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# **Multi-Objective Optimal Power Flow on the IEEE 14-Bus Test System**

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## Abstract

This project presents a comprehensive approach to solving the Multi-Objective Optimal Power Flow (MO-OPF) problem on the IEEE 14-bus test system. The optimization framework targets two key objectives: minimizing the total generation cost and enhancing the voltage profile across the network. The generation cost is modeled as a quadratic function of active power, while the voltage profile objective minimizes deviations from the nominal voltage of 1.0 per unit. A weighted sum method is used to combine both objectives into a single formulation, allowing systematic exploration of trade-offs between them.

To enhance flexibility and avoid reliance on arbitrarily fixed weight values, Pareto front analysis is additionally employed across a range of weight combinations. This allows for a more informed and structured selection of operating points that reflect a logical balance between economic efficiency and voltage stability. The approach offers a practical and adaptable framework for real-world power system optimization.

## 1 Introduction

Power grids are very large, complicated networks designed to deliver electricity both economically and with high reliability. As pressures accumulate—more stringent emission regulations, increased integration of renewables, and higher reliability mandates—grid managers are increasingly reaching for Optimal Power Flow (OPF) techniques.

But modern power grids demand better than cost minimization. The operators must also ensure voltage stability in order to ensure system reliability and power quality. This dual challenge has necessitated Multi-Objective OPF (MO-OPF) methodologies that balance trade-offs between conflicting objectives—like cost minimization versus voltage profile improvement.

This project is addressing two main aims:

- Minimizing overall generation cost (typically expressed as a quadratic function of generator output)
- Improving voltage quality by minimizing deviations from the ideal 1.0 per-unit voltage value

A commonly employed strategy is the weighted sum approach, which pools objectives with adjustable weights. Trade-offs may be manipulated by varying these weights by operators. It is not a straightforward activity to pick the "optimal" weights, though.

Pareto methods overcome this through the provision of a set of optimal trade-offs, referred to as the Pareto front, without predefining weights. Decision-makers may select the ideal solution based on system conditions and priorities thereafter.

This study makes use of the <sup>2</sup>IEEE 14-bus test system to explain the MO-OPF approach. The actual generator mix, lines, and loads of the system are taken as a true testing environment. We make use of both weighted sum and Pareto approaches for demonstrating how efficiently operators can solve the cost–voltage trade-off problem. The structure also remains open for future objectives such as the minimization of emission or loss.

## 2 Literature Review

### 2.1 Review 1:

Optimal Power Flow (OPF) is a fundamental framework for ensuring power networks operate efficiently and safely. Traditionally, OPF was employed to reduce generation cost under voltage constraints, while recent formulations include objectives like voltage stability, power loss reduction, and emission minimization. Early OPF softwares utilized traditional optimization techniques like linear programming and quadratic programming and Newton-type approaches. Efficient for convex, smooth problems, these struggled with real-world systems not being linear and multimodal, opening the way for heuristic and metaheuristic approaches. They are more versatile but at increased computation and reduced transparency.

Among classical techniques, the weighted sum approach is common in multi-objective OPF (MO-OPF). By summing different objectives into a single function, it allows operators to alter the relative importance given to any goal through weight parameters—helpful in balancing goals like cost reduction and improvement in voltage profile.

In general, MO-OPF is interested in minimizing generation cost (expressed as a quadratic function) and maintaining voltage quality (by minimizing deviation from 1.0 p.u.). The weighted-sum method offers an operational means for investigating the trade-off, although the choice of weights must be determined in terms of system priorities.

Although Pareto-based methods portray the trade-off space in an more explicit manner, the weighted-sum method wins acceptance because it is simple, efficient, and could be readily employed as the starting point for advanced or data-intensive methodologies.

### 2.2 Review 2:

With growing uncertainties caused by renewable integration, market volatility, and climate change, OPF techniques have evolved towards stochastic, robust, and distributionally robust models. While these techniques enhance risk management, they increase complexity as well.

Deterministic MO-OPF remains applicable when system parameters are well established and simplicity is sought. Of them, the weighted-sum technique is widely used for its ability to aggregate multiple objectives into one function, allowing practical trade-off analysis.

### 3.1 Notations and Model Parameters

$f$  : Total objective function

$w_1, w_2$  : Weights for cost and voltage deviation

$N_g$  : Number of generators

$N_b$  : Number of buses

$a_i, b_i, c_i$  : Cost coefficients for generator  $i$

$V_{ref}$  : Reference voltage magnitude ( typically 1.0 p.u.)

$P_{Li}$  : Real power load at bus  $i$

$Q_{Li}$  : Reactive power load at bus  $i$

$G_{ij}$  : Real part of admittance between bus  $i$  and  $j$

$B_{ij}$  : Imaginary part of admittance between bus  $i$  and  $j$

$S_{ij}^{max}$  : Maximum apparent power flow limit on line  $i \rightarrow j$

### 3.2 Decision Variables

$P_{Gi}$  : Real power generated at bus  $i$  ( MW)

$Q_{Gi}$  : Reactive power generated at bus  $i$  ( MVar)

$V_i$  : Voltage magnitude at bus  $i$  ( p.u.)

$\theta_i$  : Voltage angle at bus  $i$  ( radians)

### 3.3 Multi-Objective Function

We minimize the objective function  $f$  to achieve a trade-off between reducing generation cost (first term) and improving voltage profile by minimizing deviations from reference voltages (second term).

$$f = w_1 \cdot \sum_{i=1}^{N_g} \left( a_i P_{Gi}^2 + b_i P_{Gi} + c_i \right) + w_2 \cdot \sum_{j=1}^{N_b} \left( V_j - V_{ref} \right)^2$$

### 3.4 Constraints

#### Equality Constraints ( Power Flow Equations)

1. Active Power Balance: (for all  $i$  in  $N_b$ )

$$P_{G_i} - P_{L_i} = V_i \sum_{j=1}^{N_b} V_j [G_{ij} \cos(\theta_i - \theta_j) + B_{ij} \sin(\theta_i - \theta_j)]$$

2. **Reactive Power Balance:** (for all  $i$  in  $N_b$ )

$$Q_{G_i} - Q_{L_i} = V_i \sum_{j=1}^{N_b} V_j [G_{ij} \sin(\theta_i - \theta_j) - B_{ij} \cos(\theta_i - \theta_j)]$$

### **Inequality Constraints**

1. **Generator Operating Limits:** (for all  $i$  in  $N_b$ )

$$P_{G_i}^{\min} \leq P_{G_i} \leq P_{G_i}^{\max}$$

$$Q_{G_i}^{\min} \leq Q_{G_i} \leq Q_{G_i}^{\max}$$

2. **Voltage Magnitude Limits:** (for all  $i$  in  $N_b$ )

$$V_i^{\min} \leq V_i \leq V_i^{\max} \quad (\text{usually } 0.95 \leq V_i \leq 1.05 \text{ p.u.})$$

3. **Line Flow Limits:** (for all  $i, j$  in  $N_b$ )

$$S_{ij} = \sqrt{P_{ij}^2 + Q_{ij}^2} \leq S_{ij}^{\max}$$

4. **Slack Bus Constraint:**

$$V_1 = 1.0 \text{ p.u.} \quad \theta_1 = 0 \text{ rad}$$

## **4 Methodology**

### **4.1 Method 1:**

Optimal power flow (OPF) analysis was performed on the base-case IEEE 14-bus system of MATPOWER's case14 dataset in MATLAB. The generator cost matrix (gencost) was verified and updated to ensure quadratic cost coefficients were defined for all five generators. Major system data—base MVA, bus admittance matrix (Ybus), generator limits, voltage limits, and loads—were extracted. Here, the script also stored the original bus and branch data into two Excel files (bus\_data.xlsx, branch\_data.xlsx)(in Appendix) with load, voltage, and line parameter values for note-taking. The Ybus matrix was divided into real (G) and imaginary (B) components for use in power balance equations, and generator cost coefficients (a, b, c) were utilized to define the cost objective.

