

What is the open-circuit voltage gain,  $\mu_f$ , in  $V_V$  for an NPN BJT operating in the forward-active region at  $27^\circ C$  with  $I_C = 75 \mu A$ ? Use  $\beta = 127$ ,  $V_A = 75V$ , and  $V_t = kT/q = 26mV$ .

$$M_f = g_m \cdot r_o \quad g_m = \frac{I_C}{V_t} \quad r_o = \frac{V_A}{I_C} \quad M_f = 0.02907 \cdot 99206.35 \\ (756 \times 10^{-6}) A \quad 75V \quad = 2883.93$$

$$g_m = \frac{(756 \times 10^{-6})A}{(26 \times 10^{-2})V} = 0.02907 \quad r_o = \frac{75V}{(756 \times 10^{-6})A} = 99206.35$$

22. What is the device transconductance,  $g_m$ , in  $\text{mA/V}$  for an NMOS FET operating in saturation with  $I_d = 200 \text{ mA}$ ? Use  $W/L = 50$  and  $k' = 100 \text{ mA/V}^2$ . Neglect the effects of channel-length modulation and body effect.

$$I_1 = \frac{E_{V2} - V_{BE1}}{R_{B1}} \quad I_2 = \frac{E_{V2} - V_{BE2}}{R_{B2}} \quad I_3 = \frac{E_{V2} - V_{BE3}}{R_{B3}}$$

For the BST bias circuit shown, what is the emitter voltage,  $V_E$ , in volts? Use  $V_{CC} = 8\text{ V}$ ,  $V_{EE} = -7\text{ V}$ ,  $V_B = -2.6\text{ V}$ ,  $R_C = 4.9\text{ k}\Omega$ , and  $R_E = 5.9\text{ k}\Omega$ . Assume that the transistor is in the forward-active region, with  $\beta = 48$  and  $|V_{BE(\text{on})}| = 0.7\text{ V}$ .

$$V_{CE} = V_{CC} - V_B - V_E$$

$$I_E R_E = 8 - (-2.6) - 0.7$$

$$V_E = V_{CC} - I_E R_E$$

$$V_E = 8 - 9.9 = -1.9 \text{ V}$$

$$I_E = \frac{9.9}{R_E} = \frac{9.9 \text{ V}}{5900 \Omega} = 0.00167797 \text{ A}$$

For the MOSFET bias circuit shown, what is the source current,  $I_S$ , in milliamperes? Assume the transistor is in the saturation region, and use:  $V_{dd} = 11V$ ,  $R_{g1} = 41.7k\Omega$ ,  $R_{g2} = 59.8k\Omega$ ,  $R_d = 1.0k\Omega$ ,  $R_s = 8.2k\Omega$ ,  $V_t = -0.7V$ , and  $|V_{on}| = 0.18$ .

$$V_g = \left( \frac{R_{g2}}{R_{g1} + R_{g2}} \right) V_{dd} = \left( \frac{59800}{41100 + 59800} \right) 11 = 6.481 \text{ V}$$

$$|V_{og}| = |V_{on}| + |V_{t1}| = 0.18 + 0.7 = 0.88 \text{ V}$$

$$V_s = V_{sg} + V_g = 0.88 + 6.481 = 7.361 \text{ V}$$

$$I_S = \frac{V_{dd} - V_s}{R_S} = \frac{11 - 7.361}{8200} = 0.000444 \text{ A} = 0.444 \text{ mA}$$

What is the low frequency voltage gain for the amplifier shown at 27°C with  $R_d = 16.5\text{ k}\Omega$ ,  $R_S = 0.6\text{ k}\Omega$  and  $R_g = 3.9\text{ k}\Omega$ ? Use  $w/L = 17$ ,  $I_D = 328\mu\text{A}$ ,  $V_{TN} = 0.5\text{ V}$ ,  $k_n = 100\text{ mA/V}^2$ .

The circuit diagram shows a common-emitter configuration. The input voltage \$V\_i\$ is connected to the base terminal through a resistor \$R\_G\$. The collector terminal is connected to ground through a load resistor \$R\_L\$, which is in series with an output voltage \$V\_o\$. The collector terminal is also connected to the emitter terminal through a feedback resistor \$R\_f\$. The emitter terminal is connected to ground through a resistor \$R\_E\$.

Given values: \$V\_{DD} = 6.00V\$, \$R\_L = 328\Omega\$, \$R\_E = 17\Omega\$, \$R\_f = 100\Omega\$, \$R\_G = 100\Omega\$, \$k' = 100\$, \$I\_D = 1mA\$.

Calculation of \$g\_m\$:

$$g_m = \sqrt{2} (k'n) (W/L) (I_D) = \sqrt{2} (100 \times 10^{-6}) (17) (328 \times 10^{-6}) = 0.001056 \text{ mho}$$

Calculation of \$AV\$:

$$AV = \frac{R_L}{R_E + 1/g_m} = \frac{6.00}{6.00 + (1/0.001056)} = 0.38786 = 0.388$$

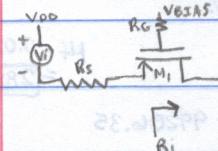
What is the low frequency voltage gain for the amplifier shown at 27°C with  $R_C = 24.3\text{ k}\Omega$ ,  $R_E = 0.1\text{ k}\Omega$ , and  $R_{bc} = 0.5\text{ k}\Omega$ ? Use  $I_C = 305\text{ mA}$ ,  $\beta = 32$ , and  $V_T = 26\text{ mV}$ .

