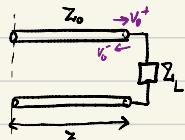


Feb 3

## Power flow in lossless transmission line



$$P = \operatorname{Re} \left\{ V I^* \right\}$$

$\tilde{\cong}$  conjugate

$$\begin{aligned} P &= \operatorname{Re} \left\{ (V_0^+ e^{j\beta z} + V_0^- e^{-j\beta z}) (I_0^+ e^{j\beta z} - I_0^- e^{-j\beta z})^* \right\} \\ &= \operatorname{Re} \left\{ (V_0^+ e^{j\beta z} + V_0^- e^{-j\beta z}) \left( \frac{V_0^+}{Z_0} e^{-j\beta z} - \frac{V_0^-}{Z_0} e^{+j\beta z} \right)^* \right\} \\ &= \operatorname{Re} \left\{ \frac{|V_0|^2}{Z_0} - \frac{|V_0|^2}{Z_0} + \frac{V_0^+ V_0^-}{Z_0} e^{-j2\beta z} - \frac{V_0^+ V_0^-}{Z_0} e^{+j2\beta z} \right\} \quad \text{Z}_0 \text{ is real for Lossless lines} \\ &= \operatorname{Re} \left\{ \frac{|V_0|^2}{Z_0} (1 - 1)^2 + \frac{|V_0|^2}{Z_0} (e^{+j2\beta z} - e^{-j2\beta z}) \right\} \\ &= \operatorname{Re} \left\{ \frac{|V_0|^2}{Z_0} (1 - 1)^2 + \frac{|V_0|^2}{Z_0} (2 j \sin 2\beta z) \right\} \end{aligned}$$

Thus

$$\frac{1}{2} P = |V_0|^2 (1 - 1)^2 \frac{1}{Z_0} = P^+ - P^- \quad P^+ = \frac{|V_0|^2}{Z_0}, \quad P^- = \frac{|V_0|^2}{Z_0}$$

## Lossy line (Polar 2.7)

$$\hookrightarrow \text{Lossy: } \gamma = \sqrt{(j\omega L + R)(j\omega C + G)}, \quad Z = \sqrt{j\omega L + R} \quad j\omega C + G$$

$$Z = \sqrt{\frac{L}{C}} \cdot \sqrt{\frac{1 + R/j\omega L}{1 + G/j\omega C}}$$

complex

Notes ① wave attenuates as it travels

② phase shift between V and I

$$V(z) = V_0^+ e^{-j\gamma z} + V_0^- e^{+j\gamma z}$$

$$I(z) = \frac{V_0^+}{Z_0} e^{-j\gamma z} - \frac{V_0^-}{Z_0} e^{+j\gamma z}$$

$$\text{low-loss line: } \gamma = \frac{1}{2} \{ R \sqrt{\frac{L}{C}} + G \sqrt{\frac{C}{L}} \}$$

$R \ll \omega L, G \ll \omega C$

$$\beta = \omega \sqrt{\frac{L}{C}}$$

The loss often described as quality factor: ②

$$Q = \omega \frac{\text{average energy storage}}{\text{power loss}} = \omega \frac{+P/v_g}{-dP/dz} \quad \begin{matrix} \text{v}_g: \text{group velocity} \\ \text{energy propagation velocity} \end{matrix}$$

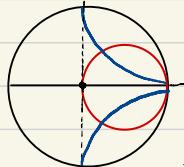
$$V(z) = V_0 e^{-\gamma z} \cdot e^{-j\beta z}$$

$$I(z) = I_0 e^{-\gamma z} e^{-j\beta z}$$

$$P = \frac{|V_0|^2}{Z_0} e^{-2\gamma z} \rightsquigarrow \frac{\partial P}{\partial z} = -2\gamma P$$

$$Q = \omega \frac{P/v_g}{2\alpha P} = \frac{\omega}{2\alpha v_g} \quad \begin{matrix} \text{dispersionless case} \\ v_p = v_g = \frac{C}{\beta} \Rightarrow Q = \frac{\beta}{2\alpha} \end{matrix}$$

Smith chart  $\rightarrow$  graphic aid for solving transmission equation



$\Rightarrow$  Polar plot of voltage reflection coefficient

$$\Gamma = |\Gamma| e^{j\theta} \rightarrow \text{for passive system } |\Gamma| \leq 1$$

$\tilde{\cong}$  complex

$\Rightarrow$  Normalized to impedance  $Z_0$

$$\hookrightarrow \text{Load } Z_L \Rightarrow Z_L = \frac{Z_0}{Z_0 + \Gamma}$$

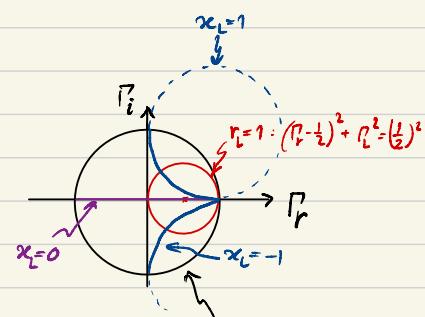
$$\Gamma = \frac{Z_L - 1}{Z_L + 1} = |\Gamma| e^{j\theta}$$