Optimization parameters were <sup>4</sup> **Bus Voltage magnitudes, Voltage Angles, and Real and Reactive power outputs of generators (Pg and Qg)**. Initial guesses were specified within feasible limits.

A weighted objective function was formulated based on total generation cost and voltage deviation from 1.0 p.u. and their respective weights as 0.7 and 0.3. Constraints were set to ensure power balance at all buses, apply generator and voltage limits, fix the slack bus angle to 0°, and restrict line flows to below 100 MVA.

The nonlinear <sup>5</sup> **optimization problem** was solved by **MATLAB's fmincon** using the **Interior-point algorithm** and high iteration and tight tolerance parameters to ensure accuracy. Finally, **voltage and angle plots** were generated in order to plot the optimal solution.

## 4.2 Method 2:

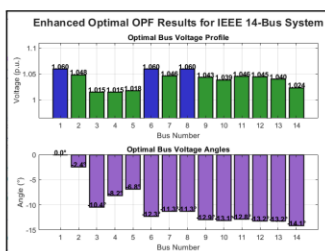
As a continuation of the previous multi-objective OPF solution, a **Pareto front-based approach** was employed to examine generation cost versus voltage deviation trade-offs in a systematic manner. Instead of employing fixed weights, the **epsilon-constraint method** <sup>3</sup> was used to generate a set of Pareto-optimal solutions by adjusting the permissible voltage deviation over a pre-specified range. For each solution point, the cost was minimized with an upper limit on voltage deviation. A Pareto front was constructed using these solutions for the range of cost-optimal to voltage-optimal operation.

Gradients between nearby Pareto points were utilized to compute equivalent weight pairs ( $w_1$  for cost,  $w_2$  for voltage deviation) per solution. Weights were normalized and expressed to demonstrate balanced trade-offs, dominating objectives, and ideal configurations to aid in making choices. The approach facilitated improved informed decisions among OPF solutions based on system priorities rather than predetermined fixed weightings.

## 5 Results

### 5.1 Results for Method 1:

The adjoining graph illustrates a well-controlled voltage and angle profile <sup>6</sup> achieved under the weighted sum optimization for the IEEE 14-bus system. As shown in the bar plots, all bus voltages lie within acceptable operational limits, with generator buses (1, 6, and 8) maintaining the highest



voltage level of 1.060 p.u. and the lowest voltages, approximately 1.015 p.u., observed at Buses 3 and 4. The voltage angles display a smooth and continuous decline from 0° at the slack bus (Bus 1) to -14.1° at Bus 14, indicating stable and consistent directional power flow across the network.

These trends are also confirmed by the numerical results, which show the effectiveness of the optimization in fulfilling both goals. The **cost of generation** was reduced to a minimum of

```
Optimal Bus Voltages and Angles:
Bus 1: V = 1.0600 p.u., theta = 0.0000 rad (0.00°)
Bus 2: V = 1.0485 p.u., theta = -0.0423 rad (-2.42°)
Bus 3: V = 1.0148 p.u., theta = -0.1822 rad (-10.44°)
Bus 4: V = 1.0153 p.u., theta = -0.1428 rad (-8.18°)
Bus 5: V = 1.0177 p.u., theta = -0.1193 rad (-6.84°)
Bus 6: V = 1.0600 p.u., theta = -0.2149 rad (-12.31°)
Bus 7: V = 1.0463 p.u., theta = -0.1971 rad (-11.29°)
Bus 8: V = 1.0600 p.u., theta = -0.1971 rad (-11.29°)
Bus 9: V = 1.0432 p.u., theta = -0.2255 rad (-12.92°)
Bus 10: V = 1.0387 p.u., theta = -0.2287 rad (-13.10°)
Bus 11: V = 1.0457 p.u., theta = -0.2241 rad (-12.84°)
Bus 12: V = 1.0448 p.u., theta = -0.2300 rad (-13.18°)
Bus 13: V = 1.0398 p.u., theta = -0.2312 rad (-13.25°)
Bus 14: V = 1.0235 p.u., theta = -0.2459 rad (-14.09°)

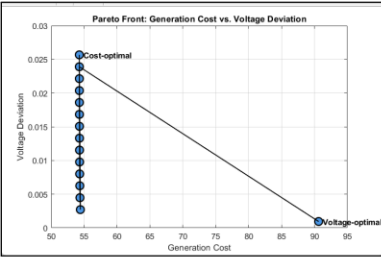
Optimal Generator Outputs:
Generator at Bus 1: Pg = 1.3807 p.u. (138.07 MW), Qg = 0.0000 p.u. (0.00 MVar)
Generator at Bus 2: Pg = 1.3074 p.u. (130.74 MW), Qg = 0.2223 p.u. (22.23 MVar)
Generator at Bus 3: Pg = 0.0000 p.u. (0.00 MW), Qg = 0.2974 p.u. (29.74 MVar)
Generator at Bus 6: Pg = 0.0000 p.u. (0.00 MW), Qg = 0.1054 p.u. (10.54 MVar)
Generator at Bus 8: Pg = 0.0000 p.u. (0.00 MW), Qg = 0.0826 p.u. (8.26 MVar)
Total Generation Cost: 54.2712
Voltage Profile Metric: 0.025657
```

**54.2712**, showcasing economic effectiveness, and the **voltage profile metric** reduced to **0.025657**, signifying low deviation from nominal voltage. Only Buses 1 and 2 produced real power with generations of 138.07 MW and 130.74 MW, respectively. Reactive support was given by Buses 3, 6, and 8.

Overall, the outcomes verify that the weighted sum approach effectively balances cost reduction with voltage stability throughout the network.

5.2 Results for Method 2:

The Pareto front achieved by the epsilon-constraint method shows the trade-off relationship

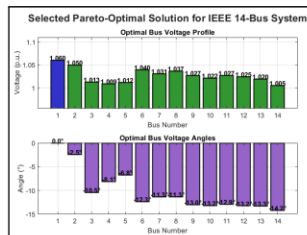
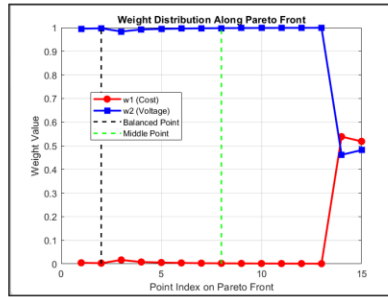


between voltage deviation and generation cost. The curve shows that reducing generation cost leads to larger voltage deviations, and the reverse. This reverse relationship illustrates the nature of multi-objective optimization—where the improvement in one objective normally sacrifices another. The smooth continuity of points along the front reveals a well-behaved

optimization process and a well-balanced range of feasible solutions.

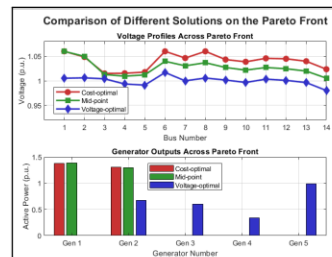


In the adjoining figure, discrete Pareto-optimal solutions are plotted for selected values of the epsilon constraint. Each point represents an optimal solution obtained for a fixed upper bound on voltage deviation. The graph illustrates how the generation cost decreases gradually as the permissible deviation increases. This confirms that the cost function responds effectively to variations in the constraint and enables a range of optimal trade-off solutions to be explored based on operational priorities.



