

Fusion Plasma Theory 2

Lecture 20 - 21 : Chapman - Enskog - Braginskii

① Chapman - Enskog process

- Asymptotic expansions of the Boltzmann kinetic equation
- follows a hierarchy of temporal and spatial scales and solves the kinetic equation order by order in the scale separations.
- Time-scale ordering by Chapman - Enskog

$$\frac{Df}{Dt} \equiv \frac{df}{dt} + \vec{v} \cdot \vec{\nabla} f + \vec{a} \cdot \frac{d\vec{v}}{dt} = C[f]$$

ordering by Knudsen number $K_n \equiv \frac{\lambda_{mfp}}{L} \equiv \epsilon \ll 1$

$$\text{and } v \gg v_E/L \gg D/L^2 \quad (\Leftrightarrow t_0 \ll t_1 \ll t_2)$$

$$\left\{ \begin{array}{l} t_0 \sim v^{-1} : \text{collisional transport} \\ t_1 \sim L/v_E \sim (L/\lambda_{mfp})(\lambda_{mfp}/v_E) \sim (L/\lambda_{mfp}) v^{-1} \sim t_0/\epsilon : \text{non-dissipative time-scale (MHD)} \\ t_2 \sim D/L^2 \sim (L^2/\lambda_{mfp}^2) v^{-1} \sim t_0/\epsilon^2 : \text{dissipative and transport time scale.} \end{array} \right.$$

- Multi-scale analysis in Chapman - Enskog

$$\left(\frac{D}{Dt_0} + \epsilon \frac{D}{Dt_1} + \epsilon^2 \frac{D}{Dt_2} \right) (f_0 + \epsilon f_1 + \epsilon^2 f_2 + \dots) = C[f_0 + \epsilon f_1 + \epsilon^2 f_2 + \dots]$$

i) Zeroth-order

$$\frac{Df_0}{Dt_0} = C[f_0] \quad \leftarrow \text{we will drop this by assuming kinetic equilibrium.}$$

(this happens instantaneously in the subsidiary time scales)

To go for next-orders, consider the collisional operator expansion first

$$\begin{aligned} C[f] &= C[f_0 + \epsilon f_1 + \epsilon^2 f_2 + \dots, f_0 + \epsilon f_1 + \epsilon^2 f_2 + \dots] \\ &= \underbrace{C[f_0, f_0]}_{C[f_0]} + \epsilon \underbrace{(C[f_0, f_1] + C[f_1, f_0])}_{\hat{C}f_1} + \epsilon^2 \underbrace{(C[f_0, f_2] + C[f_2, f_0] + C[f_1, f_1])}_{\hat{C}f_2 + C[f_1]} \end{aligned}$$

$$\text{Resulting equations: } \left\{ \begin{array}{l} 0 = C[f_0] \\ \frac{Df_0}{Dt_1} = \hat{C}f_1 \\ \frac{Df_0}{Dt_2} + \frac{Df_1}{Dt_1} = \hat{C}f_2 + C[f_1] \end{array} \right.$$

$D = C[f_0]$ gives local Maxwellian :

$$f_M(\vec{x}, t) = n(\vec{x}, t) \left(\frac{m}{2\pi T(\vec{x}, t)} \right)^{3/2} \exp\left(-m \frac{\vec{x} - \vec{u}(\vec{x}, t)}{2T(\vec{x}, t)}\right)$$

An important assumption is that n, \vec{u}, T are true values, which are consistent with the total distribution function.

Let's put $f_0 = f_M$ to the first-order equation: $\frac{Df_0}{Dt_1} = \hat{C} f_1$

one will have the homogeneous solutions: $\hat{C} f_1^{\text{homo}} = 0$.

$$(1) \underline{f_1^{\text{homo}} = (1, \vec{v}, v^2) f_M. \text{ (or } f_1^{\text{homo}} = (A + \vec{B} \cdot \vec{v} + C v^2) f_M)}$$

The linear combinations can be used to adjust n', \vec{u}', T' from f_0 to be consistent with true n, \vec{u}, T .

(2) To have a solution, the equation must meet the solvability conditions by Fredholm alternative theorem in the first place.

$$\frac{Df_0}{Dt_1} = \hat{C} f_1 \Rightarrow \underline{\langle (1, \vec{v}, v^2) f_M, \frac{Df_M}{Dt_1} \rangle = \int (1, \vec{v}, v^2) \frac{Df_M}{Dt_1} d\vec{v} = 0}$$

↳ These are just particle, momentum, energy conservation of Maxwellian.

*note

: Fredholm alternative theorem

Solution f_1 이 존재하기 위해서는, $\hat{C} f_1 \neq \text{null space}$ 와 $\frac{Df_0}{Dt_1}$ 가 수직이어야 한다.

$$\Rightarrow \langle (1, \vec{v}, v^2) f_M, \frac{Df_M}{Dt_1} \rangle = \int (1, \vec{v}, v^2) \frac{Df_M}{Dt_1} d\vec{v} = 0 \text{ 성립! by conservation.}$$

- Second-order solvability condition

The same solvability condition is applied. Both linearized \hat{C} and C operators have the solution of $(1, \vec{v}, v^2) f_M$. To have the solution order f_2 , it must meet the solvability condition:

$$\int d\vec{v} (1, \vec{v}, v^2) \left(\frac{Df_M}{Dt_2} + \frac{Df_1}{Dt_1} \right) = 0$$

i) $\int d\vec{v} (1, \vec{v}, v^2) \frac{Df_m}{Dt} = 0 \rightarrow$ Euler (conservation) equation

ii) $\int d\vec{v} (1, \vec{v}, v^2) \frac{Df_i}{Dt} = \int d\vec{v} (1, \vec{v}, v^2) \left(\frac{df_i}{dt} + \vec{v} \cdot \vec{\nabla} f_i + \vec{a} \cdot \frac{d\vec{v}}{dt} \right) = \vec{v} \cdot \int d\vec{v} (1, \vec{v}, v^2) \vec{\nabla} f_i$

$$\left(\vec{a} \cdot \frac{d\vec{v}}{dt} = \frac{d}{dt} (\vec{a} f_i) - \left(\frac{d}{dt} \vec{a} \right) f_i = \frac{d}{dt} (\vec{a} f_i) + \frac{q}{m} \frac{d}{dt} (\vec{v} \times \vec{B}) = 0, \quad \frac{d}{dt} = 0 \right)$$

\Rightarrow Systematic conclusion of Chapman - Enskog kinetic asymptotic expansion:

$$\underbrace{\int d\vec{v} (1, \vec{v}, v^2) \frac{Df_m}{Dt}}_{\text{Nondissipative part}} = \underbrace{-\vec{v} \cdot \int d\vec{v} (1, \vec{v}, v^2) \vec{\nabla} f_i}_{\text{dissipative flux}} \quad \text{Solvability condition returns the transport equation}$$

② Preface for Braginskii

- Braginskii vs. Chapman-Enskog

(1) Magnetization brings anisotropy (2) Two components creates frictional exchange even in Maxwellian.

- Assumption: $K_n = \epsilon \ll 1$, $\rho/L \sim O(\epsilon)$, and high-fbw ordering $\vec{U}_{i,e} \sim v_{ti} \ll v_{te}$.

③ Transformation of kinetic equation on a moving frame.

$$\vec{w} = \vec{v} - \vec{u}(\vec{x}, t) \Rightarrow f(\vec{x}, \vec{v}, t) \rightarrow f(\vec{x}, \vec{w}, t)$$

$$\left(\begin{aligned} \frac{d}{dt} \Big|_{\vec{v}} &= \frac{d}{dt} \Big|_{\vec{w}} + \frac{d\vec{w}}{dt} \Big|_{\vec{v}} \cdot \frac{d}{d\vec{w}} = \frac{d}{dt} \Big|_{\vec{w}} - \frac{d\vec{u}}{dt} \cdot \frac{d}{d\vec{w}} \\ \frac{d}{d\vec{x}} \Big|_{\vec{v}} &= \frac{d}{d\vec{x}} \Big|_{\vec{w}} + \frac{d\vec{w}}{d\vec{x}} \Big|_{\vec{v}} \cdot \frac{d}{d\vec{w}} = \frac{d}{d\vec{x}} \Big|_{\vec{w}} - \vec{\nabla} \vec{u} \cdot \frac{d}{d\vec{w}} \end{aligned} \right)$$

New kinetic equation becomes:

$$\frac{Df}{Dt} = \frac{df}{dt} + \vec{v} \cdot \frac{df}{d\vec{x}} + \vec{a} \cdot \frac{d\vec{v}}{dt} = C[f]$$

$$\frac{df}{dt} + \vec{w} \cdot \vec{\nabla} f + \vec{w} \cdot \vec{\nabla} f - \vec{w} \cdot \vec{\nabla} \vec{u} \frac{df}{d\vec{w}} + \left[\frac{q}{m} (\vec{E}' + \vec{w} \times \vec{B}) - \frac{d\vec{w}}{dt} \right] \cdot \frac{d\vec{w}}{dt} = C[f]$$

$$\Rightarrow \frac{df}{dt} + \vec{w} \cdot \vec{\nabla} f + \left[\frac{q}{m} (\vec{E}' + \vec{w} \times \vec{B}) - \frac{d\vec{w}}{dt} \right] \cdot \frac{d\vec{w}}{dt} - \vec{w} \cdot \vec{\nabla} \vec{u} \frac{df}{d\vec{w}} = C[f]$$

$$\text{where } \vec{E}' = \vec{E} + \vec{u} \times \vec{B} \quad \text{and} \quad \frac{d}{dt} = \frac{d}{dt} + \vec{u} \cdot \vec{\nabla}$$

