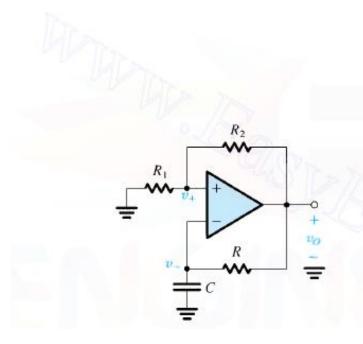
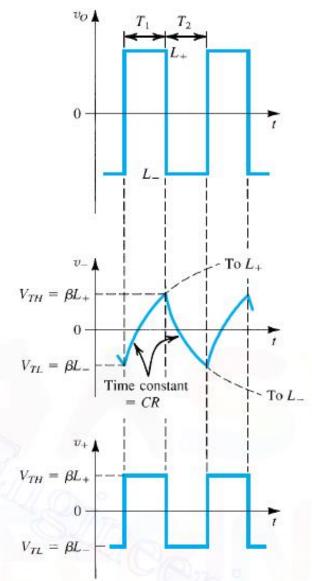
# Lecture 33

#### Astable Multivibrator





• During the charging interval  $T_1$  the voltage  $v_1$  across the capacitor at any time t, with t=0 at the beginning of  $T_1$ , is given by

$$v_{-} = L_{+} - (L_{+} - \beta L_{-})e^{-t/\tau}$$

where  $\tau = CR$ . Substituting  $v_{-} = \beta L_{+}$  at  $t = T_{1}$  gives

$$T_1 = \tau \ln \frac{1 - \beta (L_-/L_+)}{1 - \beta}$$

Similarly, during the discharge interval  $T_2$  the voltage  $v_-$  at any time t, with t = 0 at the beginning of  $T_2$ , is given by

$$V_{-} = L_{-} - (L_{-} - \beta L_{+}) e^{-t/\tau}$$

Substituting  $v_- = \beta L_-$  at  $t = T_2$  gives

$$T_2 = \tau \ln \frac{1 - \beta (L_+/L_-)}{1 - \beta}$$



• When both saturation levels are of same magnitude,

• When both saturation levels are of same magnitude,

Symmetrical word TITE

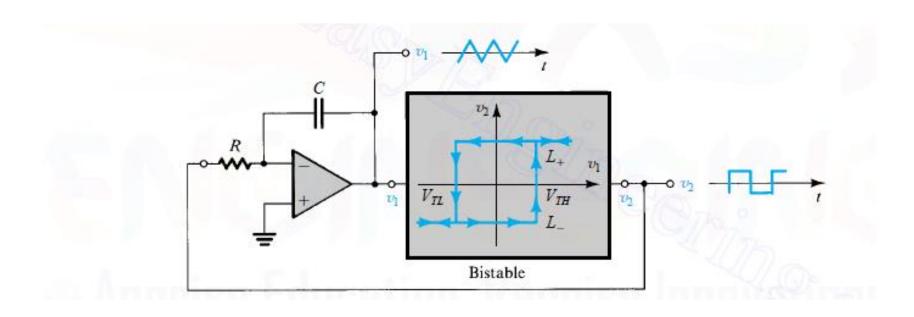
Sommetrical word TITE

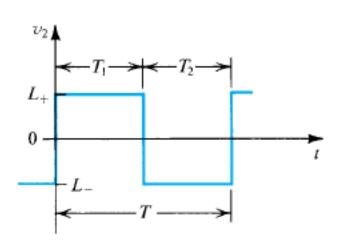
Some Speriod TITE

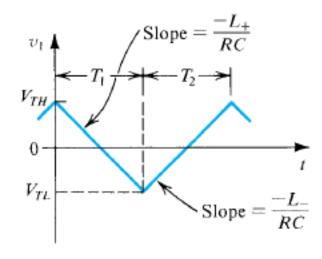
= 27 ln I-B

Cascading an integrator with astable mulitivibrator?

