

## Lecture-4

### Analog Communications

*Abstract:*

#### Pre-envelope

For the real valued signal  $g(t)$ , the pre-envelope is defined as

$$g_p(t) = g(t) + j\hat{g}(t) \quad (1)$$

We know that

$$FT\{\hat{g}(t)\} = -j \operatorname{sign}(f)G(f) \quad (2)$$

If we take the Fourier transform of (1), we get

$$G_p(f) = G(f) + jFT\{\hat{g}(t)\}$$

in which using (2), we obtain

$$G_p(f) = G(f) + j\{-j \operatorname{sign}(f)G(f)\}$$

leading to

$$G_p(f) = G(f) + \operatorname{sign}(f)G(f)$$

which can be expressed as

$$G_p(f) = \begin{cases} 2G(f) & f > 0 \\ G(0) & f = 0 \\ 0 & f < 0. \end{cases} \quad (3)$$

Note that

$$sgn(f) = \begin{cases} 1 & f > 0 \\ 0 & f = 0 \\ -1 & f < 0. \end{cases}$$

### Summary for the Pre-Envelope Calculation of a Signal

1) The pre-envelope of  $g(t)$  can be calculated using

$$g_p(t) = g(t) + j\hat{g}(t).$$

where  $\hat{g}(t)$  is the Hilbert transform of  $g(t)$ .

2) The pre-envelope of  $g(t)$  can be calculated first calculating the Fourier transform of  $g(t)$ , i.e., finding  $G(f)$ , and next evaluating

$$G_p(f) = \begin{cases} 2G(f) & f > 0 \\ G(0) & f = 0 \\ 0 & f < 0. \end{cases}$$

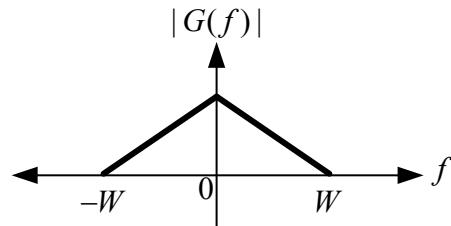
and lastly taking the inverse Fourier transform of  $G_p(f)$ , we get  $g_p(t)$ , i.e.,

$$g_p(t) = 2 \int_0^{\infty} G(f) e^{j2\pi ft} df.$$

### Low-Pass Signal

If the magnitude spectrum of a signal is centered around the origin, the signal is called a low pass signal.

The Fourier transform of a typical low-pass signal is as shown in Figure-1.

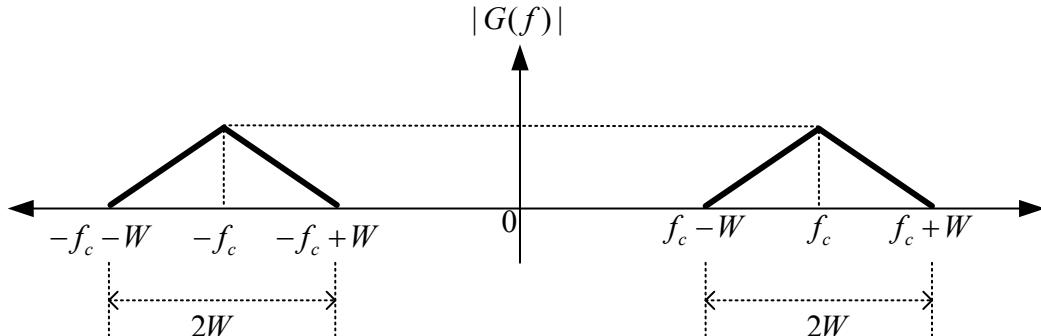


**Figure-1**

### Band-pass Signal

If the magnitude spectrum of a signal is centered around frequencies  $\pm f_c$ , then the signal is called a band-pass signal.

The magnitude spectrum of a typical band-pass signal is depicted in Figure-2.



