

Concept of Stress Lecture 11

Engineering Mechanics - ME102 Rishi Raj

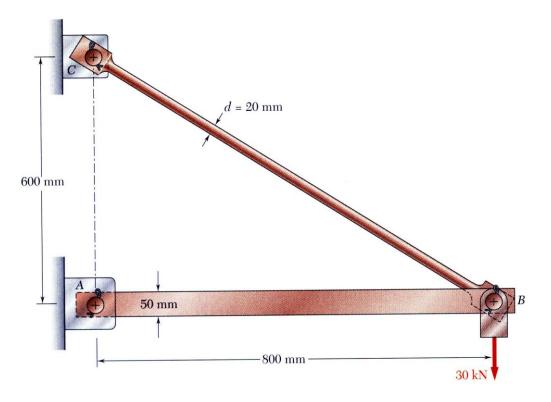
Concept of Stress



- The main objective of the study of mechanics of materials is to provide the future engineer with the means of analyzing and designing various machines and load bearing structures.
- Both the analysis and design of a given structure involve the determination of *stresses* and deformations. This chapter is devoted to the concept of stress.

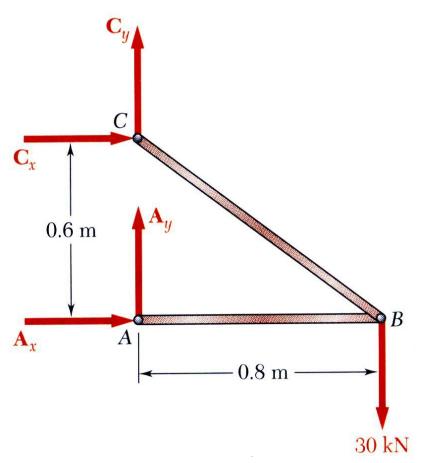
Review of Statics





- The structure is designed to support a 30 kN load
- The structure consists of a boom and rod joined by pins (zero moment connections) at the junctions and supports
- Perform a static analysis to determine the internal force in each structural member and the reaction forces at the supports

Structure Free-Body Diagram



- Structure is detached from supports and the loads and reaction forces are indicated
- Conditions for static equilibrium:

$$\sum M_{C} = 0 = A_{x}(0.6 \,\mathrm{m}) - (30 \,\mathrm{kN})(0.8 \,\mathrm{m})$$

$$A_{x} = 40 \,\mathrm{kN}$$

$$\sum F_{x} = 0 = A_{x} + C_{x}$$

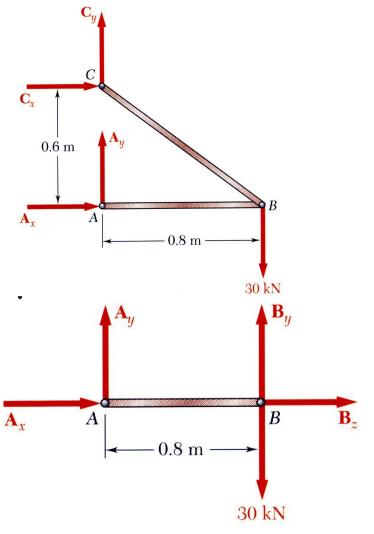
$$C_{x} = -A_{x} = -40 \,\mathrm{kN}$$

$$\sum F_{y} = 0 = A_{y} + C_{y} - 30 \,\mathrm{kN} = 0$$

$$A_{y} + C_{y} = 30 \,\mathrm{kN}$$

 A_{v} and C_{v} can not be determined from these equations

Component Free-Body Diagram



- In addition to the complete structure, each rechno component must satisfy the conditions for static equilibrium
- Consider a free-body diagram for the boom:

$$\sum M_B = 0 = -A_y(0.8 \,\mathrm{m})$$

$$A_{y} = 0$$

substitute into the structure equilibrium equation

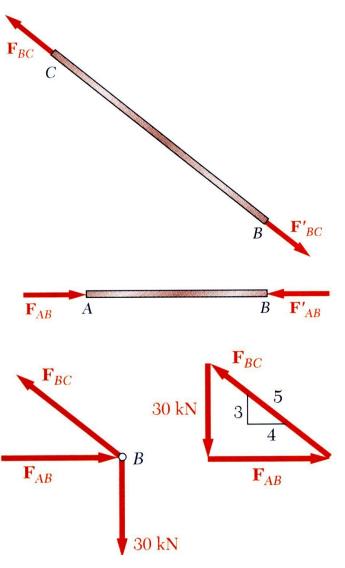
$$C_y = 30 \text{kN}$$

Results:

$$A = 40 \,\mathrm{kN} \rightarrow C_x = 40 \,\mathrm{kN} \leftarrow C_y = 30 \,\mathrm{kN} \uparrow$$

