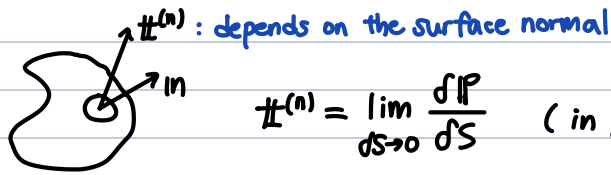


Ch5. Stress

5.1 Surface traction (force per unit area)



$$t^{(n)} = \lim_{dS \rightarrow 0} \frac{dF}{dS} \quad (\text{in general, } t \text{ does not align with } n)$$

5.2 Components of stress

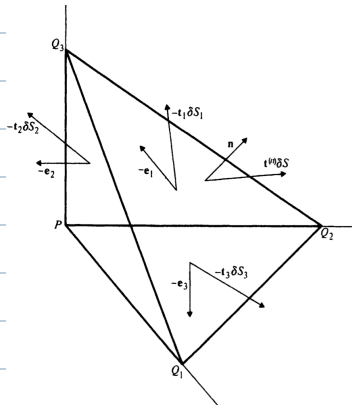
t_i : surface traction if $n = e_i$

$t_i \equiv T_{ij} e_j$, Note : $T_{11} > 0$ if x-positive side pulls the surface.
(정의) $T_{11} < 0$ if x-positive side compresses the surface.

T_{11}, T_{22}, T_{33} : normal or direct stress components.

T_{12}, T_{13} : shearing stress components.

5.3 The traction on any surface.



$$-t_1 dS_1 - t_2 dS_2 - t_3 dS_3 + t^{(n)} dS + \rho b dV = \rho f dV$$

$$dS = dS \cdot n, \quad dS_i = dS \cdot e_i = dS n_i$$

$$\therefore t^{(n)} = n_i t_i + \rho \frac{dV}{dS} (f - b)$$

$\rightarrow 0$ as $dS \rightarrow 0$ ($\because dS \sim L^2, dV \sim L^3$)

$$t^{(n)} = n_i t_i = n_i T_{ij} e_j \rightarrow \underline{t_j^{(n)} = n_i T_{ij}}$$

5.4 Transformation of stress components

$$t_j^{(n)} = n_i T_{ij} \rightarrow \bar{t}_j^{(n)} = \bar{n}_i \bar{T}_{ij} \quad (\Rightarrow T_{ij} \text{ 와 } \bar{T}_{ij} \text{ 의 관계를 찾아보자})$$

$$\bar{t}_j^{(n)} = M_{jk} t_k^{(n)} = M_{jk} n_i T_{ik} = \underline{n_i T_{ik} M_{kj}^T}$$

$$= M_{im} n_m \bar{T}_{ij} = \underline{n_m M_{mi}^T \bar{T}_{ij}}$$

$$\therefore \underline{n^T \bar{T} M^T = n^T M^T \bar{T}} \Rightarrow n^T (\bar{T} M^T - M^T \bar{T}) = 0 \text{ for any } n^T.$$

$$\Rightarrow \bar{T} M^T = M^T \bar{T} \Rightarrow \underline{\bar{T} = M \bar{T} M^T}$$

$$\text{or } \underline{\bar{T}_{ij} = M_{ik} T_{kl} M_{lj}^T = M_{ik} M_{lj}^T T_{kl}} \Rightarrow \underline{t_j^{(n)} = n \cdot \bar{T}}$$

$\hookrightarrow \bar{T}$ is a tensor

5.5 Equation of equilibrium

$$\begin{cases} \iint_S \mathbf{t}^{(n)} dS = \iiint_R \rho \mathbf{b} dV = 0 & \leftarrow \text{force balance} \\ \iint_S \mathbf{x} \times \mathbf{t}^{(n)} dS + \iiint_R \rho \mathbf{x} \times \mathbf{b} dV = 0 & \leftarrow \text{couple (torque)} \end{cases}$$

$$\iint_S n_i T_{ij} dS + \iiint_R \rho b_j dV = 0$$

$$(\text{바탕정리}) \rightarrow \iiint_R \left(\frac{d}{dx_i} T_{ij} + \rho b_j \right) dV = 0 \text{ for any } R. \quad \therefore \frac{d}{dx_i} T_{ij} + \rho b_j = 0$$