$$Z_L = \frac{1 + |\Gamma| e^{j\theta}}{1 - |\Gamma| e^{j\theta}}$$

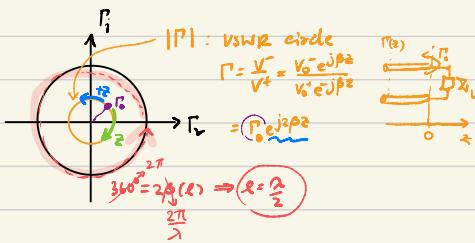
$$Z_L = \Gamma_L + jx_L = \frac{(1 + \beta_r) + j\beta_i}{(1 - \beta_r) - j\beta_i}$$

$$\beta_r = \frac{1 + \beta_r^2 - \beta_i^2}{(1 - \beta_r)^2 + \beta_i^2} \Rightarrow (\beta_r - \frac{x_L}{1 + \beta_r})^2 + \beta_i^2 = \left(\frac{1}{1 + \beta_r}\right)^2$$

$$\beta_i = \frac{2\beta_i}{(1 + \beta_r)^2 + \beta_i^2} \Rightarrow (\beta_i - 1)^2 + (\beta_i - \frac{x_L}{\beta_i})^2 = \left(\frac{1}{\beta_i}\right)^2$$



Feb 5



### Comments on Smith chart

① As move along the line away from the load, |Γ| varies

→ magnitude constant; phase will decrease (toward gen)

② As frequency increases, phase of |Γ| tends to decrease but the movement is complex

③ Normalized impedance

$$Z = \frac{P-1}{P+1}$$

• example:  $Z_L = 40+j70 \Omega$  terminates  $100 \Omega$  transmission line ( $l = 0.3 \lambda$ )

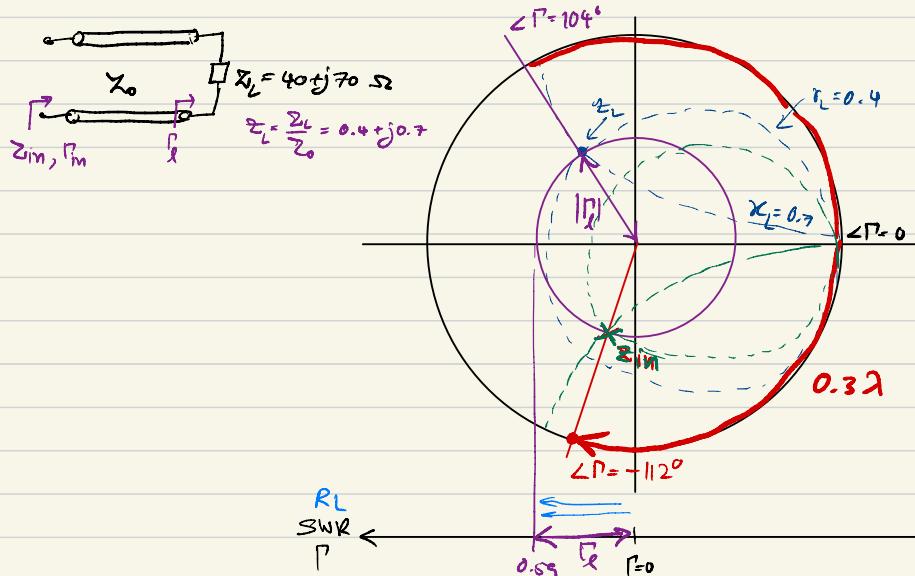
Find ① reflection coefficient at the load →  $\Gamma = 0.59 e^{j104^\circ}$

②  $\Gamma$  at the input of the line →  $\Gamma = 0.59 e^{-j112^\circ}$

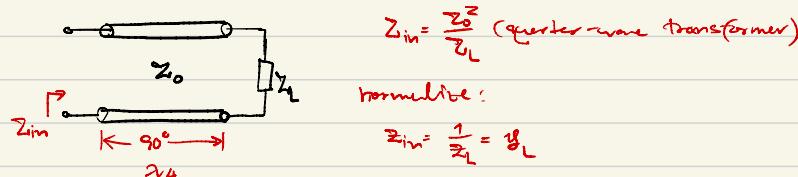
③  $Z_{in} \rightarrow z_{in} = 100(0.365 - j0.611) \Omega$

④ VSWR → 3.87

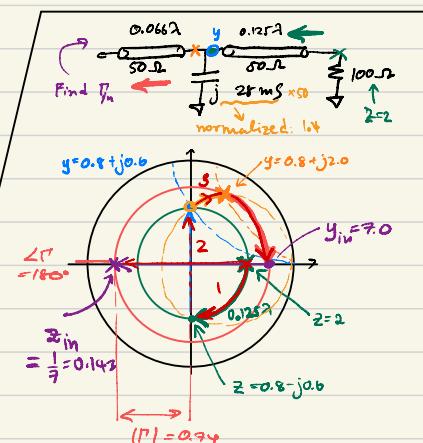
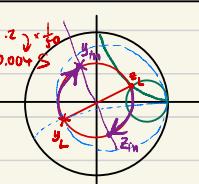
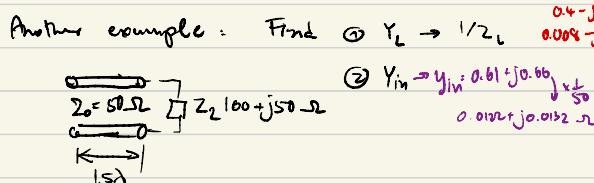
⑤ Return loss → 4.6 dB



What would happen if I terminate  $Z_L$  with  $90^\circ$  transmission line



Rotate  $180^\circ$  of original  $Z_L$ , you can set  $y_L$  on the impedance Smith chart.



$$\therefore |\Gamma|_{in} = 0.74 e^{j180^\circ} = -0.74$$