}{dw} \\ = \frac{df_e}{dt} + \vec{w} \cdot \vec{\nabla} f_e - \left(\frac{e}{m} \vec{E}' + \frac{d\vec{u}_e}{dt} \right) \frac{df_e}{dw} - \vec{w} \cdot \vec{\nabla} \vec{u} \cdot \frac{df_e}{dw} - V_{ei} \frac{\vec{m}\vec{w} \cdot \vec{u}}{T_e} f_{me} \end{aligned}$$

Expanding $f_e = f_{eo} + f_{ei} + \dots$,

i) zeroth-order equation (LHS: $O(\epsilon^{-1})$, RHS: $O(1)$) \rightarrow LHS \gg RHS.

$$\underline{C_{ee}^l [f_e] + V_{ei} L_{ei} [f_e] + \frac{e}{m} \vec{w} \times \vec{B} \cdot \frac{df_e}{dw} = 0} \quad \Rightarrow \quad f_{eo} = f_{me} \text{ (Maxwellian)}$$

ii) next-order equation

*note $\ln f_{me} = \text{const} + \ln n_e - \frac{3}{2} \ln T_e + \frac{m\vec{w}^2}{2T_e}$

$$\left(\frac{d}{dt} f_m = f_m \frac{d}{dt} \ln f_m = f_m \left(\frac{d}{dt} \ln n_e - \frac{3}{2} \frac{d}{dt} \ln T_e + \frac{m\vec{w}^2}{2T_e} \frac{d}{dt} \ln T_e \right) = f_m \left(\frac{d}{dt} \ln n_e + \left(\frac{m\vec{w}^2}{2T_e} - \frac{3}{2} \right) \frac{d}{dt} \ln T_e \right) \right)$$

$$\vec{w} \cdot \vec{\nabla} f_m = f_m \left(\vec{w} \cdot \vec{\nabla} \ln n_e + \left(\frac{m\vec{w}^2}{2T_e} - \frac{3}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_e \right)$$

$$\frac{df_m}{dw} = -\frac{m\vec{w}}{T} f_m.$$

$$\begin{aligned} C_{ee}^l [f_{ei}] + V_{ei} L_{ei} [f_{ei}] + \frac{e}{m} \vec{w} \times \vec{B} \cdot \frac{df_{ei}}{dw} \\ = \left[\frac{d}{dt} \ln n_e + \left(\frac{m\vec{w}^2}{2T_e} - \frac{3}{2} \right) \frac{d}{dt} \ln T_e + \vec{w} \cdot \vec{\nabla} \ln n_e + \left(\frac{m\vec{w}^2}{2T_e} - \frac{3}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_e \right. \\ \left. + \frac{m\vec{w}}{T_e} \left(\frac{e}{m} \vec{E}' + \frac{d\vec{u}_e}{dt} \right) + \frac{m\vec{w} \vec{w}}{T_e} \cdot \vec{\nabla} \vec{u}_e - V_{ei} \frac{\vec{m}\vec{w} \cdot \vec{u}}{T_e} \right] f_{me} \end{aligned}$$

< Braginskii's correction equation >

- Solvability condition of the first-order Chapman-Enskog expansion

$$\int d\vec{w} (\vec{1}, \vec{w}, \vec{w}^2) \times \text{RHS} = 0$$

* note that $\left(\begin{array}{l} \int w_x f_{me}(w) dw = 0 \\ \quad (\text{odd part}) \end{array} \quad \& \quad \begin{array}{l} \int w_x w_y f_{me}(w) dw = 0 \\ \quad (\text{서로 다른 성분은 odd 번수가 0}) \end{array} \right)$

1 Particle conservation.

$$\int d\vec{w} \vec{1} \cdot (\text{RHS}) = 0$$

$$\text{i)} \int d\vec{w} \left[\frac{d \ln n_e}{dt} f_{me} \right] = n_e \frac{d \ln n_e}{dt}$$

$$\text{ii)} \int d\vec{w} \left[\left(\frac{mw^2}{2T_e} - \frac{3}{2} \right) \frac{d \ln T_e}{dt} f_{me} \right] = \frac{d \ln T_e}{dt} \left(\frac{3p_e}{2T_e} - \frac{3}{2} n_e \right) = 0$$

$$\text{iii)} \int d\vec{w} \left[\vec{w} \cdot \vec{\nabla} \ln n_e + \left(\frac{mw^2}{2T_e} - \frac{3}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_e + \frac{m\vec{w}}{T_e} \left(\frac{e}{m} \vec{E}' + \frac{d\vec{u}}{dt} \right) - v_{ci} \frac{m\vec{w} \cdot \vec{u}}{T_e} \right] f_{me} = 0$$

$$\text{iv)} \int d\vec{w} \left[\frac{m\vec{w}\vec{w}}{T_e} \cdot \vec{\nabla} n_e f_{me} \right] = \frac{p_e}{T_e} \cdot \vec{\nabla} n_e = n_e \left(\vec{\nabla} n_e \right)$$

$$\therefore \text{(i)} + \text{(iv)} \Rightarrow \boxed{\frac{d \ln n_e}{dt} = - \vec{\nabla} \cdot \vec{u}_e}$$

2 Momentum conservation

$$\int d\vec{w} \cdot \vec{w} \cdot (\text{RHS}) = 0$$

* note $\int m w^2 f_{me} dw = 3n_e T_e$
 $\int (mw^2)^2 f_{me} dw = 15n_e T_e^2 / \int w^4 f_{me} dw = 15n_e \left(\frac{T_e}{m} \right)^2$

$$\text{i)} \int d\vec{w} \left[\frac{d}{dt} \ln n_e + \left(\frac{mw^2}{2T_e} - \frac{3}{2} \right) \frac{d}{dt} \ln T_e + \frac{m\vec{w}\vec{w}}{T_e} \cdot \vec{\nabla} n_e \right] \vec{w} f_{me} = 0$$

$$\text{ii)} \int d\vec{w} \left[\vec{w} \cdot \vec{\nabla} \ln n_e \right] \vec{w} f_{me} = \frac{\vec{\nabla} n_e}{n_e} \frac{p_e}{m_e} = \frac{T_e}{m_e} \vec{\nabla} n_e$$

$$\text{iii)} \int d\vec{w} \left[\left(\frac{mw^2}{2T_e} - \frac{3}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_e \right] \vec{w} f_{me} = \int d\vec{w} \left[\left(\frac{mw^2}{2T_e} - \frac{3}{2} \right) \vec{w} \vec{w} \cdot \frac{\vec{\nabla} T_e}{T_e} \right] f_{me}$$

$$= \int d\vec{w} \frac{mw^2}{2T_e} \vec{w} \vec{w} \frac{\vec{\nabla} T_e}{T_e} f_{me} - \frac{3p_e}{2m_e} \frac{\vec{\nabla} T_e}{T_e} = \frac{m \vec{\nabla} T_e}{2T_e^2} \int d\vec{w} \frac{1}{3} \vec{w}^4 f_{me} - \frac{3n_e}{2m_e} \vec{\nabla} T_e = \frac{m \vec{\nabla} T_e}{6T_e^2} \frac{15n_e T_e^2}{m^2} - \frac{3n_e}{2m_e} \vec{\nabla} T_e$$

$$= \left(\frac{5}{2} - \frac{3}{2} \right) \frac{n_e}{m_e} \vec{\nabla} T_e = \frac{n_e \vec{\nabla} T_e}{m_e}$$

$$\text{iv)} \int d\vec{w} \left[\frac{m\vec{w}}{T_e} \left(\frac{e}{m} \vec{E}' + \frac{d\vec{u}}{dt} \right) \right] \vec{w} f_{me} = \frac{m}{T_e} \frac{n_e T_e}{m} \left(\frac{e}{m} \vec{E}' + \frac{d\vec{u}}{dt} \right) = n_e \left(\frac{e}{m} \vec{E}' + \frac{d\vec{u}}{dt} \right)$$

$$\text{v)} \int d\vec{w} \left[-v_{ci} \frac{m\vec{w} \cdot \vec{u}}{T_e} \right] \vec{w} f_{me} = -v_{ci} \frac{m_e}{T_e} \left(\frac{n_e T_e}{m} \right) \vec{u} = -n_e v_{ci} \vec{u} = -\frac{1}{m} \vec{R}_{el}$$

$$\therefore \text{To sum-up, } = \frac{T_e}{m_e} \vec{\nabla} n_e + \frac{n_e}{m_e} \vec{\nabla} T_e + n_e \left(\frac{e}{m} \vec{E}' + \frac{d\vec{v}_e}{dt} \right) - \frac{1}{m} \vec{R}_{ei}^{(o)} = 0$$

$$\Rightarrow \frac{d\vec{v}_e}{dt} = -\frac{e}{m_e} \vec{E}' + \frac{\vec{R}_{ei}^{(o)} - \vec{\nabla}(n_e T_e)}{m_e n_e}$$