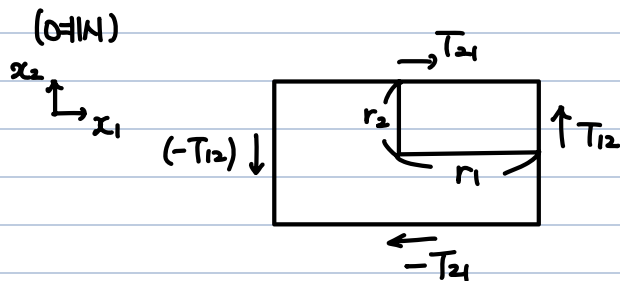
$$\iint_S \epsilon_{jpk} x_p n_r T_{rk} dS + \iiint_R \epsilon_{jpk} \rho x_p b_k dV = 0$$

$$(\text{바탕정리}) \rightarrow \iiint_R \epsilon_{jpk} \left(\frac{d}{dx_r} (x_p T_{rk}) + \rho x_p b_k \right) dV = 0 \text{ for any } R.$$

$$\therefore \epsilon_{jpk} \left(\frac{d}{dx_r} (x_p T_{rk}) + \rho x_p b_k \right) = 0$$

$$\epsilon_{jpk} (T_{pk} + x_p \frac{d}{dx_r} T_{rk} + \rho x_p b_k) = \epsilon_{jpk} T_{pk} = 0$$

$$\therefore \epsilon_{jpk} T_{pk} = 0 \Rightarrow \boxed{T_{pk} = T_{kp}} : \text{stress tensor is a symmetric tensor.}$$



$$\hookrightarrow : r_1 r_2 (T_{12} - T_{21}) = I \ddot{\theta} \sim \rho r_1 r_2 (r_1^2 + r_2^2)$$

매우 작은 r_1, r_2 에 대해,
 $T_{12} \neq T_{21}$ 이면 $\ddot{\theta} = \infty$ 이므로, $T_{12} = T_{21}$ 이다.

5.6 Principal Stress components, principal axes of stress and stress invariants.

$\mathbf{t}^{(n)} \not\parallel \mathbf{n}$ in general. but,

If $\mathbf{t}^{(n)} \parallel \mathbf{n}$, then $\mathbf{t}^{(n)} = T \mathbf{n}$. ($\mathbf{t}^{(n)} = \mathbf{n} \mathbf{T} = T \mathbf{n}$)

$$\rightarrow n_i T_{ij} = T n_j \rightarrow T_{ji} n_i = T n_j \text{ (using } T_{ij} = T_{ji} \text{)}$$

$$\text{or } (T_{ij} n_j - T n_i) = (T_{ij} - T \delta_{ij}) n_j = 0, \mathbf{T} \cdot \mathbf{n} = T \mathbf{n}$$

$T \rightarrow T_1, T_2, T_3$: principal components $T_1 \geq T_2 \geq T_3$

$\mathbf{n}_1, \mathbf{n}_2, \mathbf{n}_3$: principal axes

\hookrightarrow If taken a basis vectors at P , $T_{ij} \rightarrow$ diagonalized.

(In general, principal directions vary from point to point)

* (예제 5.1, 5.2) 확인하기

Invariants : $J_1 = T_1 + T_2 + T_3 = \text{tr } \mathbf{T} = T_{ii}$

$$J_2 = -(\tau_{12}\tau_{13} + \tau_{13}\tau_{11} + \tau_{11}\tau_{22}) = \frac{1}{2}(\text{tr} \Pi - (\text{tr} \Pi)^2) = \frac{1}{2}(\tau_{ij}\tau_{ij} - \tau_{ii}\tau_{jj})$$

$$J_3 = \tau_{11}\tau_{22}\tau_{33} = \det \Pi$$

5.7 The stress deviator tensor

$$\Pi = \mathcal{S} + \frac{1}{3}J_1 \mathbb{I} \quad (\mathcal{S} = \Pi - \frac{1}{3}J_1 \mathbb{I}) \quad \text{or} \quad T_{ij} = S_{ij} + \frac{1}{3}J_1 \delta_{ij} \rightarrow \underline{S_{ii} = 0}$$

$$(\text{If } T_{ij} = -p \delta_{ij} + S_{ij} \text{ where } p = -\frac{1}{3}T_{kk} = -\frac{1}{3}J_1 = -\frac{1}{3}\text{tr} \Pi)$$

$$\text{If } S_{ij} = 0 \rightarrow \underline{T_{ij} = -p \delta_{ij}} : \text{pure hydrostatic state of stress}$$

The principal axes of \mathcal{S} = same of those Π .

$$S_1 + S_2 + S_3 = 0 \quad \text{and} \quad S_1 = T_1 - \frac{1}{3}(T_1 + T_2 + T_3) = \frac{1}{3}(2T_1 - T_2 - T_3)$$