$G_m = \frac{I_c}{V_t} = \frac{(305 \times 10^{-6})A}{(26 \times 10^{-3})V} = 0.01173$ 
 $r_{pi} = \frac{\beta}{g_m} = \frac{32}{0.01173} = 2727.8689\Omega$

$A_v = \frac{B \cdot R_L}{R_B + r_{pi} + (\beta + 1)R_E} = \frac{32 \cdot 24300}{500 + 2727.87 + (33)100} = 119.12$

What is the low frequency input resistance,  $R_i$ , in  $\text{k}\Omega$  for the amplifier shown at  $27^\circ\text{C}$  with  $R_d = 15.6\text{k}\Omega$ ,  $R_s = 0.4\text{k}\Omega$  and  $R_g = 4.8\text{k}\Omega$ ? Use:  $w/L = 53$ ,  $I_d = 248\text{mA}$ ,  $V_{TP} = -0.5\text{V}$ ,  $k'n = 40\text{mA/V}^2$ .

27.



$$I_d = \frac{1}{2} k'n (V_{ds} - V_t)^2$$

$$I_d = g_m = k'n (V_{gs} - V_t) = k'n \sqrt{\frac{2 I_d}{k_n}}$$

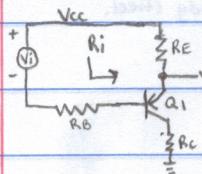
$$g_m = \sqrt{2(k'n)(I_d)} = \sqrt{2(0.00212)(248 \times 10^{-6})} = 0.001025436$$

$$R_i = 1/g_m = 1/0.001025436 = 975.19\Omega$$

$$k'n = k'n \cdot w/L = (40 \times 10^{-6})(53) = 0.00212$$

What is the low frequency input resistance,  $R_i$ , in  $\text{k}\Omega$  for the amplifier shown at  $27^\circ\text{C}$  with  $R_c = 47.0\text{k}\Omega$ ,  $R_e = 0.6\text{k}\Omega$  and  $R_b = 0.5\text{k}\Omega$ ? Use:  $I_c = 282\text{mA}$ ,  $\beta = 20$ ,  $V_t = 26\text{mV}$ .

28.



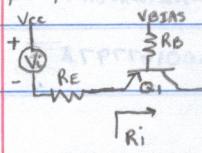
$$g_m = \frac{I_c}{V_t} = \frac{(282 \times 10^{-6})}{(26 \times 10^{-3})} = 0.010846$$

$$r_\pi = \frac{\beta}{g_m} = \frac{20}{0.010846} = 1843.97$$

$$R_i = r_\pi + (\beta + 1)R_e = 1843.97 + (20)(600) = 14443.97\Omega = 14.4\text{k}\Omega$$

What is the low frequency output resistance,  $R_o$ , in  $\text{k}\Omega$  for the amplifier shown at  $27^\circ\text{C}$  with  $R_c = 79.3\text{k}\Omega$ ,  $R_e = 0.1\text{k}\Omega$ , and  $R_b = 0.6\text{k}\Omega$ ? Use:  $I_c = 270\text{mA}$ ,  $\beta = 41$ ,  $V_A = 10\text{V}$ ,  $V_t = 26\text{mV}$ .

29.



$$g_m = \frac{I_c}{V_t} = \frac{(270 \times 10^{-6})}{(26 \times 10^{-3})} = 0.0103846$$

$$R_o = R_c || r_o(1 + g_m R_E)$$

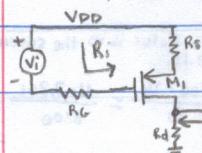
$$37037.037(1 + (0.0103846)100) = 75198.58$$

$$R_o = \frac{1}{79300} + \frac{1}{75198.58} = 0.000025856$$

$$R_o = \frac{1}{0.000025856} = 38676 = 38.7\text{k}\Omega$$

What is the low frequency output resistance,  $R_o$ , in  $\text{k}\Omega$  for the amplifier shown at  $27^\circ\text{C}$  with  $R_d = 98.5\text{k}\Omega$ ,  $R_s = 0.9\text{k}\Omega$ , and  $R_g = 3.8\text{k}\Omega$ ? Use:  $w/L = 16$ ,  $I_d = 520\text{mA}$ ,  $V_{TP} = -0.5\text{V}$ ,  $k'n = 40\text{mA/V}^2$ ,  $\lambda = 0.10$ .

30.



$$g_m = \sqrt{2k'n(w/L)} I_d = \sqrt{2(40 \times 10^{-6})(16)(520 \times 10^{-6})} = 0.0008158$$

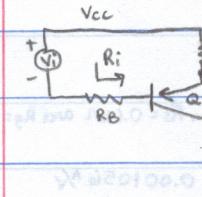
$$g_{mb} = 0, g_{de} = \lambda \cdot I_d = 0.10 \cdot (520 \times 10^{-6}) = 0.000052$$

$$R_o = R_d || r_o(1 + (g_m + g_{mb} + g_{de})R_s) = 98500 || 19230.77(1 + (0.0008158 + 0 + 0.000052)900)$$

$$R_o = 98500 || 34250.385 \rightarrow R_o = 25413.58 = 25\text{k}\Omega$$

Estimate the maximum low frequency voltage gain for the amplifier shown at  $27^\circ\text{C}$  with  $R_c = 43.3\text{k}\Omega$ ,  $R_e = 2.9\text{k}\Omega$  and  $R_b = 0.4\text{k}\Omega$ .

31.



$$V_{out} = V_{in} \cdot \frac{R_c}{R_c + R_b} = 13.18 \cdot \frac{43.3}{43.3 + 0.4} = 13.18 \cdot 0.991 = 13.18$$