Tuning the time constant of the RC circuit.







$$\frac{V_{TH} - V_{TL}}{T_1} = \frac{L_+}{CR}$$

from which we obtain

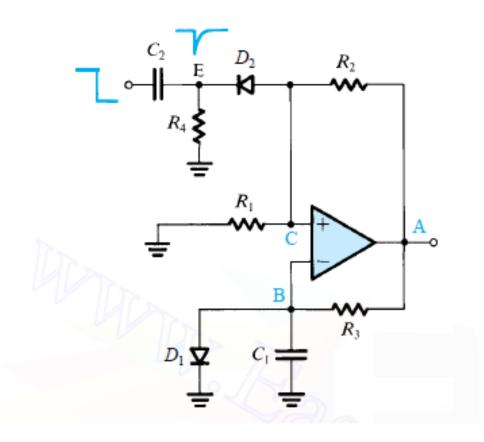
$$T_1 = CR \frac{V_{TH} - V_{TL}}{L_+}$$

Similarly, during  $T_2$  we have

$$\frac{V_{TH} - V_{TL}}{T_2} = \frac{-L_{-}}{CR}$$

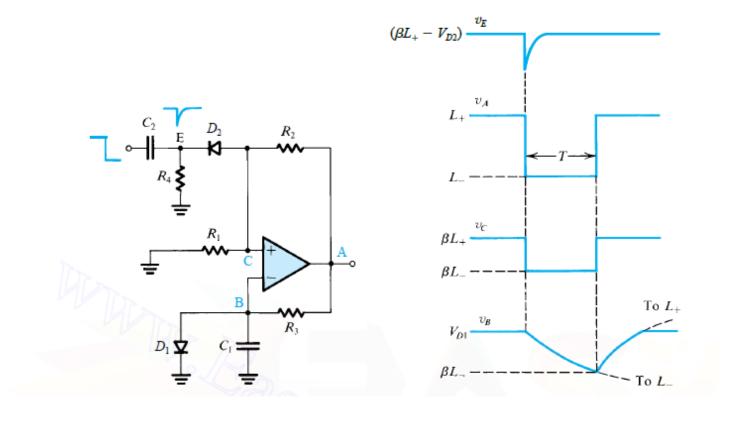
from which we obtain

$$T_2 = CR \frac{V_{TH} - V_{TL}}{-L_-}$$



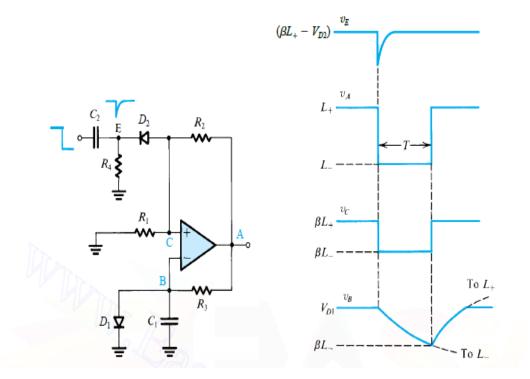
# Lecture 34

# Monostable Multivibrator (An Op-Amp based circuit)



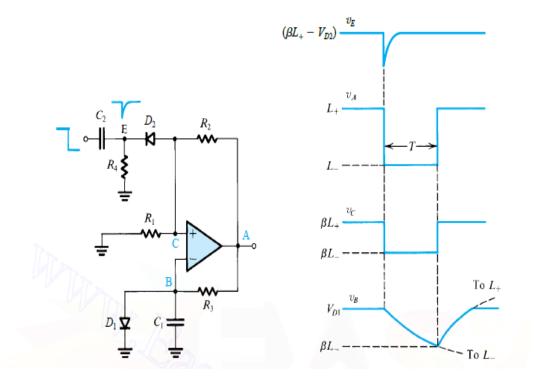
#### Monostable Multivibrator

- ullet A clamping diode  $D_1$  is added across the Capacitor  $C_1$
- A trigger circuit  $(C_2, D_2, and R_4)$  is connected to the noninverting terminal.
- Only one stable state. When the output is  $L_+$  in the absence of any triggering signal.
- $\bullet$  <please check what happens when the output is  $L_+>$
- $D_1$  is conducting, voltage level at the node B is clamped at one diode drop.



