

# Optimal LQR Control

## Topics Covered

- Introduction to state-space models.
- State-feedback control.
- Linear Quadratic Regulator (LQR) optimization.

## Prerequisites

- Filtering laboratory experiment.
- Rotary Pendulum Modeling laboratory experiment.
- Rotary pendulum module is attached to the QUBE-Servo 2.

# 1 Background

Linear Quadratic Regulator (LQR) theory is a technique that is ideally suited for finding the parameters of the pendulum balance controller in the Rotary Pendulum Modeling laboratory experiment. Given that the equations of motion of the system can be described in the form

$$\dot{x} = Ax + Bu,$$

where  $A$  and  $B$  are the state and input system matrices, respectively, the LQR algorithm computes a control law  $u$  such that the performance criterion or cost function

$$J = \int_0^{\infty} (x_{ref} - x(t))^T Q (x_{ref} - x(t)) + u(t)^T R u(t) dt \quad (1.1)$$

is minimized. The design matrices  $Q$  and  $R$  hold the penalties on the deviations of state variables from their setpoint and the control actions, respectively. When an element of  $Q$  is increased, therefore, the cost function increases the penalty associated with any deviations from the desired setpoint of that state variable, and thus the specific control gain will be larger. When the values of the  $R$  matrix are increased, a larger penalty is applied to the aggressiveness of the control action, and the control gains are uniformly decreased.

In our case the state vector  $x$  is defined

$$x = \begin{bmatrix} \theta & \alpha & \dot{\theta} & \dot{\alpha} \end{bmatrix}^T. \quad (1.2)$$

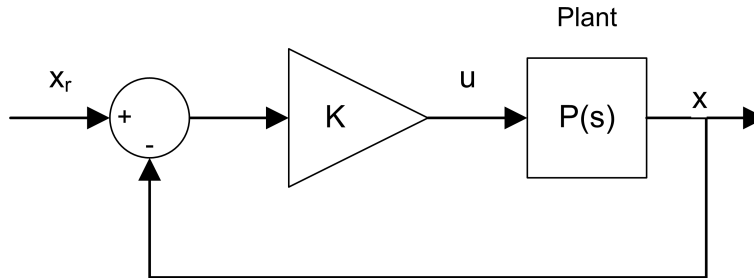


Figure 1.1: Block diagram of balance state-feedback control for rotary pendulum

Since there is only one control variable,  $R$  is a scalar. The reference signal  $x_{ref}$  is set to  $\begin{bmatrix} \theta_r & 0 & 0 & 0 \end{bmatrix}^T$ , and the control strategy used to minimize cost function  $J$  is thus given by

$$u = K(x_{ref} - x) = k_{p,\theta}(\theta_r - \theta) - k_{p,\alpha}\alpha - k_{d,\theta}\dot{\theta} - k_{d,\alpha}\dot{\alpha}. \quad (1.3)$$

This control law is a state-feedback control and is illustrated in Figure 1.1. It is equivalent to the PD control explained in the Rotary Pendulum Modeling laboratory experiment.

## 2 In-Lab Exercises

### 2.1 LQR Control Design

LQR design theory is available through the **LABVIEW™ Control Design & Simulation** module. Given a model of the system in state-space form (with system matrices  $A$  and  $B$ ) and the weighting matrices  $Q$  and  $R$ , the LQR function in the *Control Design* Toolkit automatically minimizes the cost function Equation 1.1 computes the optimal feedback control gain automatically.

In this experiment, the state-space model is already available. In the laboratory, the effect of changing the  $Q$  weighting matrix while  $R$  is fixed to 1 on the cost function  $J$  will be explored.

1. In the *QUBE-Servo 2* project file, expand the *Windows* target as well as the *LQR Design* virtual folder. Run the *QUBE-Servo 2 ROTPEN State-Space Model.vi* shown in Figure 2.1. This loads the *QUBE-Servo 2* rotary pendulum state-space model matrices  $A, B, C$ , and  $D$  and saves it to the file *qube\_servo\_2\_rotpen\_model* in a folder called *Rotary Pen Model*.