The bar chart shows how generation cost decreases with increasing epsilon values. As the voltage deviation constraint is relaxed, the cost drops steadily, highlighting the benefit of allowing slight flexibility. This supports earlier findings and offers a clearer comparison across discrete scenarios for informed cost optimization.

This figure corroborates the cost analysis by showing the respective voltage deviation profile for each epsilon value. An increasing deviation trend is apparent, which exactly replicates the cost savings seen earlier. This verifies the expected trade-off pattern, as more relaxed deviation limits allow the system to be more cost-effective but with poorer voltage quality.



Detailed Results for Pareto Solution:  
Generation Cost: 54.2961, Voltage Deviation: 0.013311

Optimal Bus Voltages and Angles:

Bus 1:  $V = 1.0600$  p.u.,  $\theta = 0.0000$  rad ( $0.00^\circ$ )  
 Bus 2:  $V = 1.0498$  p.u.,  $\theta = -0.0433$  rad ( $-2.48^\circ$ )  
 Bus 3:  $V = 1.0128$  p.u.,  $\theta = -0.1829$  rad ( $-10.48^\circ$ )  
 Bus 4:  $V = 1.0094$  p.u.,  $\theta = -0.1421$  rad ( $-8.14^\circ$ )  
 Bus 5:  $V = 1.0120$  p.u.,  $\theta = -0.1184$  rad ( $-6.78^\circ$ )  
 Bus 6:  $V = 1.0397$  p.u.,  $\theta = -0.2155$  rad ( $-12.35^\circ$ )  
 Bus 7:  $V = 1.0306$  p.u.,  $\theta = -0.1979$  rad ( $-11.34^\circ$ )  
 Bus 8:  $V = 1.0368$  p.u.,  $\theta = -0.1979$  rad ( $-11.34^\circ$ )  
 Bus 9:  $V = 1.0271$  p.u.,  $\theta = -0.2275$  rad ( $-13.03^\circ$ )  
 Bus 10:  $V = 1.0217$  p.u.,  $\theta = -0.2306$  rad ( $-13.21^\circ$ )  
 Bus 11:  $V = 1.0271$  p.u.,  $\theta = -0.2255$  rad ( $-12.92^\circ$ )  
 Bus 12:  $V = 1.0246$  p.u.,  $\theta = -0.2312$  rad ( $-13.25^\circ$ )  
 Bus 13:  $V = 1.0198$  p.u.,  $\theta = -0.2326$  rad ( $-13.33^\circ$ )  
 Bus 14:  $V = 1.0054$  p.u.,  $\theta = -0.2482$  rad ( $-14.22^\circ$ )

These graphs are confirmed by the numerical results, which show the effectiveness of using the Pareto front analysis for optimization in fulfilling both goals. The cost of

Optimal Generator Outputs:  
 Generator at Bus 1: Pg = 1.2900 p.u. (139.00 MW), Qg = 0.0000 p.u. (0.00 MVar)  
 Generator at Bus 2: Pg = 1.2995 p.u. (129.95 MW), Qg = 0.3493 p.u. (34.93 MVar)  
 Generator at Bus 3: Pg = 0.0000 p.u. (0.00 MW), Qg = 0.3039 p.u. (30.39 MVar)  
 Generator at Bus 6: Pg = 0.0000 p.u. (0.00 MW), Qg = 0.0349 p.u. (3.49 MVar)  
 Generator at Bus 8: Pg = 0.0000 p.u. (0.00 MW), Qg = 0.0368 p.u. (3.68 MVar)

generation was reduced to a minimum of **54.2961**, and the voltage profile metric reduced to **0.013311**, signifying low deviation

from nominal voltage. Buses 1 and 2 produced real power with generations of 139.00 MW and 129.95 MW, respectively. Reactive support was given by Buses 3, 6, and 8. Overall, the outcomes show that the Pareto front analysis is a logical and effective way to deal with real-life multi-objective functions.

## 6 Conclusion

This project achieves a technique of solving <sup>1</sup>the Multi-Objective Optimal Power Flow (MO-OPF) problem using the IEEE 14-bus test system. By applying dual goals of reducing total generation cost and enhancing voltage profile, the research gives a practicable framework for solving economic and stability concerns in power system operation. Though the weighted sum approach proved effective to combine the cost and voltage objectives into one function, Pareto front analysis was employed to generate a collection of optimal, non-dominated solutions that offer a broader perspective of the balance of cost and voltage. The approach is devoid of the limitations of relying on a single set of pre-specified weights and allows operators to select best-suited solutions according to available system conditions.

The application of both techniques in the MO-OPF framework equips power system operators with enhanced decision-making capacities to deal with the advanced and dynamic requirements of modern power systems, enabling wiser and robust operating strategies.

## 7 References

Reference 1: Ebeed, M., Kamel, S., & Jurado, F. (2018). *Optimal Power Flow Using Recent Optimization Techniques. In Classical and Recent Aspects of Power System Optimization (Chapter 7, pp. 157-183). Academic Press.*

Reference 2: Roald, L. A., Pozo, D., Papavassiliou, A., Molzahn, D. K., Kazempour, J., & Conejo, A. (2023). *Power systems optimization under uncertainty: A review of methods and applications. Electric Power Systems Research, 214, 108725.*  
<https://www.elsevier.com/locate/epsr>