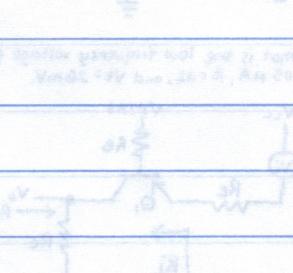
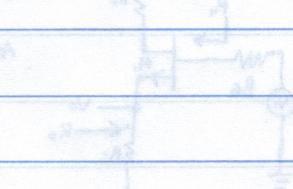
$$\frac{R_c}{R_c + R_b} = \frac{43300}{43300 + 400} = 0.991 = 1$$

$$A_{FE,0} = 20 \cdot 18.0 = 360$$

J.F. 200.0.0.0 =  $\frac{R_c}{R_c + R_b} = \frac{43.3}{43.3 + 0.4} = 0.991 = 1$

$$E_{F10,0} = \frac{43.3 \cdot 18.0}{43.3 + 0.4} = \frac{399.4}{43.7} = 9.07$$

$$S_{F11} = \frac{43.3 \cdot 18.0}{43.3 + 18.0} = \frac{781.4}{61.3} = 12.67$$



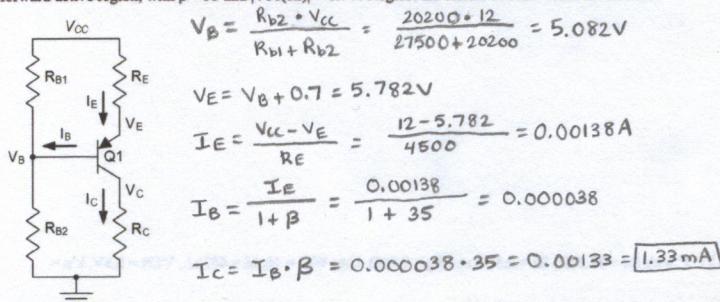
21. What is the open-circuit voltage gain,  $\mu_f$ , in V/V for an PNP BJT operating in the forward-active region at 27°C with  $I_c = 859\mu A$ ? Use:  $\beta = 18$ ,  $V_A = 65V$  and  $V_t = kT/q = 26mV$ .

$$g_m = \frac{I_c}{V_t} = \frac{(859 \times 10^{-6})}{(26 \times 10^{-3})} = 0.033 \quad r_o = \frac{V_A}{I_c} = \frac{65}{(859 \times 10^{-6})} = 75669.383 \quad \mu_f = g_m \cdot r_o = 0.033 \cdot 75669.383 = 2500$$

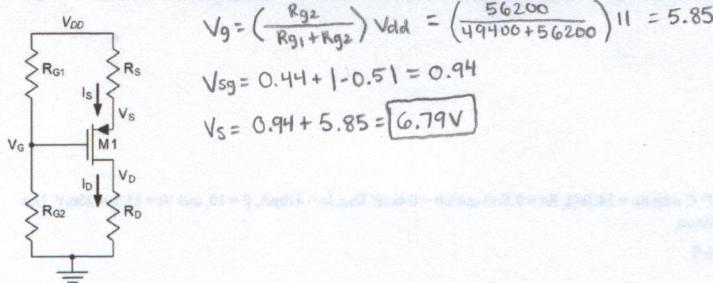
22. What is the output resistance,  $r_{ds}$ , in kΩ for an NMOS FET operating in saturation with  $I_d = 835\mu A$ ? Use:  $k = 0.40$

$$r_{ds} = \frac{1}{I_d \cdot k} = \frac{1}{(835 \times 10^{-6}) \cdot 0.40} = 2994.0119 = 2.99k\Omega$$

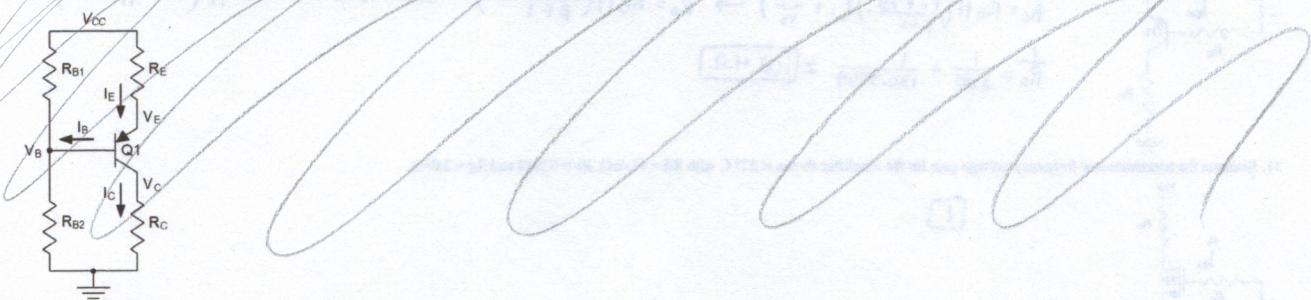
23. For the BJT bias circuit shown, what is the collector current,  $I_c$ , in millamps? Use  $V_{cc} = 12V$ ,  $R_{b1} = 27.5k\Omega$ ,  $R_{b2} = 20.2k\Omega$ ,  $R_c = 1.1k\Omega$ , and  $R_e = 4.5k\Omega$ . Assume that the transistor is in the forward-active region, with  $\beta = 35$  and  $|V_{be(on)}| = 0.7V$ . Neglect the effects of base-width modulation.



24. For the MOSFET bias circuit shown, what is the source voltage,  $V_s$ , in Volts? Assume that the transistor is in the saturation region, and use:  $V_{dd} = 11V$ ,  $R_{g1} = 49.4k\Omega$ ,  $R_{g2} = 56.2k\Omega$ ,  $R_d = 4.1k\Omega$ ,  $R_s = 9.7k\Omega$ ,  $V_t = -0.5V$ , and  $|V_{on}| = 0.44$ . (Remember that  $|V_{on}| = |V_{ov}| = |V_{gsl} - |V_i||$ ) Neglect the effect of channel-length modulation and body effect.



25. For the BJT bias circuit shown, what is the collector current,  $I_c$ , in millamps? Use  $V_{cc} = 12V$ ,  $R_{b1} = 27.5k\Omega$ ,  $R_{b2} = 20.2k\Omega$ ,  $R_c = 1.1k\Omega$ , and  $R_e = 4.5k\Omega$ . Assume that the transistor is in the forward-active region, with  $\beta = 35$  and  $|V_{be(on)}| = 0.7V$ . Neglect the effects of base-width modulation.