Reaction forces are directed along boom and rod

Method of Joints



- The boom and rod are 2-force members, items to the boom and rod are 2-force members, items to the boom and rod are 2-force members. the members are subjected to only two forces which are applied at member ends
- For equilibrium, the forces must be parallel to to an axis between the force application points, equal in magnitude, and in opposite directions

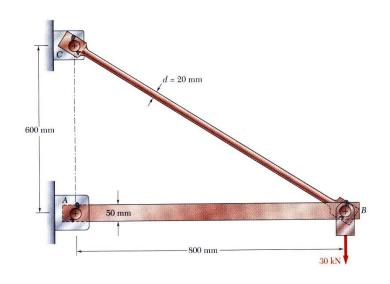
Joints must satisfy the conditions for static equilibrium which may be expressed in the form of a force triangle:

$$\sum \vec{F}_B = 0$$

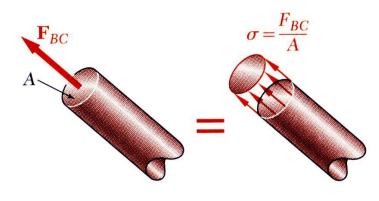
$$\frac{F_{AB}}{4} = \frac{F_{BC}}{5} = \frac{30 \text{ kN}}{3}$$

$$F_{AB} = 40 \text{ kN} \qquad F_{BC} = 50 \text{ kN}$$

Stress Analysis



$$d_{BC}$$
 = 20 mm



Can the structure safely support the 30 km load?

• From a statics analysis

$$F_{AB}$$
 = 40 kN (compression)
 F_{BC} = 50 kN (tension)

 At any section through member BC, the internal force is 50 kN with a force intensity or <u>stress</u> of

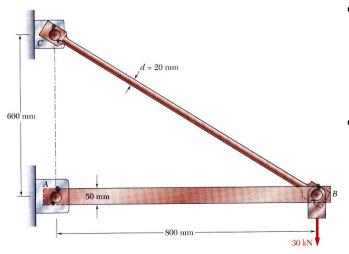
$$\sigma_{BC} = \frac{P}{A} = \frac{50 \times 10^3 \text{ N}}{314 \times 10^{-6} \text{ m}^2} = 159 \text{ MPa}$$

• From the material properties for steel, the allowable stress is

$$\sigma_{\rm all} = 165 \, \rm MPa$$

- Conclusion: the strength of member *BC* is adequate
- Similar analysis should be done for the AB in compression as well as the pins!

Design



- Design of new structures requires selection of appropriate materials and component dimensions to meet performance requirements
- For reasons based on cost, weight, availability, etc., the choice is made to construct the rod from aluminum (σ_{all} = 100 MPa). What is an appropriate choice for the rod diameter?

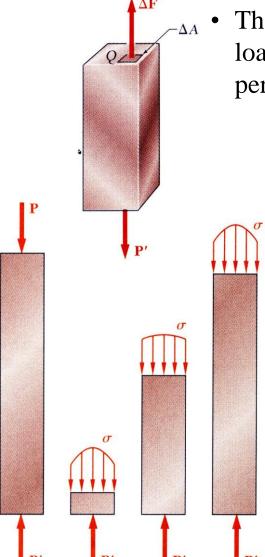
$$\sigma_{all} = \frac{P}{A} \qquad A = \frac{P}{\sigma_{all}} = \frac{50 \times 10^3 \,\text{N}}{100 \times 10^6 \,\text{Pa}} = 500 \times 10^{-6} \,\text{m}^2$$

$$A = \pi \frac{d^2}{4}$$

$$d = \sqrt{\frac{4A}{\pi}} = \sqrt{\frac{4(500 \times 10^{-6} \,\text{m}^2)}{\pi}} = 2.52 \times 10^{-2} \,\text{m} = 25.2 \,\text{mm}$$

• An aluminum rod 26 mm or more in diameter is adequate

Axial Loading: Normal Stress



• The resultant of the internal forces for an axially loaded member is *normal* to a section cut perpendicular to the member axis.

• The force intensity on that section is defined as the normal stress.

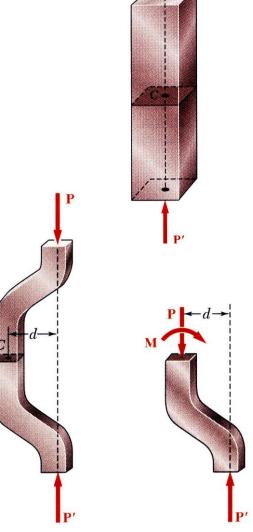
$$\sigma = \lim_{\Delta A \to 0} \frac{\Delta F}{\Delta A} \qquad \sigma_{ave} = \frac{P}{A}$$

• The normal stress at a particular point may not be equal to the average stress but the resultant of the stress distribution must satisfy

$$P = \sigma_{ave} A = \int dF = \int_{A} \sigma \, dA$$

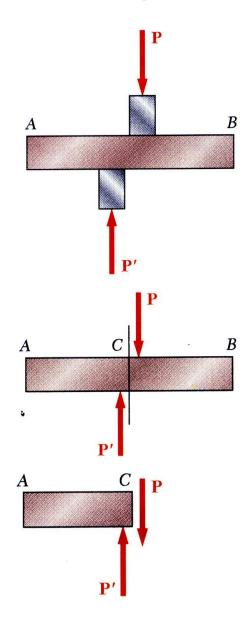
• The detailed distribution of stress is statically indeterminate, i.e., can not be found from statics alone.