③ Energy conservation

$$\int \vec{w}^2 \cdot (\text{RHS}) d\vec{w} = 0$$

* note $\int w^2 f_{me} dw = 3n_e \left(\frac{T_e}{m_e} \right)$, $\int w^4 f_{me} dw = 15n_e \left(\frac{T_e}{m_e} \right)^2$

$$\text{i) } \int d\vec{w} w^2 \left[\frac{d \ln n_e}{dt} f_{me} \right] = \frac{3n_e T_e}{m} \frac{d \ln n_e}{dt}$$

$$\text{ii) } \int d\vec{w} w^2 \left[\left(\frac{m_w^2}{2T_e} - \frac{3}{2} \right) \frac{d \ln T_e}{dt} f_{me} \right] = \frac{d \ln T_e}{dt} \left[\frac{m_w}{2T_e} 15n_e \left(\frac{T_e}{m_e} \right)^2 - \frac{3}{2} \cdot 3n_e \left(\frac{T_e}{m_e} \right) \right] = 3 \frac{n_e T_e}{m} \frac{d \ln T_e}{dt}$$

$$\text{iii) } \int d\vec{w} w^2 \left[\frac{m_w \vec{w}}{T_e} \vec{\nabla} u_e f_{me} \right] = \frac{m_e}{T_e} \cdot \int \frac{1}{3} w^4 \vec{I} \vec{\nabla} u_e f_{me} = 5 \frac{m_e}{T_e} n_e \left(\frac{T_e}{m_e} \right)^2 \vec{\nabla} \cdot \vec{u}_e = 5 \frac{n_e T_e}{m_e} \vec{\nabla} \cdot \vec{u}_e$$

$$\text{iv) } \int d\vec{w} \cdot (\text{etc...}) = 0 \quad (\text{odd-part})$$

$$\therefore \text{To sum-up, } \frac{d \ln n_e}{dt} + \frac{d \ln T_e}{dt} + \frac{5}{3} \vec{\nabla} \cdot \vec{u}_e = 0 \Rightarrow (-\vec{\nabla} \cdot \vec{u}_e) + \frac{d \ln T_e}{dt} + \frac{5}{3} \vec{\nabla} \cdot \vec{u}_e = 0$$

$$\Rightarrow \frac{d \ln T_e}{dt} = -\frac{2}{3} \vec{\nabla} \cdot \vec{u}_e$$

- Inserting 3 conservation eqns to Braginskii's correction equation for electrons:

$$\left(\begin{aligned} & C_{ee} [f_{ei}] + V_{ei} L_{ei} [f_{ei}] + \frac{e}{m} \vec{w} \times \vec{B} \cdot \frac{d f_{ei}}{d \vec{w}} \\ &= \left[\underbrace{\frac{d \ln n_e}{dt}}_a + \left(\frac{m_w^2}{2T_e} - \frac{3}{2} \right) \frac{d \ln T_e}{dt} + \underbrace{\vec{w} \cdot \vec{\nabla} \ln n_e}_e + \left(\frac{m_w^2}{2T_e} - \frac{3}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_e \right. \\ & \quad \left. + \underbrace{\frac{m_w}{T_e} \cdot \left(\frac{e}{m} \vec{E}' + \frac{d \vec{v}_e}{dt} \right)}_e + \underbrace{\frac{m_w \vec{w}}{T_e} \cdot \vec{\nabla} u_e}_f - V_{ei} \underbrace{\frac{m_w \vec{u}'}{T_e}}_g \right] f_{me} \end{aligned} \right)$$

$$(e) = \frac{m_w}{T_e} \cdot \left[\frac{\vec{R}_{ei}^{(o)}}{m n_e} - \frac{T_e \vec{\nabla} n_e + n_e \vec{\nabla} T_e}{m n_e} \right] = \frac{\vec{w} \cdot \hat{(mn V_{ei} \vec{u})}}{m n_e} = \vec{w} \cdot \vec{\nabla} \ln T_e - \vec{w} \cdot \vec{\nabla} \ln n_e$$

$$\rightarrow (c) + (e)_3 = 0$$

$$\rightarrow (d) + (e)_2 = \left(\frac{m_w^2}{2T_e} - \frac{5}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_e$$

$$\rightarrow (g) + (e)_1 = \frac{m}{T_e} (V_{ei} - V_{ci}) \vec{w} \cdot \vec{u}$$

$$\vec{w}_L = \frac{d}{dr} (\vec{w}_L \times \hat{b}) = \frac{d}{dr} (sinr \hat{x} - cosr \hat{y}) = cosr \hat{x} + sinr \hat{y}$$

$$\boxed{3} \quad \vec{q}_{\perp e} = -T_e \int d\vec{w} \vec{w}_L L_1^{(3/2)}(x) \tilde{f}_{ei}^{(1)} = -T_e \int d\vec{w} \frac{1}{f_r} (\vec{w}_L \times \hat{b}) L_1^{(3/2)}(x) \tilde{f}_{ei}^{(1)}$$

부분적분 $\rightarrow = T_e \int d\vec{w} (\vec{w}_L \times \hat{b}) L_1^{(3/2)}(x) \frac{d\tilde{f}_{ei}^{(1)}}{dr} \leftarrow$ 이제 우리는 $\tilde{f}_{ei}^{(1)}$ 이 아니라 $\frac{d\tilde{f}_{ei}^{(1)}}{dr}$ 만 알면 됨.

* note eq.(49)

$$W_{ce} \frac{d\tilde{f}_{ei}^{(1)}}{dr} = -C_{ee} [\tilde{f}_{ei}^{(0)}] - V_{ei} L_{ei} [\tilde{f}_{ei}^{(0)}] + f_{me} \frac{m(V_{ci} - V_{te})}{T_e} \vec{w}_L \cdot \vec{u}$$

$$\vec{q}_{\perp e} = \frac{T_e}{W_{ce}} \int d\vec{w} (\vec{w}_L \times \hat{b}) L_1^{(3/2)}(x) f_{me} \left[1 - \frac{3\sqrt{\pi}}{4} \left(\frac{V_{te}}{W} \right)^3 \right] \frac{2\vec{w}_L \cdot (\vec{u}_i - \vec{u}_e)}{V_{te}^2 Z_{ci}}$$

$$+ \frac{T_e}{W_{ce}^2} \int d\vec{w} (\vec{w}_L \times \hat{b}) L_1^{(3/2)}(x) \left[C_{ee} + V_{ei} L_{ei} \right] (f_{me} L_1^{(3/2)}(x) (\vec{w}_L \times \hat{b}) \cdot \vec{v} / n_{Te})$$

$$\therefore \vec{q}_{\perp e} = \frac{3}{2} \frac{P_c}{Z_{ci} W_{ce}} \hat{b} \times (\vec{u}_i - \vec{u}_e) - 4.66 \frac{P_c}{m_e Z_{ci} W_{ce}^2} \vec{D}_\perp T_e$$