26. What is the low frequency voltage gain for the amplifier shown at 27°C with  $R_c = 32.7k\Omega$ ,  $R_e = 0.5k\Omega$  and  $R_b = 0.8k\Omega$ ? Use:  $I_c = 631\mu A$ ,  $\beta = 50$ , and  $V_t = kT/q = 26mV$ . Neglect the effect of base-width modulation.

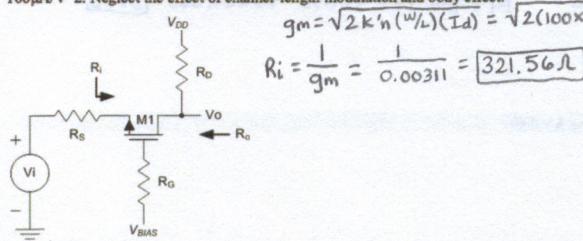
$$g_m = \frac{I_c}{V_t} = \frac{(631 \times 10^{-6})}{(26 \times 10^{-3})} = 0.0243$$

$$r_{\pi} = \frac{\beta}{g_m} = \frac{50}{0.0243} = 2060.22$$

$$A_V = \frac{(\beta+1)R_E}{R_B + r_{\pi} + (\beta+1)R_E} = \frac{(51)500}{800 + 2060.22 + (51)500} = 0.899$$

27. What is the low frequency input resistance,  $R_i$ , in Ω for the amplifier shown at 27°C with  $R_d = 48.4k\Omega$ ,  $R_s = 10.0k\Omega$  and  $R_g = 7.6k\Omega$ ? Use:  $W/L = 95$ ,  $I_d = 509\mu A$ ,  $V_{TN} = 0.5V$ ,  $k' = 100\mu A/V^2$ . Neglect the effect of channel-length modulation and body effect.

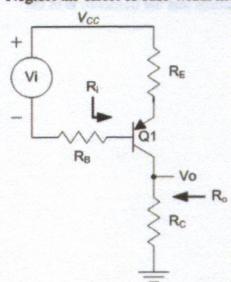
27. What is the low frequency input resistance,  $R_i$ , in  $\Omega$  for the amplifier shown at  $27^\circ C$  with  $R_d = 48.4\text{k}\Omega$ ,  $R_s = 10.0\text{k}\Omega$  and  $R_g = 7.6\text{k}\Omega$ ? Use:  $W/L = 95$ ,  $I_d = 509\mu\text{A}$ ,  $V_{TN} = 0.5\text{V}$ ,  $k'n = 100\mu\text{A/V}^2$ . Neglect the effect of channel-length modulation and body effect.



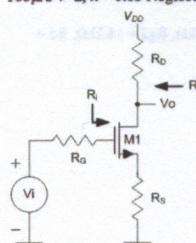
$$g_m = \sqrt{2k'n(W/L)(I_d)} = \sqrt{2(100 \times 10^{-6})(95)(509 \times 10^{-6})} = 0.00311$$

$$R_i = \frac{1}{g_m} = \frac{1}{0.00311} = 321.56\Omega$$

28. What is the low frequency input resistance,  $R_i$ , in  $\text{k}\Omega$  for the amplifier shown at  $27^\circ C$  with  $R_c = 44.3\text{k}\Omega$ ,  $R_e = 4.3\text{k}\Omega$  and  $R_b = 0.3\text{k}\Omega$ ? Use:  $I_c = 449\mu\text{A}$ ,  $\beta = 12$ , and  $V_t = kT/q = 26\text{mV}$ . Neglect the effect of base-width modulation.



29. What is the low frequency output resistance,  $R_o$ , in  $\text{k}\Omega$  for the amplifier shown at  $27^\circ C$  with  $R_d = 37.2\text{k}\Omega$ ,  $R_s = 0.8\text{k}\Omega$  and  $R_g = 2.9\text{k}\Omega$ . Use:  $W/L = 16$ ,  $I_d = 482\mu\text{A}$ ,  $V_{TN} = 0.5\text{V}$ ,  $k'n = 100\mu\text{A/V}^2$ ,  $\lambda = 0.05$ . Neglect body effect.

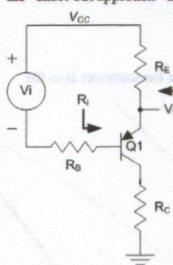


$$g_m = \frac{(V_{GS} - V_{TN})}{V_t} = \frac{(0.8 - 0.5)}{26 \times 10^{-3}} = 12.31$$

$$r_{\pi} = k_n \frac{W}{L} (V_{GS} - V_{TN}) (1 + \lambda V_{DS}) = 0.05 \times 12.31 \times (1 + 0.05 \times 0.8) = 0.634 \times 12.31 = 7.674 \text{ k}\Omega$$

$$R_o = \frac{1037.34\Omega \times R_d}{1037.34\Omega + R_d} = \frac{1037.34\Omega \times 37.2\Omega}{1037.34\Omega + 37.2\Omega} = 36.8\Omega$$

30. What is the low frequency output resistance,  $R_o$ , in  $\Omega$  for the amplifier shown at  $27^\circ C$  with  $R_c = 34.7\text{k}\Omega$ ,  $R_e = 0.5\text{k}\Omega$  and  $R_b = 0.8\text{k}\Omega$ ? Use:  $I_c = 410\mu\text{A}$ ,  $\beta = 10$ , and  $V_t = kT/q = 26\text{mV}$ . Use the "short-cut approach" discussed in class, and neglect the effect of base-width modulation.