⊕ Electron kinetic equation.

$$C_{ee}^L[f_e] + v_{ei} L_{ei}[f_e] + v_{ei} \frac{m\vec{w} \cdot \vec{u}}{T_e} f_{me}$$

$$= \frac{df_e}{dt} + \vec{w} \cdot \vec{\nabla} f_e - \left(\frac{e}{m} (\vec{E}' + \vec{w} \times \vec{B}) + \frac{d\vec{u}_e}{dt} \right) \cdot \frac{df_e}{d\vec{w}} - \vec{w} \cdot \vec{\nabla} \vec{u} \cdot \frac{df_e}{d\vec{w}}$$

↓

$$C_{ee}^L[f_e] + v_{ei} L_{ei}[f_e] + \frac{e}{m} \vec{w} \times \vec{B} \cdot \frac{df_e}{d\vec{w}}$$

$$= \frac{df_e}{dt} + \vec{w} \cdot \vec{\nabla} f_e - \left(\frac{e}{m} \vec{E}' + \frac{d\vec{u}_e}{dt} \right) \cdot \frac{df_e}{d\vec{w}} - \vec{w} \cdot \vec{\nabla} \vec{u} \cdot \frac{df_e}{d\vec{w}} - v_{ei} \frac{m\vec{w} \cdot \vec{u}}{T_e} f_{me}$$

Expanding $f_e = f_{e0} + f_{e1} + \dots$

i) zeroth-order equation (LHS: $O(E^{-1})$, RHS: $O(1)$) \therefore LHS \gg RHS.

$$C_{ee}^L[f_e] + v_{ei} L_{ei}[f_e] + \frac{e}{m} \vec{w} \times \vec{B} \cdot \frac{df_e}{d\vec{w}} = 0 \Rightarrow f_{e0} = f_{me} \text{ (Maxwellian)}$$

ii) next-order equation

*note $\ln f_{me} = \text{const} + \ln n_e - \frac{3}{2} \ln T_e + \frac{m\vec{w}^2}{2T_e}$

$$\frac{d}{dt} f_m = f_m \frac{d}{dt} \ln f_m = f_m \left(\frac{d}{dt} \ln n_e - \frac{3}{2} \frac{d}{dt} \ln T_e + \frac{m\vec{w}^2}{2T_e} \frac{d}{dt} \ln T_e \right) = f_m \left(\frac{d}{dt} \ln n_e + \left(\frac{m\vec{w}^2}{2T_e} - \frac{3}{2} \right) \frac{d}{dt} \ln T_e \right)$$

$$\vec{w} \cdot \vec{\nabla} f_m = f_m (\vec{w} \cdot \vec{\nabla} \ln n_e + \left(\frac{m\vec{w}^2}{2T_e} - \frac{3}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_e)$$

$$\frac{df_m}{d\vec{w}} = -\frac{m\vec{w}}{T_e} f_m$$

$$C_{ee}^L[f_{e1}] + v_{ei} L_{ei}[f_{e1}] + \frac{e}{m} \vec{w} \times \vec{B} \cdot \frac{df_{e1}}{d\vec{w}}$$

$$= \left[\frac{d}{dt} \ln n_e + \left(\frac{m\vec{w}^2}{2T_e} - \frac{3}{2} \right) \frac{d}{dt} \ln T_e + \vec{w} \cdot \vec{\nabla} \ln n_e + \left(\frac{m\vec{w}^2}{2T_e} - \frac{3}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_e \right. \\ \left. + \frac{m\vec{w}}{T_e} \left(\frac{e}{m} \vec{E}' + \frac{d\vec{u}_e}{dt} \right) + \frac{m\vec{w} \cdot \vec{w}}{T_e} \cdot \vec{\nabla} \vec{u} - v_{ei} \frac{m\vec{w} \cdot \vec{u}}{T_e} \right] f_{me}$$

< Braginskii's correction equation >

- Solvability condition of the first-order Chapman-Enskog expansion

$$\int d\vec{w} (1, \vec{w}, w^2) \times \text{RHS} = 0$$

*note that $\left(\begin{array}{l} \int w_x f_{ne}(w) dw = 0 \quad \& \quad \int w_x w_y f_{ne}(w) dw = 0 \\ \text{(odd part)} \quad \quad \quad \text{(서로 다른 성분을 odd 번 곱하기)} \end{array} \right)$

1 Particle conservation.

$$\int d\vec{w} 1 \cdot (\text{RHS}) = 0$$

$$\text{i)} \int d\vec{w} \left[\frac{d \ln n_e}{dt} f_{ne} \right] = n_e \frac{d \ln n_e}{dt}$$

$$\text{ii)} \int d\vec{w} \left[\left(\frac{mw^2}{2T_e} - \frac{3}{2} \right) \frac{d \ln T_e}{dt} f_{ne} \right] = \frac{d \ln T_e}{dt} \left(\frac{3p_e}{2T_e} - \frac{3}{2} n_e \right) = 0$$

$$\text{iii)} \int d\vec{w} \left[\vec{w} \cdot \vec{\nabla} \ln n_e + \left(\frac{mw^2}{2T_e} - \frac{3}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_e + \frac{m\vec{w}}{T_e} \left(\frac{e}{m} \vec{E}' + \frac{d\vec{u}_e}{dt} \right) - v_{ei} \frac{m\vec{w} \cdot \vec{u}}{T_e} \right] f_{ne} = 0$$

$$\text{iv)} \int d\vec{w} \left[\frac{m\vec{w}\vec{w}}{T_e} : \vec{\nabla} \vec{u}_e f_{ne} \right] = \frac{\vec{p}_e}{T_e} : \vec{\nabla} \vec{u}_e = n_e (\vec{\nabla} \vec{u}_e)$$

$$\therefore \text{(i)} + \text{(iv)} \Rightarrow \boxed{\frac{d \ln n_e}{dt} = -\vec{\nabla} \cdot \vec{u}_e}$$

2 Momentum conservation

(*note $\int m w^2 f_{ne} dw = 3 n_e T_e$
 $\int (m w^2)^2 f_{ne} dw = 15 n_e T_e^2 / \int w^4 f_{ne} dw = 15 n_e \left(\frac{T_e}{m} \right)^2$)

$$\int d\vec{w} \cdot \vec{w} \cdot (\text{RHS}) = 0$$

$$\text{i)} \int d\vec{w} \left[\frac{d}{dt} \ln n_e + \left(\frac{mw^2}{2T_e} - \frac{3}{2} \right) \frac{d}{dt} \ln T_e + \frac{m\vec{w}\vec{w}}{T_e} : \vec{\nabla} \vec{u}_e \right] \vec{w} f_{ne} = 0$$

$$\text{ii)} \int d\vec{w} \left[\vec{w} \cdot \vec{\nabla} \ln n_e \right] \vec{w} f_{ne} = \frac{\vec{\nabla} n_e}{n_e} \frac{p_e}{m_e} = \frac{T_e}{m_e} \vec{\nabla} n_e$$

$$\begin{aligned} \text{iii)} \int d\vec{w} \left[\left(\frac{mw^2}{2T_e} - \frac{3}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_e \right] \vec{w} f_{ne} &= \int d\vec{w} \left[\left(\frac{mw^2}{2T_e} - \frac{3}{2} \right) \vec{w}\vec{w} \cdot \frac{\vec{\nabla} T_e}{T_e} \right] f_{ne} \\ &= \int d\vec{w} \frac{mw^2}{2T_e} \vec{w}\vec{w} \frac{\vec{\nabla} T_e}{T_e} f_{ne} - \frac{3p_e}{2m_e} \frac{\vec{\nabla} T_e}{T_e} = \frac{m\vec{\nabla} T_e}{2T_e^2} \int d\vec{w} \frac{1}{3} w^4 f_{ne} - \frac{3n_e}{2m_e} \vec{\nabla} T_e = \frac{m\vec{\nabla} T_e}{6T_e^2} \frac{15n_e T_e^2}{m^2} - \frac{3n_e}{2m_e} \vec{\nabla} T_e \\ &= \left(\frac{5}{2} - \frac{3}{2} \right) \frac{n_e}{m_e} \vec{\nabla} T_e = \frac{n_e \vec{\nabla} T_e}{m_e} \end{aligned}$$

$$\text{iv)} \int d\vec{w} \left[\frac{m\vec{w}}{T_e} \left(\frac{e}{m} \vec{E}' + \frac{d\vec{u}_e}{dt} \right) \right] \vec{w} f_{ne} = \frac{m}{T_e} \frac{n_e T_e}{m} \left(\frac{e}{m} \vec{E}' + \frac{d\vec{u}_e}{dt} \right) = n_e \left(\frac{e}{m} \vec{E}' + \frac{d\vec{u}_e}{dt} \right)$$

$$\text{v)} \int d\vec{w} \left[-v_{ei} \frac{m\vec{w} \cdot \vec{u}}{T_e} \right] \vec{w} f_{ne} = -v_{ei} \frac{m_e}{T_e} \left(\frac{n_e T_e}{m} \right) \vec{u} = -n_e v_{ei} \vec{u} = -\frac{1}{m} \vec{R}_{ei}$$

∴ To sum-up, $= \frac{T_e}{m_e} \vec{\nabla} n_e + \frac{n_e}{m_e} \vec{\nabla} T_e + n_e \left(\frac{e}{m} \vec{E}' + \frac{d\vec{u}_e}{dt} \right) - \frac{1}{m} \vec{R}_{ei}^{(0)} = 0$

$$\Rightarrow \boxed{\frac{d\vec{u}_e}{dt} = -\frac{e}{m_e} \vec{E}' + \frac{\vec{R}_{ei}^{(0)} - \vec{\nabla}(n_e T_e)}{m_e n_e}}$$

