

# TWO DIMENSIONAL FIR FILTERS

## CONTENTS

1. FIR FILTERS
2. IMPLEMENTATION OF FIR FILTERS
3. DESIGN OF FIR FILTERS
  - WINDOWING METHOD
  - LEAST SQUARES METHOD
  - TRANSFORMATION METHOD

## REFERENCES:

D.E. Dudgeon and R.M. Mersereau, **MULTIDIMENSIONAL DIGITAL SIGNAL PROCESSING**. ENGLEWOOD CLIFFS, NJ: PRENTICE-HALL, INC., 1984.

## 1. FIR FILTERS

- An FIR (finite impulse response) or nonrecursive filter is one whose impulse response is of finite duration. The impulse response is always absolutely summable and the FIR filters are always stable.
- IIR filters have infinite impulse response and are usually implemented as a multidimensional difference equation of finite order. They may or may not be stable but may be less complex to realize than equivalent FIR filters. Design is quite different from 1-D IIR filters.

A **zero-phase FIR filter** satisfies:

$$H(\omega_1, \omega_2) = H^*(\omega_1, \omega_2) \Leftrightarrow h(n_1, n_2) = h^*(n_1, n_2). \quad (1)$$

i.e the **frequency and impulse responses are real**. Linear-phase filters are readily obtained from a zero-phase FIR filter by inserting appropriate number of delays.

## 2. IMPLEMENTATION OF FIR FILTERS

### 2.1 Direct Convolution

Since the impulse response of a FIR filter is of **finite extent**, its output can be computed with the convolution sum:

$$y(n_1, n_2) = \sum_{n_1=0}^{N_1-1} \sum_{n_2=0}^{N_2-1} h(k_1, k_2) x(n_1 - k_1, n_2 - k_2). \quad (2-1)$$

Due to the **symmetry** of the impulse response in the zero-phase filter, the number of multiplications and additions can be **approximately halved**.

### 2.2 Discrete Fourier Transform Implementation of FIR Filters

Let  $w(n_1, n_2)$  be the **linear convolution** of  $h(n_1, n_2)$  and  $x(n_1, n_2)$ :

$$w(n_1, n_2) = x(n_1, n_2) ** h(n_1, n_2). \quad (2-1)$$

Taking Fourier transforms of both sides:

$$W(\omega_1, \omega_2) = H(\omega_1, \omega_2)X(\omega_1, \omega_2), \quad (2-2)$$

and **sampling**  $\omega_1$  and  $\omega_2$  respectively at  $\frac{2\pi k_1}{N_1}$  and  $\frac{2\pi k_2}{N_2}$  gives:

$$W(k_1, k_2) = H(k_1, k_2)X(k_1, k_2). \quad (2-3)$$

$y(n_1, n_2)$ , the inverse DFT of  $W$ , will then be the **circular convolution** of  $h(n_1, n_2)$  and  $x(n_1, n_2)$ . If  $N_1$  and  $N_2$  are chosen to be sufficiently large,  $y(n_1, n_2) = w(n_1, n_2)$ .

Discrete Fourier transform implementation of FIR, using the fast Fourier transform (FFT), is very **efficient for high order** filters but it **requires lot of storage**. Convolution sum has high arithmetic complexity but moderate storage. A compromise is to use *block convolution* such as the *overlap save and overlap add methods*.

### 3. Design of FIR Filters

#### 3.1 Windowing Methods

Let  $i(n_1, n_2)$  and  $I(\omega_1, \omega_2)$  be the **impulse** and **frequency** responses for the ideal filter, respectively. Similarly, let  $h(n_1, n_2)$  and  $H(\omega_1, \omega_2)$  be the impulse and frequency responses of the filter to be designed.