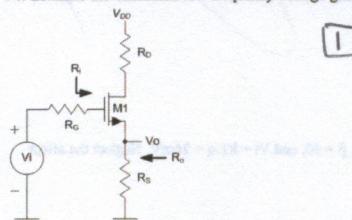
$$g_m = \frac{I_c}{V_t} = \frac{(410 \times 10^{-6})}{(26 \times 10^{-3})} = 0.015769$$

$$r_{\pi} = \frac{\beta}{g_m} = \frac{10}{0.015769} = 634.15$$

$$R_o = R_E \parallel \left( \frac{r_{\pi} + R_b}{\beta + 1} \right) (1 + \frac{R_c}{R_o}) \rightarrow R_o = R_E \parallel \left( \frac{r_{\pi} + R_b}{\beta + 1} \right) \quad \text{Since } r_o = \infty \Rightarrow 500 \parallel \left( \frac{634.15 + 800}{11} \right)$$

$$\frac{1}{R_o} = \frac{1}{500} + \frac{1}{130.3769} = 103.4\Omega$$

31. Estimate the maximum low frequency voltage gain for the amplifier shown at  $27^\circ C$  with  $R_d = 42.4\text{k}\Omega$ ,  $R_s = 0.2\text{k}\Omega$  and  $R_g = 2.0\text{k}\Omega$ .



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25. What is the low frequency voltage gain for the amplifier shown at  $27^\circ C$  with  $R_c = 39.2\text{k}\Omega$ ,  $R_e = 4.5\text{k}\Omega$  and  $R_b = 0.3\text{k}\Omega$ ? Use  $I_c = 668\mu\text{A}$ ,  $\beta = 74$ , and  $V_t = 26\text{mV}$ .

$$I_c = 668\mu\text{A}$$

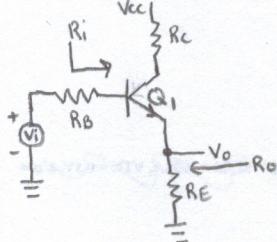
$$\beta = 74$$

$$V_t = 26\text{mV}$$

$$g_m = \frac{I_c}{V_t} = \frac{(668 \times 10^{-6})}{(26 \times 10^{-3})} = 0.02569$$

$$r_{\pi} = \frac{\beta}{g_m} = \frac{74}{0.02569} = 2880.24$$

$$A_v = \frac{(B+1)(R_E)}{R_B + r_{\pi} + (B+1)R_E} = \frac{(74+1)(4500)}{300 + 2880.24 + (74+1)4500} = 0.99$$



21. What is the base-to-emitter resistance,  $r_\pi$ , in kΩ for an NPN BJT operating in the forward-active region at 27°C with  $I_c = 708\mu A$ ? Use:  $\beta = 50$  and  $V_t = kT/q = 26mV$ .

$$g_m = \frac{I_c}{V_t} = \frac{(708 \times 10^{-6})}{(26 \times 10^{-3})} = 0.02723$$

$$r_\pi = \frac{\beta}{g_m} = \frac{50}{0.02723} = 1836.16\Omega = 1.84k\Omega$$

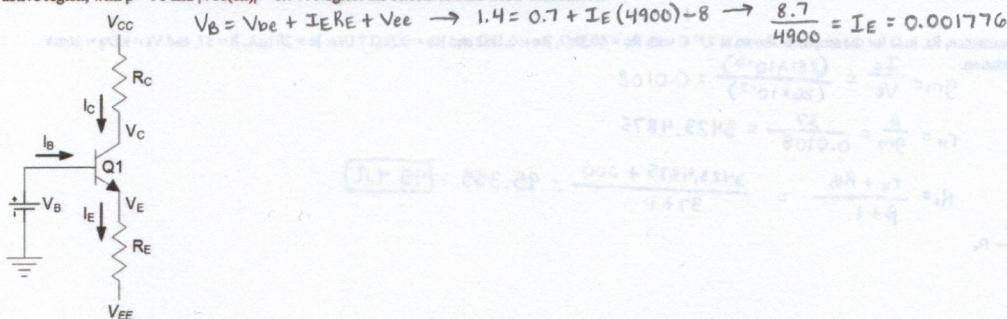
22. What is the open-circuit voltage gain,  $g_m$ , in V/V for an PMOS FET operating in saturation with  $I_d = 923\mu A$  and  $V_{on} = |V_{gs}-V_t| = 734mV$ ? Use:  $\lambda = 0.49$

$$g_m = \frac{2I_d}{V_{on}} = \frac{2(923 \times 10^{-6})}{(734 \times 10^{-3})} = 0.002515$$

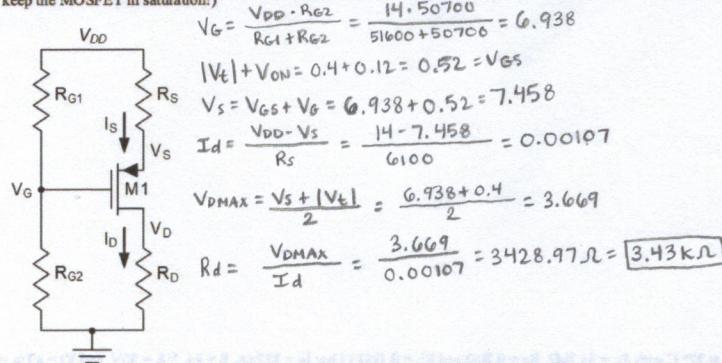
$$\text{gain} = r_o \cdot g_m = 2211.0686 \cdot 0.002515 = 5.56$$

$$r_o = \frac{1}{\lambda \cdot I_d} = \frac{1}{0.49 \cdot (923 \times 10^{-6})} = 2211.0686$$

23. For the BJT bias circuit shown, what is the collector voltage,  $V_c$ , in volts? Use  $V_{cc} = 5V$ ,  $V_{ee} = -8V$ ,  $V_b = 1.4V$ ,  $R_c = 4.5k\Omega$ , and  $R_e = 4.9k\Omega$ . Assume that the transistor is in the forward-active region, with  $\beta = 91$  and  $|V_{be(on)}| = 0.7V$ . Neglect the effects of base-width modulation.