③ Energy conservation

*note $\int \vec{w}^2 f_{me} d\vec{w} = 3n_e \left(\frac{T_e}{m_e} \right)$, $\int \vec{w}^4 f_{me} d\vec{w} = 15n_e \left(\frac{T_e}{m_e} \right)^2$

$\int \vec{w}^2 \cdot (\text{RHS}) d\vec{w} = 0$

i) $\int d\vec{w} \vec{w}^2 \left[\frac{dn_e}{dt} f_{me} \right] = \frac{3n_e T_e}{m} \frac{dn_e}{dt}$

ii) $\int d\vec{w} \vec{w}^2 \left[\left(\frac{m\vec{w}^2}{2T_e} - \frac{3}{2} \right) \frac{dT_e}{dt} f_{me} \right] = \frac{dT_e}{dt} \left[\frac{m_e}{2T_e} 15n_e \left(\frac{T_e}{m_e} \right)^2 - \frac{3}{2} \cdot 3n_e \left(\frac{T_e}{m_e} \right) \right] = 3 \frac{n_e T_e}{m} \frac{dT_e}{dt}$

iii) $\int d\vec{w} \vec{w}^2 \left[\frac{m\vec{w}\vec{w}}{T_e} \cdot \vec{\nabla} u_e f_{me} \right] = \frac{m_e}{T_e} \cdot \int \frac{1}{3} \vec{w}^4 \vec{I} = \vec{\nabla} u_e f_{me} = 5 \frac{m_e}{T_e} n_e \left(\frac{T_e}{m_e} \right)^2 \vec{\nabla} \cdot \vec{u}_e = 5 \frac{n_e T_e}{m_e} \vec{\nabla} \cdot \vec{u}_e$

iv) $\int d\vec{w} \cdot (\text{etc}_{iii}) = 0$ (odd-part)

∴ To sum-up, $\frac{dn_e}{dt} + \frac{dT_e}{dt} + \frac{5}{3} \vec{\nabla} \cdot \vec{u}_e = 0 \Rightarrow (-\vec{\nabla} \cdot \vec{u}_e) + \frac{dT_e}{dt} + \frac{5}{3} \vec{\nabla} \cdot \vec{u}_e = 0$

$$\Rightarrow \boxed{\frac{dT_e}{dt} = -\frac{2}{3} \vec{\nabla} \cdot \vec{u}_e}$$

- Inserting 3 conservation eqns to Braginskii's correction equation for electrons:

$$\left(C_{ee}^1 [f_{ei}] + \nu_{ei} L_{ei} [f_{ei}] + \frac{e}{m} \vec{w} \times \vec{B} \cdot \frac{df_{ei}}{d\vec{w}} \right. \\ \left. = \left[\underbrace{\frac{dn_e}{dt}}_a + \underbrace{\left(\frac{m\vec{w}^2}{2T_e} - \frac{3}{2} \right) \frac{dT_e}{dt}}_b + \underbrace{\vec{w} \cdot \vec{\nabla} \ln n_e}_c + \underbrace{\left(\frac{m\vec{w}^2}{2T_e} - \frac{3}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_e}_d \right. \right. \\ \left. \left. + \underbrace{\frac{m\vec{w}}{T_e} \cdot \left(\frac{e}{m} \vec{E}' + \frac{d\vec{u}_e}{dt} \right)}_e + \underbrace{\frac{m_e \vec{w}\vec{w}}{T_e} \cdot \vec{\nabla} u_e}_f - \underbrace{\nu_{ei} \frac{m\vec{w} \cdot \vec{u}}{T_e}}_g \right] f_{me} \right) \\ (e) = \frac{m\vec{w}}{T_e} \left[\frac{\vec{R}_{ei}^{(0)}}{m_e} - \frac{T_e \vec{\nabla} n_e + n_e \vec{\nabla} T_e}{m_e} \right] = \frac{\vec{w} \cdot (m\nu_{ei} \hat{u})}{n_e T_e} - \vec{w} \cdot \vec{\nabla} \ln T_e - \vec{w} \cdot \vec{\nabla} \ln n_e$$

→ (c) + (e)₃ = 0

→ (d) + (e)₂ = $\left(\frac{m\vec{w}^2}{2T_e} - \frac{5}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_e$

→ (g) + (e)₁ = $\frac{m}{T_e} (\nu_{ei} - \nu_{ei}) \vec{w} \cdot \vec{u}$

$$\vec{w}_\perp = \frac{d}{dt}(\vec{w}_\perp \times \hat{b}) = \frac{d}{dt}(s\omega r \hat{x} - \cos r \hat{y}) = \omega s r \hat{x} + s\omega r \hat{y}$$

$$\boxed{3} \quad \vec{q}_{\perp e} = -T_e \int d\vec{w} \vec{w}_\perp L_1^{(3/2)}(x) \tilde{f}_{e1}^{(1)} = -T_e \int d\vec{w} \frac{d}{dr}(\vec{w}_\perp \times \hat{b}) L_1^{(3/2)}(x) \tilde{f}_{e1}^{(1)}$$

부등식 $\Rightarrow T_e \int d\vec{w} (\vec{w}_\perp \times \hat{b}) L_1^{(3/2)}(x) \frac{d\tilde{f}_{e1}^{(1)}}{dr}$ & 이제 이걸 $\tilde{f}_{e1}^{(1)}$ 이 아니라 $\frac{d\tilde{f}_{e1}^{(1)}}{dr}$ 만 알면 됨.

* note eq. (49)

$$\left(w_{ce} \frac{d\tilde{f}_{e1}^{(1)}}{dr} = -C_{ee} [\tilde{f}_{e1}^{(0)}] - v_{ei} \mathcal{L}_{ei} [\tilde{f}_{e1}^{(0)}] + f_{me} \frac{m(v_{ei} - v_{ci})}{T_e} \vec{w}_\perp \cdot \vec{u} \right)$$

$$\begin{aligned} \vec{q}_{\perp e} &= \frac{T_e}{w_{ce}} \int d\vec{w} (\vec{w}_\perp \times \hat{b}) L_1^{(3/2)}(x) f_{me} \left[1 - \frac{3\sqrt{\pi}}{4} \left(\frac{v_{te}}{w} \right)^3 \right] \frac{2\vec{w}_\perp \cdot (\vec{u}_i - \vec{u}_e)}{v_{te}^2 \mathcal{Z}_{ci}} \\ &+ \frac{T_e}{w_{ce}^2} \int d\vec{w} (\vec{w}_\perp \times \hat{b}) L_1^{(3/2)}(x) [C_{ee}^l + v_{ei} \mathcal{L}_{ei}] (f_{me} L_1^{(3/2)}(x) (\vec{w}_\perp \times \hat{b}) \cdot \vec{\nabla} \ln T_e) \end{aligned}$$

$$\boxed{\vec{q}_{\perp e} = \frac{3}{2} \frac{P_e}{\mathcal{Z}_{ci} w_{ce}} \hat{b} \times (\vec{u}_i - \vec{u}_e) - 4.66 \frac{P_e}{m_e \mathcal{Z}_{ci} w_{ce}^2} \vec{\nabla}_\perp T_e}$$

⑧ Electron friction force

$$\begin{aligned} \boxed{1} \quad R_{lei} &= \frac{m_e n_e}{\mathcal{Z}_{ci}} (u_{||i} - u_{||e}) - \frac{3\sqrt{\pi}}{4 \mathcal{Z}_{ci}} m_e v_{te}^3 \int d\vec{w} \frac{w_{||}}{w^3} \langle f_{e1} \rangle \\ &= \frac{m_e n_e}{\mathcal{Z}_{ci}} (u_{||i} - u_{||e}) \left\{ 1 - \frac{3\sqrt{\pi}}{2} \frac{v_{te}}{n_e} \int d\vec{w} \frac{w_{||}}{w^3} f_{me} \left[0.284 L_1^{(3/2)}(x) + 0.032 L_2^{(3/2)}(x) \right] \right\} \\ &\quad - \frac{5}{2} n_e \hat{b} \cdot \vec{\nabla} T_e \times \frac{3\sqrt{\pi}}{2} \frac{v_{te}}{n_e} \int d\vec{w} \frac{w_{||}^2}{w^3} f_{me} \left[0.506 L_1^{(3/2)}(x) - 0.253 L_2^{(3/2)}(x) \right] \\ &= \frac{m_e n_e}{\mathcal{Z}_{ci}} (u_{||i} - u_{||e}) \left[1 - 0.284 \int_0^\infty dx e^{-x} L_1^{(3/2)}(x) - 0.032 \int_0^\infty dx e^{-x} L_2^{(3/2)}(x) \right] \\ &\quad - \frac{5}{2} n_e \hat{b} \cdot \vec{\nabla} T_e \left[0.506 \int_0^\infty dx e^{-x} L_1^{(3/2)}(x) - 0.253 \int_0^\infty dx e^{-x} L_2^{(3/2)}(x) \right] \end{aligned}$$

$$\boxed{R_{lei} = 0.51 \frac{m_e n_e}{\mathcal{Z}_{ci}} (u_{||i} - u_{||e}) - 0.71 n_e \hat{b} \cdot \vec{\nabla} T_e}$$