- In the windowing methods,  $h(n_1, n_2)$  is obtained by multiplying  $i(n_1, n_2)$  by a finite length window function  $w(n_1, n_2)$  of finite support  $R$ .

$$h(n_1, n_2) = i(n_1, n_2)w(n_1, n_2). \quad (3-1-1)$$

$H(\omega_1, \omega_2)$  is obtained by a frequency-domain convolution of  $I(\omega_1, \omega_2)$  with  $W(\omega_1, \omega_2)$ :

$$H(\omega_1, \omega_2) = \frac{1}{(2\pi)^2} \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} I(\Omega_1, \Omega_2) W(\omega_1 - \Omega_1, \Omega_2 - \omega_2) d\Omega_1 d\Omega_2. \quad (3-1-2)$$

In many filter design problems, the **desired filter behavior is specified through  $I(\omega_1, \omega_2)$**  rather than  $i(n_1, n_2)$ . we must either compute  $i(n_1, n_2)$  analytically or approximate it by sampling  $I(\omega_1, \omega_2)$  densely over  $(\omega_1, \omega_2)$  and then performing an IDFT. To minimize aliasing error, the length of the IDFT should be several times larger than the extent of R.

**For zero-phase filter**, the **window** should also be **zero-phase**. The 2-D window is usually generated from 1-D windows as follows

$$w_R(n_1, n_2) = w_1(n_1)w_2(n_2). \quad (3-1-3a)$$

$$w_C(n_1, n_2) = w(\sqrt{n_1^2 + n_2^2}). \quad (3-1-3b)$$

(3-1-3a) has a **rectangular region of support**. (3-1-3b) has nearly **circular region of support**.

The Fourier transform of the rectangular window is:

$$W_R(\omega_1, \omega_2) = W_1(\omega_1)W_2(\omega_2). \quad (3-1-4)$$

The Fourier transform of  $w_C(n_1, n_2)$  resembles, but differs in detail from, a circularly rotated version of the 1-D Fourier transform of  $w(t)$ .

■ Common windows are rectangular, Hanning, and Kaiser windows.

### Design Example

Design an (11x11)-point FIR with ideal filter response:

$$I(\omega_1, \omega_2) = \begin{cases} 1, & \omega_1^2 + \omega_2^2 \leq (0.4\pi)^2 \\ 0, & \text{otherwise, } -\pi \leq \omega_1, \omega_2 \leq \pi \end{cases}. \quad (3-1-5)$$

For zero-phase filter, the region of support is:

$$R = \{(n_1, n_2) : -5 \leq n_1, n_2 \leq 5\}. \quad (3-1-6)$$

The ideal impulse response  $i(n_1, n_2)$ , is computed by taking the inverse Fourier transform of  $I(\omega_1, \omega_2)$ :

$$i(n_1, n_2) = \frac{0.2J_1(0.4\pi\sqrt{n_1^2 + n_2^2})}{\sqrt{n_1^2 + n_2^2}}. \quad (3-1-7)$$