⑧ Electron friction force

$$\begin{aligned} \text{II} \quad R_{lei} &= \frac{m_e n_e}{Z_{ci}} (U_{IIIi} - U_{IIIe}) - \frac{3\sqrt{\pi}}{4 Z_{ci}} m_e V_{te}^3 \int d\vec{w} \frac{w_{11}}{w^3} \langle f_{ei} \rangle \\ &= \frac{m_e n_e}{Z_{ci}} (U_{IIIi} - U_{IIIe}) \left\{ 1 - \frac{3\sqrt{\pi}}{2} \frac{V_{te}}{n_e} \int d\vec{w} \frac{w_{11}}{w^3} f_{me} \left[0.284 L_1^{(3/2)}(x) + 0.032 L_2^{(3/2)}(x) \right] \right\} \\ &\quad - \frac{5}{2} n_e \hat{b} \cdot \vec{v} T_e \times \frac{3\sqrt{\pi}}{2} \frac{V_{te}}{n_e} \int d\vec{w} \frac{w_{11}^2}{w^3} f_{me} \left[0.506 L_1^{(3/2)}(x) - 0.253 L_2^{(3/2)}(x) \right] \\ &= \frac{m_e n_e}{Z_{ci}} (U_{IIIi} - U_{IIIe}) \left[1 - 0.284 \int_0^\infty x e^{-x} L_1^{(3/2)}(x) - 0.032 \int_0^\infty x e^{-x} L_2^{(3/2)}(x) \right] \\ &\quad - \frac{5}{2} n_e \hat{b} \cdot \vec{v} T_e \left[0.506 \int_0^\infty x e^{-x} L_1^{(3/2)}(x) - 0.253 \int_0^\infty x e^{-x} L_2^{(3/2)}(x) \right] \end{aligned}$$

$$R_{lei} = 0.51 \frac{m_e n_e}{Z_{ci}} (U_{IIIi} - U_{IIIe}) - 0.71 n_e \hat{b} \cdot \vec{v} T_e$$

(Parallel friction force)

Same as Spitzer-Harm : 0.51

$$\boxed{\text{Q}} \quad \vec{g}_{Ne} = -T_e \int d\vec{w} \vec{w}_\perp L_1^{(3/2)}(\gamma) \tilde{f}_{e1} = \int d\vec{w} \vec{w}_\perp [L_1^{(3/2)}(\gamma)]^2 f_{Me} \frac{\vec{w}_\perp \times \hat{b}}{W_{ce}} \cdot \vec{\nabla} T_e$$

$$= \frac{1}{W_{ce}} \int_{-1}^1 d\xi \int_0^\infty dw w^2 \int_0^{2\pi} d\gamma [L_1^{(3/2)}]^2 f_{Me} \vec{w}_\perp \vec{w}_\perp \times \hat{b} \cdot \vec{\nabla} T_e$$

$$\left(\int_0^{2\pi} \vec{w}_\perp \vec{w}_\perp d\gamma = \pi W_\perp^2 (\hat{I} - \hat{b}\hat{b}) \right)$$

$$\vec{g}_{Ne} = \frac{\pi}{W_{ce}} \int_{-1}^1 d\xi \int_0^\infty dw w^2 [L_1^{(3/2)}]^2 f_{Me} (\hat{I} - \hat{b}\hat{b}) \times \hat{b} \cdot \vec{\nabla} T_e$$

$$(W_\perp^2 = W^2 - W_{||}^2 = (1-\xi^2)W^2, \quad \int_{-1}^1 (1-\xi^2) d\xi = 2 - \frac{2}{3} = \frac{4}{3},$$

$$\vec{g}_{Ne} = \frac{\pi}{W_{ce}} \frac{4}{3} \int_0^\infty dk \chi^{3/2} \left(\frac{V_{te}}{2} \right) [L_1^{(3/2)}]^2 \frac{n_e}{\pi^{3/2} V_{te}^3} e^{-x} (\hat{I} - \hat{b}\hat{b}) \times \hat{b} \cdot \vec{\nabla} T_e$$

$$= \frac{4n_e}{3W_{ce}\sqrt{\pi}} \underbrace{\frac{V_{te}^2}{2}}_{\frac{T_e}{M}} \underbrace{\int_0^\infty e^{-x} \chi^{3/2} [L_1^{(3/2)}]^2 dk}_{15\sqrt{\pi}/8} \cdot \underbrace{(\hat{I} - \hat{b}\hat{b}) \times \hat{b} \cdot \vec{\nabla} T_e}_{\downarrow}$$

$$(\hat{I} - \hat{b}\hat{b}) \times \hat{b} \cdot \vec{\nabla} T_e = (\hat{x}\hat{x} + \hat{y}\hat{y}) \times \hat{z} \cdot \vec{\nabla} T_e = -\hat{x}\hat{y} \cdot \vec{\nabla} T_e + \hat{y}\hat{x} \cdot \vec{\nabla} T_e = -\hat{x} \frac{\partial T_e}{\partial y} + \hat{y} \frac{\partial T_e}{\partial x} = \hat{b} \times \vec{\nabla} T_e$$

$$\therefore \vec{g}_{Ne} = \frac{4}{3\sqrt{\pi}} \frac{P_e}{m_e W_{ce}} \frac{15\sqrt{\pi}}{8} \hat{b} \times \vec{\nabla} T_e = \frac{5}{2} \frac{P_e}{m_e W_{ce}} \hat{b} \times \vec{\nabla} T_e$$

$$\boxed{\vec{g}_{Ne} = \frac{5}{2} \frac{P_e}{m_e W_{ce}} \hat{b} \times \vec{\nabla} T_e}$$

- Friction force $\vec{R}_{ei} = -m_e \int d\vec{w} V_s^{ei} \vec{w} (f_{eo} + f_{ei})$

$$\underline{\vec{R}_{ei}} = \frac{m_e n_e}{2 \tau_{ei}} (\vec{u}_i - \vec{u}_e) - \frac{3\sqrt{\pi}}{4 \tau_{ei}} m_e V_{te}^3 \int d\vec{w} \frac{\vec{w}}{w^3} (\langle f_{ei} \rangle + \hat{f}_{ei}^{(o)}) \equiv \vec{R}_{\parallel ei} + \vec{R}_{\perp ei}$$

⑦ Electron heat flux

$$\text{II } \vec{q}_{\parallel ie} = -T_e \int d\vec{w} \vec{w} L_1^{(3/2)}(x) \langle f_{ei} \rangle = -T_e \int d\vec{w} w_{\parallel b} \hat{L}_1^{(3/2)}(b) \langle f_{ei} \rangle$$

$$\left(\int d\vec{w} = 2\pi \int_{-1}^1 d\xi \int_0^\infty w^2 dw, \quad w_{\parallel} = w\xi \right)$$

$$\vec{q}_{\parallel ie} = -T_e \cdot 2\pi \int_{-1}^1 d\xi \int_0^\infty dw \cdot w^2 (w\xi) L_1^{(3/2)}(x) \\ \times \int w \xi f_{me} L_1^{(3/2)}(x) \left[0.506 \frac{5}{2} \tau_{ei} \hat{b} \hat{b} \cdot \vec{\nabla} T_e + 0.284 \frac{m_e (\vec{u}_{\parallel ii} - \vec{u}_{\parallel ei})}{T_e} \right]$$

$$= -\frac{4\pi}{3} \int_0^\infty dw w^4 \left[L_1^{(3/2)}(x) \right]^2 f_{me} \left[0.506 \frac{5}{2} \tau_{ei} \hat{b} \hat{b} \cdot \vec{\nabla} T_e + 0.284 m_e (\vec{u}_{\parallel ii} - \vec{u}_{\parallel ei}) \right]$$

$$\left(x = \frac{w^2}{V_{te}^2}, \quad 2w dw = V_{te}^2 dx \rightarrow w^4 dw = \frac{4}{V_{te}^2} x^2 \frac{V_{te}^2}{2w} dx = \frac{1}{2} V_{te}^5 x^{3/2} dx \right)$$

$$f_{me} = n_e \left(\frac{1}{\pi V_{te}^2} \right)^{3/2} \exp \left(-\frac{w^2}{V_{te}^2} \right) = \frac{n_e}{\pi^{3/2} V_{te}^3} \exp(-x)$$

$$\vec{q}_{\parallel ie} = -\frac{4\pi}{3} \frac{n_e}{\pi^{3/2}} \frac{V_{te}^2}{2} \left[0.506 \frac{5}{2} \tau_{ei} \hat{b} \hat{b} \cdot \vec{\nabla} T_e + 0.284 m_e (\vec{u}_{\parallel ii} - \vec{u}_{\parallel ei}) \right] \underbrace{\int_0^\infty e^{-x} x^{3/2} \left[L_1^{(3/2)}(x) \right]^2}_{= 15.5\pi/8}$$

$$\therefore \vec{q}_{\parallel ie} = -3.1b \frac{p_e \tau_{ei}}{m_e} \hat{b} \hat{b} \cdot \vec{\nabla} T_e - 0.71 p_e (\vec{u}_{\parallel ii} - \vec{u}_{\parallel ei}) \hat{b}$$

parallel conductivity

friction.

one can obtain a_0, a_1 from $(LHS) = (RHS)$, which gives $\langle fei \rangle$

In particular for $Z=1$.

$$\langle f_{\text{el}} \rangle = W_{11} f_{\text{Me}} L_1^{(3/2)} \left(\frac{W^2}{V_{\text{Te}}^2} \right) \left[0.506 \times \frac{5}{2} \hat{\text{Z}_{\text{el}}} \hat{\vec{b}} \cdot \vec{v} \ln \text{Te} + 0.284 \times \frac{m_e (U_{111} - U_{111})}{T_e} \right] \\ - W_{11} f_{\text{Me}} L_2^{(3/2)} \left(\frac{W^2}{V_{\text{Te}}^2} \right) \left[0.253 \times \frac{5}{2} \hat{\text{Z}_{\text{el}}} \hat{\vec{b}} \cdot \vec{v} \ln \text{Te} - 0.032 \times \frac{m_e (U_{111} - U_{111})}{T_e} \right]$$

where $m = M_e$ and $\vec{u} = \vec{u}_i - \vec{u}_e$.