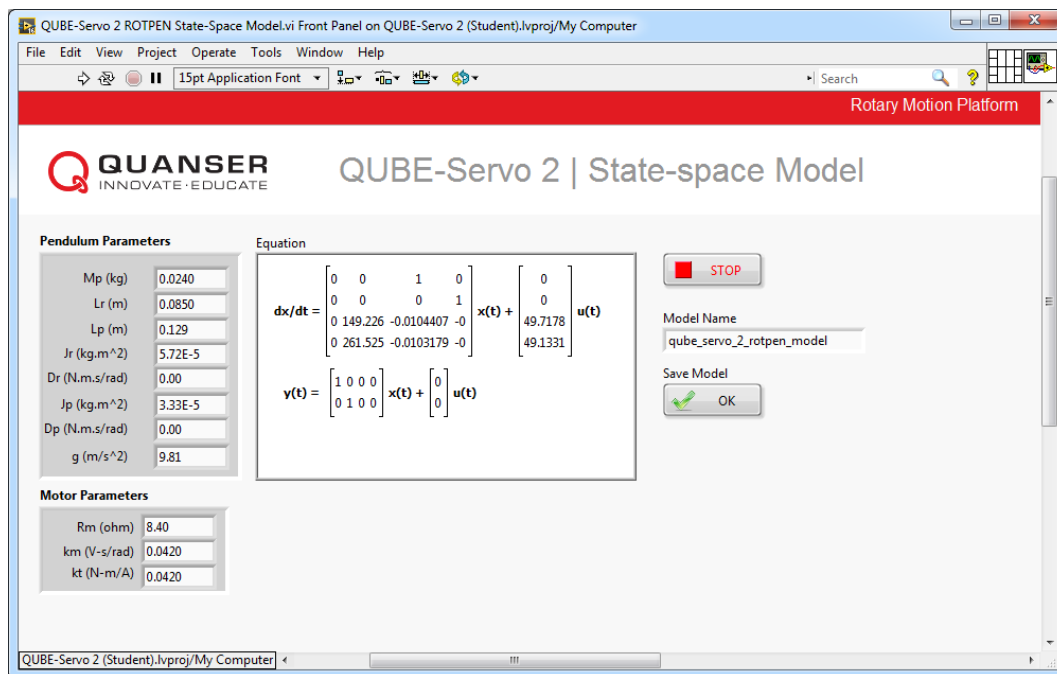


Figure 2.1: VI to generate QUBE-Servo 2 ROTPEN State-Space Model

2. Proceed to design a VI similar to Figure 2.2 to find the open-loop poles of the system. Use *Read Model* from *File* to load the model file you just saved (saved in the *Rotary Pen Model* folder). What do you notice about the location of the open-loop poles? How does that affect the system?
3. Use the *CD Read Model from File* and *CD Linear Quadratic Regular* VIs as shown in Figure 2.3 to generate the control gain  $K$ . Generate  $K$  using the following weighting matrices:

$$Q = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \text{and} \quad R = 1.$$

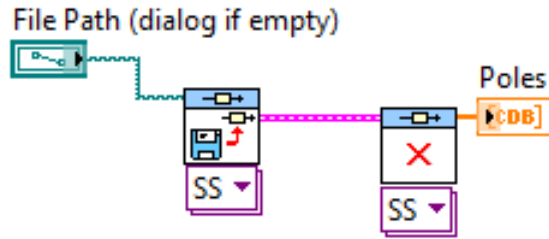
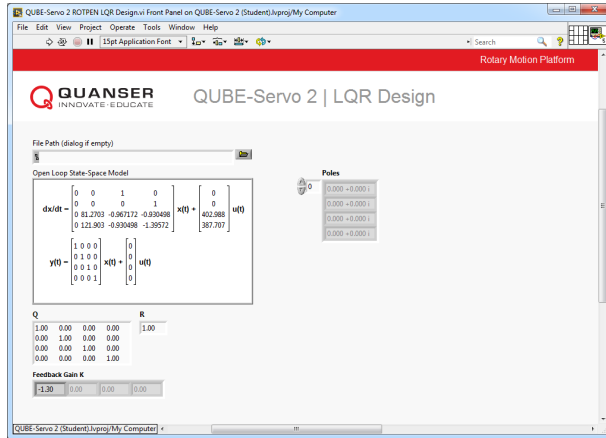
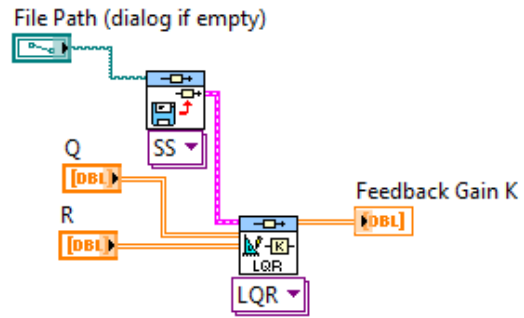