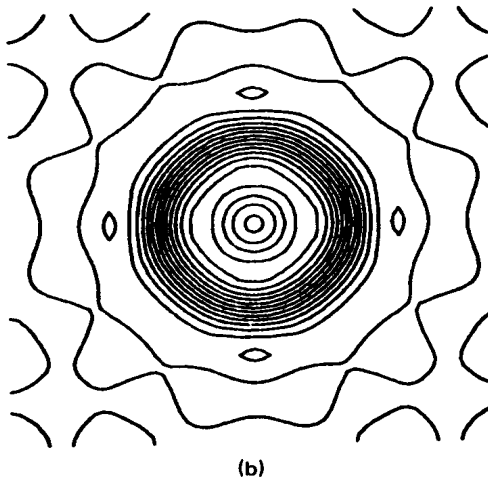
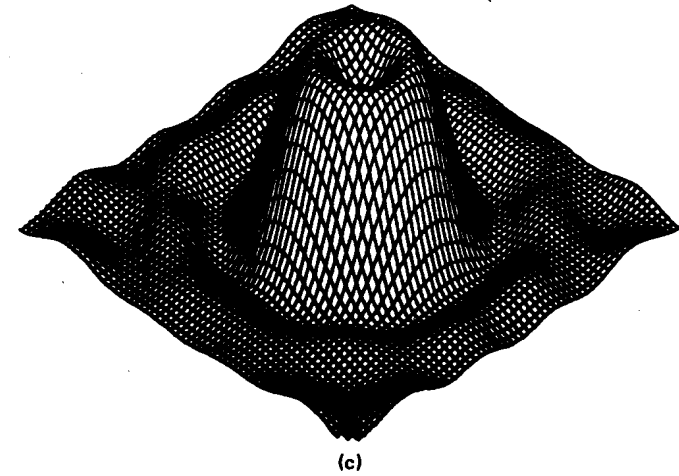
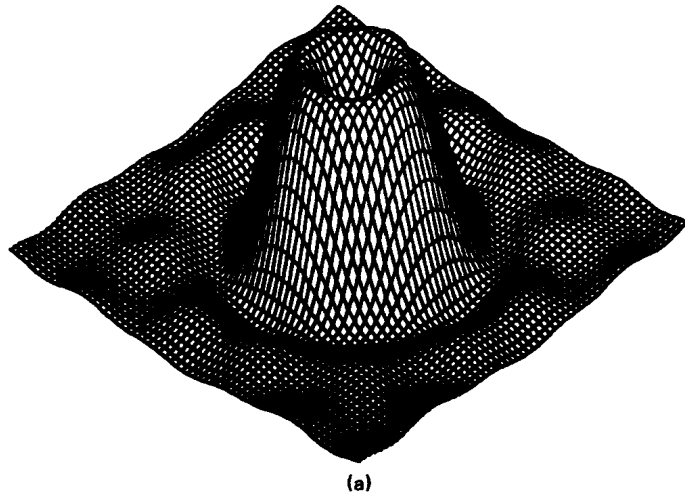
where  $J_1(x)$  is the Bessel function of the first kind of order 1.

Using Kaiser window, the two windows are:

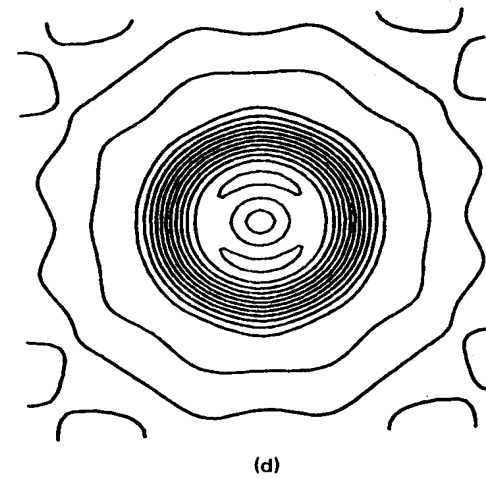
$$w_R(n_1, n_2) = \begin{cases} \frac{I_0[\alpha\sqrt{1-(n_1/5)^2}]I_0[\alpha\sqrt{1-(n_2/5)^2}]}{I_0^2[\alpha]}, & |n_1| \leq 5, |n_2| \leq 5 \\ 0 & \text{otherwise} \end{cases} \quad (3-1-8)$$

$$w_C(n_1, n_2) = \begin{cases} \frac{I_0[\alpha\sqrt{1-(n_1^2 + n_2^2)/25}]}{I_0^2[\alpha]}, & n_1^2 + n_2^2 \leq 25. \\ 0 & \text{otherwise} \end{cases} \quad (3-1-9)$$





**Figure 3.4** Frequency responses of two  $11 \times 11$  FIR lowpass filters designed using windows. (a) Perspective plot of a design based on an outer product window. (b) Contour plot. (c) Perspective plot of a design based on a rotated window. (d) Contour plot. The contours are shown for values of  $H$  between  $-0.1$  and  $1.1$  in increments of  $0.1$ . (Courtesy of Russell M. Mersereau, from *Two-Dimensional Digital Signal Processing I*, Thomas S. Huang, ed., *Topics in Applied Physics*, Vol. 42, © 1981 Springer-Verlag.)



**Figure 3.4** (Continued)

Following the approach of Kaiser in 1-D case, a formula for the filter order  $N$  in terms of its specification  $\delta_p, \delta_s$  and  $\Delta\omega = \omega_s - \omega_p$  can be experimentally developed:

$$N_R \approx \frac{-20 \log_{10} \sqrt{\delta_p \delta_s} - 8}{2.10 \cdot \Delta\omega}. \quad (3-1-10)$$

$$N_C \approx \frac{-20 \log_{10} \sqrt{\delta_p \delta_s} - 7}{2.18 \cdot \Delta\omega}. \quad (3-1-11)$$

The filter order is approximately the same.