< Parallel friction force >

Same as Spitzer-Härm: 0.51

$$\begin{aligned} \boxed{2} \quad \vec{q}_{\perp e} &= -T_e \int d\vec{w} \vec{w}_{\perp} L_1^{(3/2)}(\chi) \tilde{f}_{e1}^{(2)} = \int d\vec{w} \vec{w}_{\perp} [L_1^{(3/2)}(\chi)]^2 f_{Mc} \frac{\vec{w}_{\perp} \times \hat{b}}{w_{ce}} \cdot \vec{\nabla} T_e \\ &= \frac{1}{w_{ce}} \int_{-1}^1 d\xi \int_0^{\infty} d\omega w^2 \int_0^{2\pi} d\gamma (L_1^{(3/2)})^2 f_{Mc} \vec{w}_{\perp} \vec{w}_{\perp} \times \hat{b} \cdot \vec{\nabla} T_e \end{aligned}$$

$$\left(\int_0^{2\pi} \vec{w}_{\perp} \vec{w}_{\perp} d\gamma = \pi w_{\perp}^2 (\hat{I} - \hat{b}\hat{b}) \right)$$

$$\vec{q}_{\perp e} = \frac{\pi}{w_{ce}} \int_{-1}^1 d\xi \int_0^{\infty} d\omega w^2 w_{\perp}^2 (L_1^{(3/2)})^2 f_{Mc} (\hat{I} - \hat{b}\hat{b}) \times \hat{b} \cdot \vec{\nabla} T_e$$

$$(w_{\perp}^2 = w^2 - w_{\parallel}^2 = (1 - \xi^2) w^2, \quad \int_{-1}^1 (1 - \xi^2) d\xi = 2 - \frac{2}{3} = \frac{4}{3})$$

$$\begin{aligned} \vec{q}_{\perp e} &= \frac{\pi}{w_{ce}} \frac{4}{3} \int_0^{\infty} d\chi \chi^{3/2} \left(\frac{\sqrt{v_{Te}}}{2} \right)^5 (L_1^{(3/2)})^2 \frac{n_e}{\pi^{3/2} v_{Te}^3} e^{-\chi} (\hat{I} - \hat{b}\hat{b}) \times \hat{b} \cdot \vec{\nabla} T_e \\ &= \frac{4n_e}{3w_{ce}\sqrt{\pi}} \underbrace{\frac{v_{Te}^2}{2} \int_0^{\infty} e^{-\chi} \chi^{3/2} (L_1^{(3/2)})^2 d\chi}_{15\sqrt{\pi}/8} \cdot (\hat{I} - \hat{b}\hat{b}) \times \hat{b} \cdot \vec{\nabla} T_e \end{aligned}$$

$$(\hat{I} - \hat{b}\hat{b}) \times \hat{b} \cdot \vec{\nabla} T_e = (\hat{x}\hat{x} + \hat{y}\hat{y}) \times \hat{z} \cdot \vec{\nabla} T_e = -\hat{x}\hat{y} \cdot \vec{\nabla} T_e + \hat{y}\hat{x} \cdot \vec{\nabla} T_e = -\hat{x} \frac{\partial T_e}{\partial y} + \hat{y} \frac{\partial T_e}{\partial x} = \hat{b} \times \vec{\nabla} T_e$$

$$\therefore \vec{q}_{\perp e} = \frac{4}{3\sqrt{\pi}} \frac{p_e}{m_e w_{ce}} \frac{15\sqrt{\pi}}{8} \hat{b} \times \vec{\nabla} T_e = \frac{5}{2} \frac{p_e}{m_e w_{ce}} \hat{b} \times \vec{\nabla} T_e \quad \boxed{\vec{q}_{\perp e} = \frac{5}{2} \frac{p_e}{m_e w_{ce}} \hat{b} \times \vec{\nabla} T_e}$$

- Friction force $\vec{R}_{ei} = -m_e \int d\vec{w} v_s^{ei} \vec{w} (f_{e0} + f_{e1})$

$$\vec{R}_{ei} = \frac{m_e n_e}{T_{ei}} (\vec{u}_i - \vec{u}_e) - \frac{3\sqrt{\pi}}{4 T_{ei}} m_e v_{te}^3 \int d\vec{w} \frac{\vec{w}}{w^3} \left(\langle f_{e1} \rangle + \tilde{f}_{e1}^{(0)} \right) \equiv \vec{R}_{||ei} + \vec{R}_{\perp ei}$$

⑦ Electron heat flux

$$\vec{q}_{||e} = -T_e \int d\vec{w} \vec{w} L_1^{(3/2)}(x) \langle f_{e1} \rangle = -T_e \int d\vec{w} w_{||} \hat{b} L_1^{(3/2)}(x) \langle f_{e1} \rangle$$

$$(\int d\vec{w} = 2\pi \int_{-1}^1 d\xi \int_0^\infty w^2 dw, \quad w_{||} = w\xi)$$

$$\vec{q}_{||e} = -T_e \cdot 2\pi \int_{-1}^1 d\xi \int_0^\infty dw \cdot w^2 (w\xi) L_1^{(3/2)}(x)$$

$$\times \int w\xi f_{me} L_1^{(3/2)}(x) \left[0.506 \frac{5}{2} T_{ei} \hat{b} \hat{b} \cdot \vec{\nabla} T_e + 0.284 \frac{m_e (\vec{u}_{||i} - \vec{u}_{||e})}{T_e} \right]$$

$$= -\frac{4\pi}{3} \int_0^\infty dw w^4 \left[L_1^{(3/2)}(x) \right]^2 f_{me} \left[0.506 \frac{5}{2} T_{ei} \hat{b} \hat{b} \cdot \vec{\nabla} T_e + 0.284 m_e (\vec{u}_{||i} - \vec{u}_{||e}) \right]$$

$$\left(x = \frac{w^2}{v_{te}^2}, \quad 2w dw = v_{te}^2 dx \rightarrow w^4 dw = v_{te}^4 x^2 \cdot \frac{v_{te}^2}{2w} dx = \frac{1}{2} v_{te}^5 x^{3/2} dx \right)$$

$$f_{me} = n_e \left(\frac{1}{\pi v_{te}^2} \right)^{3/2} \exp\left(-\frac{w^2}{v_{te}^2}\right) = \frac{n_e}{\pi^{3/2} v_{te}^3} \exp(-x)$$

$$\vec{q}_{||e} = -\frac{4\pi}{3} \frac{n_e}{\pi^{3/2}} \frac{v_{te}^2}{2} \left[0.506 \frac{5}{2} T_{ei} \hat{b} \hat{b} \cdot \vec{\nabla} T_e + 0.284 m_e (\vec{u}_{||i} - \vec{u}_{||e}) \right] \underbrace{\int_0^\infty e^{-x} x^{3/2} \left[L_1^{(3/2)}(x) \right]^2 dx}_{= 15\sqrt{\pi}/8}$$

$$\vec{q}_{||e} = -3.16 \frac{\rho_e T_{ei}}{m_e} \hat{b} \hat{b} \cdot \vec{\nabla} T_e - 0.71 \rho_e (\vec{u}_{||i} - \vec{u}_{||e}) \hat{b}$$

parallel conductivity

friction.

one can obtain a_0, a_1 from $(LHS) = (RHS)$, which gives $\langle f_{ei} \rangle$.

In particular for $Z=1$,

$$\langle f_{ei} \rangle = W_{\perp} f_{me} L_1^{(3/2)} \left(\frac{W^2}{v_{Te}^2} \right) \left[0.506 \times \frac{5}{2} Z e i b \cdot \vec{\nabla} \ln T_e + 0.284 \times \frac{m_e (v_{i||} - v_{e||})}{T_e} \right] \\ - W_{\perp} f_{me} L_2^{(3/2)} \left(\frac{W^2}{v_{Te}^2} \right) \left[0.253 \times \frac{5}{2} Z e i b \cdot \vec{\nabla} \ln T_e - 0.032 \times \frac{m_e (v_{i||} - v_{e||})}{T_e} \right]$$

where $m = m_e$ and $\vec{u} = \vec{w}_i - \vec{w}_e$.

6) Gyro-dependent electron distribution function

one can subtract the gyro-independent part from full equation.

$$C_{ei}^{\perp}[\tilde{f}_{ei}] + v_{ei} \mathcal{L}[\tilde{f}_{ei}] + W_{ce} \frac{d\tilde{f}_{ei}}{dY} = \left[\left(\frac{mW^2}{2T_e} - \frac{5}{2} \right) \vec{w}_{\perp} \cdot \vec{\nabla} \ln T_e + \frac{m(v_{ei} - v_{ei})}{T_e} \vec{w}_{\perp} \cdot \vec{u} \right] f_{me}$$

With $W_{ce} \gg v_{ei}$, one can make the subsequent ordering (last piece of Braginskii's electron correction equation)

$$\tilde{f}_{ei} = \tilde{f}_{ei}^{(0)} + \tilde{f}_{ei}^{(1)}$$

$$i) \quad W_{ce} \frac{d\tilde{f}_{ei}^{(0)}}{dY} = f_{me} \left(\frac{mW^2}{2T_e} - \frac{5}{2} \right) \vec{w}_{\perp} \cdot \vec{\nabla} \ln T_e \quad (\text{Lowest-order})$$

$$\text{Integrating over:} \quad \frac{d\tilde{f}_{ei}^{(0)}}{dY} = \frac{f_{me}}{W_{ce}} \left(\frac{mW^2}{2T_e} - \frac{5}{2} \right) W_{\perp} (\hat{x} \cos Y + \hat{y} \sin Y) \vec{\nabla} \ln T_e$$

$$\tilde{f}_{ei}^{(0)} = -\frac{f_{me}}{W_{ce}} L_1^{(3/2)}(x) \cdot W_{\perp} (\hat{x} \sin Y - \hat{y} \cos Y) \vec{\nabla} \ln T_e \quad \left. \begin{array}{l} \vec{w}_{\perp} \times \hat{b} = \hat{x} \sin Y - \hat{y} \cos Y \\ \Rightarrow \tilde{f}_{ei}^{(0)} = -f_{me} L_1^{(3/2)}(x) \frac{\vec{w}_{\perp} \times \hat{b}}{W_{ce}} \cdot \vec{\nabla} \ln T_e \end{array} \right\}$$

$$ii) \quad W_{ce} \frac{d\tilde{f}_{ei}^{(1)}}{dY} = -C_{ei}^{\perp}[\tilde{f}_{ei}^{(0)}] - v_{ei} \mathcal{L}[\tilde{f}_{ei}^{(0)}] + f_{me} \frac{m(v_{ei} - v_{ei})}{T_e} \vec{w}_{\perp} \cdot \vec{u} \quad (\text{Next-order})$$