Centric & Eccentric Loading



- A uniform distribution of stress in a section infers that the line of action for the resultant of the internal forces passes through the centroid of the section.
 - A uniform distribution of stress is only possible if the concentrated loads on the end sections of two-force members are applied at the section centroids. This is referred to as *centric loading*.
 - If a two-force member is *eccentrically loaded*, then the resultant of the stress distribution in a section must yield an axial force and a moment.
 - The stress distributions in eccentrically loaded members cannot be uniform or symmetric.

Shearing Stress



Forces P and P' are applied transversely to the member AB.

- Corresponding internal forces act in the plane of section *C* and are called *shearing* forces.
- The resultant of the internal shear force distribution is defined as the *shear* of the section and is equal to the load *P*.
- The corresponding average shear stress is,

$$\tau_{\text{ave}} = \frac{P}{A}$$

- Shear stress distribution varies from zero at the member surfaces to maximum values that may be much larger than the average value.
- The shear stress distribution cannot be assumed to be uniform.

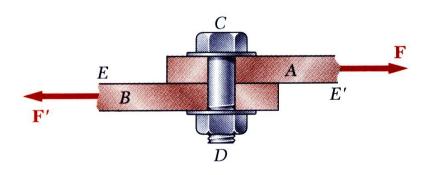
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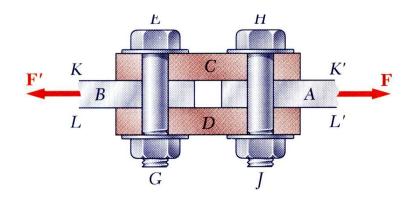
Shearing Stress Examples

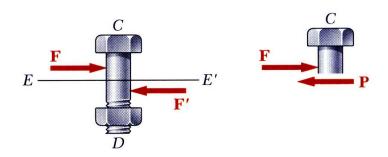


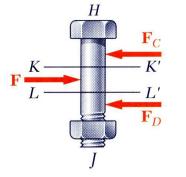


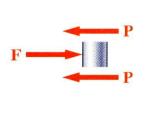










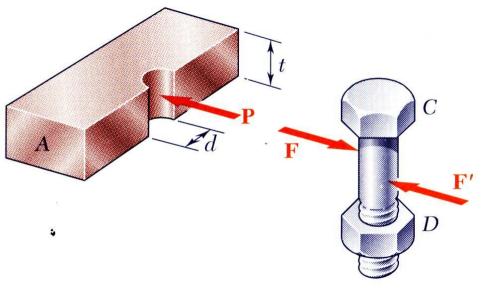


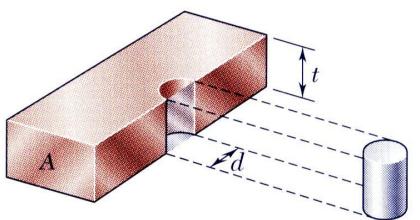
$$\tau_{\text{ave}} = \frac{P}{A} = \frac{F}{A}$$

$$\tau_{\text{ave}} = \frac{P}{A} = \frac{F}{2A}$$

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Bearing Stress in Connections





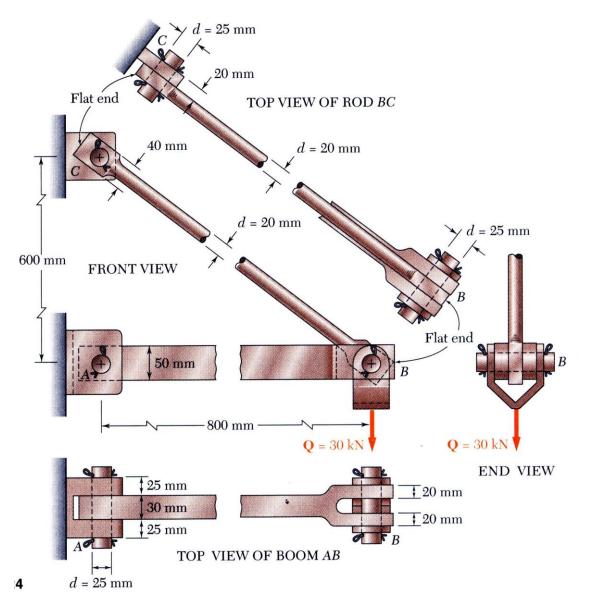
- Bolts, rivets, and pins create stresses on the points of contact or bearing surfaces of the members they connect.
- The resultant of the force distribution on the surface is equal and opposite to the force exerted on the pin.
- Corresponding average force intensity is called the bearing stress,

$$\sigma_{\rm b} = \frac{P}{A} = \frac{P}{t d}$$

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Stress Analysis & Design Example