⑥ Gyro-dependent electron distribution function

one can subtract the gyro-independent part from full equation

$$C_{co}^{\wedge} \left[\overset{\wedge}{f_{\text{fe}_1}} \right] + V_{ci} f \left[\overset{\wedge}{f_{\text{fe}_1}} \right] + W_{ce} \frac{df_{\text{fe}_1}}{dy} = \left[\left(\frac{mw^2}{2Te} - \frac{5}{2} \right) \vec{W}_L \cdot \vec{J} |_{nTe} + \frac{m(\overset{\wedge}{V_{ci}} - V_{ci})}{Te} \vec{W}_L \cdot \vec{U} \right] f_{me}$$

With $\omega \gg \omega_{ei}$, one can make the subsequent ordering (last piece of Braginskii's electron correction equation)

$$\tilde{f}_{ei} = \tilde{f}_{ei}^{(0)} + \tilde{f}_{ei}^{(1)}$$

$$i) \quad \text{We} \frac{df_1^{(o)}}{dr} = f_{me} \left(\frac{m\omega^2}{2T_0} - \frac{5}{2} \right) \vec{N_L} \cdot \vec{\sigma} \ln T_e \quad (\text{Lowest-order})$$

$$\text{Integrating over : } \frac{d\vec{f}_{ei}}{dy} = \frac{f_{Me}}{W_{ce}} \left(\frac{m\omega^2}{2T_e} - \frac{5}{2} \right) W_2 (\hat{x} \cos y + \hat{y} \sin y) \vec{J}_{inTe}$$

$$\tilde{f}_{\text{el}}^{(0)} = -\frac{f_{\text{me}}}{W_{\text{cc}}} L_1^{(3/2)}(x) \cdot W_2(\hat{x} \sin v - \hat{y} \cos v) \vec{D} \ln T_c$$

$$\Rightarrow \tilde{f}_{\text{el}}^{(0)} = -f_{\text{me}} L_1^{(3/2)}(x) \frac{\vec{w}_\perp \times \hat{b}}{W_{\text{cc}}} \cdot \vec{D} \ln T_c$$

$$ii) \quad \text{Wce} \frac{\partial f_{el}^{(1)}}{\partial v} = -C_{el}^s \tilde{f}_{el}^{(0)} - V_{el} P \tilde{f}_{el}^{(0)} + f_{me} \frac{m(v_{el} - v_{el})}{T_e} \vec{w} \cdot \vec{u} \quad (\text{Next-order})$$

Now one has $f_{\text{el}} = \langle f_{\text{el}} \rangle + \tilde{f}_{\text{el}}^{(0)} + \tilde{f}_{\text{el}}^{(1)}$ and can evaluate electron heat flux

$$\vec{f}_e = \int d\vec{w} \vec{w} \left(\frac{1}{2} m \omega^2 - \frac{5}{2} T_e \right) f_{cl}$$

$$= -Te \int d\vec{w} \vec{w} L_1^{(3/2)}(\eta) (\langle f_{11} \rangle + \tilde{f}_{11}^{(0)} + \tilde{f}_{11}^{(1)}) \equiv \overset{\text{parallel}}{\vec{q}_{11c}} + \overset{\text{diamagnetic}}{\vec{q}_{11c}} + \overset{\text{perpendicular}}{\vec{q}_{11c}}$$

This part can be solved in the same way as the Spitzer-Harm,
using the associated Laguerre polynomial expansion.

$$\langle f_{ei} \rangle = \frac{2W_{ii}}{Nte^2} f_{Me} \sum_{k=1}^{(3/2)} a_{ik} L_k^{(3/2)}(x). \quad \leftarrow k \geq 1 \text{ and } V_{ii} \rightarrow W_{ii} \text{ (notable difference)}$$

$$(i) \text{ LHS} : \int W_{ii} L_k^{(3/2)}(x) \left\{ C_{ei}^k [\langle f_{ei} \rangle] + V_{ei} L_{ei} [\langle f_{ei} \rangle] \right\} d\vec{w}$$

$$= - \frac{n_e}{Ze_i Z} \begin{pmatrix} \sqrt{2} + \frac{13}{4} z & \frac{3\sqrt{2}}{4} + \frac{69}{16} z \\ \frac{3\sqrt{2}}{4} + \frac{69}{16} z & \frac{45\sqrt{2}}{16} + \frac{433}{64} z \end{pmatrix} \begin{pmatrix} a_0 \\ a_1 \end{pmatrix} \quad \begin{matrix} \text{From} \\ \leftarrow \text{Eq}(55) \text{ in Lec. 19.} \end{matrix}$$

$$(ii) \text{ RHS} : \int d\vec{w} W_{ii} L_k^{(3/2)} f_{Me} \left\{ \left(\frac{W^2}{Vte^2} - \frac{5}{2} \right) W_{ii} \hat{b} \cdot \vec{\nabla} \ln T_e + \left[1 - \frac{3\sqrt{\pi}}{4} \left(\frac{Vte}{W} \right)^3 \right] \frac{2W_{ii} U_{ii}}{Vte^2 Ze_i} \right\}$$

$$W_{ii} = \frac{v^2 g^2}{2} \int d\vec{w} W^2 \hat{g} L_k^{(3/2)}(x) f_{Me} \left[\left(x - \frac{5}{2} \right) \hat{b} \cdot \vec{\nabla} \ln T_e + \left(1 - \frac{3\sqrt{\pi}}{4x^{3/2}} \right) \frac{2U_{ii}}{Vte^2 Ze_i} \right]$$

$$\left(* n_{te} f_{Me} = n_e \left(\frac{m_e}{2\pi T_e} \right)^{1/2} \exp \left(- \frac{m_e W^2}{2T_e} \right) = \frac{n_e}{\pi^{3/2}} \frac{1}{Vte^3} \exp(-x) \right)$$

$$\left(\int d\vec{w} = 2\pi \int_{-1}^1 dx \int_0^\infty W^2 dw = \pi Vte^3 \int_{-1}^1 dx \int_0^\infty x^{1/2} dx, \quad x = \frac{W^2}{Vte^2} \right)$$

$$= \frac{2n_e Vte^2}{3\sqrt{\pi}} \int_0^\infty dx x^{3/2} e^{-x} L_k^{(3/2)}(x) \left[-L_1^{(3/2)}(x) \hat{b} \cdot \vec{\nabla} \ln T_e + \left(1 - \frac{3\sqrt{\pi}}{4x^{3/2}} \right) \frac{2U_{ii}}{Vte^2 Ze_i} \right]$$

$$= - \frac{4}{3\sqrt{\pi}} \frac{n_e}{m} \hat{b} \cdot \vec{\nabla} T_e \times \int_{k=1}^{\infty} \frac{15\sqrt{\pi}}{8} - \frac{n_e U_{ii}}{Ze_i} \times \left(1 - \delta_{k0} + \frac{3}{2} \delta_{k1} + \frac{15}{8} \delta_{k2} + \dots \right)$$

$$k=1 \rightarrow \left[- \frac{n_e}{Ze_i} \left(\frac{5}{2} \frac{Ze_i}{m} \hat{b} \cdot \vec{\nabla} T_e + \frac{3}{2} U_{ii} \right) \right]$$