**Figure-2**

### Bandwidth

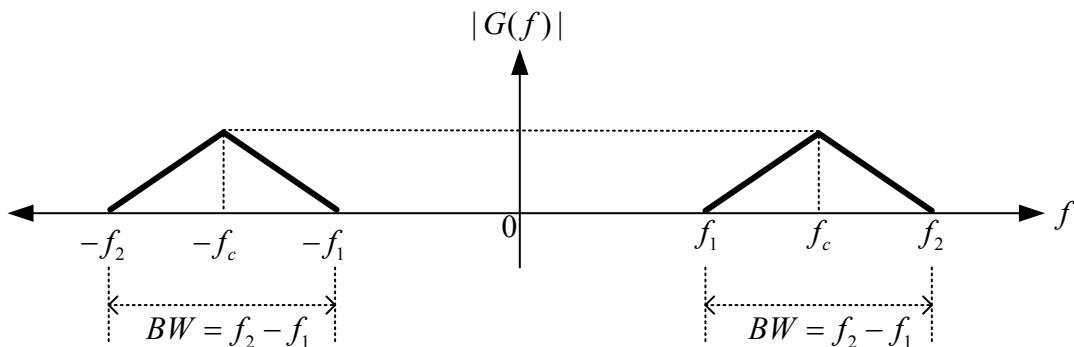
Signal bandwidth is the difference between the largest and the smallest positive frequencies in the magnitude spectrum of a signal.

Signal bandwidth can be defined in different ways. Two well-known definitions are the null-to-null bandwidth and 3-dB bandwidth.

### Null-to-Null Bandwidth

In null-to-null bandwidth definition, the amplitude of the frequencies used for the bandwidth calculation can go up to 0.

The calculation of the null-to-null bandwidth is depicted in Figure-3.



**Figure-3**

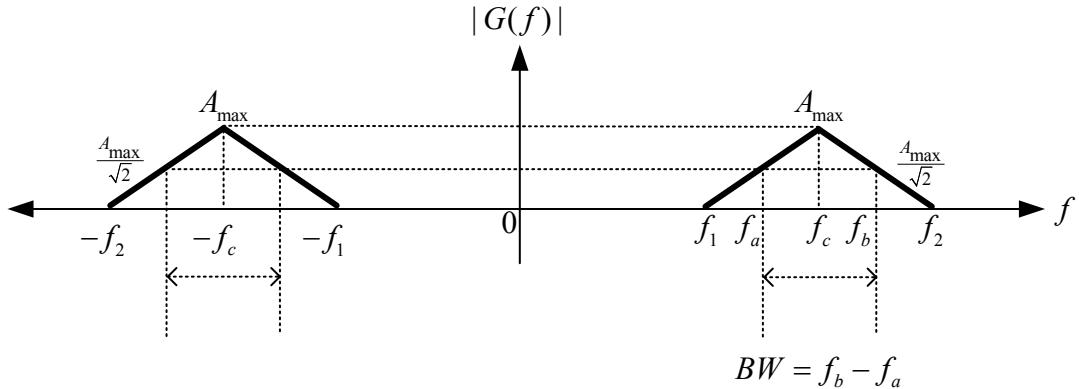
### 3-dB Bandwidth

In 3-dB bandwidth definition, the amplitude of the frequencies used for the bandwidth calculation should be larger than equal to

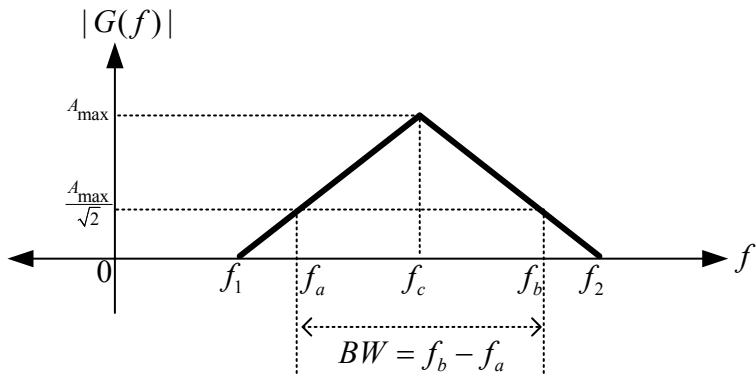
$$\frac{A_{max}}{\sqrt{2}}$$

where  $A_{max}$  is the maximum value of the magnitude spectrum.