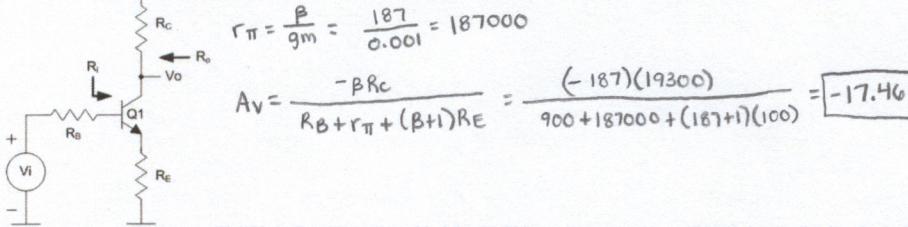
24. For the MOSFET bias circuit shown, what value of  $R_d$  in kilohms is needed to allow the maximum possible peak-to-peak signal swing on the drain without clipping? Use:  $V_{dd} = 14V$ ,  $R_{g1} = 51.6k\Omega$ ,  $R_{g2} = 50.7k\Omega$ ,  $R_s = 6.1k\Omega$ ,  $V_t = -0.4V$ , and  $|V_{on}| = 0.12$ . (Remember that  $|V_{on}| = |V_{ov}| = |V_{gs}| - |V_t|$ ) Neglect the effect of channel-length modulation and body effect. (Hint: Be sure to keep the MOSFET in saturation!)  $V_G = \frac{V_{dd} \cdot R_{g2}}{R_{g1} + R_{g2}} = \frac{14 \cdot 50.7}{51.6 + 50.7} = 6.938$



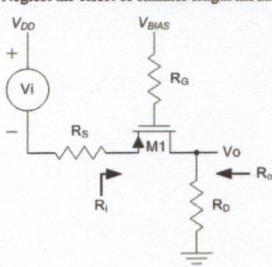
25. What is the low frequency voltage gain for the amplifier shown at 27°C with  $R_c = 19.3k\Omega$ ,  $R_e = 0.1k\Omega$  and  $R_b = 0.9k\Omega$ ? Use:  $I_c = 26\mu A$ ,  $\beta = 187$ , and  $V_t = kT/q = 26mV$ . Neglect the effect of base-width modulation.

$$g_m = \frac{I_c}{V_t} = \frac{(26 \times 10^{-6})}{(26 \times 10^{-3})} = 0.001$$

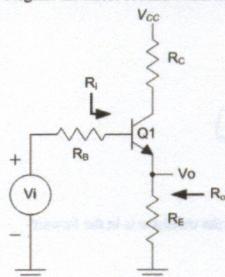
$$r_\pi = \frac{\beta}{g_m} = \frac{187}{0.001} = 187000$$



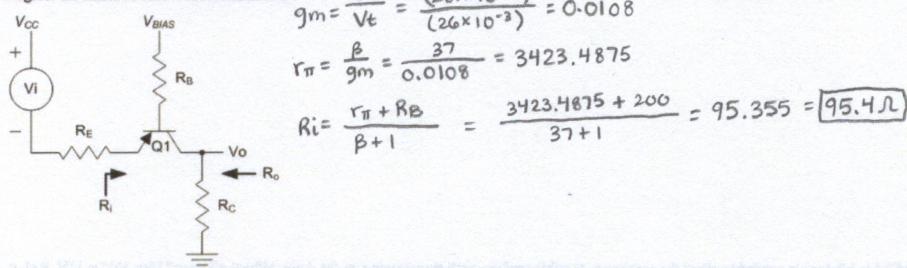
26. What is the low frequency voltage gain for the amplifier shown at 27°C with  $R_d = 34.6k\Omega$ ,  $R_s = 1.1k\Omega$  and  $R_g = 1.5k\Omega$ ? Use:  $W/L = 17$ ,  $I_d = 697\mu A$ ,  $V_{tp} = -0.5V$ ,  $k'p = 40\mu A/V^2$ . Neglect the effect of channel-length modulation and body effect.



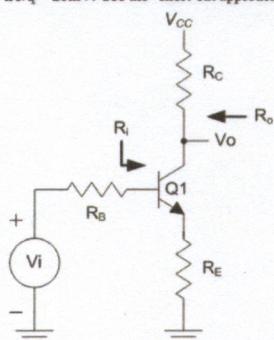
27. What is the low frequency input resistance,  $R_i$ , in  $\Omega$  for the amplifier shown at  $27^\circ C$  with  $R_c = 33.7\text{k}\Omega$ ,  $R_e = 0.4\text{k}\Omega$  and  $R_b = 0.3\text{k}\Omega$ ? Use:  $I_c = 129\mu\text{A}$ ,  $\beta = 189$ , and  $V_t = kT/q = 26\text{mV}$ . Neglect the effect of base-width modulation.



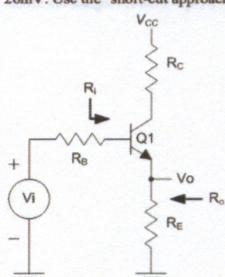
28. What is the low frequency input resistance,  $R_i$ , in  $\Omega$  for the amplifier shown at  $27^\circ C$  with  $R_c = 40.3\text{k}\Omega$ ,  $R_e = 0.1\text{k}\Omega$  and  $R_b = 0.2\text{k}\Omega$ ? Use:  $I_c = 281\mu\text{A}$ ,  $\beta = 37$ , and  $V_t = kT/q = 26\text{mV}$ . Neglect the effect of base-width modulation.



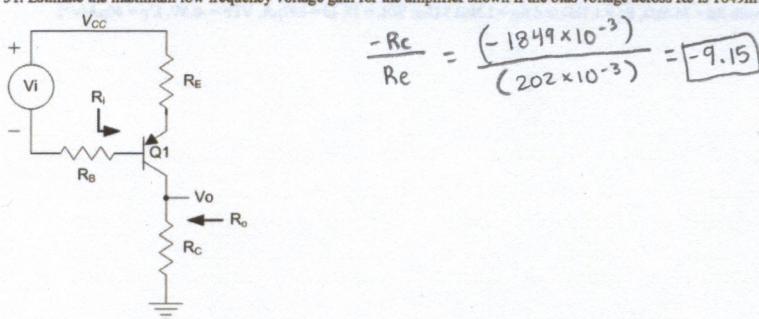
29. What is the low frequency output resistance,  $R_o$ , in  $\text{k}\Omega$  for the amplifier shown at  $27^\circ C$  with  $R_c = 76.4\text{k}\Omega$ ,  $R_e = 0.5\text{k}\Omega$  and  $R_b = 0.6\text{k}\Omega$ ? Use:  $I_c = 876\mu\text{A}$ ,  $\beta = 193$ ,  $V_A = 50\text{V}$ , and  $V_t = kT/q = 26\text{mV}$ . Use the "short-cut approach" discussed in class.