$$k=2 \rightarrow \left[\frac{15}{8} U_{ii} \right]$$

$$* \text{note} \left\{ \begin{array}{l} k=0 \quad \int_0^\infty dx e^{-x} = \Gamma(1) = 1 \\ k=1 \quad \int_0^\infty dx e^{-x} \left(\frac{5}{2} - x \right) = \frac{5}{2} \Gamma(1) - \Gamma(2) = \frac{3}{2} \end{array} \right. \quad \left(\Gamma(z+1) = z \Gamma(z) \right)$$

$$k=2 \quad \int_0^\infty dx e^{-x} \left(\frac{35}{8} - \frac{7}{2} x + \frac{1}{2} x^2 \right) = \frac{35}{8} \Gamma(1) - \frac{7}{2} \Gamma(2) + \frac{1}{2} \Gamma(3) = \frac{35}{8} - \frac{7}{2} + \frac{2}{2} = \frac{15}{8}$$

$$\downarrow$$

$$\int_0^\infty dx x^{3/2} e^{-x} L_k^{(3/2)}(x) \left(1 - \frac{3\sqrt{\pi}}{4x^{3/2}} \right) = \frac{3\sqrt{\pi}}{4} - \frac{3\sqrt{\pi}}{4} \left(\int_0^\infty dx e^{-x} L_k^{(3/2)}(x) \right)$$

$$= \frac{3\sqrt{\pi}}{4} \left(1 - \delta_{k0} + \frac{3}{2} \delta_{k1} + \frac{15}{8} \delta_{k2} + \dots \right)$$

$$(a) = -\vec{\nabla} \cdot \vec{u} e$$

$$(b) = \left(\frac{m w^2}{2 T_e} - \frac{3}{2} \right) \left(-\frac{2}{3} \vec{\nabla} \cdot \vec{u} e \right) = -\frac{m w^2}{3 T_e} \vec{\nabla} \cdot \vec{u} e + \vec{\nabla} \cdot \vec{u} e$$

$$(f) = \frac{m}{T_e} \vec{w} \vec{w} : \vec{\nabla} \vec{u} e$$

$$\rightarrow (a) + (b) + (f) = \frac{m_e}{T_e} \left(\vec{w} \vec{w} - \frac{w^2}{3} \overset{\leftrightarrow}{I} \right) : \vec{\nabla} \vec{u} e = \frac{m}{2 T_e} \left(\vec{w} \vec{w} - \frac{w^2}{3} \overset{\leftrightarrow}{I} \right) : \overset{\leftrightarrow}{w}_e$$

$$\text{where } \overset{\leftrightarrow}{w}_e = \vec{\nabla} \vec{u} + (\vec{\nabla} \vec{u})^\top - \frac{2}{3} (\vec{\nabla} \cdot \vec{u}) \overset{\leftrightarrow}{I} \quad (\text{rate of strain tensor})$$

$$\Rightarrow C_{ee}^l [f_{ei}] + V_{ei} L_{ei} [f_{ai}] + \frac{e}{m} \vec{w} \times \vec{B} \frac{d f_{ei}}{d \vec{w}}$$

$$= \left[\left(\frac{m w^2}{2 T_e} - \frac{5}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_e + \frac{m (V_{ei} - V_{ai})}{T_e} \vec{w} \cdot \vec{u} + \frac{m}{2 T_e} \left(\vec{w} \vec{w} - \frac{w^2}{3} \overset{\leftrightarrow}{I} \right) : \overset{\leftrightarrow}{w}_e \right] f_{me}$$

where $\overset{\leftrightarrow}{w} = (\vec{\nabla} \vec{u}) + (\vec{\nabla} \vec{u})^\top - \frac{2}{3} (\vec{\nabla} \cdot \vec{u}) \overset{\leftrightarrow}{I}$ and $V_{ei}(v) = \frac{3\sqrt{\pi}}{4} \left(\frac{v_{Te}}{w} \right)^3 V_{ei}$

(1) Thermo dynamic force (2) friction force Viscous force due to flow shear.

⑤ Gyro-averaged electron distribution function

$$\text{Now use } \vec{w} = w_{||} \hat{b} + w_{\perp} (\hat{x} \cos \gamma + \hat{y} \sin \gamma) \rightarrow \frac{e}{m} \vec{w} \times \vec{B} \cdot \frac{d f_{ei}}{d \vec{w}} = W_{ee} \frac{d f}{d \gamma}$$

$$\left(\frac{e}{m} \vec{w} \times \vec{B} \cdot \frac{d f_{ei}}{d \vec{w}} = \frac{eB}{m} [w_{\perp} (\sin \gamma \hat{x} - \cos \gamma \hat{y})] \cdot [\hat{x} \frac{d f_{ei}}{d w_x} + \hat{y} \frac{d f_{ei}}{d w_y}] = \frac{eB}{m} w_{\perp} \left(\sin \gamma \frac{d f}{d w_x} - \cos \gamma \frac{d f}{d w_y} \right) = W_{ee} \frac{d f}{d \gamma} \right)$$

*note: $\frac{d f}{d \gamma} = \frac{d w_x}{d \gamma} \frac{d f}{d w_x} + \frac{d w_y}{d \gamma} \frac{d f}{d w_y} = w_{\perp} (-\sin \gamma \frac{d f}{d w_x} + \cos \gamma \frac{d f}{d w_y})$

Compared to the hydrodynamic Chapman-Enskog, a magnetized plasma contains the fast gyro motion making kinetic response strongly anisotropic. \Rightarrow Let's perform gyro-averaging to isolate parallel & perpendicular directions

$$f_{ei} = \langle f_{ei} \rangle + \tilde{f}_{ei} \quad \text{where } \langle f_{ei} \rangle = \frac{1}{2\pi} \int f_{ei} d\gamma$$

to isolate parallel & perpendicular directions

$$\text{From } \langle C_{ee}^l [f_{ei}] \rangle = C_{ee}^l [\langle f_{ei} \rangle], \quad \langle L [f_{ei}] \rangle = L [\langle f_{ei} \rangle]$$

This is what
Braginskii did.

$$\langle \vec{w} \rangle = w_{||} \hat{b}, \quad \langle \vec{w} \vec{w} \rangle = w_{||}^2 \hat{b} \hat{b} + \frac{1}{2} w_{\perp}^2 (\overset{\leftrightarrow}{I} - \hat{b} \hat{b}), \quad \text{and } \overset{\leftrightarrow}{w} \triangleq 0 \quad (\text{viscous-term})$$

$$\Rightarrow C_{ee}^l [\langle f_{ei} \rangle] + V_{ei} L_{ei} [\langle f_{ei} \rangle] = \left[\left(\frac{m w^2}{2 T_e} - \frac{5}{2} \right) w_{||} \hat{b} \cdot \vec{\nabla} \ln T_e + \frac{m (V_{ei} - V_{ai})}{T_e} w_{||} w_{||} \right] f_{me}$$

$\langle \text{gyro-averaged part} \rangle$

$$\begin{aligned}
 \boxed{2} \quad \vec{R}_{\text{tei}} &= \frac{m_e n_e}{Z_{\text{ei}}} (\vec{U}_{\perp i} - \vec{U}_{\perp e}) - \frac{3\sqrt{\pi}}{4 Z_{\text{ei}}} m_e V_{\text{Te}}^3 \int d\vec{w} \frac{\vec{w}_\perp}{w^3} \hat{f}_{\text{ei}}^{(o)} \\
 &= \frac{m_e n_e}{Z_{\text{ei}}} (\vec{U}_{\perp i} - \vec{U}_{\perp e}) + \frac{3\sqrt{\pi}}{4 W_{\text{ce}} Z_{\text{ei}}} m_e V_{\text{Te}}^3 \int d\vec{w} \frac{\vec{w}_\perp}{w^3} f_{\text{me}} L_1^{(3/2)}(x) \vec{w}_\perp \cdot \hat{b} \times \vec{v} \ln T_e \\
 &= \frac{m_e n_e}{Z_{\text{ei}}} (\vec{U}_{\perp i} - \vec{U}_{\perp e}) + \frac{3n_e}{4 W_{\text{ce}} Z_{\text{ei}}} \int_{-1}^1 d\gamma \left(-\frac{\gamma^2}{2} \right) \int_0^\infty dx e^{-x} L_1^{(3/2)}(x) \hat{b} \times \vec{v} T_e \\
 &= \frac{m_e n_e}{Z_{\text{ei}}} (\vec{U}_{\perp i} - \vec{U}_{\perp e}) + \frac{3}{2} \frac{n_e}{W_{\text{ce}} Z_{\text{ei}}} \hat{b} \times \vec{v} T_e
 \end{aligned}$$