Now one has $f_{ei} = \langle f_{ei} \rangle + \tilde{f}_{ei}^{(0)} + \tilde{f}_{ei}^{(1)}$ and can evaluate electron heat flux

$$\vec{q}_e = \int d\vec{w} \vec{w} \left(\frac{1}{2} m w^2 - \frac{5}{2} T_e \right) f_{ei}$$

$$= -T_e \int d\vec{w} \vec{w} L_1^{(3/2)}(x) (\langle f_{ei} \rangle + \tilde{f}_{ei}^{(0)} + \tilde{f}_{ei}^{(1)}) \equiv \vec{q}_{||e} + \vec{q}_{\perp e} + \vec{q}_{\perp e}$$

parallel diamagnetic perpendicular.

This part can be solved in the same way as the Spitzer-Härm, using the associated Laguerre polynomial expansion.

$$\langle f_{ei} \rangle = \frac{2W_{ii}}{V_{te}^2} f_{me} \sum_{k=1}^{\infty} a_k L_k^{(3/2)}(x) \quad \leftarrow k \geq 1 \text{ and } V_{ii} \rightarrow W_{ii} \text{ (notable difference)}$$

$$(i) \text{ LHS} = \int W_{ii} L_k^{(3/2)}(x) \left\{ C_{ei} [\langle f_{ei} \rangle] + V_{ei} L_{ei} [\langle f_{ei} \rangle] \right\} d\vec{W}$$

$$= -\frac{n_e}{Z_{ei} Z} \begin{pmatrix} \sqrt{2} + \frac{13}{4} Z & \frac{3\sqrt{2}}{4} + \frac{69}{16} Z \\ \frac{3\sqrt{2}}{4} + \frac{69}{16} Z & \frac{45\sqrt{2}}{16} + \frac{433}{64} Z \end{pmatrix} \begin{pmatrix} a_0 \\ a_1 \end{pmatrix} \quad \begin{matrix} \text{From} \\ \leftarrow E_9(55) \text{ in Lec. 19.} \end{matrix}$$

$$(ii) \text{ RHS} = \int d\vec{W} W_{ii} L_k^{(3/2)} f_{me} \left\{ \left(\frac{W^2}{V_{te}^2} - \frac{5}{2} \right) W_{ii} \hat{b} \cdot \vec{\nabla} \ln T_e + \left[1 - \frac{3\sqrt{\pi}}{4} \left(\frac{V_{te}}{W} \right)^3 \right] \frac{2W_{ii} V_{ii}}{V_{te}^2 Z_{ei}} \right\}$$

$$W_{ii}^2 = W^2 \hat{b}^2 \quad \rightarrow \quad = \int d\vec{W} W^2 L_k^{(3/2)}(x) f_{me} \left[\left(x - \frac{5}{2} \right) \hat{b} \cdot \vec{\nabla} \ln T_e + \left(1 - \frac{3\sqrt{\pi}}{4x^{3/2}} \right) \frac{2V_{ii}}{V_{te}^2 Z_{ei}} \right]$$

$$\left(\begin{array}{l} \text{*note } f_{me} = n_e \left(\frac{m_e}{2\pi T_e} \right)^{3/2} \exp\left(-\frac{m_e W^2}{2T_e}\right) = \frac{n_e}{\pi^{3/2}} \frac{1}{V_{te}^3} \exp(-x) \\ \int d\vec{W} = 2\pi \int_{-1}^1 d\hat{b} \int_0^\infty W^2 dW = \pi V_{te}^3 \int_{-1}^1 d\hat{b} \int_0^\infty x^{1/2} dx, \quad x = \frac{W^2}{V_{te}^2} \end{array} \right)$$

$$= \frac{2n_e V_{te}^2}{3\sqrt{\pi}} \int_0^\infty dx x^{3/2} e^{-x} L_k^{(3/2)}(x) \left[-L_1^{(3/2)}(x) \hat{b} \cdot \vec{\nabla} \ln T_e + \left(1 - \frac{3\sqrt{\pi}}{4x^{3/2}} \right) \frac{2V_{ii}}{V_{te}^2 Z_{ei}} \right]$$

$$= -\frac{4}{3\sqrt{\pi}} \frac{n_e}{m} \hat{b} \cdot \vec{\nabla} T_e \times \frac{15\sqrt{\pi}}{8} - \frac{n_e V_{ii}}{Z_{ei}} \left(1 - \frac{1}{2} \delta k_0 + \frac{3}{2} \delta k_1 + \frac{15}{8} \delta k_2 + \dots \right)$$

$$k=1 \rightarrow -\frac{n_e}{Z_{ei}} \left(\frac{5}{2} \frac{Z_{ei}}{m} \hat{b} \cdot \vec{\nabla} T_e + \frac{3}{2} V_{ii} \right)$$

$$k=2 \rightarrow \frac{15}{8} V_{ii}$$

$$\left(\Gamma(z+1) = z \Gamma(z) \right)$$

$$\text{*note} \left\{ \begin{array}{l} k=0 \quad \int_0^\infty dx e^{-x} = \Gamma(1) = 1 \\ k=1 \quad \int_0^\infty dx e^{-x} \left(\frac{5}{2} - x \right) = \frac{5}{2} \Gamma(1) - \Gamma(2) = \frac{3}{2} \\ k=2 \quad \int_0^\infty dx e^{-x} \left(\frac{35}{8} - \frac{7}{2}x + \frac{1}{2}x^2 \right) = \frac{35}{8} \Gamma(1) - \frac{7}{2} \Gamma(2) + \frac{1}{2} \Gamma(3) = \frac{35}{8} - \frac{7}{2} + \frac{1}{2} = \frac{15}{8} \end{array} \right.$$

$$\downarrow$$

$$\int_0^\infty dx x^{3/2} e^{-x} L_k^{(3/2)}(x) \left(1 - \frac{3\sqrt{\pi}}{4x^{3/2}} \right) = \frac{3\sqrt{\pi}}{4} - \frac{3\sqrt{\pi}}{4} \left(\int_0^\infty dx e^{-x} L_k^{(3/2)}(x) \right)$$

$$= \frac{3\sqrt{\pi}}{4} \left(1 - \delta k_0 + \frac{3}{2} \delta k_1 + \frac{15}{8} \delta k_2 + \dots \right)$$

$$(a) = -\vec{\nabla} \cdot \vec{u}_e$$

$$(b) = \left(\frac{m\bar{w}^2}{2T_e} - \frac{3}{2} \right) \left(-\frac{2}{3} \vec{\nabla} \cdot \vec{u}_e \right) = -\frac{m\bar{w}^2}{3T_e} \vec{\nabla} \cdot \vec{u}_e + \vec{\nabla} \cdot \vec{u}_e$$

$$(f) = \frac{m}{T_e} \vec{w} \vec{w} : \vec{\nabla} \vec{u}_e$$

$$\rightarrow (a) + (b) + (f) = \frac{m_e}{T_e} \left(\vec{w} \vec{w} - \frac{\bar{w}^2}{3} \mathbf{I} \right) : \vec{\nabla} \vec{u}_e = \frac{m}{2T_e} \left(\vec{w} \vec{w} - \frac{\bar{w}^2}{3} \mathbf{I} \right) : \vec{w}_e$$

$$\text{where } \vec{w}_e = \vec{\nabla} \vec{u} + (\vec{\nabla} \vec{u})^T - \frac{2}{3} (\vec{\nabla} \cdot \vec{u}) \mathbf{I} \quad (\text{rate of strain tensor})$$

$$\Rightarrow \boxed{C_{ee}^A [f_{e1}] + \nu_{ei} \mathcal{L}_{ei} [f_{e1}] + \frac{e}{m} \vec{w} \times \vec{B} \cdot \frac{df_{e1}}{d\vec{w}}}$$

$$= \left[\left(\frac{m\bar{w}^2}{2T_e} - \frac{5}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_e + \frac{m(\hat{\nu}_{ei} - \nu_{ei})}{T_e} \vec{w} \cdot \vec{u} + \frac{m}{2T_e} \left(\vec{w} \vec{w} - \frac{\bar{w}^2}{3} \mathbf{I} \right) : \vec{w}_e \right] f_{me}$$

$$\text{where } \vec{w} = \left(\vec{\nabla} \vec{u} \right) + \left(\vec{\nabla} \vec{u} \right)^T - \frac{2}{3} (\vec{\nabla} \cdot \vec{u}) \mathbf{I} \quad \text{and} \quad \nu_{ei}(v) = \frac{3\sqrt{\pi}}{4} \left(\frac{v_{te}}{\bar{w}} \right)^3 \hat{\nu}_{ei}$$

(1) Thermodynamic force (2) friction force Viscous force due to flow shear.