Figure 2.2: Find poles of loaded state-space model



(a) Front Panel



(b) Block Diagram

Figure 2.3: Generate LQR control gain using loaded state-space model

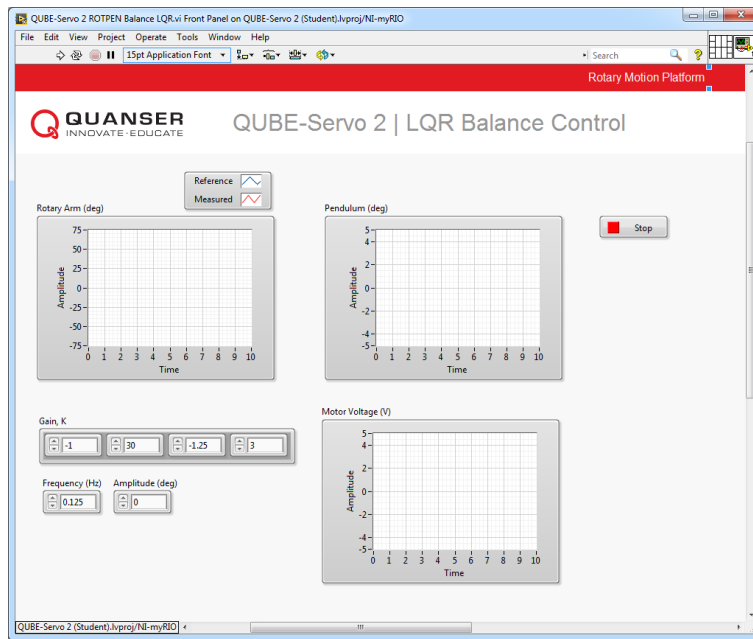
4. Change the LQR weighting matrix to the following and generate a new gain control gain:

$$Q = \begin{bmatrix} 5 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \text{and} \quad R = 1.$$

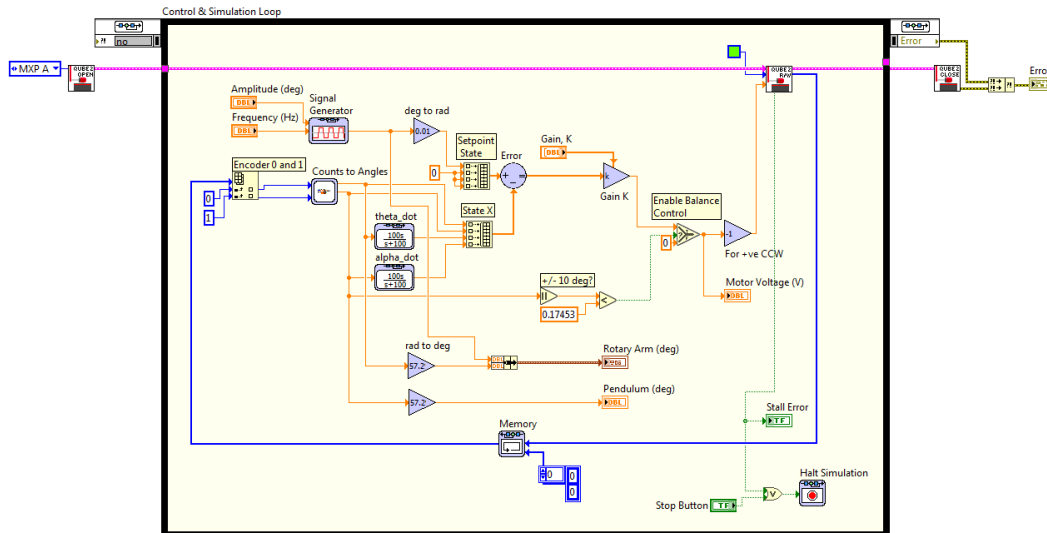
Record the gain generated. How does changing  $q_{11}$  affect the generated control gain? Based on the description of LQR in the background section, is this what you expected?

## 2.2 LQR-Based Balance Control

Based on the VI developed in the Rotary Pendulum Modeling laboratory experiment, construct a VI similar to that shown in Figure 2.4 that balances the pendulum on the QUBE-Servo 2 Rotary Pendulum system using an adjustable feedback control gain  $K$ .



(a) Front Panel



(b) Block Diagram

Figure 2.4: VI to run optimized balance controller

1. Either open QUBE-Servo 2 ROTPEN LQR Design.vi from the LQR Design virtual folder, or use the VI generated in the previous part of this laboratory experiment to generate the control gain  $K$  based on LQR and the QUBE-Servo 2 model.
2. Using the VI you made in the Rotary Pendulum Modeling laboratory experiment, construct the controller shown in Figure 2.4:
  - Using the angles from the Counts to Angles subsystem you designed in the Rotary Pendulum Modeling laboratory experiment (which converts encoder counts to radians), build state  $x$  given in Equation 1.2. As shown in Figure 2.4 use high-pass filters  $100s/(s+100)$  to compute the velocities  $\dot{\theta}$  and  $\dot{\alpha}$ .
  - Add the necessary Sum and Gain blocks to implement the state-feedback control given in Equation 1.3. Since the control gain is a vector, make sure the gain block is configured to matrix type multiplication.
  - Add the Signal Generator block in order to generate a varying, desired arm angle  $\theta_r$ . To generate a reference state  $x_r$ , make sure you include a Build Array VI to get  $\begin{bmatrix} \theta_r & 0 & 0 & 0 \end{bmatrix}^T$ .