⑨ Summary: Electron transport coefficients by Braginskii

$$q_{\parallel ee} = -k_{\parallel ee} \nabla_{\parallel} T_e - 0.71 p_e (U_{\parallel ee} - U_{\parallel ii}) \quad (k_{\parallel ee} \equiv 3.16 \frac{p_e Z_{\text{ei}}}{m_e})$$

$$\vec{q}_{\perp ee} = \frac{5}{2} \frac{p_e}{m_e W_{\text{ce}}} \hat{b} \times \vec{v} T_e$$

$$\vec{q}_{\text{fe}} = -k_{\perp ee} \vec{v}_{\perp} T_e + \frac{3}{2} \frac{p_e}{Z_{\text{ei}} W_{\text{ce}}} \hat{b} \times (\vec{U}_{\perp i} - \vec{U}_{\perp e}) \quad (k_{\perp ee} = 4.66 \frac{p_e}{m_e Z_{\text{ei}} W_{\text{ce}}})$$

$$\overset{\leftrightarrow}{T}_{ee} \approx 0$$

$$R_{\parallel ei} = \gamma_{\parallel} e^2 n_e^2 (U_{\parallel ii} - U_{\parallel ee}) - 0.71 n_e \nabla_{\parallel} T_e \quad (\gamma_{\parallel} \equiv 0.51 \frac{m_e}{n_e e^2 Z_{\text{ei}}})$$

$$\vec{R}_{\perp ei} = \gamma_{\perp} e^2 n_e^2 (\vec{U}_{\perp i} - \vec{U}_{\perp e}) + \frac{3}{2} \frac{n_e}{W_{\text{ce}} Z_{\text{ei}}} \hat{b} \times \vec{v} T_e \quad (\gamma_{\perp} \equiv \frac{m_e}{n_e e^2 Z_{\text{ei}}})$$

$$Q_{ie} = \frac{3 m_e n_e}{m_i Z_{\text{ei}}} (T_e - T_i)$$

(10) Ion kinetic equation

Assume: ion-ion collisions are dominant. (neglect all e-i terms in electron eqn).

$$\Rightarrow C_{ii}^{\ell} [f_{ii}] + w_{ci} \frac{df_{ii}}{dr} = \left[\left(\frac{m_i w^2}{2T_i} - \frac{5}{2} \right) \vec{w} \cdot \vec{v} \ln T_i + \frac{m_i}{2T_i} (\vec{w} \cdot \vec{w} - \frac{w^2}{3} I) : \vec{w} \right] f_{Mi}$$

However, we cannot neglect ion viscosity w_i (unlike electron viscosity $w_e \approx 0$)

$$f_{ii} = \langle f_{ii} \rangle + \tilde{f}_{ii}$$

$$\Rightarrow C_{ii}^{\ell} [\langle f_{ii} \rangle] = \left[\left(\frac{m_i w^2}{2T_i} - \frac{5}{2} \right) W_{ii} \hat{b} \cdot \vec{v} \ln T_i + \frac{m_i}{2T_i} \left(W_{ii}^2 - \frac{w_{\perp}^2}{2} \right) \left(\hat{b}\hat{b} - \frac{1}{3} I \right) : \vec{w} \right] f_{Mi}$$

$$\left(\begin{aligned} * \text{note} \quad & \langle \vec{w} \cdot \vec{w} \rangle - \frac{w^2}{3} I = W_{ii} \hat{b} \hat{b} + \frac{w_{\perp}^2}{2} (\hat{I} - \hat{b} \hat{b}) - \left(\frac{W_{ii}^2}{3} + \frac{w_{\perp}^2}{3} \right) \hat{I} \\ & = W_{ii}^2 (\hat{b} \hat{b} - \frac{1}{3} I) - \frac{w_{\perp}^2}{2} (\hat{b} \hat{b} - \frac{1}{3} I) = \left(W_{ii}^2 - \frac{w_{\perp}^2}{2} \right) (\hat{b} \hat{b} - \frac{1}{3} I) \end{aligned} \right)$$

(11) Associated Laguerre polynomials for angular distribution

Expansion for ion kinetic equation:

$$\langle f_{ii} \rangle = \underbrace{\frac{2W_{ii}}{Vt_i^2} f_{Mi} \sum_{k=1}^{(3/2)} a_k L_k^{(3/2)}(x)}_{\equiv \langle f_{ii} \rangle_a} + \underbrace{\frac{2}{3} \left(\frac{W_{ii}^2 - w_{\perp}^2/2}{p_i Vt_i^2} \right) f_{Mi} \sum_{k=0}^{(5/2)} b_k L_k^{(5/2)}(x)}_{\equiv \langle f_{ii} \rangle_b},$$

One can see that $\langle f_{ii} \rangle_b$ is closely related to viscous tensor.

$$\begin{aligned} & \left(\hat{b}\hat{b} - \frac{1}{3} I \right) \int d\vec{w} m_i \left(W_{ii}^2 - \frac{w_{\perp}^2}{2} \right) \langle f_{ii} \rangle_b \\ & = \left(\hat{b}\hat{b} - \frac{1}{3} I \right) \int d\vec{w} m_i \left(W_{ii}^2 - \frac{w_{\perp}^2}{2} \right) \frac{2}{3} \left(\frac{W_{ii}^2 - w_{\perp}^2/2}{p_i Vt_i^2} \right) f_{Mi} \sum_{k=0}^{(5/2)} b_k L_k^{(5/2)}(x) \\ & \left(\begin{aligned} * \text{note} \quad & \int d\vec{w} = 2\pi \int_{-1}^1 d\varphi \int_0^\infty w^2 dw = \pi Vt_i^3 \int_{-1}^1 d\varphi \int_0^\infty x^{1/2} dx, \quad W_{ii}^2 - \frac{w_{\perp}^2}{2} = w^2 \left(\frac{w^2}{3} - \frac{(1-\varphi^2)}{2} \right) = w^2 \left(\frac{3\varphi^2-1}{2} \right) \\ & f_{Mi} = \frac{n_i}{\pi^{3/2} Vt_i^3} e^{-x} \quad \frac{4}{3\pi Vt_i^4} = Vt_i^2 x \left(\frac{3\varphi^2-1}{2} \right) \end{aligned} \right) \\ & = \left(\hat{b}\hat{b} - \frac{1}{3} I \right) \int_{-1}^1 d\varphi \int_0^\infty \frac{\pi Vt_i^3}{(n_i m_i Vt_i^2/2) Vt_i^2} x^{1/2} dx \left(\frac{2}{3} \frac{m_i}{(n_i m_i Vt_i^2/2) Vt_i^2} \right) \cdot \left(Vt_i^2 x^2 \left(\frac{3\varphi^2-1}{2} \right)^2 \right) \\ & \times \left(\frac{W_{ii}}{\pi^{3/2} Vt_i^3} e^{-x} \right) \sum_{k=0}^{(5/2)} b_k L_k^{(5/2)} \\ & = \left(\hat{b}\hat{b} - \frac{1}{3} I \right) \frac{4}{3\pi} \int_{-1}^1 d\varphi \left(\frac{3\varphi^2-1}{2} \right)^2 \sum_{k=0}^{(5/2)} b_k \int_0^\infty x^{5/2} e^{-x} L_k^{(5/2)}(x) L_k^{(5/2)}(x) \\ & = \left(\hat{b}\hat{b} - \frac{1}{3} I \right) b_0 \quad \leftarrow b_0 (+ L_0^{(5/2)}) \text{ is parallel component of the viscous tensor.} \end{aligned}$$

$$\left(\frac{w_{||}^2}{2} - \frac{w_\perp^2}{2} \right) = w^2 P_2(\xi)$$

Also, notice that $P_1(\xi) = \xi = \frac{w_{||}}{w}$, $P_2(\xi) = \frac{1}{2}(3\xi^2 - 1)$: Legendre polynomial

Then, $\langle f_{ii} \rangle_a + \langle f_{ii} \rangle_b = 2\int_{-1}^1 \xi P_1(\xi) f_{Mi} \sum_k \frac{a_k}{Vt_i} L_k^{(3/2)}(x) + \frac{2}{3} \int_{-1}^1 \xi P_2(\xi) f_{Mi} \sum_k \frac{b_k}{P_i} L_k^{(5/2)}(x)$

↳ one can separate the calculation $\langle f_{ii} \rangle_a$ and $\langle f_{ii} \rangle_b$ due to the orthogonality.

$$\left(\int_{-1}^1 d\xi P_p(\xi) P_q(\xi) \right) = \frac{2}{2p+1} \delta_{pq}$$

② Gyro-averaged ion distribution function.