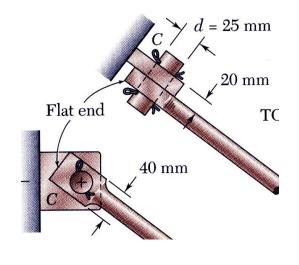




- Would like to determine the stresses in the members and connections of the structure shown.
- From a statics analysis: $F_{AB} = 40 \text{ kN (compression)}$ $F_{RC} = 50 \text{ kN (tension)}$
- Must consider maximum normal stresses in AB and BC, and the shearing stress and bearing stress at each pinned connection

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Rod & Boom Normal Stresses



- The rod is in tension with an axial force of 50 kM
- At the rod center, the average normal stress in the circular cross-section ($A = 314 \times 10^{-6} \text{m}^2$) is $\sigma_{BC} = +159$ MPa.
- At the flattened rod ends, the smallest cross-sectional area occurs at the pin centerline,

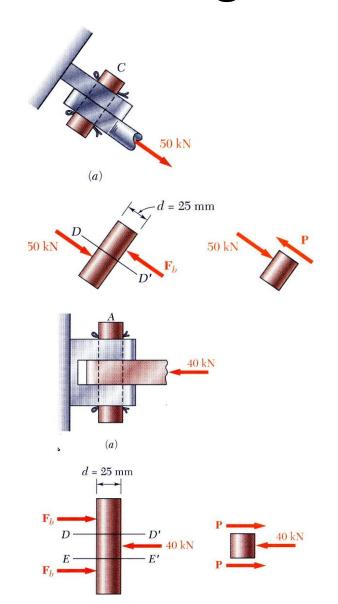
$$A = (20 \text{ mm})(40 \text{ mm} - 25 \text{ mm}) = 300 \times 10^{-6} \text{ m}^2$$

$$\sigma_{BC,end} = \frac{P}{A} = \frac{50 \times 10^3 N}{300 \times 10^{-6} \text{ m}^2} = 167 \text{ MPa}$$

- The boom is in compression with an axial force of 40 kN and average normal stress of –26.7 MPa.
- The minimum area sections at the boom ends are unstressed since the boom is in compression.

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Pin Shearing Stresses



• The cross-sectional area for pins at $A_{\bullet}B_{\bullet}$, and C_{\bullet}

$$A = \pi r^2 = \pi \left(\frac{25 \,\mathrm{mm}}{2}\right)^2 = 491 \times 10^{-6} \,\mathrm{m}^2$$

• The force on the pin at *C* is equal to the force exerted by the rod *BC*,

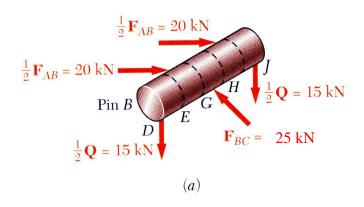
$$\tau_{C,ave} = \frac{P}{A} = \frac{50 \times 10^3 \,\text{N}}{491 \times 10^{-6} \,\text{m}^2} = 102 \,\text{MPa}$$

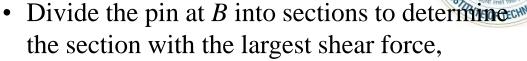
• The pin at *A* is in double shear with a total force equal to the force exerted by the boom *AB*,

$$\tau_{A,ave} = \frac{P}{A} = \frac{20 \text{ kN}}{491 \times 10^{-6} \text{ m}^2} = 40.7 \text{ MPa}$$

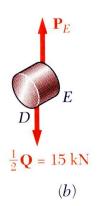
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Pin Shearing Stresses



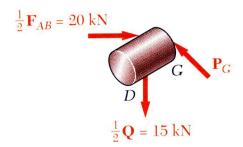


$$P_E = 15 \text{kN}$$
 $P_G = 25 \text{kN (largest)}$



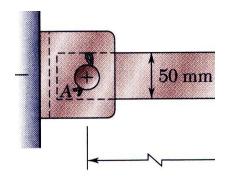
• Evaluate the corresponding average shearing stress,

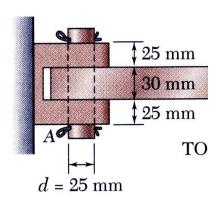
$$\tau_{B,ave} = \frac{P_G}{A} = \frac{25 \,\text{kN}}{491 \times 10^{-6} \,\text{m}^2} = 50.9 \,\text{MPa}$$