- Set  $K$  in the QUBE-Servo 2 ROTPEN Balance LQR.vi to the gain that was generated in Step 3 of the LQR Control Design part of this lab.
- Set the Signal Generator block to the following:
  - Type = Square
- On the front panel, set the Amplitude (deg) control 0 and the Frequency (Hz) control to 0.125.
- Run the VI.
- Manually rotate the pendulum in the upright position until the controller engages.
- Once the pendulum is balanced, set the Amplitude (deg) control to 30 to make the arm angle go between  $\pm 30^\circ$ . The scopes should read something similar to Figure 2.5. Attach your response of the rotary arm, pendulum, and controller voltage.

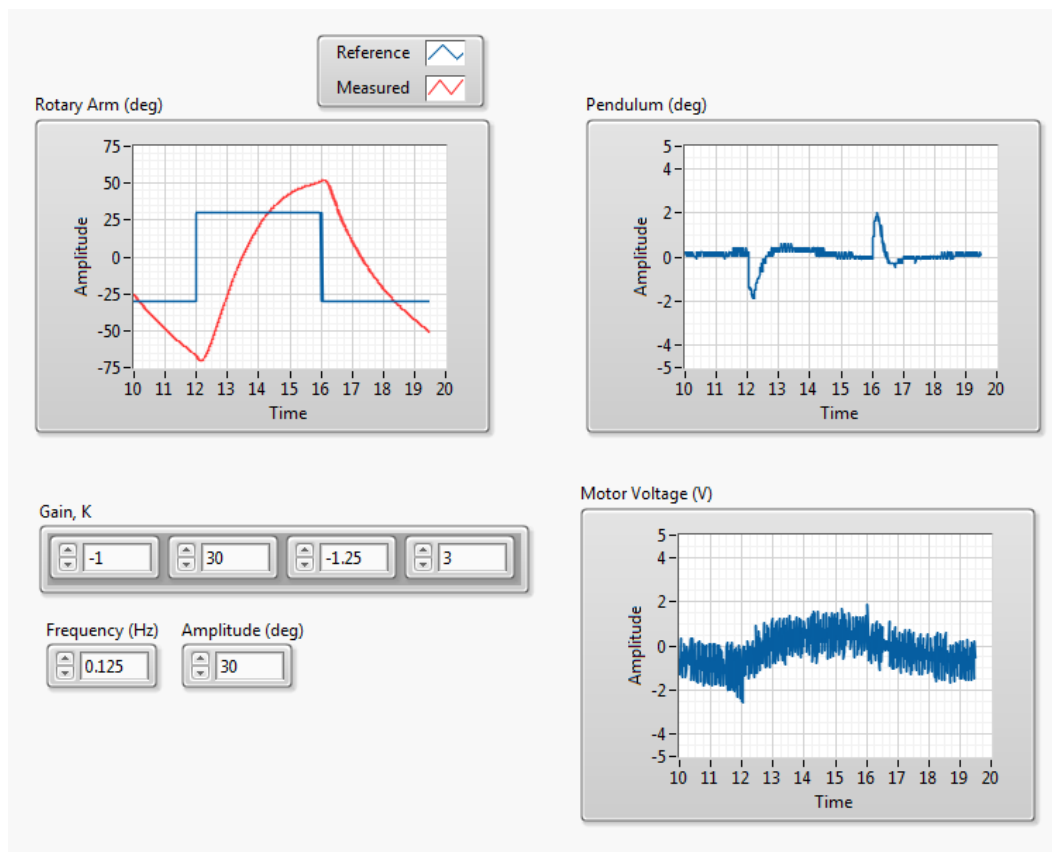


Figure 2.5: QUBE-Servo 2 rotary pendulum response

- Set  $K$  to the gain that was generated in the last step of the LQR Control Design part of this lab.
- Examine and describe the change in the *Rotary Arm (deg)* and *Pendulum (deg)* scopes.
- Adjust the diagonal elements of  $Q$  matrix to reduce how much the pendulum angle deflects (i.e. overshoots) when the arm angle changes. Describe your experimental procedure to find the necessary control gain.
- List the resulting LQR  $Q$  matrix and control gain  $K$  used to yield the desired results. Attach the responses using this new control gain and briefly outline how the response changed.
- Click on the Stop button to stop the VI.

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Printed in Markham, Ontario.

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