이제 $\langle f_{ii} \rangle_a$ 와 $\langle f_{ii} \rangle_b$ 를 각각 따로 구해보자!

① $\int d\vec{w} w_{||} L_k^{(3/2)} C_{ii}^k [\langle f_{ii} \rangle_a] = \frac{n_i}{Z_{ii}} \begin{pmatrix} 1 & 3/4 \\ 3/4 & 45/16 \end{pmatrix} \begin{pmatrix} a_1 \\ a_2 \end{pmatrix} \Rightarrow \begin{matrix} a_1 = \dots \\ a_2 = \dots \end{matrix}$

$$\int d\vec{w} w_{||} L_k^{(3/2)}(x) f_{Mi} \left(x^2 - \frac{5}{2} \right) w_{||} \hat{b} \cdot \vec{v} \ln T_i = -\frac{5}{2} \frac{p_i}{m_i} (\hat{b} \cdot \vec{v} \ln T_i) f_{ki}$$

$$\Rightarrow \langle f_{ii} \rangle_a = w_{||} f_{Mi} Z_{ii} (\hat{b} \cdot \vec{v} \ln T_i) \left[\frac{25}{16} L_1^{(3/2)}(x) - \frac{5}{12} L_2^{(5/2)}(x) \right]$$

② $\int d\vec{w} \left(w_{||}^2 - w_\perp^2/2 \right) L_k^{(5/2)}(x) C_{ii}^k [\langle f_{ii} \rangle] = -\frac{6}{5} \frac{n_i}{Z_{ii}} \begin{pmatrix} 1 & 3/4 \\ 3/4 & 205/48 \end{pmatrix} \begin{pmatrix} b_0 \\ b_1 \end{pmatrix} \Rightarrow \begin{matrix} b_0 = \dots \\ b_1 = \dots \end{matrix}$

$$\begin{aligned} \int d\vec{w} \left(w_{||}^2 - w_\perp^2/2 \right) L_k^{(5/2)}(x) &= \frac{m_i}{2T_i} \left(w_{||}^2 - w_\perp^2/2 \right) (\hat{b}\hat{b} - \frac{1}{3}\hat{I}) \stackrel{\leftrightarrow}{=} W_i f_{Mi} \\ &= m_i n_i \int d\vec{w} \left(w_{||}^2 - \frac{w_\perp^2}{2} \right)^2 L_k^{(5/2)}(x) \frac{f_{Mi}}{Vt_i^2} (\hat{b}\hat{b} - \frac{1}{3}\hat{I}) \stackrel{\leftrightarrow}{=} W_i = \frac{3}{2} p_i n_i (\hat{b}\hat{b} - \frac{1}{3}\hat{I}) \stackrel{\leftrightarrow}{=} W_i f_{ki} \end{aligned}$$

$$\Rightarrow \langle f_{ii} \rangle_b = - \left(\frac{w_{||}^2 - w_\perp^2/2}{Vt_i^2} \right) f_{Mi} Z_i (\hat{b}\hat{b} - \frac{1}{3}\hat{I}) \stackrel{\leftrightarrow}{=} W_i \left[\frac{1025}{1068} L_0^{(5/2)}(x) - \frac{45}{267} L_1^{(5/2)}(x) \right]$$

③ Gyro-dependent ion distribution function.

$$\begin{aligned} \vec{W} \vec{W} - \frac{w^2}{3} \hat{I} &= \left(w_{||}^2 - \frac{w_\perp^2}{2} \right) \left(\hat{b}\hat{b} - \frac{1}{3}\hat{I} \right) \\ &= \underbrace{W_{||}^2 \hat{b}\hat{b}}_{W_{||}^2 \hat{b}\hat{b}} + \underbrace{W_{||} \vec{W}_\perp}_{\vec{W}_\perp \vec{W}_\perp} + \underbrace{W_\perp \vec{W}_{||}}_{\vec{W}_\perp \vec{W}_{||}} + \underbrace{W_\perp^2 \hat{I}}_{W_\perp^2 \hat{I}} - \frac{w^2}{3} \hat{I} + \left(-w_{||}^2 \hat{b}\hat{b} + \frac{1}{3} w_{||}^2 \hat{I} + \frac{w_\perp^2}{2} \hat{b}\hat{b} - \frac{1}{6} w_\perp^2 \hat{I} \right) \\ &= (*) - \frac{w_\perp^2}{3} \hat{I} - \frac{w_{||}^2}{2} \hat{I} + \frac{w_{||}^2}{3} \hat{I} + \frac{w_\perp^2}{2} (\hat{b}\hat{b} - \frac{1}{3}\hat{I}) \\ &= \vec{W}_{||} \vec{W}_\perp + \vec{W}_\perp \vec{W}_{||} + \vec{W}_\perp \vec{W}_\perp + (w_\perp^2/2) (\hat{b}\hat{b} - \frac{1}{3}\hat{I}) \end{aligned}$$

$$\Rightarrow C_{ii}^k [\tilde{f}_{ii}] + w_{ci} \frac{d\tilde{f}_{ii}}{dy} = f_{Mi} \left(\frac{w^2}{Vt_i^2} - \frac{5}{2} \right) \vec{W}_\perp \cdot \vec{v} \ln T_i + f_{Mi} \left[\frac{\vec{W}_{||} \vec{W}_\perp + \vec{W}_\perp \vec{W}_{||} + \vec{W}_\perp \vec{W}_\perp + (w_\perp^2/2)(\hat{I} - \hat{b}\hat{b})}{Vt_i^2} \right] \stackrel{\leftrightarrow}{=} W_i$$

Similarly to electrons, take ordering $\tilde{f}_{ii} = \tilde{f}_{ii}^{(0)} + \tilde{f}_{ii}^{(1)}$

i) Lowest-order

$$w_{ci} \frac{d\tilde{f}_{ii}^{(0)}}{dr} = f_{Mi} \left(\frac{\omega^2}{Vt_i^2} - \frac{5}{2} \right) \vec{w}_\perp \cdot \vec{D} \ln T + f_{Mi} \left[\frac{\vec{w}_{ii} \vec{w}_\perp + \vec{w}_\perp \vec{w}_{ii} + \vec{w}_\perp \vec{w}_\perp - (\omega_\perp^2/2)(\vec{I} - \vec{b}\vec{b})}{Vt_i^2} \right] \leftrightarrow : w_i$$

↓ Integrate

$$\tilde{f}_{ii}^{(0)} = f_{Mi} L_1^{(3/2)}(\lambda) \frac{\vec{w}_\perp \times \hat{b}}{w_{ci}} \cdot \vec{D} \ln T_i$$

$$+ f_{Mi} \left[\frac{\vec{w}_{ii} \vec{w}_\perp \times \hat{b} + \vec{w}_\perp \vec{w}_{ii} \times \hat{b} + (\omega_\perp^2/4)[(\hat{x}\hat{x} - \hat{y}\hat{y}) \sin 2r - (\hat{x}\hat{y} + \hat{y}\hat{x}) \cos 2r]}{Vt_i^2 w_{ci}} \right] \leftrightarrow : w_i$$

ii) Next-order

$$w_{ci} \frac{d\tilde{f}_{ii}^{(1)}}{dr} = -C_{ii}^l \left[\tilde{f}_{ii}^{(0)} \right] \quad \text{Once again, it's not necessary to integrate the equation}$$

- Ion heat flux

$$\vec{q}_i = -T_i \int d\vec{w} \vec{w} L_1^{(3/2)}(\lambda) (\langle f_{ii} \rangle + \tilde{f}_{ii}^{(0)} + \tilde{f}_{ii}^{(1)}) \equiv \vec{q}_{||i} + \vec{q}_{\perp i} + \vec{q}_{\perp i}$$