30. What is the low frequency output resistance,  $R_o$ , in  $\Omega$  for the amplifier shown at  $27^\circ C$  with  $R_c = 33.7\text{k}\Omega$ ,  $R_e = 0.2\text{k}\Omega$  and  $R_b = 0.1\text{k}\Omega$ ? Use:  $I_c = 227\mu\text{A}$ ,  $\beta = 84$ ,  $V_A = 50\text{V}$ , and  $V_t = kT/q = 26\text{mV}$ . Use the "short-cut approach" discussed in class, and neglect the effect of base-width modulation.



31. Estimate the maximum low frequency voltage gain for the amplifier shown if the bias voltage across  $R_c$  is 1849mV and the bias voltage across  $R_e$  is 202mV.

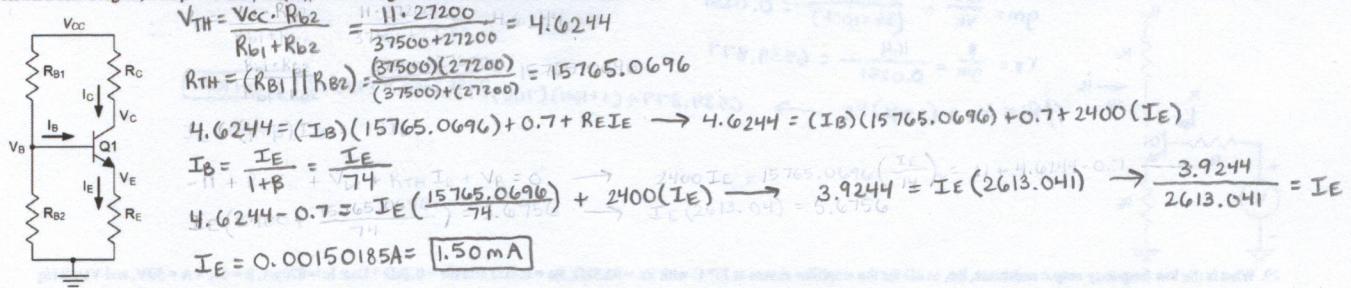


21. What is the transconductance, gm, in mA/V for a PNP BJT operating in the forward-active region at 27°C with  $I_C = 632\mu A$ ? Use  $V_t = kT/q = 26mV$ .

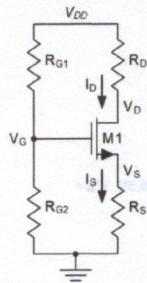
$$gm = \frac{I_C}{V_t} = \frac{(632 \times 10^{-6})}{(26 \times 10^{-3})} = 0.02431 \text{ A/V} \rightarrow 24.31 \frac{\text{mA}}{\text{V}}$$

22. What is the device transconductance, gm, in mA/V for a PMOS FET operating in saturation with  $I_d = 423\mu A$  and  $V_{on} = |V_{gs}-V_t| = 115mV$ ? Neglect the effects of channel-length modulation and body effect.

23. For the BJT bias circuit shown, what is the emitter current,  $I_E$ , in millamps? Use  $V_{cc} = 11V$ ,  $R_{b1} = 37.5k\Omega$ ,  $R_{b2} = 27.2k\Omega$ ,  $R_c = 4.2k\Omega$ , and  $R_e = 2.4k\Omega$ . Assume that the transistor is in the forward-active region, with  $\beta = 73$  and  $|V_{be(on)}| = 0.7V$ . Neglect the effects of base-width modulation.

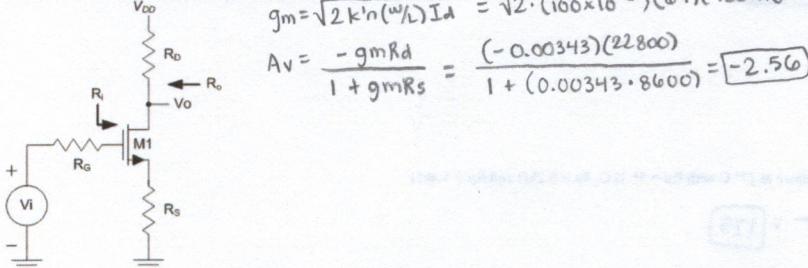


24. For the MOSFET bias circuit shown, what value of  $R_d$  in kilohms is needed to allow the maximum possible peak-to-peak signal swing on the drain without clipping? Use:  $V_{dd} = 13V$ ,  $R_{g1} = 43.9k\Omega$ ,  $R_{g2} = 43.5k\Omega$ ,  $R_s = 9.6k\Omega$ ,  $V_t = 0.6V$ , and  $V_{on} = 0.43$ . (Remember that  $V_{on} = V_{ov} = V_{gs}-V_t$ ) Neglect the effect of channel-length modulation and body effect. (Hint: Be sure to keep the MOSFET in saturation!)