Pin Bearing Stresses







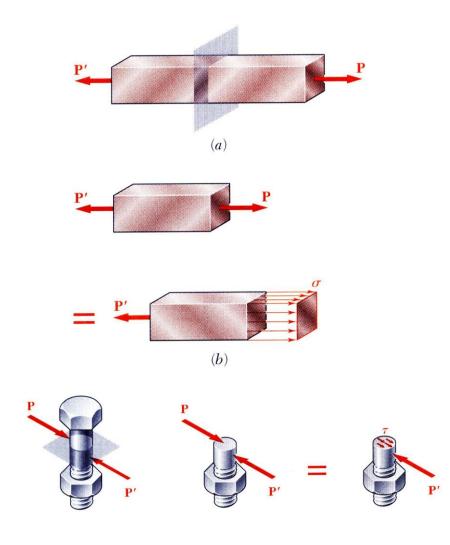
• To determine the bearing stress at A in the boom AB, we have t = 30 mm and d = 25 mm,

$$\sigma_b = \frac{P}{td} = \frac{40 \,\text{kN}}{(30 \,\text{mm})(25 \,\text{mm})} = 53.3 \,\text{MPa}$$

• To determine the bearing stress at A in the bracket, we have t = 2(25 mm) = 50 mm and d = 25 mm,

$$\sigma_b = \frac{P}{td} = \frac{40 \,\text{kN}}{(50 \,\text{mm})(25 \,\text{mm})} = 32.0 \,\text{MPa}$$

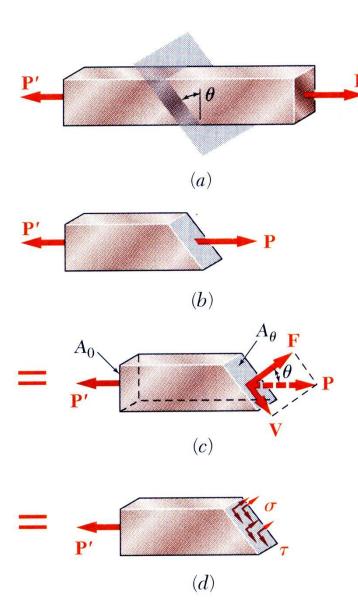
Stress in Two Force Members



- Axial forces on a two force member result in only normal stresses on a plane cut perpendicular to the member axis.
- Transverse forces on bolts and pins result in only shear stresses on the plane perpendicular to bolt or pin axis.
- Will show that either axial or transverse forces may produce both normal and shear stresses with respect to a plane other than one cut perpendicular to the member axis.

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Stress on an Oblique Plane



- Pass a section through the member forming an angle θ with the normal plane.
- From equilibrium conditions, the distributed forces (stresses) on the plane must be equivalent to the force *P*.
- Resolve *P* into components normal and tangential to the oblique section,

$$F = P\cos\theta$$
 $V = P\sin\theta$

 The average normal and shear stresses on the oblique plane are

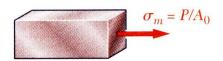
$$\sigma = \frac{F}{A_{\theta}} = \frac{P \cos \theta}{A_0 / \cos \theta} = \frac{P}{A_0} \cos^2 \theta$$

$$\tau = \frac{V}{A_{\theta}} = \frac{P\sin\theta}{A_0/\cos\theta} = \frac{P}{A_0}\sin\theta\cos\theta$$

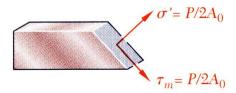
Maximum Stresses



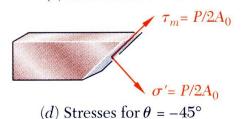
(a) Axial loading



(b) Stresses for $\theta = 0$



(c) Stresses for $\theta = 45^{\circ}$



Normal and shearing stresses on an oblique plane

$$\sigma = \frac{P}{A_0} \cos^2 \theta \quad \tau = \frac{P}{A_0} \sin \theta \cos \theta$$

• The maximum normal stress occurs when the reference plane is perpendicular to the member axis,

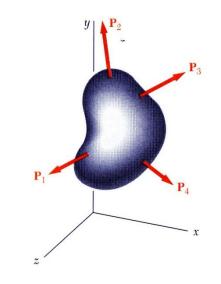
$$\sigma_{\rm m} = \frac{P}{A_0} \quad \tau' = 0$$

• The maximum shear stress occurs for a plane at $\pm 45^{\circ}$ with respect to the axis,

$$\tau_m = \frac{P}{A_0} \sin 45 \cos 45 = \frac{P}{2A_0} = \sigma'$$

Stress Under General Loadings



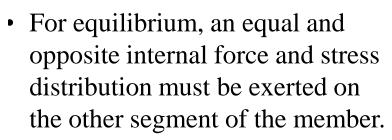


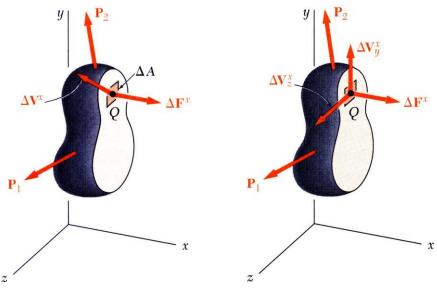
A member subjected to a general combination of loads is cut into two segments by a plane passing through Q