#### Monostable Multivibrator

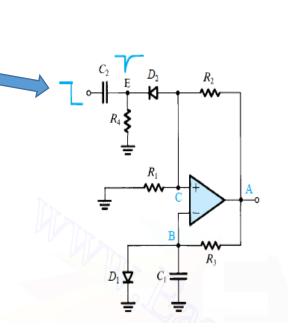
- $D_1$  is conducting, voltage level at the node B is clamped at one diode drop above the ground.
- We select  $R_4 \gg R_1$ . So, the current through  $D_2$  is negligible.
- Voltage at the noninverting terminal is approximately  $\beta L_+$ , where  $\beta = \frac{R_1}{R_1 + R_2}$
- The stable state is maintained, because  $\beta L_{+} >$  one diode drop above ground.

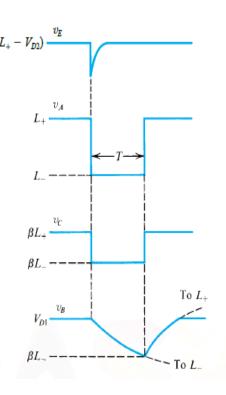


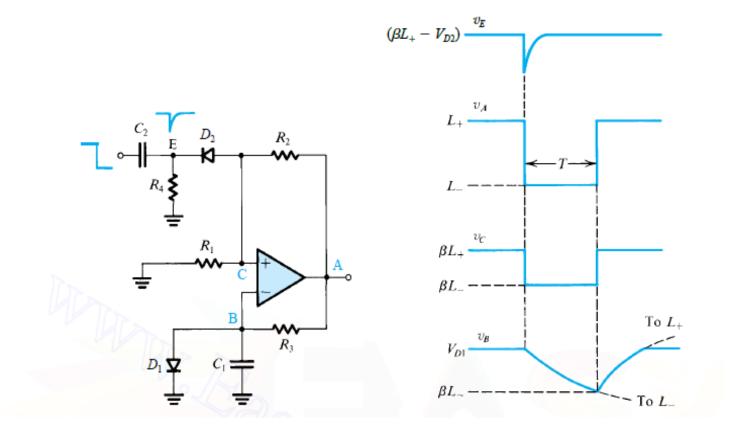
#### Monostable Multivibrator

 Now see what happens when a negativegoing triggering voltage is applied

- $D_2$  is conducting heavily, pulling voltage level at the node C down.
- So, for a sufficiently large triggering voltage the op amp has a negative input (i.e., B is at higher potential than C).
- Output changes to L\_
- $D_2$  is cut off. Triggering section is isolated.







The negative voltage at A causes  $D_1$  to cut off, and  $C_1$  begins to discharge exponentially toward L with a time constant  $C_1R_3$ . The monostable multivibrator is now in its *quasi-stable state*, which will prevail until the declining  $v_B$  goes below the voltage at node C, which is  $\beta L$ . At this instant the op-amp output switches back to L and the voltage at node C goes back to  $\beta L$ . Capacitor  $C_1$  then charges toward L until diode  $D_1$  turns on and the circuit returns to its stable state.

From the figure , we observe that a negative pulse is generated at the output during the quasi-stable state. The duration T of the output pulse is determined from the exponential waveform of  $v_B$ ,

$$v_B(t) = L_- - (L_- - V_{D1})e^{-t/C_1R_3}$$

From the figure, we observe that a negative pulse is generated at the output during the quasi-stable state. The duration T of the output pulse is determined from the exponential waveform of  $v_B$ ,

$$v_B(t) = L_- - (L_- - V_{D1})e^{-t/C_1R_3}$$

by substituting  $v_B(T) = \beta L$ ,

$$\beta L_{-} = L_{-} - (L_{-} - V_{D1}) e^{-T/C_{1}R_{3}}$$

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$$v_B(t) = L_- - (L_- - V_{D1})e^{-t/C_1R_3}$$