## 8 Appendix

### Method 1:

```
1 function analyze_opt_case14()
2 % Load MATPOWER's 14-bus case and define constants
3 mpc = case14;
4 define_constants;
5
6 % Ensure generator cost data exists (5 generators for case14)
7 if size(mpc.genconst, 2) < 7
8     mpc.genconst = [
9         2, 0, 0, 2, 0.02, 10, 100;
10        2, 0, 0, 2, 0.04, 8, 80;
11        2, 0, 0, 2, 0.03, 12, 120;
12        2, 0, 0, 2, 0.05, 15, 150;
13        2, 0, 0, 2, 0.025, 9, 90;
14    ];
15 end
16 % Set branch limits (RATE A)
17 mpc.branch(:, RATE_A) = 100; % 100 MVA limit
18
19 %% Extract System Parameters
20 baseMVA = mpc.baseMVA;
21 nb = size(mpc.bus, 1); % Number of buses (14 for case14)
22 ng = size(mpc.gen, 1); % Number of generators (5 for case14)
23 nl = size(mpc.branch, 1); % Number of branches
24 slack_bus = find(mpc.bus(:, BUS_TYPE) == 3);
25
26 % Admittance matrix
27 [Ybus, ~, ~] = makeYbus(baseMVA, mpc.bus, mpc.branch);
28 G = real(Ybus);
29 B = imag(Ybus);
30
31 %% Generator data
32 Pmin = mpc.gen(:, PHIN) / baseMVA;
33 Pmax = mpc.gen(:, PHAX) / baseMVA;
34 Qmin = mpc.gen(:, QMIN) / baseMVA;
35 Qmax = mpc.gen(:, QMAX) / baseMVA;
36 if size(mpc.genconst, 2) >= 7
37     a = mpc.genconst(:, 5);
38     b = mpc.genconst(:, 6);
39     c = mpc.genconst(:, 7);
40 else
41     a = 0.01 * ones(ng, 1);
42     b = 10 * ones(ng, 1);
43     c = 100 * ones(ng, 1);
44 end
45 Vmin = mpc.bus(:, VMIN);
46 Vmax = mpc.bus(:, VMAX);
47 Pd = mpc.bus(:, PD) / baseMVA;
48 Qd = mpc.bus(:, QD) / baseMVA;
49
50 %% Optimization Setup
51 w1 = 0.7; % Weight on generation cost
52 w2 = 0.3; % Weight on voltage deviations
53 Vref = 1.0;
54 % Initial guess for decision variables: [V; theta; Pg; Qg]
55 V0 = ones(nb, 1);
56 theta0 = zeros(nb, 1);
57 Pg0 = zeros(ng, 1);
58 Qg0 = zeros(ng, 1);
59 % Map generator bus indices & set mid-range generation values
60 for i = 1:ng
61     Pg0(i) = (Pmax(i) + Pmin(i)) / 2;
62     Qg0(i) = (Qmax(i) + Qmin(i)) / 2;
63 end
64 x0 = [V0; theta0; Pg0; Qg0];
65 % Define variable bounds
66 lb_V = Vmin;
67 ub_V = Vmax;
68 lb_theta = -pi * ones(nb, 1);
69 ub_theta = pi * ones(nb, 1);
70 lb_theta(slack_bus) = 0;
71 ub_theta(slack_bus) = 0;
72 lb_Pg = Pmin;
73 ub_Pg = Pmax;
74 lb_Qg = Qmin;
75 ub_Qg = Qmax;
76 lb = [lb_V; lb_theta; lb_Pg; lb_Qg];
77 ub = [ub_V; ub_theta; ub_Pg; ub_Qg];
78
79 %% Define Objective and Constraint Functions
80 objfun = @(x) opt_objective(x, nb, ng, gen_buses, a, b, c, w1, w2, Vref);
81 nonlcon = @(x) opt_constraints(x, nb, ng, nl, gen_buses, G, B, Pd, Qd, slack_bus, mpc.branch(:, RATE_A));
82
83 %% Optimization Options and Solve with fmincon
84 options = optimoptions('fmincon', 'Algorithm', 'interior-point', ...
85     'Display', 'iter', 'MaxFunctionEvaluations', 10000, ...
86     'MaxIterations', 1000, 'OptimalityTolerance', 1e-6, 'ConstraintTolerance', 1e-6);
87
88 [x_opt, fval, exitflag, output] = fmincon(objfun, x0, [], [], [], [], lb, ub, nonlcon, options);
89
90 %% Extract Results
91 V_opt = x_opt(1:nb);
92 theta_opt = x_opt(nb+1:2*nb);
93 Pg_opt = x_opt(2*nb+1:2*nb+ng);
94 Qg_opt = x_opt(2*nb+ng+1:end);
95
96 %% Display Numerical Results
97 disp('Optimal Bus Voltages and Angles:');
98 for i = 1:nb
99     fprintf('Bus %2d: V = %.4f p.u., theta = %.4f rad (%.2f°)\n', ...
100         i, V_opt(i), theta_opt(i), theta_opt(i)*180/pi);
101 end
102 disp('Optimal Generator Outputs:');
103 for i = 1:ng
```

```

99 fprintf('Generator at Bus %d: Pg = %.4f p.u. (%.2f MW), Qg = %.4f p.u. (%.2f MVar)\n', ...
100 gen_buses(i), Pg_opt(i), Pg_opt(i)*baseVA, Qg_opt(i), Qg_opt(i)*baseVA);
101 end
102 total_cost = sum(a.*Pg_opt.^2 + b.*Pg_opt + c);
103 fprintf('Total Generation Cost: %.4f\n', total_cost);
104 voltage_metric = sum((V_opt - Vref).^2);
105 fprintf('Voltage Profile Metric: %.6f\n', voltage_metric);
106 % Losses = calculate losses(V_opt, theta_opt, mpc_branch, baseVA);
107 % fprintf('Total System Losses: %.4f MW\n', losses);
108 % Enhanced Visual Outputs
109 figure('Name', 'Optimal OPF Results - IEEE 14-Bus', 'Color', [1 1 1]);
110 t = tiledlayout(2, 1, 'Padding', 'compact', 'TileSpacing', 'compact');
111 % Voltage Profile Plot
112 nexttile;
113 hBarVolt = bar(V_opt, 'FaceColor', 'flat', 'EdgeColor', 'k', 'LineWidth', 1.2);
114 % Apply gradient coloring based on voltage levels
115 for k = 1:length(V_opt)
116     if V_opt(k) < 0.95
117         hBarVolt.Data(k,:) = [0.8 0.2 0.2]; % Red tones for low voltages
118     elseif V_opt(k) > 1.05
119         hBarVolt.Data(k,:) = [0.2 0.2 0.8]; % Blue tones for high voltages
120     else
121         hBarVolt.Data(k,:) = [0.2 0.6 0.2]; % Green for acceptable voltage
122     end
123 end
124 grid on; box on;
125 xlabel('Bus Number');
126 ylabel('Voltage (p.u.)');
127 title('Optimal Bus Voltage Profile');
128 ylim(min(V_opt)+0.05, max(V_opt)+0.05);
129 xticks(1:length(V_opt));
130 % Annotate each bar with its voltage value
131 for k = 1:length(V_opt)
132     text(k, V_opt(k)+0.005, sprintf('%.3f', V_opt(k)), ...
133          'HorizontalAlignment', 'center', 'FontSize', 9, 'FontWeight', 'bold');
134 end
135 % Voltage Angle Plot
136 nexttile;
137 hBarAngle = bar(theta_opt*180/pi, 'FaceColor', [0.6 0.4 0.8], 'EdgeColor', 'k', 'LineWidth', 1.2);
138 grid on; box on;
139 xlabel('Bus Number');
140 ylabel('Angle (°)');
141 title('Optimal Bus Voltage Angles');
142 xticks(1:length(theta_opt));
143 % Annotate each angle value (in degrees)
144 for k = 1:length(theta_opt)
145     text(k, (theta_opt(k)*180/pi)+0.5, sprintf('%.1f°', theta_opt(k)*180/pi), ...
146          'HorizontalAlignment', 'center', 'FontSize', 9, 'FontWeight', 'bold');
147 end
148 % Add an overall title for the tiled layout
149 title(t, 'Enhanced Optimal OPF Results for IEEE 14-Bus System', 'FontSize', 14, 'FontWeight', 'bold');
150 end
151 % Objective Function
152 function f = opf_objective(x, nb, ng, gen_buses, a, b, c, w1, w2, Vref)
153 % Extract voltage and generator power values
154 V = x(1:nb);
155 Pg = x(2*nb+1:2*nb+ng);
156 % Generation cost (quadratic model)
157 gen_cost = sum(a.*Pg.^2 + b.*Pg + c);
158 % Voltage deviation cost
159 voltage_term = sum((V - Vref).^2);
160 % Weighted combined objective
161 f = w1*gen_cost + w2*voltage_term;
162 end
163 % Nonlinear Constraints
164 function [c, ceq] = opf_constraints(x, nb, ng, nl, gen_buses, G, B, Pd, Qd, slack_bus, Smax)
165 % Extract decision variables
166 V = x(1:nb);
167 theta = x(nb+1:2*nb);
168 Pg = x(2*nb+1:2*nb+ng);
169 Qg = x(2*nb+ng+1:2*nb+2*ng);
170 % Map generator outputs to their buses
171 Pg_bus = zeros(nb, 1);
172 Qg_bus = zeros(nb, 1);
173 for i = 1:ng
174     Pg_bus(gen_buses(i)) = Pg(i);
175     Qg_bus(gen_buses(i)) = Qg(i);
176 end
177 % Power balance equations for each bus
178 Pbalance = zeros(nb, 1);
179 Qbalance = zeros(nb, 1);
180 for i = 1:nb
181     P_inj = 0;
182     Q_inj = 0;
183     for j = 1:nb
184         angle_diff = theta(i) - theta(j);
185         P_inj = P_inj + V(i) * V(j) * (G(i,j) * cos(angle_diff) + B(i,j) * sin(angle_diff));
186         Q_inj = Q_inj + V(i) * V(j) * (B(i,j) * cos(angle_diff) - G(i,j) * sin(angle_diff));
187     end
188     Pbalance(i) = Pg_bus(i) - P_inj;
189     Qbalance(i) = Qg_bus(i) - Q_inj;
190 end
191 % Line flow constraints
192 line_flow = [];
193 if ~isempty(Smax) && Smax(1) == 999
194     line_flow = compute_lineflows(V, theta, nb, nl, G, B, Smax);
195 end
196 c = line_flow;
197 ceq = [Pbalance; Qbalance];
198 end