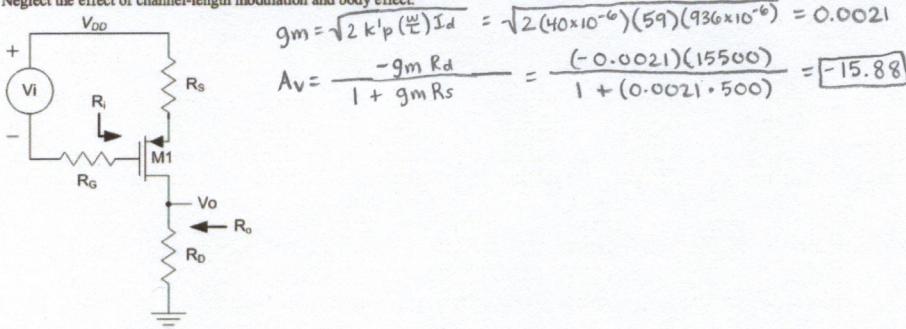


25. What is the low frequency voltage gain for the amplifier shown at 27°C with  $R_d = 22.8k\Omega$ ,  $R_s = 8.6k\Omega$  and  $R_g = 8.1k\Omega$ ? Use:  $W/L = 64$ ,  $I_d = 920\mu A$ ,  $V_{tn} = 0.5V$ ,  $k'n = 100\mu A/V^2$ . Neglect the effect of channel-length modulation and body effect.

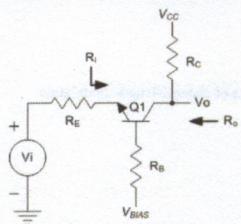
$$gm = \sqrt{2k'n(\omega/L)I_d} = \sqrt{2 \cdot (100 \times 10^{-6})(64)(920 \times 10^{-6})} = 0.00343$$



26. What is the low frequency voltage gain for the amplifier shown at 27°C with  $R_d = 15.5k\Omega$ ,  $R_s = 0.5k\Omega$  and  $R_g = 5.4k\Omega$ ? Use:  $W/L = 59$ ,  $I_d = 936\mu A$ ,  $V_{tp} = -0.5V$ ,  $k'p = 40\mu A/V^2$ . Neglect the effect of channel-length modulation and body effect.



27. What is the low frequency input resistance,  $R_i$ , in  $\Omega$  for the amplifier shown at  $27^\circ C$  with  $R_c = 38.7\text{k}\Omega$ ,  $R_E = 0.2\text{k}\Omega$  and  $R_b = 0.7\text{k}\Omega$ ? Use:  $I_c = 874\mu\text{A}$ ,  $\beta = 124$ , and  $V_t = kT/q = 26\text{mV}$ . Neglect the effect of base-width modulation.

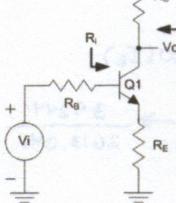


28. What is the low frequency input resistance,  $R_i$ , in  $\text{k}\Omega$  for the amplifier shown at  $27^\circ C$  with  $R_c = 31.4\text{k}\Omega$ ,  $R_E = 0.7\text{k}\Omega$  and  $R_b = 0.7\text{k}\Omega$ ? Use:  $I_c = 652\mu\text{A}$ ,  $\beta = 164$ , and  $V_t = kT/q = 26\text{mV}$ . Neglect the effect of base-width modulation.

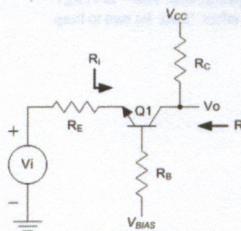
$$g_m = \frac{I_c}{V_t} = \frac{(652 \times 10^{-6})}{(26 \times 10^{-3})} = 0.0251$$

$$r_{\pi} = \frac{\beta}{g_m} = \frac{164}{0.0251} = 6539.877$$

$$R_i = r_{\pi} + (1+\beta)R_E \rightarrow 6539.877 + (1+164)(700) = 122039.877\Omega = 122.04\text{k}\Omega$$



29. What is the low frequency output resistance,  $R_o$ , in  $\text{k}\Omega$  for the amplifier shown at  $27^\circ C$  with  $R_c = 96.5\text{k}\Omega$ ,  $R_E = 0.4\text{k}\Omega$  and  $R_b = 0.2\text{k}\Omega$ ? Use:  $I_c = 870\mu\text{A}$ ,  $\beta = 51$ ,  $V_A = 50\text{V}$ , and  $V_t = kT/q = 26\text{mV}$ . Use the "short-cut approach" discussed in class.

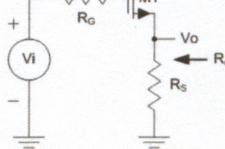


30. What is the low frequency output resistance,  $R_o$ , in  $\Omega$  for the amplifier shown at  $27^\circ C$  with  $R_d = 21.6\text{k}\Omega$ ,  $R_s = 1.0\text{k}\Omega$  and  $R_g = 7.5\text{k}\Omega$ . Use:  $W/L = 95$ ,  $I_d = 990\mu\text{A}$ ,  $V_{TN} = 0.5\text{V}$ ,  $k'n = 100\mu\text{A/V}^2$ ,  $\lambda = 0$ . Neglect body effect.

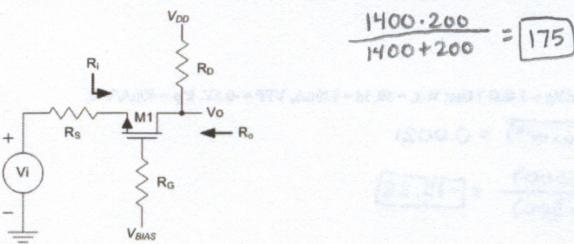
$$g_m = \sqrt{2k'n(\lambda/L)(I_d)} = \sqrt{2 \cdot (100 \times 10^{-6})(95)(990 \times 10^{-6})} = 0.00434$$

$$R_o = R_s || \left( \frac{1}{g_m} \right) = \frac{1}{R_o} = \frac{1}{R_s} + g_m \Rightarrow \frac{1}{1000} + 0.00434 = 0.00533705$$

$$R_o = \frac{1}{0.00533705} = 187.37\Omega$$



31. Estimate the maximum low frequency voltage gain for the amplifier shown at  $27^\circ C$  with  $R_d = 35.1\text{k}\Omega$ ,  $R_s = 0.2\text{k}\Omega$  and  $R_g = 1.4\text{k}\Omega$ .



$$\frac{1400 \cdot 200}{1400 + 200} = 175$$