by substituting  $v_B(T) = \beta L$ ,

$$\beta L_{-} = L_{-} - (L_{-} - V_{D1}) e^{-T/C_{1}R_{3}}$$

which yields

$$T = C_1 R_3 \ln \left( \frac{V_{D1} - L_{-}}{\beta L_{-} - L_{-}} \right)$$

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$$v_B(t) = L_- - (L_- - V_{D1})e^{-t/C_1R_3}$$

by substituting  $v_B(T) = \beta L$ ,

$$\beta L_{-} = L_{-} - (L_{-} - V_{D1}) e^{-T/C_{1}R_{3}}$$

which yields

$$T = C_1 R_3 \ln \left( \frac{V_{D1} - L_{-}}{\beta L_{-} - L_{-}} \right)$$

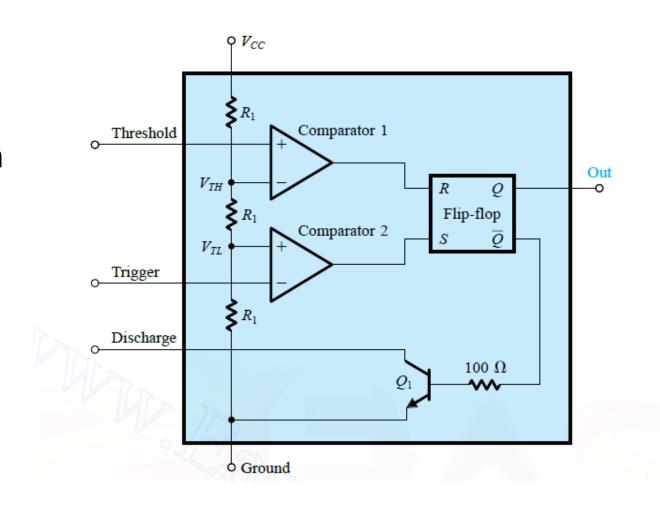
For  $V_{D1} \ll |L_{-}|$ , this equation can be approximated by

$$T \simeq C_1 R_3 \ln \left( \frac{1}{1 - \beta} \right)$$

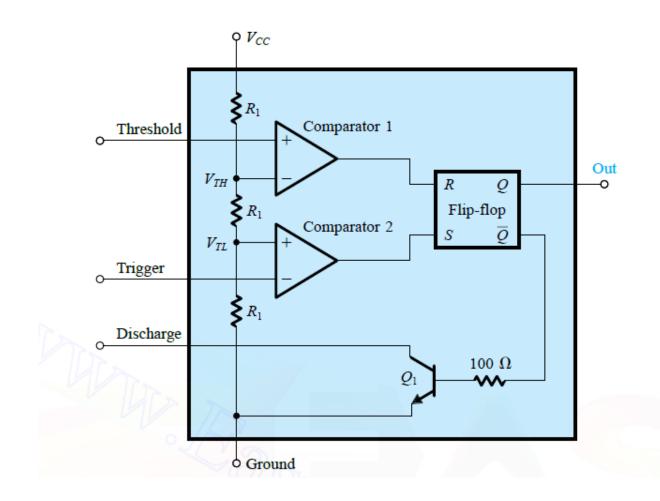
#### Integrated Circuit Timer

Commercially available integrated-circuit packages exist that contain the bulk of the circuitry needed to implement monostable and astable multivibrators with precise characteristics. In this section we discuss the most popular of such ICs, the 555 timer. Introduced in 1972 by the Signetics Corporation as a bipolar integrated circuit, the 555 is also available in CMOS technology and from a number of manufacturers.