> The distribution of internal stress components may be defined as,

$$\sigma_x = \lim_{\Delta A \to 0} \frac{\Delta F^x}{\Delta A}$$

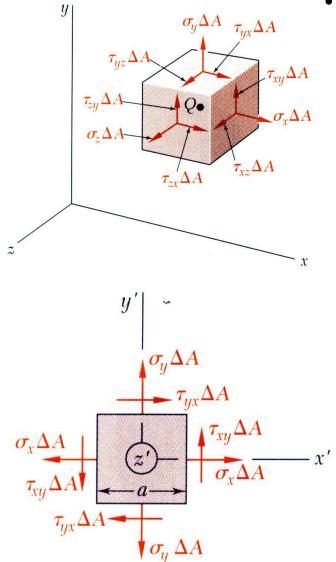
$$\tau_{xy} = \lim_{\Delta A \to 0} \frac{\Delta V_y^x}{\Delta A} \quad \tau_{xz} = \lim_{\Delta A \to 0} \frac{\Delta V_z^x}{\Delta A}$$





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State of Stress



How many components of stresses we have?

- Stress components are defined for the planes cut parallel to the x, y and z axes. For equilibrium, equal and opposite stresses are exerted on the hidden planes.
 - The combination of forces generated by the stresses must satisfy the conditions for equilibrium:

$$\sum F_x = \sum F_y = \sum F_z = 0$$
$$\sum M_x = \sum M_y = \sum M_z = 0$$

• Consider the moments about the z axis:

$$\sum M_z = 0 = (\tau_{xy} \Delta A) a - (\tau_{yx} \Delta A) a$$

$$\tau_{xy} = \tau_{yx}$$
similarly, $\tau_{yz} = \tau_{zy}$ and $\tau_{yz} = \tau_{zy}$

• It follows that only 6 components of stress are required to define the complete state of stress

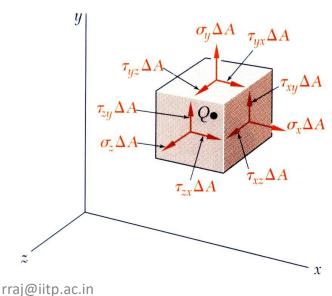
Nomenclature

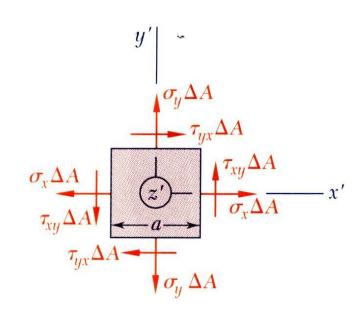


au_{AB}

A implies the axis perpendicular to the plane along with the shear stress acts

B implies the direction of shear stress





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• At a point, shear stress cannot take place in one plane only, an equal shear stress must be exerted on another plane perpendicular to the first one.

Factor of Safety

Structural members or machines must be designed such that the working stresses are less than the ultimate strength of the material.

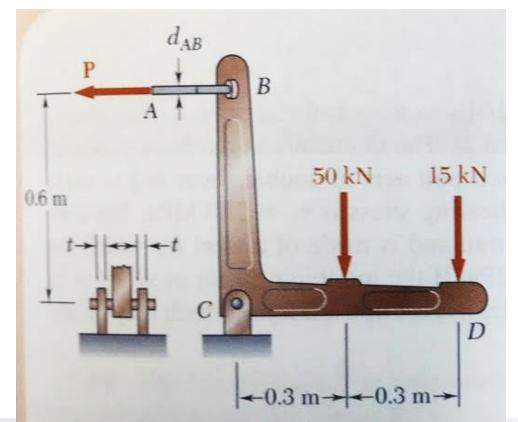
$$FS$$
 = Factor of safety

$$FS = \frac{\sigma_{\rm u}}{\sigma_{\rm all}} = \frac{\text{ultimate stress}}{\text{allowable stress}}$$

Factor of safety considerations:

- uncertainty in material properties
- uncertainty of loadings
- uncertainty of analyses
- number of loading cycles
- types of failure
- maintenance requirements and deterioration effects
- importance of member to structures integrity
- risk to life and property
- influence on machine function