The window parameter  $\alpha$  can be determined from the desired attenuation of the filter as follows

$$ATT = -20 \log_{10} \sqrt{\delta_p \delta_s}. \quad (3-1-12)$$

For the **outer product windows**,  $\alpha$  has been **experimentally determined** to be

$$\alpha \approx \begin{cases} 0.42(ATT - 19.3)^{0.4} + 0.089(ATT - 19.3), & 20 < ATT < 60 \\ 0, & ATT < 20 \end{cases} \quad (3-1-13)$$

For the **rotated window**,  $\alpha$  is approximately given by:

$$\alpha \approx \begin{cases} 0.56(ATT - 20.2)^{0.4} + 0.083(ATT - 20.2), & 20 < ATT < 60 \\ 0, & ATT < 20 \end{cases} \quad (3-1-14)$$

### 3.2 Optimal least squares FIR Filter Design

Let 
$$E(\omega_1, \omega_2) = H(\omega_1, \omega_2) - I(\omega_1, \omega_2) \quad (3-2-1)$$

be the **error function** in the filter approximation. One approach to design the filter is to choose the coefficients of the filter to minimize some function of this error, such as its  $L_p$  **norm**:

$$E_p = \sqrt[p]{\frac{1}{4\pi^2} \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} |E(\omega_1, \omega_2)|^p d\omega_1 d\omega_2} . \quad (3-2-2)$$

Filters designed using different error criteria can be quite different.

The frequency response of an FIR filter with support  $R$  is given by:

$$\begin{aligned} H(\omega_1, \omega_2) &= \sum_{(n_1, n_2) \in R} h(n_1, n_2) \exp(-jn_1\omega_1 - jn_2\omega_2) \\ &= \sum_{i=1}^F a(i) \phi_i(\omega_1, \omega_2) . \end{aligned} \quad (3-2-3)$$

The functions  $\{\phi_i(\omega_1, \omega_2)\}$  are called the **basis functions** of the approximation. For the **zero-phase filter**,

$$\phi_i(\omega_1, \omega_2) = \begin{cases} 2 \cos(n_1 \omega_1 + n_2 \omega_2) & (n_1, n_2) \neq (0, 0) \\ 1 & (n_1, n_2) = (0, 0) \end{cases} \quad (3-2-4)$$

### 3.2.1 Least-Squares Design

The function to be minimized is:

$$E_2 = \frac{1}{4\pi^2} \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} |E(\omega_1, \omega_2)|^2 d\omega_1 d\omega_2 \quad (3-2-5)$$

Substituting (3-2-3) into (3-2-5), one gets

$$E_2 = \frac{1}{4\pi^2} \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} \left| \sum_{i=1}^F a(i) \phi_i(\omega_1, \omega_2) - I(\omega_1, \omega_2) \right|^2 d\omega_1 d\omega_2 \quad (3-2-6)$$

Differentiating (3-20) wrt to  $a(i)$  and setting the derivatives to 0 gives the set of  $F$  linear equations:

$$\sum_{i=1}^F a(i) \phi_{ik} = I_k, k = 1, 2, \dots, F. \quad (3-2-7)$$

where  $\phi_{ik} = \frac{1}{4\pi^2} \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} \phi_i(\omega_1, \omega_2) \phi_k(\omega_1, \omega_2) d\omega_1 d\omega_2$  and (3-2-8)

$$I_k = \frac{1}{4\pi^2} \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} I(\omega_1, \omega_2) \phi_k(\omega_1, \omega_2) d\omega_1 d\omega_2. \quad (3-2-9)$$

If  $\{\phi_i(\omega_1, \omega_2)\}$ 's are orthogonal, the solution is simply:  $a(i) = I_i / \phi_{ii}$ . Filter designed using least squares may not be satisfactory due to large passband and stopband ripples. The integrals (3-2-8) and (3-2-9) may also be difficult to evaluate and it can be approximated by the following summation:

$$E_2 = \sum_m W_m [H(\omega_{1m}, \omega_{2m}) - I(\omega_{1m}, \omega_{2m})] \quad (3-2-10)$$

$\omega_{1m}, \omega_{2m}$  are called the constraint frequencies.