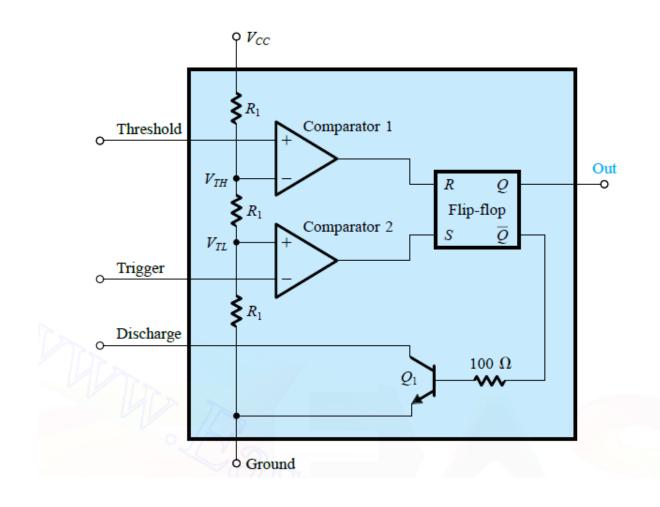
- 2 comparators
- 1 SR flip-flop
- 1 transistor as electronic switch
- 1 power supply (typically 5 V.)
- 1 resistive voltage divider consisting 3 equally valued resistors.



- Two threshold/reference voltages for two comparators.
- $V_{TH} = \frac{2}{3}V_{CC}$   $V_{TL} = \frac{1}{3}V_{CC}$

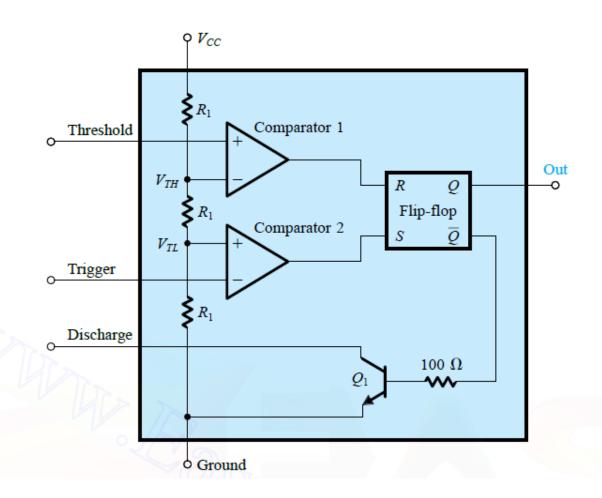


 Recall that SR flip-flops are bistable multivibrators with two complementary outputs.



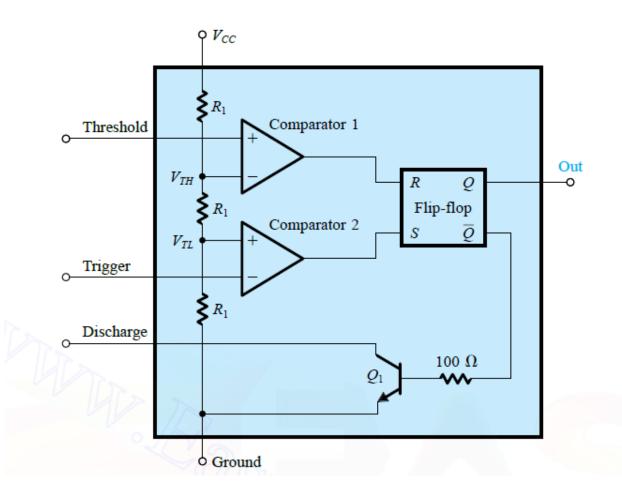
• The `Threshold' terminal of the IC package (external pin): connected to the positive terminal of the comparator 1