```

```

199 % Compute Line Flow
200 function c = computelineflow(V, theta, nb, nl, G, B, Smax)
201 c = [];
202 line_count = 0;
203 for i = 1:nb
204     for j = i+1:nb
205         if abs(G(i,j)) > 1e-6 || abs(B(i,j)) > 1e-6
206             line_count = line_count + 1;
207             if line_count <= nl
208                 angle_diff = theta(i) - theta(j);
209                 Pij = V(i)^2 * G(i,j) - V(i)*V(j) * (G(i,j)*cos(angle_diff) + B(i,j)*sin(angle_diff));
210                 Qij = -V(i)^2 * B(i,j) - V(i)*V(j) * (G(i,j)*sin(angle_diff) - B(i,j)*cos(angle_diff));
211                 Sij = sqrt(Pij^2 + Qij^2);
212                 c = [c; Sij - Smax(line_count)];
213             end
214         end
215     end
216 end
217 end
218

```

## Method 2:

```

1 function analyze_opt_case4_pareto()
2 % Load MATPOWER's 14-bus case and define constants
3 mpc = case4;
4 define_constants;
5 % Ensure generator cost data exists (5 generators for case4)
6 if size(mpc.gencost, 2) < 7
7     mpc.gencost = [
8         2, 0, 0, 2, 0.02, 10, 100;
9         2, 0, 0, 2, 0.04, 8, 80;
10        2, 0, 0, 2, 0.03, 12, 120;
11        2, 0, 0, 2, 0.05, 15, 150;
12        2, 0, 0, 2, 0.025, 9, 90;
13    ];
14 end
15 % Set branch limits (RATE_A)
16 mpc.branch(:, RATE_A) = 100; % 100 MVA limit
17 % Extract System Parameters
18 baseVA = mpc.baseVA;
19 nb = size(mpc.bus, 1); % Number of buses (14 for case4)
20 ng = size(mpc.gen, 1); % Number of generators (5 for case4)
21 nl = size(mpc.branch, 1); % Number of branches
22 slack_bus = find(mpc.bus(:, BUS_TYPE) == 3);
23 % Admittance matrix
24 [Ybus, ~] = makeYbus(baseVA, mpc.bus, mpc.branch);
25 G = real(Ybus);
26 B = imag(Ybus);
27 % Generator data
28 Pmin = mpc.gen(:, PMIN) / baseVA;
29 Pmax = mpc.gen(:, PMAX) / baseVA;
30 Qmin = mpc.gen(:, QMIN) / baseVA;
31 Qmax = mpc.gen(:, QMAX) / baseVA;
32 if size(mpc.gencost, 2) > 7
33     a = mpc.gencost(:, 5);
34     b = mpc.gencost(:, 6);
35     c = mpc.gencost(:, 7);
36 else
37     a = 0.01 * ones(ng, 1);
38     b = 10 * ones(ng, 1);
39     c = 100 * ones(ng, 1);
40 end
41 Vmin = mpc.bus(:, VMIN);
42 Vmax = mpc.bus(:, VMAX);
43 Pd = mpc.bus(:, PD) / baseVA;
44 Qd = mpc.bus(:, QD) / baseVA;
45 % Optimization Setup
46 Vref = 1.0;
47 % Initial guess for decision variables: [V; theta; Pg; Qg]
48 V0 = ones(nb, 1);
49 theta0 = zeros(nb, 1);
50 Pg0 = zeros(ng, 1);
51 Qg0 = zeros(ng, 1);
52 % Map generator bus indices & set mid-range generation values
53 gen_buses = mpc.gen(:, 1);
54 for i = 1:ng
55     Pg0(i) = (Pmax(i) + Pmin(i)) / 2;
56     Qg0(i) = (Qmax(i) + Qmin(i)) / 2;
57 end
58 u0 = [V0; theta0; Pg0; Qg0];
59 % Define variable bounds
60 lb_V = Vmin;
61 ub_V = Vmax;
62 lb_theta = -pi * ones(nb, 1);
63 ub_theta = pi * ones(nb, 1);
64 lb_theta(slack_bus) = 0;
65 ub_theta(slack_bus) = 0;
66 lb_Pg = Pmin;
67 ub_Pg = Pmax;
68 lb_Qg = Qmin;
69 ub_Qg = Qmax;
70 lb = [lb_V; lb_theta; lb_Pg; lb_Qg];
71 ub = [ub_V; ub_theta; ub_Pg; ub_Qg];
72 % Generate Pareto Front using epsilon-constraint method
73 % Define number of points on the Pareto front
74 num_points = 15;
75 % Find the range of each objective
76 % First, optimize for cost only
77 objfun_cost = @(x) optf_cost_objective(x, nb, ng, gen_buses, a, b, c);
78 noncon = @(x) optf_constraints(x, nb, ng, nl, gen_buses, G, B, Pd, Qd, slack_bus, mpc.branch(:, RATE_A)/baseVA);
79 options = optimoptions('fmincon', 'Algorithm', 'interior-point', ...
80     'Display', 'iter', 'MaxFunctionEvaluations', 10000, ...
81     'MaxIterations', 1000, 'OptimalityTolerance', 1e-6, 'ConstraintTolerance', 1e-6);
82 [x_cost, fval_cost, ~] = fmincon(objfun_cost, u0, lb, ub, noncon, options);
83 % Extract cost-optimal results
84 V_opt = x_cost(1:nb);
85 voltage_dev_at_cost_opt = sum((V_opt - Vref).^2);