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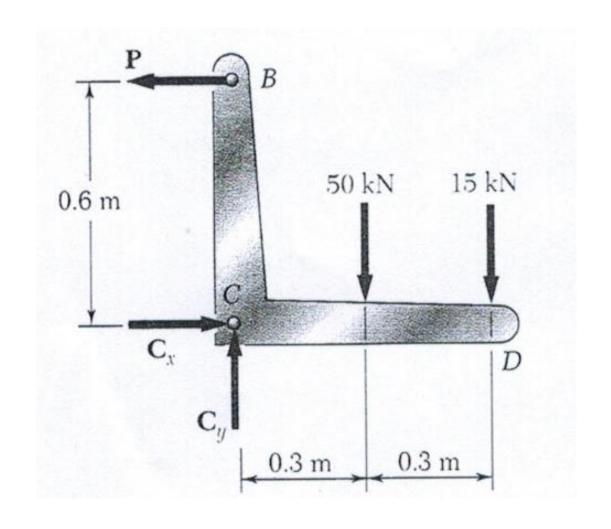




Two forces are applied to the bracket BCD as shown. (a) Knowing that the control rod AB is to be made of a steel having an ultimate normal stress of 600 MPa, determine the diameter of the rod for which the factor of safety with respect to failure will be 3.3. (b) The pin at C is to be made of a steel having an ultimate shearing stress of 350 MPa. Determine the diameter of the pin C for which the factor of safety with respect to shear will also be 3.3. (c) Determine the required thickness of the bracket supports at C knowing that the allowable bearing stress of the steel used in 300 Mpa.

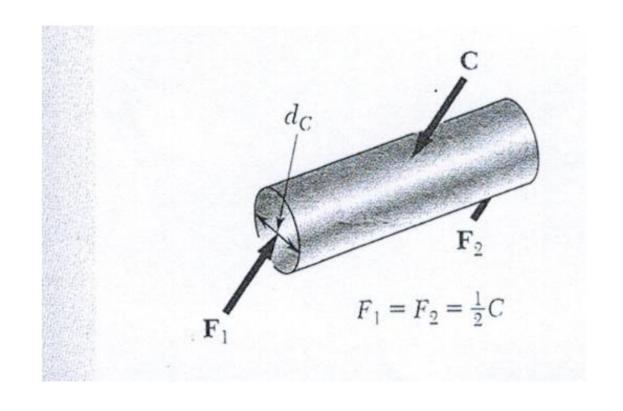
First Step: Bracket FBD

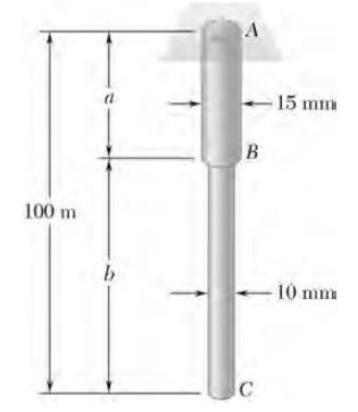




Second Step: Pin FBD

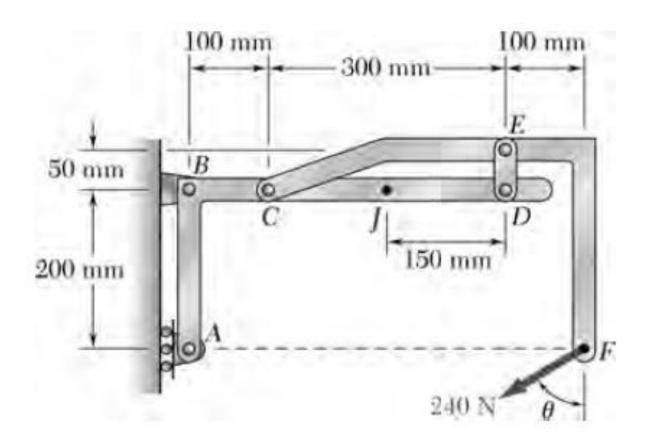






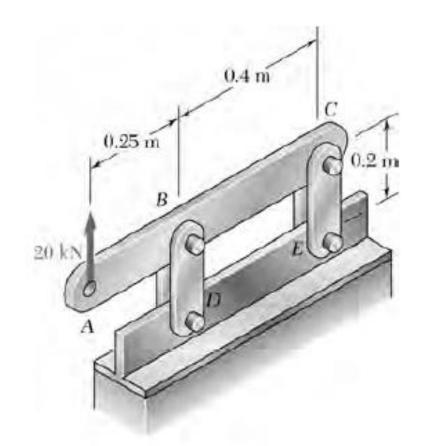


Two brass rods AB and BC, each of uniform diameter, will be brazed together at B to form a nonuniform rod of total length 100 m, which will be suspended from a support at A as shown. Knowing that the density of brass is 8470 kg/m^3 , determine (a) the length of rod AB for which the maximum normal stress in ABC is minimum, (b) the corresponding value of the maximum normal stress.