⑤ Gyro-averaged electron distribution function

$$\text{Now use } \vec{w} = w_{||} \hat{b} + w_{\perp} (\hat{x} \cos \gamma + \hat{y} \sin \gamma) \rightarrow \frac{e}{m} \vec{w} \times \vec{B} \cdot \frac{df_{e1}}{d\vec{w}} = w_{ce} \frac{df}{d\gamma}$$

$$\left(\frac{e}{m} \vec{w} \times \vec{B} \cdot \frac{df_{e1}}{d\vec{w}} = \frac{eB}{m} [w_{\perp} (\sin \gamma \hat{x} - \cos \gamma \hat{y})] \cdot \left[\hat{x} \frac{df_{e1}}{dw_x} + \hat{y} \frac{df_{e1}}{dw_y} \right] = \frac{eB}{m} w_{\perp} (\sin \gamma \frac{df}{dw_x} - \cos \gamma \frac{df}{dw_y}) = w_{ce} \frac{df}{d\gamma} \right.$$

$$\left. \begin{array}{l} \text{*note } \frac{df}{d\gamma} = \frac{dw_x}{d\gamma} \frac{df}{dw_x} + \frac{dw_y}{d\gamma} \frac{df}{dw_y} = w_{\perp} (-\sin \gamma \frac{df}{dw_x} + \cos \gamma \frac{df}{dw_y}) \end{array} \right)$$

Compared to the hydrodynamic Chapman-Enskog, a magnetized plasma contains the fast gyromotion making kinetic response strongly anisotropic. \Rightarrow Let's perform gyro-averaging

$$f_{e1} = \langle f_{e1} \rangle + \tilde{f}_{e1} \quad \text{where } \langle f_{e1} \rangle = \frac{1}{2\pi} \int f_{e1} d\gamma$$

to isolate parallel & perpendicular directions

$$\text{From } \langle C_{ee}^A [f_{e1}] \rangle = C_{ee}^A [\langle f_{e1} \rangle], \quad \langle \mathcal{L}_{ei} [f_{e1}] \rangle = \mathcal{L}_{ei} [\langle f_{e1} \rangle]$$

$$\langle \vec{w} \rangle = w_{||} \hat{b}, \quad \langle \vec{w} \vec{w} \rangle = w_{||}^2 \hat{b} \hat{b} + \frac{1}{2} w_{\perp}^2 (\mathbf{I} - \hat{b} \hat{b}), \quad \text{and } \vec{w} \perp \vec{B} \quad (\text{viscous-term})$$

This is what Braginskii did.

$$\Rightarrow \boxed{C_{ee}^A [\langle f_{e1} \rangle] + \nu_{ei} \mathcal{L}_{ei} [\langle f_{e1} \rangle] = \left[\left(\frac{m\bar{w}^2}{2T_e} - \frac{5}{2} \right) w_{||} \hat{b} \cdot \vec{\nabla} \ln T_e + \frac{m(\hat{\nu}_{ei} - \nu_{ei})}{T_e} w_{||} w_{||} \right] f_{me}}$$

$\langle \text{gyro-averaged part} \rangle$

$$\begin{aligned}
\boxed{2} \quad \vec{R}_{\perp ci} &= \frac{m_e n_e}{Z_{ei}} (\vec{u}_{\perp i} - \vec{u}_{\perp e}) - \frac{3\sqrt{\pi}}{4 Z_{ei}} m_e v_{Te}^3 \int d\vec{w} \frac{\vec{w}_{\perp}}{w^3} \tilde{f}_{ei}^{(0)} \\
&= \frac{m_e n_e}{Z_{ei}} (\vec{u}_{\perp i} - \vec{u}_{\perp e}) + \frac{3\sqrt{\pi}}{4 \omega_{ce} Z_{ei}} m_e v_{Te}^3 \int d\vec{w} \frac{\vec{w}_{\perp}}{w^3} f_{me} L_1^{(3/2)}(x) \vec{w}_{\perp} \cdot \hat{b} \times \vec{\nabla} \ln T_e \\
&= \frac{m_e n_e}{Z_{ei}} (\vec{u}_{\perp i} - \vec{u}_{\perp e}) + \frac{3 n_e}{4 \omega_{ce} Z_{ei}} \int_{-1}^1 d\frac{x}{2} (1-x^2) \int_0^{\infty} dx e^{-x} L_1^{(3/2)}(x) \hat{b} \times \vec{\nabla} T_e \\
&= \frac{m_e n_e}{Z_{ei}} (\vec{u}_{\perp i} - \vec{u}_{\perp e}) + \frac{3}{2} \frac{n_e}{\omega_{ce} Z_{ei}} \hat{b} \times \vec{\nabla} T_e
\end{aligned}$$

① Summary: Electron transport coefficients by Braginskii

$$\begin{aligned}
q_{\parallel e} &= -k_{\parallel e} \nabla_{\parallel} T_e - 0.71 p_e (u_{\parallel i} - u_{\parallel e}) \quad (k_{\parallel e} \equiv 3.16 \frac{p_e Z_{ei}}{m_e}) \\
\vec{q}_{\perp e} &= \frac{5}{2} \frac{p_e}{m_e \omega_{ce}} \hat{b} \times \vec{\nabla} T_e \\
\vec{q}_{\perp e} &= -k_{\perp e} \vec{\nabla}_{\perp} T_e + \frac{3}{2} \frac{p_e}{Z_{ei} \omega_{ce}} \hat{b} \times (\vec{u}_{\perp i} - \vec{u}_{\perp e}) \quad (k_{\perp e} \equiv 4.66 \frac{p_e}{m_e Z_{ei} \omega_{ce}^2}) \\
\vec{\Pi}_e &\approx 0 \\
R_{\parallel ei} &= \gamma_{\parallel} e^2 n_e^2 (u_{\parallel i} - u_{\parallel e}) - 0.71 n_e \nabla_{\parallel} T_e \quad (\gamma_{\parallel} \equiv 0.51 \frac{m_e}{n_e e^2 Z_{ei}}) \\
\vec{R}_{\perp ei} &= \gamma_{\perp} e^2 n_e^2 (\vec{u}_{\perp i} - \vec{u}_{\perp e}) + \frac{3}{2} \frac{n_e}{\omega_{ce} Z_{ei}} \hat{b} \times \vec{\nabla} T_e \quad (\gamma_{\perp} \equiv \frac{m_e}{n_e e^2 Z_{ei}}) \\
Q_{ie} &= \frac{3 m_e n_e}{m_i Z_{ei}} (T_e - T_i)
\end{aligned}$$

(10) Ion kinetic equation

Assume: ion-ion collisions are dominant. (neglect all e-i terms in electron eqn).

$$\Rightarrow C_{ii}^f[f_{i1}] + w_{ci} \frac{df_{i1}}{dy} = \left[\left(\frac{m_i w^2}{2T_i} - \frac{5}{2} \right) \vec{w} \cdot \vec{\nabla} \ln T_i + \frac{m_i}{2T_i} \left(\vec{w} \vec{w} - \frac{w^2}{3} \mathbf{I} \right) : \vec{w}_i \right] f_{mi}$$

However, we cannot neglect ion viscosity w_i (unlike electron viscosity $w_e \approx 0$)

$$f_{i1} = \langle f_{i1} \rangle + \hat{f}_{i1}$$

$$\Rightarrow C_{ii}^f[\langle f_{i1} \rangle] = \left[\left(\frac{m_i w^2}{2T_i} - \frac{5}{2} \right) w_{ii} \hat{b} \cdot \vec{\nabla} \ln T_i + \frac{m_i}{2T_i} \left(w_{ii}^2 - \frac{w_{\perp}^2}{2} \right) \left(\hat{b}\hat{b} - \frac{1}{3} \mathbf{I} \right) : \vec{w}_i \right] f_{mi}$$

$$\left(\begin{array}{l} \text{*note } \langle \vec{w} \vec{w} \rangle - \frac{w^2}{3} \mathbf{I} = w_{ii}^2 \hat{b}\hat{b} + \frac{w_{\perp}^2}{2} (\mathbf{I} - \hat{b}\hat{b}) - \left(\frac{w_{ii}^2}{3} + \frac{w_{\perp}^2}{3} \right) \mathbf{I} \\ = w_{ii}^2 \left(\hat{b}\hat{b} - \frac{1}{3} \mathbf{I} \right) - \frac{w_{\perp}^2}{2} \left(\hat{b}\hat{b} - \frac{1}{3} \mathbf{I} \right) = \left(w_{ii}^2 - \frac{w_{\perp}^2}{2} \right) \left(\hat{b}\hat{b} - \frac{1}{3} \mathbf{I} \right) \end{array} \right)$$

(11) Associated Laguerre polynomials for angular distribution

Expansion for ion kinetic equation:

$$\langle f_{i1} \rangle = \underbrace{\frac{2w_{ii}}{v_{ti}^2} f_{mi} \sum_{k=1}^{\infty} a_k L_k^{(3/2)}(x)}_{\equiv \langle f_{i1} \rangle_a} + \underbrace{\frac{2}{3} \left(\frac{w_{ii}^2 - w_{\perp}^2/2}{p_i v_{ti}^2} \right) f_{mi} \sum_{k=0}^{\infty} b_k L_k^{(5/2)}(x)}_{\equiv \langle f_{i1} \rangle_b}$$

One can see that $\langle f_{i1} \rangle_b$ is closely related to viscous tensor.