```

```

86 fprintf('Min Cost Solution: Cost = %.4f, Voltage Deviation = %.6f\n', fval_cost, voltage_dev_at_cost_opt);
87 % Then, optimize for voltage profile only
88 objfun_voltage = @(x) opt_voltage_objective(x, nb, Vref);
89 [x_volt, fval_volt, ~, ~] = fmincon(objfun_voltage, x0, [], [], [], [], lb, ub, nonlin, options);
90 % Extract voltage-optimal results
91 cost_at_volt_opt = opt_cost_objective(x_volt, nb, ng, gen_buses, a, b, k);
92 fprintf('Min Voltage Deviation Solution: Cost = %.4f, Voltage Deviation = %.6f\n', cost_at_volt_opt, fval_volt);
93 % Define the range of epsilon
94 if voltage_dev_at_cost_opt > fval_volt
95     epsilon_values = linspace(fval_volt, voltage_dev_at_cost_opt, num_points);
96 else
97     epsilon_values = linspace(fval_volt, 2*voltage_dev_at_cost_opt, num_points);
98 end
99 % Create arrays to store Pareto front results
100 pareto_cost = zeros(num_points, 1);
101 pareto_voltage_dev = zeros(num_points, 1);
102 pareto_solutions = cell(num_points, 1);
103 % Store cost-optimal solution
104 pareto_cost(1) = fval_cost;
105 pareto_voltage_dev(1) = voltage_dev_at_cost_opt;
106 pareto_solutions(1) = x_cost;
107 % Store voltage-optimal solution
108 pareto_cost(num_points) = cost_at_volt_opt;
109 pareto_voltage_dev(num_points) = fval_volt;
110 pareto_solutions(num_points) = x_volt;
111 % Solve for Pareto-optimal solutions using epsilon constraint method
112 for i = 2:num_points-1
113     epsilon = epsilon_values(i);
114     fprintf('Solving for epsilon = %.6f (%d/%d)\n', epsilon, i, num_points);
115     % Create constraint function with voltage deviation limit
116     nonlin_epsilon = @(x) opt_constraints_with_epsilon(x, nb, ng, nl, gen_buses, G, B, PD, Qd, slack_bus, npc_branch);
117     % Solve with cost as objective and voltage deviation as constraint
118     [x_pareto, fval_pareto, exitflag, ~] = fmincon(objfun_cost, x0, [], [], [], [], lb, ub, nonlin_epsilon, options);
119     if exitflag > 0
120         % Store successful solution
121         pareto_cost(i) = fval_pareto;
122         pareto_voltage_dev(i) = opt_voltage_objective(x_pareto, nb, Vref);
123         pareto_solutions(i) = x_pareto;
124         fprintf('Found solution: Cost = %.4f, Voltage Deviation = %.6f\n', pareto_cost(i), pareto_voltage_dev(i));
125     else
126         fprintf('No solution found for epsilon = %.6f\n', epsilon);
127         % Use previous solution
128         pareto_cost(i) = pareto_cost(i-1);
129         pareto_voltage_dev(i) = pareto_voltage_dev(i-1);
130         pareto_solutions(i) = pareto_solutions(i-1);
131     end
132 end
133 % Filter invalid or identical solutions
134 idx = 1;
135 valid_cost = pareto_cost(idx);
136 valid_volt = pareto_voltage_dev(idx);
137 valid_solutions = {pareto_solutions{idx}};
138 for i = 2:num_points
139     if ~isnan(pareto_cost(i)) && ~isnan(pareto_voltage_dev(i)) && ...
140         (abs(pareto_cost(i) - valid_cost(end)) > 1e-4 || abs(pareto_voltage_dev(i) - valid_volt(end)) > 1e-6)
141         valid_cost = [valid_cost; pareto_cost(i)];
142         valid_volt = [valid_volt; pareto_voltage_dev(i)];
143         valid_solutions = [valid_solutions; pareto_solutions(i)];
144     end
145 end
146 % Display and Visualize Pareto Front
147 % Plot Pareto front
148 figure('Name', 'Pareto Front - OPF Multi-Objective', 'Color', [1 1 1]);
149 scatter(valid_cost, valid_volt, 100, 'filled', 'MarkerFaceColor', [0.3 0.8 0.9], 'MarkerEdgeColor', 'k', 'LineWidth', 1.5);
150 hold on;
151 plot(valid_cost, valid_volt, 'k-', 'LineWidth', 1.2);
152 xlabel('Generation Cost');
153 ylabel('Voltage Deviation');
154 title('Pareto Front: Generation Cost vs. Voltage Deviation');
155 grid on; box on;
156 text(valid_cost(1), valid_volt(1), 'Cost-optimal', 'fontWeight', 'bold');
157 text(valid_cost(end), valid_volt(end), 'Voltage-optimal', 'fontWeight', 'bold');
158 % Extract the solution for detailed analysis (mid-point of Pareto front as an example)
159 mid_idx = ceil(length(valid_cost) / 2);
160 x_selected = valid_solutions{mid_idx};
161 % Extract values from selected solution
162 V_opt = x_selected(1:nb);
163 theta_opt = x_selected(nb+1:2*nb);
164 Pg_opt = x_selected(2*nb+1:2*nb+ng);
165 Qg_opt = x_selected(2*nb+ng+1:end);
166 % Extract weights from the Pareto front
167 extract_weights_from_pareto(valid_cost, valid_volt, valid_solutions);
168 % Display Numerical Results for selected solution
169 fprintf('\nDetailed Results for Pareto Solution:\n');
170 fprintf('Generation Cost: %.4f, Voltage Deviation: %.6f\n', valid_cost(mid_idx), valid_volt(mid_idx));
171 fprintf('\nOptimal Bus Voltages and Angles:\n');
172 for i = 1:nb
173     fprintf('Bus %d: V = %.4f p.u., theta = %.4f rad (%.2f°)\n', ...
174         i, V_opt(i), theta_opt(i), theta_opt(i)*180/pi);
175 end
176 fprintf('\nOptimal Generator Outputs:\n');
177 for i = 1:ng
178     fprintf('Generator at Bus %d: Pg = %.4f p.u. (%.2f MW), Qg = %.4f p.u. (%.2f MVar)\n', ...
179         gen_buses(i), Pg_opt(i), Pg_opt(i)*baseMVA, Qg_opt(i), Qg_opt(i)*baseMVA);
180 end
181 % Enhanced Visual Outputs for Selected Solution
182 figure('Name', 'Selected Pareto Solution - 118 kV Bus', 'Color', [1 1 1]);
183 t = tiledlayout(2, 1, 'Padding', 'compact', 'TileSpacing', 'compact');
184 % Voltage Profile Plot
185 nexttile;
186 hBarVolt = bar(V_opt, 'FaceColor', 'flat', 'EdgeColor', 'k', 'LineWidth', 1.2);
187 % Apply gradient coloring based on voltage levels
188 for k = 1:length(V_opt)
189     if V_opt(k) < 0.95
190         hBarVolt.CData(k,:) = [0.8 0.2 0.2]; % Red tones for low voltages
191     elseif V_opt(k) > 1.05
192         hBarVolt.CData(k,:) = [0.2 0.2 0.8]; % Blue tones for high voltages
193     else
194         hBarVolt.CData(k,:) = [0.2 0.6 0.2]; % Green for acceptable voltage
195     end
196 end
197 grid on; box on;
198 xlabel('Bus Number');
199 ylabel('Voltage (p.u.)');
200 title('Optimal Bus Voltage Profile');