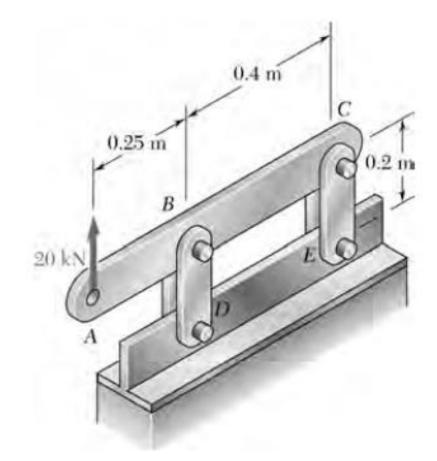


Knowing that link DE is 25 mm wide and 3 mm thick, determine the normal stress in the central portion of that link when (a) $\theta = 0$, (b) $\theta = 90^{\circ}$.



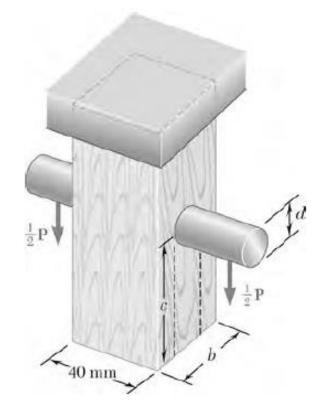


Each of the four vertical links has an 8×36 -mm uniform rectangular cross section and each of the four pins has a 16-mm diameter. Determine the maximum value of the average normal stress in the links connecting (a) points B and D, (b) points C and E.





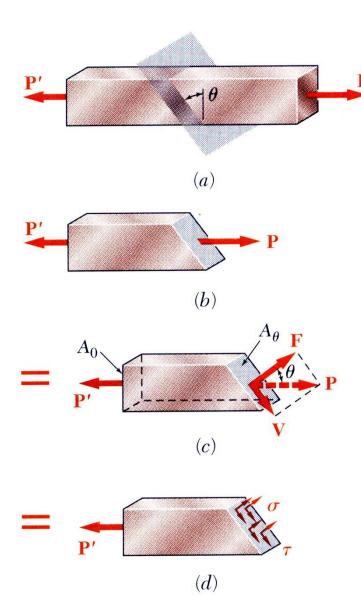
For the assembly and loading of Problem 1.7, determine (a) the average shearing stress in the pin at B, (b) the average bearing stress at B in member BD, (c) the average bearing stress at B in member ABC, knowing that this member has a 10×50 -mm uniform rectangular cross section.





A load **P** is supported as shown by a steel pin that has been inserted in a short wooden member hanging from the ceiling. The ultimate strength of the wood used is 60 MPa in tension and 7.5 MPa in shear, while the ultimate strength of the steel is 145 MPa in shear. Knowing that b = 40 mm, c = 55 mm, and d = 12 mm, determine the load **P** if an overall factor of safety of 3.2 is desired.

Stress on an Oblique Plane



- Pass a section through the member forming an angle θ with the normal plane.
- From equilibrium conditions, the distributed forces (stresses) on the plane must be equivalent to the force *P*.
- Resolve *P* into components normal and tangential to the oblique section,

$$F = P\cos\theta$$
 $V = P\sin\theta$

• The average normal and shear stresses on the oblique plane are

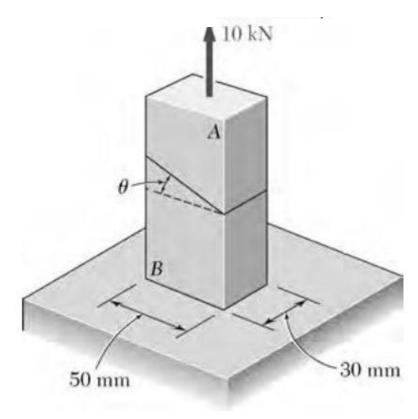
$$\sigma = \frac{F}{A_{\theta}} = \frac{P \cos \theta}{A_0 / \cos \theta} = \frac{P}{A_0} \cos^2 \theta$$

$$\tau = \frac{V}{A_{\theta}} = \frac{P\sin\theta}{A_0/\cos\theta} = \frac{P}{A_0}\sin\theta\cos\theta$$

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The two portions of member AB are glued together along a plane forming an angle θ with the horizontal. Knowing that the ultimate stress for the glued joint is 17 MPa in tension and 9 MPa in shear, determine (a) the value of θ for which the factor of safety of the member is maximum, (b) the corresponding value of the factor of safety.





Two wooden members of uniform rectangular cross section of sides a = 100 mm and b = 60 mm are joined by a simple glued joint as shown. Knowing that the ultimate stresses for the joint are σ_U = 1.26 MPa in tension and τ_U =1.50 MPa in shear, and that P = 6 kN, determine the factor of safety for the joint when (a) α = 20°, (b) α = 35°, (c) α = 45°. For each of these values of α , also determine whether the joint will fail in tension or in shear if P is increased until rupture occurs.