- Finding the coefficients  $a(i)$  that minimize  $E_2$  again involves the solution of a systems of linear equations in  $F$  unknowns.

Although the design of filters to minimize an  $L_p$  error norm other than  $p=2$  can be approached similarly, the equations that result are not linear and their solutions are not simple. General optimization techniques will be required.

### **3.2.2 Design of Zero-Phase Equiripple FIR Filters**

In the 1-D case, the **equiripple solution** can be proved to be unique and there are no numerical difficulties to limit the filter order, and the algorithm (the **Park-McClellan algorithm**) **converges rapidly**.

- For higher-dimensional cases, due primarily to the absence of a factorization theorem, the algorithms are slower to converge, more difficult to understand, and somewhat limited in their capabilities.
- An approach is to design the filters by minimizing the  $L_\infty$  norm. Very good approximation of equiripple filters with high order can be designed using nonlinear optimization, **weighted least squares (WLS)**, and more recently **semidefinite programming (SDP)**.



### 3.3 FIR Filter Design Using McClellan Transformation

The idea is to convert a 1-D zero-phase FIR filter into a multidimensional one through a substitution of variables. It is attractive for a number of reasons:

1. The designs are easy to perform;
2. 1-D FIR filter design methods are well understood;
3. using an optimal 1-D filters, it might be possible to design optimal MD filters; and
4. efficient implementation are available.

For a zero phase filter, we can write:

$$H(\omega) = \sum_{n=0}^N a(n) \cos(n\omega) = \sum_{n=0}^N a(n) T_n[\cos(\omega)], \quad (3-3-1)$$

where  $T_n$  is the n-th Chebyshev polynomial.

If we make the substitution:

$$F(\omega_1, \omega_2) \rightarrow \cos \omega, \quad (3-3-2)$$

we obtain the following 2-D frequency response:

$$H(\omega_1, \omega_2) = \sum_{n=0}^N a(n) T_n[F(\omega_1, \omega_2)]. \quad (3-3-3)$$

An M-dimensional frequency response results if an M-dimensional transformation function is used.

The simplest choice is the frequency response of a zero-phase (3x3 filter):

$$F(\omega_1, \omega_2) = A + B \cos \omega_1 + C \cos \omega_2 + D \cos(\omega_1 - \omega_2) + E \cos(\omega_1 + \omega_2). \quad (3-3-4)$$

where constants A, B, C, and D are free parameters.

## Design Example: Circular Symmetric 2D Filters

Consider the transformation with  $A = -0.5$ ,  $B = C = 0.5$ ,  $D = E = 0.25$ . This is the original transformation proposed by McClellan.

The 等势的 isopotentials close to the center are nearly circular and those towards the outside look like squares. The transformation function is:

$$F(\omega_1, \omega_2) = \frac{1}{2}(-1 + \cos \omega_1 + \cos \omega_2 + \cos \omega_1 \cos \omega_2). \quad (3-3-5)$$