- Ion viscosity

$$\begin{aligned} \overleftrightarrow{\Pi} &= \int d\vec{w} m_i (\vec{w}\vec{w} - \frac{\omega^2}{3} \vec{I}) (\langle f_{ii} \rangle + \tilde{f}_{ii}^{(0)} + \tilde{f}_{ii}^{(1)}) \\ &= (\hat{b}\hat{b} - \frac{1}{3} \vec{I}) \int d\vec{w} m_i (\vec{w}_{ii} - \frac{\omega_\perp^2}{2}) \langle f_{ii} \rangle + \int d\vec{w} m_i (\vec{w}\vec{w} - \frac{\omega^2}{3} \vec{I}) (\tilde{f}_{ii}^{(0)} + \tilde{f}_{ii}^{(1)}) \\ &= \overline{\Pi}_{||i} (\hat{b}\hat{b} - \frac{1}{3} \vec{I}) + \overline{\Pi}_{\perp i} + \overline{\Pi}_{\perp i} \\ &\quad \uparrow \quad \uparrow \quad \uparrow \\ &\text{parallel viscosity} \quad \text{gyro-viscosity} \quad \text{perpendicular viscosity} \end{aligned}$$

④ Ion transport coefficients by Braginskii

$$q_{\parallel ii} = -k_{\parallel ii} D_{\parallel i} T_i \quad (k_{\parallel ii} \equiv 3.91 \frac{p_i Z_{ii}}{m_i})$$

$$\vec{q}_{\parallel Ni} = \frac{5}{2} \frac{p_i}{m_i W_{ci}} \hat{b} \times \vec{v} T_i$$

$$\vec{q}_{\perp ii} = -k_{\perp i} D_{\perp i} T_i \quad (k_{\perp i} \equiv 2 \frac{p_i}{m_i Z_i W_{ci} c^2})$$

$$\leftrightarrow \quad \vec{T}_{\parallel ii} = -0.96 p_i Z_{ii} \frac{3}{2} \left(\hat{b} \hat{b} - \frac{1}{3} \vec{I} \right) \left(\hat{b} \hat{b} - \frac{1}{3} \vec{I} \right) \vec{W}_i \quad \rightarrow \quad M_{\parallel ii} = 0.96 p_i Z_{ii}$$

$$\leftrightarrow \quad \vec{T}_{\perp Ni} = \frac{p_i}{4 W_{ci}} \left[\hat{b} \times \vec{W}_i \cdot (\vec{I} + 3 \hat{b} \hat{b}) - (\vec{I} + 3 \hat{b} \hat{b}) \cdot \vec{W}_i \times \hat{b} \right]$$

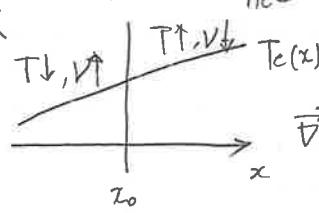
$$\leftrightarrow \quad \vec{T}_{\perp i} = -\frac{3}{10} \frac{p_i}{Z_i W_{ci} c^2} \left[(\vec{I} - \hat{b} \hat{b}) \cdot \vec{W}_i \cdot (\vec{I} + 3 \hat{b} \hat{b}) + (\vec{I} + 3 \hat{b} \hat{b}) \cdot \vec{W}_i \cdot (\vec{I} - \hat{b} \hat{b}) \right]$$

⑤ Summary.

(1) Parallel friction force.

$$R_{\parallel ie} = \gamma_{\parallel} n_e e^2 (U_{\parallel ii} - U_{\parallel ie}) - 0.71 n_e D_{\parallel i} T_e \quad (\gamma_{\parallel} \equiv 0.51 \frac{mc}{n_e e^2 c_a})$$

\uparrow
friction to electrons by ions
due to speed difference.



From $T \downarrow$ to $T \uparrow$ particle will have more momentum than from $T \uparrow$ to $T \downarrow$
particle due to difference of collision

(2) Parallel heat flux

$$q_{\parallel ie} = -k_{\parallel ie} D_{\parallel i} T_e - 0.71 p_e (U_{\parallel ii} - U_{\parallel ie}) \quad (k_{\parallel ie} \equiv 3.16 \frac{p_e T_{ei}}{mc})$$

$$q_{\parallel ii} = -k_{\parallel ii} D_{\parallel i} T_i \quad (k_{\parallel ii} \equiv 3.91 \frac{p_i T_{ii}}{m_i})$$

\uparrow
(slow electrons are more likely to collide with ions
and so are more apt to lose energy by flowing ions
than fast electrons.)

$$\Rightarrow \frac{k_{\parallel ie}}{k_{\parallel ii}} \sim 0(\sqrt{\frac{m_i}{m_e}})$$

\hookrightarrow electron heat flux is dominant.

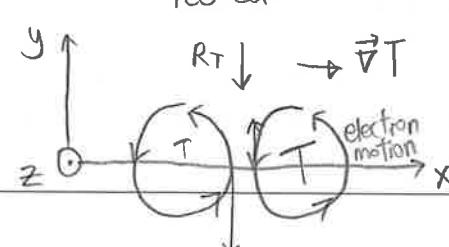
(3) Perpendicular friction force

$$\vec{R}_{\perp ei} = \gamma_{\perp} e^2 n_e^2 (\vec{U}_{\perp i} - \vec{U}_{\perp e}) + \frac{3}{2} \frac{n_e}{W_{ce} T_{ei}} \hat{b} \times \vec{v} T_e \quad (\gamma_{\perp} \equiv \frac{mc}{n_e e^2 c_a})$$

\uparrow
gyro-motion plays a role to
restrict the change in f.

$$\Rightarrow \gamma_{\perp} \approx 2 \gamma_{\parallel i}$$

* note $W_{ce} < 0$



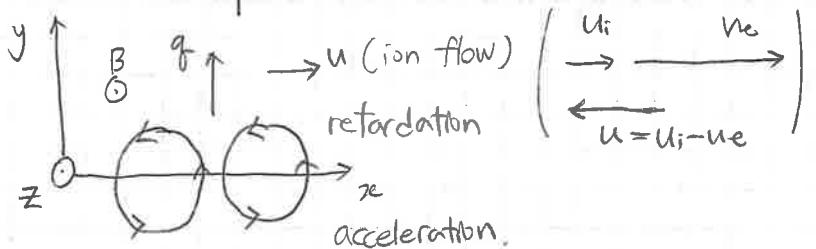
*
(양쪽이 더 빨라서
momentum이 틀리고 있는다)

(4) Perpendicular heat flux

$$\vec{q}_{\perp e} = \frac{5}{2} \frac{P_e}{m_e w_{ce}} \hat{b} \times \vec{\nabla} T_e, \quad \vec{q}_{\perp i} = \frac{5}{2} \frac{P_i}{m_i w_{ci}} \hat{b} \times \vec{\nabla} T_i \quad \leftarrow \text{diamagnetic}$$

$$\vec{q}_{\parallel e} = -k_{\perp e} \vec{\nabla}_{\perp} T_e + \frac{3}{2} \frac{P_e}{Z_e i w_{ce}} \hat{b} \times (\vec{u}_i - \vec{u}_e) \quad (k_{\perp e} \equiv 4.66 \frac{P_e}{m_e Z_e i w_{ce}^2})$$

$$\vec{q}_{\parallel i} = -k_{\perp i} \vec{\nabla}_{\perp} T_i \quad (k_{\perp i} \equiv 2 \frac{P_i}{m_i Z_i i w_{ci}^2})$$



(5) Further words

- $q_{\parallel ee} \gg q_{\perp ee} \gg q_{\perp ec}$, $q_{\parallel ee} : q_{\perp ee} : q_{\perp ec} = 1 : \frac{1}{Z_e i w_{ce}} : \frac{1}{(Z_e i w_{ce})^2}$

$$\left(\frac{Z_i i w_{ci}}{Z_e i w_{ce}} = 0 \left(\sqrt{\frac{m_e}{m_i}} \right) \right)$$

- $q_{\parallel ii} > q_{\perp ii} > q_{\perp ei}$, $q_{\parallel ii} : q_{\perp ii} : q_{\perp ei} = 1 : \frac{1}{Z_i i w_{ci}} : \frac{1}{(Z_i i w_{ci})^2}$

- $q_{\perp ee} \gg q_{\parallel ee}$, $q_{\perp ee} \sim q_{\perp ii}$, $q_{\perp ec} \ll q_{\perp ei}$

- $\frac{\leftrightarrow}{\Pi_i} \gg \frac{\leftrightarrow}{\Pi_e}$