```

```

201 ylim[min(V_opt)-0.05, max(V_opt)+0.05];
202 xticks(1:length(V_opt));
203 % Annotate each bar with its voltage value
204 for k = 1:length(V_opt)
205     text(k, V_opt(k)+0.005, sprintf('%1f', V_opt(k)), ...
206          'HorizontalAlignment', 'center', 'FontSize', 8, 'FontWeight', 'bold');
207 end
208 % Voltage Angle Plot
209 nexttile;
210 hBarAngle = bar(theta_opt*180/pi, 'FaceColor', [0.6 0.4 0.8], 'EdgeColor', 'k', 'LineWidth', 1.2);
211 grid on; box on;
212 xlabel('Bus Number');
213 ylabel('Angle (°)');
214 title('Optimal Bus Voltage Angles');
215 xticks(1:length(theta_opt));
216 % Annotate each angle value (in degrees)
217 for k = 1:length(theta_opt)
218     text(k, (theta_opt(k)*180/pi)+0.5, sprintf('%1f°', theta_opt(k)*180/pi), ...
219          'HorizontalAlignment', 'center', 'FontSize', 8, 'FontWeight', 'bold');
220 end
221 % Add an overall title for the tiled layout
222 title('Selected Pareto-Optimal Solution for IEEE 34-Bus System', 'FontSize', 14, 'FontWeight', 'bold');
223
224 %% Visualize trade-offs across Pareto front
225 % Compare voltage profiles and generator outputs across Pareto front
226 figure('Name', 'Pareto Solutions Comparison', 'Color', [1 1 1]);
227 t1 = tiledlayout(2, 1, 'Padding', 'compact', 'TileSpacing', 'compact');
228 % Select solutions to compare (first, middle, last)
229 compare_idx = [1, mid_idx, length(valid_cost)];
230 solution_names = {'Cost-optimal', 'Mid-point', 'Voltage-optimal'};
231 % Voltage profiles comparison
232 nexttile;
233 hold on;
234 colors = [0.8 0.2 0.2; 0.2 0.6 0.2; 0.2 0.2 0.8]; % Red, Green, Blue
235 markers = {'s', 'o', 'x', 'diamond'};
236 for i = 1:length(compare_idx)
237     id = compare_idx(i);
238     x_sol = valid_solutions(id);
239     V_sol = x_sol(1:nb);
240     plot(1:nb, V_sol, markers(i), 'LineWidth', 2, 'Color', colors(i,:), 'MarkerFaceColor', colors(i,:));
241 end
242 grid on; box on;
243 xlabel('Bus Number');
244 ylabel('Voltage (p.u.)');
245 title('Voltage Profiles Across Pareto Front');
246 xticks(1:nb);
247 legend(solution_names, 'Location', 'best');
248 ylim[min(Vmin)-0.02, max(Vmax)+0.02];
249 % Generator outputs comparison
250 nexttile;
251 gen_data = zeros(nG, length(compare_idx));
252 for i = 1:length(compare_idx)
253     id = compare_idx(i);
254     x_sol = valid_solutions(id);
255     Pg_sol = x_sol(2*nb+1:2*nb+nG);
256     gen_data(:,i) = Pg_sol;
257 end
258 bar2 = bar(gen_data);
259 for i = 1:length(compare_idx)
260     bar2(i).FaceColor = colors(i,:);
261 end
262 grid on; box on;
263 xlabel('Generator Number');
264 ylabel('Active Power (p.u.)');
265 title('Generator Outputs Across Pareto Front');
266 xticks(1:nG);
267 sticklabels(arrayfun(@(x) sprintf('%m W', x), 1:nG, 'UniformOutput', false));
268 legend(solution_names, 'Location', 'best');
269 title(t2, 'Comparison of Different Solutions on the Pareto Front', 'FontSize', 14, 'FontWeight', 'bold');
270
271 %%
272 %% Separate Objective Functions
273 function f = opf_cost_objective(x, nb, nG, gen_buses, a, b, c)
274 % Cost-only objective
275 Pg = x(2*nb+1:2*nb+nG);
276 f = sum(a .* Pg.^2 + b .* Pg + c);
277 end
278 function f = opf_voltage_objective(x, nb, Vref)
279 % Voltage deviation objective
280 V = x(1:nb);
281 f = sum((V - Vref).^2);
282 end
283
284 %% Nonlinear Constraints
285 function [c, ceq] = opf_constraints(x, nb, nG, nI, gen_buses, G, B, Pd, Qd, slack_bus, Smax)
286 % Extract decision variables
287 V = x(1:nb);
288 theta = x(nb+1:2*nb);
289 Pg = x(2*nb+1:2*nb+nG);
290 Qg = x(2*nb+nG+1:2*nb+2*nG);
291 % Bus generator outputs to their buses
292 Pg_bus = zeros(nb, 1);
293 Qg_bus = zeros(nb, 1);
294 for i = 1:nG
295     Pg_bus(gen_buses(i)) = Pg(i);
296     Qg_bus(gen_buses(i)) = Qg(i);
297 end
298 % Power balance equations for each bus
299 Pbalance = zeros(nb, 1);
300 Qbalance = zeros(nb, 1);
301 for i = 1:nb
302     P_in[i] = 0;
303     Q_in[i] = 0;
304     for j = 1:nb
305         angle_diff = theta(i) - theta(j);
306         P_in[i] = P_in[i] + V(i) * V(j) * (G(i,j) * cos(angle_diff) + B(i,j) * sin(angle_diff));
307         Q_in[i] = Q_in[i] + V(i) * V(j) * (B(i,j) * cos(angle_diff) - G(i,j) * sin(angle_diff));
308     end
309     Pbalance(i) = Pg_bus(i) - Pd(i) - P_in[i];
310     Qbalance(i) = Qg_bus(i) - Qd(i) - Q_in[i];
311 end
312 % Line flow constraints
313 line_flow = [];
314 if ~isempty(Smax) && Smax(1) == 999
315     line_flow = compute_lineflows(V, theta, nb, nI, G, B, Smax);
316 end
317 c = line_flow;
318 ceq = [Pbalance; Qbalance];
319
320 %% Constraints with epsilon constraint on voltage deviation
321 function [c, ceq] = opf_constraints_with_epsilon(x, nb, nG, nI, gen_buses, G, B, Pd, Qd, slack_bus, Smax, Vref, epsilon)
322 % Regular constraints
323 [c_reg, ceq] = opf_constraints(x, nb, nG, nI, gen_buses, G, B, Pd, Qd, slack_bus, Smax);

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```

322 % Epsilon constraint on voltage deviation
323 V = n(1:nb);
324 voltage_dev = sum((V - Vref).^2);
325 c_obj = voltage_dev + epsilon;
326 % Combine constraints
327 c = [c; wE; c_obj];
328 end
329 % Compute Line Flows
330 function c = computeLineFlows(V, theta, nb, nl, G, R, Smax)
331 c = [];
332 line_count = 0;
333 for i = 1:nb
334     for j = i+1:nb
335         if abs(d(i,j)) > 1e-6 || abs(R(i,j)) > 1e-6
336             line_count = line_count + 1;
337             line_count = line_count + 1;
338             angle_diff = theta(i) - theta(j);
339             Pij = V(i)^2 * G(i,j) - V(i)*V(j) * (G(i,j)*cos(angle_diff) + B(i,j)*sin(angle_diff));
340             Qij = -V(i)^2 * B(i,j) - V(i)*V(j) * (G(i,j)*sin(angle_diff) - B(i,j)*cos(angle_diff));
341             Sij = sqrt(Pij^2 + Qij^2);
342             c = [c; Sij * Smax(line_count)];
343         end
344     end
345 end
346 end
347 % Extract Weights from Pareto Front
348 function extractWeightsFromPareto(valid_cost, valid_volt, valid_solutions)
349 fprintf('n--- Weights Analysis from Pareto Front ---n');
350 fprintf('Point | Cost Value | Voltage Dev | w1 (Cost) | w2 (Voltage) | w1/w2 Ratio\n');
351 fprintf('-----n');
352 % Normalize the objectives to similar scales for fair comparison
353 max_cost = max(valid_cost);
354 min_cost = min(valid_cost);
355 max_volt = max(valid_volt);
356 min_volt = min(valid_volt);
357 norm_cost = (valid_cost - min_cost) / (max_cost - min_cost);
358 norm_volt = (valid_volt - min_volt) / (max_volt - min_volt);
359 % Calculate weights for each point based on the local gradient
360 for i = 1:length(valid_cost)
361     if i == 1
362         % First point - use forward difference
363         dc = norm_cost(i+1) - norm_cost(i);
364         dv = norm_volt(i+1) - norm_volt(i);
365     elseif i == length(valid_cost)
366         % Last point - use backward difference
367         dc = norm_cost(i) - norm_cost(i-1);
368         dv = norm_volt(i) - norm_volt(i-1);
369     else
370         % Interior points - use central difference
371         dc = norm_cost(i+1) - norm_cost(i-1);
372         dv = norm_volt(i+1) - norm_volt(i-1);
373     end
374     % Calculate gradient (slope of tangent line)
375     if abs(dc) < 1e-10
376         w1 = 0;
377         w2 = 1;
378     elseif abs(dv) < 1e-10
379         w1 = 1;
380         w2 = 0;
381     else
382         % Gradient of the Pareto front at this point
383         gradient = -dv/dc;
384         % Convert gradient to weights (w1 for cost, w2 for voltage)
385         w1 = 1 / (1 + gradient);
386         w2 = gradient / (1 + gradient);
387     end
388     % Normalize weights to sum to 1
389     sum_w = w1 + w2;
390     w1 = w1 / sum_w;
391     w2 = w2 / sum_w;
392     if w2 < 1e-10
393         ratio = "inf";
394     else
395         ratio = w1/w2;
396     end
397     % Print results
398     fprintf('Idx | X10.4f | X10.4f | X10.4f | X12.4f | X10b\n', ...
399           i, valid_cost(i), valid_volt(i), w1, w2, num2str(ratio));
400 end
401 [~, balanced_idx] = min(abs(arrayfun(@(i) (norm_cost(i) - norm_volt(i)), 1:length(valid_cost)))));
402 normalized_sum = norm_cost + norm_volt;
403 [~, min_sum_idx] = min(normalized_sum);
404 fprintf('Recommended Weight Sets:\n');
405 fprintf('1. Not balanced weights: w1 = 5.4f, w2 = 5.4f (point %d)\n', ...
406       1/(1+norm_volt(balanced_idx)/norm_cost(balanced_idx)), ...
407       1/(1+norm_cost(balanced_idx)/norm_volt(balanced_idx)), balanced_idx);
408 mid_idx = ceil(length(valid_cost) / 2);
409 if mid_idx == balanced_idx
410     fprintf('2. Middle Pareto point: w1 = 5.4f, w2 = 5.4f (point %d) (same as balanced)\n', ...
411           1/(1+norm_volt(mid_idx)/norm_cost(mid_idx)), ...
412           1/(1+norm_cost(mid_idx)/norm_volt(mid_idx)), mid_idx);
413 else
414     fprintf('3. Middle Pareto point: w1 = 5.4f, w2 = 5.4f (point %d)\n', ...
415           1/(1+norm_volt(mid_idx)/norm_cost(mid_idx)), ...
416           1/(1+norm_cost(mid_idx)/norm_volt(mid_idx)), mid_idx);
417 end
418 if min_sum_idx == balanced_idx || min_sum_idx == mid_idx
419     else
420         fprintf('3. Minimum normalized objective sum: w1 = 5.4f, w2 = 5.4f (point %d)\n', ...
421               1/(1+norm_volt(min_sum_idx)/norm_cost(min_sum_idx)), ...
422               1/(1+norm_cost(min_sum_idx)/norm_volt(min_sum_idx)), min_sum_idx);
423     end
424 figure('name', 'Weight distribution Along Pareto front', 'Color', [1 1 1]);
425 w1_values = zeros(length(valid_cost), 1);
426 w2_values = zeros(length(valid_cost), 1);
427 for i = 1:length(valid_cost)
428     if i == 1
429         dc = norm_cost(i+1) - norm_cost(i);
430         dv = norm_volt(i+1) - norm_volt(i);
431     elseif i == length(valid_cost)
432         dc = norm_cost(i) - norm_cost(i-1);
433         dv = norm_volt(i) - norm_volt(i-1);
434     else
435         dc = norm_cost(i+1) - norm_cost(i-1);
436         dv = norm_volt(i+1) - norm_volt(i-1);
437     end
438     % Calculate weights
439     if abs(dc) < 1e-10
440         w1_values(i) = 0;
441         w2_values(i) = 1;
442     elseif abs(dv) < 1e-10
443         w1_values(i) = 1;
444         w2_values(i) = 0;
445     else
446         gradient = -dv/dc;
447         w1_values(i) = 1 / (1 + gradient);
448         w2_values(i) = gradient / (1 + gradient);
449     end