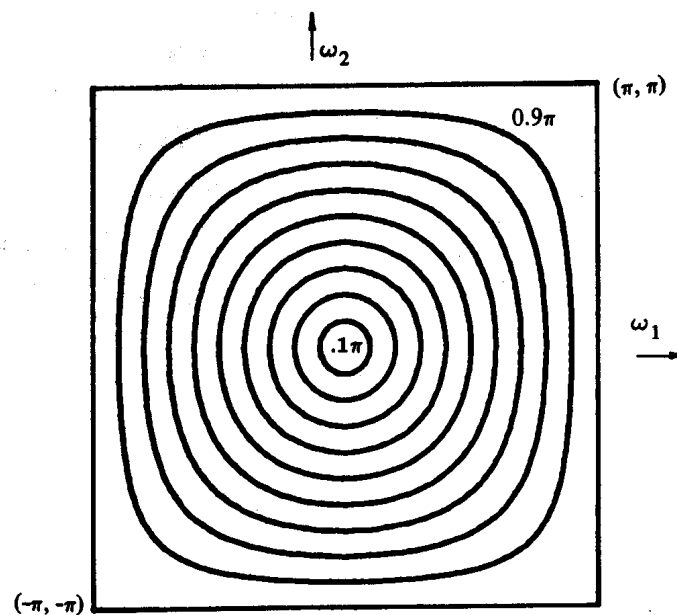
For  $\omega_2 = 0$ , we have

$$F(\omega_1, 0) = \cos \omega_1. \quad (3-3-6)$$

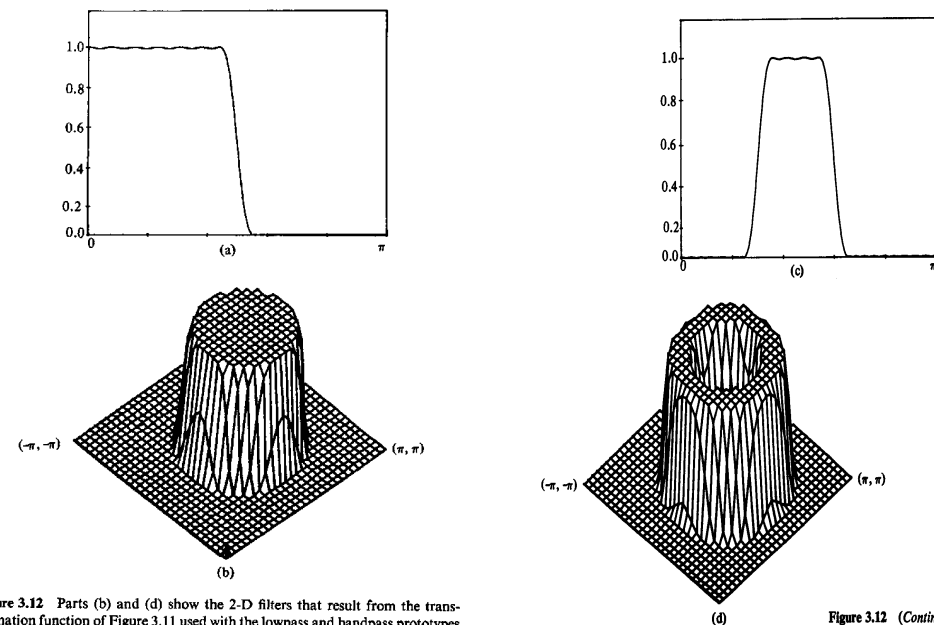
Thus,

$$H(\omega_1, 0) = H(\omega_1). \quad (3-3-7)$$

For this transformation function, the prototype frequency response becomes a cross-sectional slice of the 2-D frequency response. A 1-D lowpass filter thus produces an 2-D lowpass filter, and a 1-D bandpass filter produces an 2-D ring bandpass filter.



**Figure 3.11** Contours of constant value for the transformation function of first order with  $A = -\frac{1}{2}$ ,  $B = C = \frac{1}{2}$ ,  $D = E = \frac{1}{4}$ . The contours are shown for values of  $\omega$  in increments of  $0.1\pi$ . (Courtesy of Russell M. Mersereau, from *Two-Dimensional Digital Signal Processing I*, Thomas S. Huang, ed., *Topics in Applied Physics*, Vol. 42, © 1981 Springer-Verlag.)



**Figure 3.12** Parts (b) and (d) show the 2-D filters that result from the transformation function of Figure 3.11 used with the lowpass and bandpass prototypes shown in parts (a) and (c). (Courtesy of Russell M. Mersereau, from *Two-Dimensional Digital Signal Processing I*, Thomas S. Huang, ed., *Topics in Applied Physics*, Vol. 42, © 1981 Springer-Verlag.)

**Figure 3.12 (Continued)**

Furthermore, the height of the passband and stopband ripples in the prototype become the ripple heights in the final design.