$$\begin{aligned} & \left(\hat{b}\hat{b} - \frac{1}{3} \mathbf{I} \right) \int d\vec{w} m_i \left(w_{ii}^2 - \frac{w_{\perp}^2}{2} \right) \langle f_{i1} \rangle_b \\ &= \left(\hat{b}\hat{b} - \frac{1}{3} \mathbf{I} \right) \int d\vec{w} m_i \left(w_{ii}^2 - \frac{w_{\perp}^2}{2} \right) \frac{2}{3} \left(\frac{w_{ii}^2 - w_{\perp}^2/2}{p_i v_{ti}^2} \right) f_{mi} \sum_{k=0}^{\infty} b_k L_k^{(5/2)}(x) \end{aligned}$$

$$\left(\begin{array}{l} \text{*note } \int d\vec{w} = 2\pi \int_{-1}^1 d\xi \int_0^{\infty} w^2 dw = \pi v_{ti}^3 \int_{-1}^1 d\xi \int_0^{\infty} x^{1/2} dx, \quad w_{ii}^2 - \frac{w_{\perp}^2}{2} = w^2 \left(\frac{\xi^2}{3} - \frac{(1-\xi^2)}{2} \right) = w^2 \left(\frac{3\xi^2 - 1}{2} \right) \\ f_{mi} = \frac{n_i}{\pi^{3/2} v_{ti}^3} e^{-x} \quad \frac{4}{3\pi v_{ti}^4} = v_{ti}^2 x \left(\frac{3\xi^2 - 1}{2} \right) \end{array} \right)$$

$$\begin{aligned} &= \left(\hat{b}\hat{b} - \frac{1}{3} \mathbf{I} \right) \int_{-1}^1 d\xi \int_0^{\infty} \pi v_{ti}^3 x^{1/2} dx \left(\frac{2}{3} \frac{m_i}{(n_i m_i v_{ti}^2/2) v_{ti}^2} \right) \cdot \left(v_{ti}^4 x^2 \left(\frac{3\xi^2 - 1}{2} \right)^2 \right) \\ &\quad \times \left(\frac{n_i}{\pi^{3/2} v_{ti}^3} e^{-x} \right) \sum_{k=0}^{\infty} b_k L_k^{(5/2)}(x) \end{aligned}$$

$$= \left(\hat{b}\hat{b} - \frac{1}{3} \mathbf{I} \right) \frac{4}{3\pi} \int_{-1}^1 d\xi \left(\frac{3\xi^2 - 1}{2} \right)^2 \sum_k b_k \int_0^{\infty} x^{5/2} e^{-x} L_0^{(5/2)}(x) L_k^{(5/2)}(x)$$

$$= \left(\hat{b}\hat{b} - \frac{1}{3} \mathbf{I} \right) b_0 \quad \& \quad b_0 \left(1 + L_0^{(5/2)} \right) \text{ is parallel component of the viscous tensor.}$$

$$\left(\frac{w_{\parallel}^2}{2}\right) = w_{\perp}^2 P_2(\xi)$$

Also, notice that $P_1(\xi) = \xi = \frac{w_{\parallel}}{w}$, $P_2(\xi) = \frac{1}{2}(3\xi^2 - 1)$: Legendre polynomial

$$\text{Then, } \langle f_{i1} \rangle_a + \langle f_{i1} \rangle_b = 2\sqrt{x} P_1(\xi) f_{mi} \sum_k \frac{a_k}{v_{ti}} L_k^{(3/2)}(x) + \frac{2}{3} x P_2(\xi) \sum_k \frac{b_k}{P_i} L_k^{(5/2)}(x)$$

→ one can separate the calculation $\langle f_{i1} \rangle_a$ and $\langle f_{i1} \rangle_b$ due to the orthogonality.

$$\left(\int_{-1}^1 d\xi P_i(\xi) P_j(\xi) = \frac{2}{2i+1} \delta_{ij} \right)$$

② Gyro-averaged ion distribution function.

이제 $\langle f_{i1} \rangle_a$ 와 $\langle f_{i1} \rangle_b$ 를 각각 따로 구해보자!

$$\text{① } \int d\vec{w} w_{\parallel} L_k^{(3/2)} C_{ii}^L [\langle f_{i1} \rangle_a] = \frac{n_i}{\tau_{ii}} \begin{pmatrix} 1 & 3/4 \\ 3/4 & 45/16 \end{pmatrix} \begin{pmatrix} a_1 \\ a_2 \end{pmatrix} \Rightarrow \begin{matrix} a_1 = ______ \\ a_2 = ______ \end{matrix}$$

$$\int d\vec{w} w_{\parallel} L_k^{(3/2)}(x) f_{mi} \left(x^2 - \frac{5}{2}\right) w_{\parallel} \hat{b} \cdot \vec{\nabla} \ln T_i = -\frac{5}{2} \frac{P_i}{m_i} (\hat{b} \cdot \vec{\nabla} \ln T_e) f_{ki}$$

$$\Rightarrow \langle f_{i1} \rangle_a = w_{\parallel} f_{mi} \tau_{ii} (\hat{b} \cdot \vec{\nabla} \ln T_i) \left[\frac{25}{16} L_1^{(3/2)}(x) - \frac{5}{12} L_2^{(3/2)}(x) \right]$$

$$\text{② } \int d\vec{w} \left(w_{\parallel}^2 - \frac{w_{\perp}^2}{2} \right) L_k^{(5/2)}(x) \cdot C_{ii}^L [\langle f_{i1} \rangle] = -\frac{6}{5} \frac{n_i}{\tau_{ii}} \begin{pmatrix} 1 & 3/4 \\ 3/4 & 205/48 \end{pmatrix} \begin{pmatrix} b_0 \\ b_1 \end{pmatrix} \Rightarrow \begin{matrix} b_0 = ______ \\ b_1 = ______ \end{matrix}$$

$$\int d\vec{w} \left(w_{\parallel}^2 - \frac{w_{\perp}^2}{2} \right) L_k^{(5/2)}(x) \cdot \frac{m_i}{2T_i} \left(w_{\parallel}^2 - \frac{w_{\perp}^2}{2} \right) \left(\hat{b}\hat{b} - \frac{1}{3} \vec{I} \right) : \vec{w}_i f_{mi}$$

$$= m_i n_i \int d\vec{w} \left(w_{\parallel}^2 - \frac{w_{\perp}^2}{2} \right)^2 L_k^{(5/2)}(x) \frac{f_{mi}}{v_{ti}^2} \left(\hat{b}\hat{b} - \frac{1}{3} \vec{I} \right) : \vec{w}_i = \frac{3}{2} P_i m_i \left(\hat{b}\hat{b} - \frac{1}{3} \vec{I} \right) : \vec{w}_i f_{ki}$$

$$\Rightarrow \langle f_{i1} \rangle_b = - \left(\frac{w_{\parallel}^2 - w_{\perp}^2/2}{v_{ti}^2} \right) f_{mi} \tau_{ii} \left(\hat{b}\hat{b} - \frac{1}{3} \vec{I} \right) : \vec{w}_i \left[\frac{1025}{1068} L_1^{(5/2)}(x) - \frac{45}{267} L_2^{(5/2)}(x) \right]$$

③ Gyro-dependent ion distribution function.

$$\vec{w} \vec{w} - \frac{w^2}{3} \vec{I} = \left(w_{\parallel}^2 - \frac{w_{\perp}^2}{2} \right) \left(\hat{b}\hat{b} - \frac{1}{3} \vec{I} \right)$$

$$= \cancel{w_{\parallel}^2 \hat{b}\hat{b}} + \vec{w}_{\parallel} \vec{w}_{\perp} + \vec{w}_{\perp} \vec{w}_{\parallel} + \vec{w}_{\perp} \vec{w}_{\perp} - \frac{w^2}{3} \vec{I} + \left(-\cancel{w_{\parallel}^2 \hat{b}\hat{b}} + \frac{1}{3} w_{\parallel}^2 \vec{I} + \frac{w_{\perp}^2}{2} \hat{b}\hat{b} - \frac{1}{6} w_{\perp}^2 \vec{I} \right)$$

$$= (*) - \frac{w^2}{3} \vec{I} - \frac{w_{\perp}^2}{2} \vec{I} + \frac{w_{\parallel}^2}{3} \vec{I} + \frac{w_{\perp}^2}{2} \left(\hat{b}\hat{b} - \frac{1}{3} \vec{I} \right)$$

$$= \vec{w}_{\parallel} \vec{w}_{\perp} + \vec{w}_{\perp} \vec{w}_{\parallel} + \vec{w}_{\perp} \vec{w}_{\perp} + (w_{\perp}^2/2) \left(\hat{b}\hat{b} - \frac{1}{3} \vec{I} \right)$$

$$\Rightarrow C_{ii}^L[\tilde{f}_{i1}] + w_{ci} \frac{df_{i1}}{dy} = f_{mi} \left(\frac{w^2}{v_{ti}^2} - \frac{5}{2} \right) \vec{w}_{\perp} \cdot \vec{\nabla} \ln T_i + f_{mi} \left[\frac{\vec{w}_{\parallel} \vec{w}_{\perp} + \vec{w}_{\perp} \vec{w}_{\parallel} + \vec{w}_{\perp} \vec{w}_{\perp} + (w_{\perp}^2/2) \left(\hat{b}\hat{b} - \frac{1}{3} \vec{I} \right)}{v_{ti}^2} \right] : \vec{w}_i$$

Similarly to electrons, take ordering $\tilde{f}_{i1} = \tilde{f}_{i1}^{(0)} + \tilde{f}_{i1}^{(1)}$

i) Lowest-order

$$W_{ci} \frac{d\tilde{f}_{i1}^{(0)}}{dy} = f_{mi} \left(\frac{W^2}{v_{Ti}^2} - \frac{5}{2} \right) \vec{W}_\perp \cdot \vec{\nabla} \ln T + f_{mi} \left[\frac{\vec{W}_{11} \vec{W}_\perp + \vec{W}_\perp \vec{W}_{11} + \vec{W}_\perp \vec{W}_\perp - (W_\perp^2/2)(\hat{I} - \hat{b}\hat{b})}{v_{Ti}^2} \right] \cdot \vec{W}_i$$