The calculation of the 3-dB bandwidth is depicted in Figure-4.

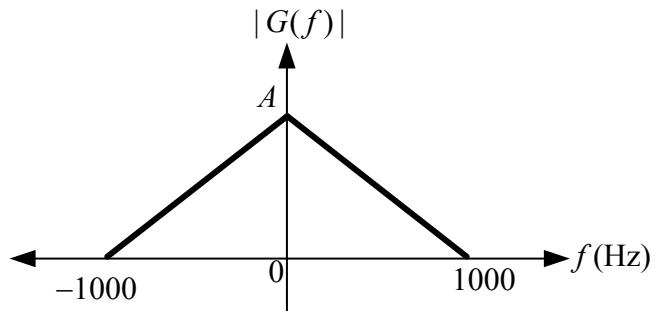


**Figure-4**



**Figure-5**

**Example:** The magnitude spectrum of a low-pass signal is given in Figure-6. What is the bandwidth of this signal?



**Figure-6**

**Solution:** The bandwidth if the signal is 1000Hz. This is a low-pass signal.

### Complex Envelope

Let  $g_p(t)$  be the pre-envelope of  $g(t)$ . The complex envelope of  $g(t)$  is calculated using

$$g_c(t) = g_p(t)e^{-j2\pi f_c t} \quad (4)$$

The Fourier transform of  $g_c(t)$  can be expressed as

$$G_c(f) = G_p(f + f_c) \quad (5)$$

Note that  $FT\{x(t)e^{j2\pi f_c t}\} = X(f - f_c)$ .

From (4), we can write that

$$g_p(t) = g_c(t)e^{j2\pi f_c t}$$

in which substituting  $g_p(t) = g(t) + j\hat{g}(t)$  we obtain

$$g(t) + j\hat{g}(t) = g_c(t)e^{j2\pi f_c t} \quad (6)$$

from which we can write that

$$g(t) = Re\{g_c(t)e^{j2\pi f_c t}\} \quad (7)$$

### Property:

If  $g(t)$  is a band-pass signal, then its complex envelope  $g_c(t)$  is a low-pass signal.

### Verification:

Let the magnitude spectrum of the band-pass signal be as in Figure-7.

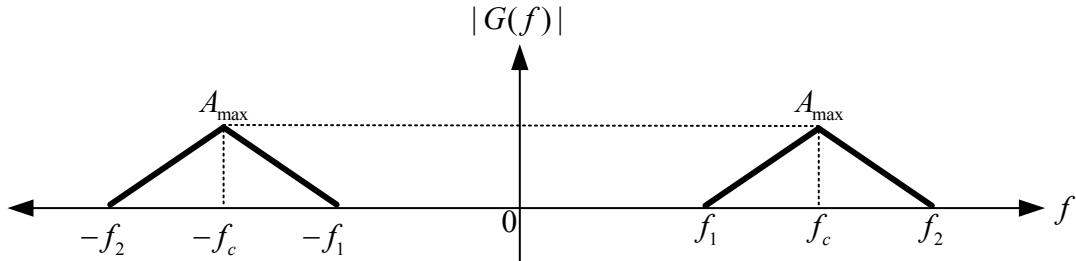
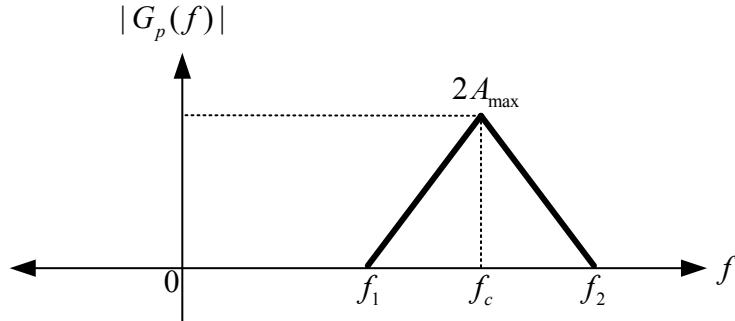