```



```
449 % Normalize
450 sum_w = w1_values(i) + w2_values(i);
451 w1_values(i) = w1_values(i) / sum_w;
452 w2_values(i) = w2_values(i) / sum_w;
453 end
454 end
455 % Plotting weights
456 plot(1:length(valid_cost), w1_values, 'r-o', 'linewidth', 2, 'MarkerFaceColor', 'r');
457 hold on;
458 plot(1:length(valid_cost), w2_values, 'b-x', 'linewidth', 2, 'MarkerFaceColor', 'b');
459 plot(balanced_idx, balanced_idx, [0 1], 'k-', 'linewidth', 1.5);
460 plot([mid_idx mid_idx], [0 1], 'g-', 'linewidth', 1.5);
461 grid on; box on;
462 xlabel('Point Index on Pareto Front');
463 ylabel('Weight Value');
464 title('Weight Distribution Along Pareto Front');
465 legend('w1 (Cost)', 'w2 (Voltage)', 'Balanced Point', 'Middle Point', 'location', 'best');
466 ylim([0 1]);
467
468 end
```

branch\_data.xlsx

	From_Bus	To_Bus	G_pu	B_pu	S_max_MVA	
2		1	2	4.999131601	-15.26308652	0
3		1	5	1.025897455	-4.234983682	0
4		2	3	1.135019192	-4.781863152	0
5		2	4	1.686033151	-5.115838326	0
6		2	5	1.701139667	-5.193927398	0
7		3	4	1.98597571	-5.068816978	0
8		4	5	6.840980661	-21.57855398	0
9		4	7	0	-4.781943382	0
10		4	9	0	-1.797979072	0
11		5	6	0	-3.967939052	0
12		6	11	1.955028563	-4.094074344	0
13		6	12	1.52596744	-3.175963965	0
14		6	13	3.098927404	-6.102755448	0
15		7	8	0	-5.676979847	0
16		7	9	0	-9.09008272	0
17		9	10	3.902049552	-10.36539413	0
18		9	14	1.424005487	-3.029050457	0
19		10	11	1.880884754	-4.402943749	0
20		12	13	2.489024587	-2.251974626	0
21		13	14	1.136994158	-2.314963475	0

bus\_data.xlsx

1	Bus	P_Load_MW	Q_Load_MVAr	V_ref_pu
2	1	0	0	1.06
3	2	21.7	12.7	1.045
4	3	94.2	19	1.01
5	4	47.8	-3.9	1.019
6	5	7.6	1.6	1.02
7	6	11.2	7.5	1.07
8	7	0	0	1.062
9	8	0	0	1.09
10	9	29.5	16.6	1.056
11	10	9	5.8	1.051
12	11	3.5	1.8	1.057
13	12	6.1	1.6	1.055
14	13	13.5	5.8	1.05
15	14	14.9	5	1.036

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