↓ Integrate

$$\tilde{f}_{i1}^{(0)} = f_{mi} L_1^{(3/2)}(x) \frac{\vec{W}_\perp \times \hat{b}}{W_{ci}} \cdot \vec{\nabla} \ln T_i + f_{mi} \left[\frac{\vec{W}_{11} \vec{W}_\perp \times \hat{b} + \vec{W}_\perp \vec{W}_{11} \times \hat{b} + (W_\perp^2/4) [(\hat{x}\hat{x} - \hat{y}\hat{y}) \sin 2\psi - (\hat{x}\hat{y} + \hat{y}\hat{x}) \cos 2\psi]}{v_{Ti}^2 W_{ci}} \right] \cdot \vec{W}_i$$

ii) Next-order

$$W_{ci} \frac{d\tilde{f}_{i1}^{(1)}}{dy} = -C_{ii}^1 [\tilde{f}_{i1}^{(0)}] \quad \& \text{ Once again, it's not necessary to integrate the equation }$$

- Ion heat flux

$$\vec{q}_i = -T_i \int d\vec{w} \vec{w} L_1^{(3/2)}(x) (\langle f_{i1} \rangle + \tilde{f}_{i1}^{(0)} + \tilde{f}_{i1}^{(1)}) \equiv \vec{q}_{\parallel i} + \vec{q}_{\perp i}$$

- Ion viscosity

$$\begin{aligned} \vec{\Pi} &= \int d\vec{w} m_i \left(\vec{w} \vec{w} - \frac{W^2}{3} \hat{I} \right) (\langle f_{i1} \rangle + \tilde{f}_{i1}^{(0)} + \tilde{f}_{i1}^{(1)}) \\ &= \left(\hat{b}\hat{b} - \frac{1}{3} \hat{I} \right) \int d\vec{w} m_i \left(W_{11}^2 - \frac{W_\perp^2}{2} \right) \langle f_{i1} \rangle + \int d\vec{w} m_i \left(\vec{w} \vec{w} - \frac{W^2}{3} \hat{I} \right) (\tilde{f}_{i1}^{(0)} + \tilde{f}_{i1}^{(1)}) \\ &= \underbrace{\Pi_{\parallel i}}_{\text{parallel viscosity}} \left(\hat{b}\hat{b} - \frac{1}{3} \hat{I} \right) + \underbrace{\Pi_{\perp i}}_{\text{gyro-viscosity}} + \underbrace{\Pi_{\perp i}}_{\text{perpendicular viscosity}} \end{aligned}$$

⑭ Ion transport coefficients by Braginskii

$$q_{||i} = -k_{||i} \nabla_{||} T_i \quad (k_{||i} \equiv 3.91 \frac{p_i Z_{ii}}{m_i})$$

$$\vec{q}_{\perp i} = \frac{5}{2} \frac{p_i}{m_i \omega_{ci}} \hat{b} \times \nabla T_i$$

$$\vec{q}_{\perp i} = -k_{\perp i} \nabla_{\perp} T_i \quad (k_{\perp i} \equiv 2 \frac{p_i}{m_i Z_{ii} \omega_{ci}^2})$$

$$\Pi_{||i} = -0.96 p_i Z_{ii} \frac{3}{2} (\hat{b}\hat{b} - \frac{1}{3} \mathbf{I}) (\hat{b}\hat{b} - \frac{1}{3} \mathbf{I}) \cdot \vec{W}_i \rightarrow \mu_{||i} = 0.96 p_i Z_{ii}$$

$$\Pi_{\perp i} = \frac{p_i}{4\omega_{ci}} \left[\hat{b} \times \vec{W}_i \cdot (\mathbf{I} + 3\hat{b}\hat{b}) - (\mathbf{I} + 3\hat{b}\hat{b}) \cdot \vec{W}_i \times \hat{b} \right]$$

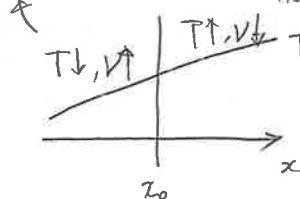
$$\Pi_{\perp i} = -\frac{3}{10} \frac{p_i}{Z_{ii} \omega_{ci}^2} \left[(\mathbf{I} - \hat{b}\hat{b}) \cdot \vec{W}_i \cdot (\mathbf{I} + 3\hat{b}\hat{b}) + (\mathbf{I} + 3\hat{b}\hat{b}) \cdot \vec{W}_i \cdot (\mathbf{I} - \hat{b}\hat{b}) \right]$$

⑮ Summary.

(1) Parallel friction force.

$$R_{||e} = \gamma_{||} n_e^2 e^2 (u_{||i} - u_{||e}) - 0.71 n_e \nabla_{||} T_e \quad (\gamma_{||} \equiv 0.51 \frac{m_e}{n_e e^2 Z_{ei}})$$

friction to electrons by ions
due to speed difference.



From $T_{||}$ to $T_{||}$ particle will have more momentum than from $T_{||}$ to $T_{||}$ particle due to difference of collision.

(2) Parallel heat flux

$$q_{||e} = -k_{||e} \nabla_{||} T_e - 0.71 p_e (u_{||i} - u_{||e}) \quad (k_{||e} \equiv 3.16 \frac{p_e Z_{ei}}{m_e})$$

$$q_{||i} = -k_{||i} \nabla_{||} T_i \quad (k_{||i} \equiv 3.91 \frac{p_i Z_{ii}}{m_i})$$

slow electrons are more likely to collide with ions and so are more apt to lose energy by flowing ions than fast electrons.

$$\Rightarrow \frac{k_{||e}}{k_{||i}} \sim 0 \left(\sqrt{\frac{m_i}{m_e}} \right)$$

↳ electron heat flux is dominant.

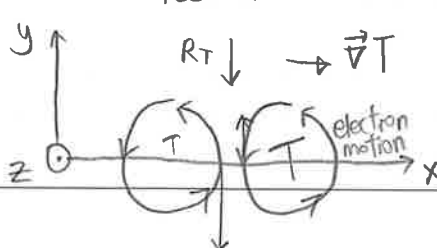
(3) Perpendicular friction force

$$\vec{R}_{\perp e} = \gamma_{\perp} e^2 n_e^2 (\vec{u}_{\perp i} - \vec{u}_{\perp e}) + \frac{3}{2} \frac{n_e}{\omega_{ce} Z_{ei}} \hat{b} \times \vec{\nabla} T_e \quad (\gamma_{\perp} \equiv \frac{m_e}{n_e e^2 Z_{ei}})$$

gyro-motion plays a role to restrict the change in f.

$$\Rightarrow \gamma_{\perp} \approx 2\gamma_{||}$$

* note $\omega_{ce} < 0$



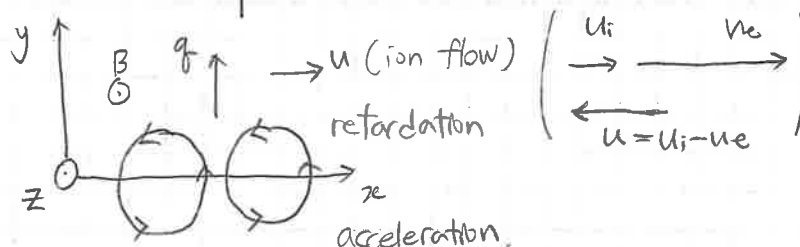
* (전자속이 더 빨라서 momentum도 더 많은다)

(4) Perpendicular heat flux.

$$\vec{q}_{Ne} = \frac{5}{2} \frac{p_e}{m_e \omega_{ce}} \hat{b} \times \vec{\nabla} T_e, \quad \vec{q}_{Ni} = \frac{5}{2} \frac{p_i}{m_i \omega_{ci}} \hat{b} \times \vec{\nabla} T_i \quad \leftarrow \text{diamagnetic}$$

$$\vec{g}_{Ze} = -k_{Ze} \vec{v}_{Te} + \frac{3}{2} \frac{\rho_e}{\tau_{ei} m_e} \hat{b} \times (\vec{u}_{Li} - \vec{u}_{Te}) \quad (k_{Ze} \equiv 4.66 \frac{\rho_e}{m_e \tau_{ei} m_e^2})$$

$$\vec{g}_{\perp i} = -k_{\perp i} \vec{\nabla}_{\perp} T_i \quad (k_{\perp i} \equiv 2 \frac{p_i}{m_i T_i \omega_{ci}^2})$$



(5) Further words

- $q_{He} \gg q_{Ne} \gg q_{Xe}$, $q_{He} : q_{Ne} : q_{Xe} = 1 : \frac{1}{Z_{eff} a_0} : \frac{1}{(Z_{eff} a_0)^2}$

$$- g_{III} > g_{AI} > g_{LI} \quad , \quad g_{III} : g_{AI} : g_{LI} = 1 : \frac{1}{z_{II} w_i} : \frac{1}{(z_{II} w_i)^2}$$

- $g_{llc} \gg g_{lli}$, $g_{llc} \sim g_{li}$, $g_{llc} \ll g_{li}$

$$- \frac{\hbar^2}{2m} \nabla^2 \psi_i \gg \frac{\hbar^2}{2m} \nabla^2 \psi_e$$

$$\frac{\sum_i W_{ci}}{\sum_i W_{ce}} = 0 \quad \left(\frac{m_e}{m_i} \right)$$