Figure-7

The magnitude spectrum of the pre-envelope signal  $g_p(t)$  can be drawn as in Figure-9 using

$$G_p(f) = \begin{cases} 2G(f) & f > 0 \\ G(0) & f = 0 \\ 0 & f < 0. \end{cases}$$

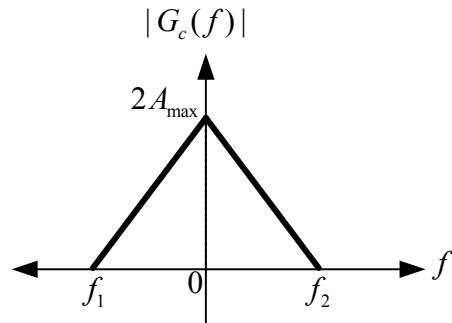


**Figure-8**

Using (5), i.e.,

$$G_c(f) = G_p(f + f_c)$$

we can draw the graph of  $G_c(f)$  as in



**Figure-9**

From (6), i.e.,

$$g(t) + j\hat{g}(t) = g_c(t)e^{j2\pi f_c t}$$

it is clear that  $g_c(t)$  is a complex number, and we can express  $g_c(t)$  as in

$$g_c(t) = g_I(t) + jg_Q(t) \quad (8)$$

Using (8) in

$$g(t) = \operatorname{Re}\{g_c(t)e^{j2\pi f_c t}\}$$

we get

$$g(t) = \operatorname{Re}\{[g_I(t) + jg_Q(t)][\cos(2\pi f_c t) + j \sin(2\pi f_c t)]\}$$

leading to

$$g(t) = \operatorname{Re}\{g_I(t) \cos(2\pi f_c t) - g_Q(t) \sin(2\pi f_c t) + j \dots\}$$

resulting in

$$g(t) = g_I(t) \cos(2\pi f_c t) - g_Q(t) \sin(2\pi f_c t)$$

### **Result Summary:**

If  $g_c(t)$  is a low-pass complex signal such that

$$g_c(t) = g_I(t) + jg_Q(t) \quad (9)$$

then

$$g(t) = \operatorname{Re}\{g_c(t)e^{j2\pi f_c t}\}$$

is a band-pass signal which can also be written as

$$g(t) = g_I(t) \cos(2\pi f_c t) - g_Q(t) \sin(2\pi f_c t).$$

The complex envelope signal

$$g_c(t) = g_I(t) + jg_Q(t) \quad (10)$$

can also be written as

$$g_c(t) = |g_c(t)|e^{j\theta(t)} \quad (11)$$

where

$$|g_c(t)| = \sqrt{g_I^2(t) + g_Q^2(t)} \text{ and } \theta(t) = \arctan \frac{g_Q(t)}{g_I(t)}.$$

The equation in (11) can be written as

$$g_c(t) = |g_c(t)| \cos \theta(t) + ja(t) \sin \theta(t) \quad (12)$$

Comparing (10) and (11), we can write that

$$g_I(t) = |g_c(t)| \cos \theta(t) \quad g_Q(t) = |g_c(t)| \sin \theta(t).$$

Besides employing using (11) in

$$g(t) = \operatorname{Re}\{g_c(t)e^{j2\pi f_c t}\}$$

we obtain

$$g(t)=|g_c(t)|\cos\bigl(2\pi f_ct+\theta(t)\bigr).$$