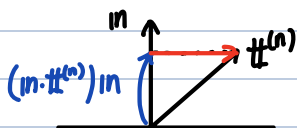
$$S_2 = T_2 - \frac{1}{3}(T_1 + T_2 + T_3) = \frac{1}{3}(2T_2 - T_1 - T_3)$$

$$S_3 = T_3 - \frac{1}{3}(T_1 + T_2 + T_3) = \frac{1}{3}(2T_3 - T_1 - T_2)$$

5.8 Shear stress

$$\text{ex) } \mathbf{n} = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \rightarrow t_j^{(n)} = n_i T_{ij} = T_{ij} \Rightarrow \underline{\mathbf{t}_1 = \begin{pmatrix} T_{11} \\ T_{12} \\ T_{13} \end{pmatrix}}$$

$$\text{"Shear stress"} = \begin{pmatrix} 0 \\ T_{12} \\ T_{13} \end{pmatrix} \rightarrow \text{magnitude} = \sqrt{T_{12}^2 + T_{13}^2}$$



$$\underline{\mathbf{t}^{(n)} - (\mathbf{n} \cdot \mathbf{t}^{(n)}) \mathbf{n} = (n_i T_{ij} - n_k n_l T_{lk} n_j) \mathbf{e}_j = n_l T_{lk} (\delta_{kj} - n_k n_j) \mathbf{e}_j}$$

When this shear stress will be maximum?

$$\begin{array}{l} \text{Coord} \\ T_1 \geq T_2 \geq T_3 \end{array} \quad \Pi = \begin{pmatrix} T_1 & 0 & 0 \\ 0 & T_2 & 0 \\ 0 & 0 & T_3 \end{pmatrix} \Rightarrow \underline{\text{when } \mathbf{n} \text{ bisects } \mathbf{n}_1 \text{ \& } \mathbf{n}_3.} \quad \Rightarrow \text{proof...?}$$

principal axes

5.9 Some simple state of stress

(a) Hydrostatic pressure (정유체압력)

$$\underline{T_{ij} = -p \delta_{ij}} \quad (\text{compression} \rightarrow T_{ij} < 0 \text{ but pressure } p > 0)$$

$$T_{11} = T_{22} = T_{33} = -p, \quad T_{12} = T_{13} = T_{32} = 0$$

(비점성)

→ Any fluid in equilibrium, or inviscid fluid (whether in equil or not)
and $p = p(x)$. (p is, in general, a function of position)

(*) In the remaining examples, body force will be neglected.

$$\frac{\partial}{\partial x_i} T_{ij} + \rho b_j = 0 \rightarrow \text{ex.) } \rho g h \text{ term will be neglected.}$$

6 T_{ij} 's, 3 eqns → one solution: $T_{ij} = \text{const} (*)$
(insufficient)

→ stress is homogeneous.

(b) Uniform tension or compressing along x_1



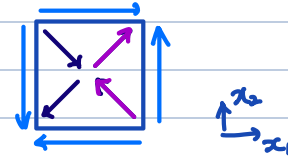
$$\Pi = \begin{pmatrix} \sigma & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}, \text{ principal axes} = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \text{ \& any two orthogonal direction.}$$

(c) Uniform shear stress in x_1 , on plane $x_2 = \text{const}$.



$$\Pi = \begin{pmatrix} 0 & \tau & 0 \\ \tau & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}, \text{ principal axes} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}, \begin{pmatrix} \frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} \\ 0 \end{pmatrix}, \begin{pmatrix} \frac{1}{\sqrt{2}} \\ -\frac{1}{\sqrt{2}} \\ 0 \end{pmatrix}$$

τ $-\tau$
(1,1)방향, (1,-1)방향



(d) Pure bending



$$\Pi = \begin{pmatrix} Cx_2 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}, \text{ principal axes: } \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \text{ \& any two orthogonal direction.}$$

(e) Plane stress

$$\Pi = \begin{pmatrix} T_{11} & T_{21} & 0 \\ T_{12} & T_{22} & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$$\begin{cases} \frac{\partial}{\partial x_1} T_{11} + \frac{\partial}{\partial x_2} T_{21} = 0 \\ \frac{\partial}{\partial x_1} T_{12} + \frac{\partial}{\partial x_2} T_{22} = 0 \end{cases} \leftarrow \text{Equilibrium eqn (w/o body force)}$$

principal axes: $\begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$ \& some orthogonal direction.

(f) pure torsion



$$\Pi = g(r) \begin{pmatrix} 0 & 0 & x_2 \\ 0 & 0 & -x_1 \\ x_2 - x_1 & 0 \end{pmatrix}$$

$r = \sqrt{x_1^2 + x_2^2}$

① force acting on surface $\mathbf{n} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \Rightarrow g(r) \begin{pmatrix} x_2 \\ -x_1 \\ 0 \end{pmatrix}$

② no force on this surface $\mathbf{n} = \frac{1}{r} \begin{pmatrix} x_1 \\ x_2 \\ 0 \end{pmatrix} \Rightarrow 0$

③ shear force $\hat{\theta}$ surface $\mathbf{n} = \frac{1}{r} \begin{pmatrix} -x_2 \\ x_1 \\ 0 \end{pmatrix} \Rightarrow g(r) \begin{pmatrix} 0 \\ 0 \\ -r \end{pmatrix}$