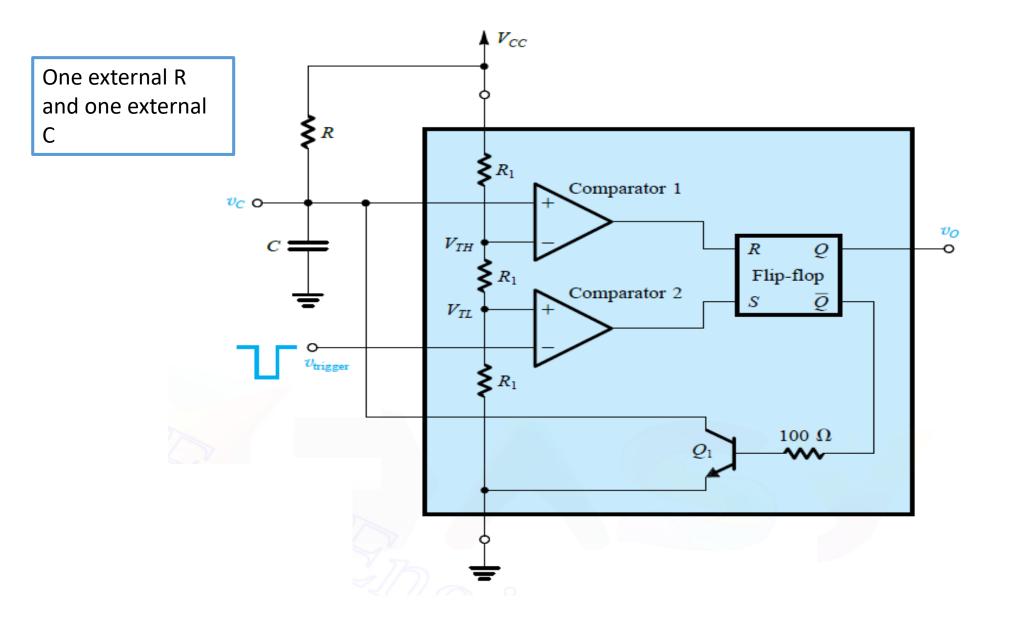
 The `Trigger' terminal of the IC package (external pin): connected to the negative terminal of the comparator 2



• The `Discharge' terminal of the IC package (external pin): connected to the `collector' of the transistor (electronic switch)

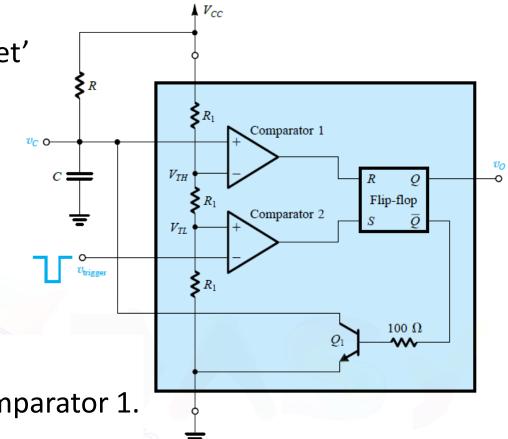
The `Out' terminal of the IC package (external pin):
 connected to the `Q' output terminal of the flip-flop





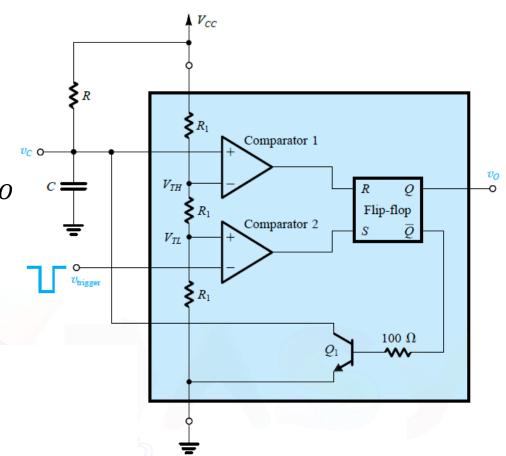
• In the stable state, the flip-flop will be in the `reset' state.

- $\overline{Q}$  output will be high.
- Will turn  $Q'_1$  transistor on.
- $v_C$  will be close to 0 V.
- Will result in a low level at the output of the comparator 1.
- $v_{trigger}$  is kept high (>  $v_{TL}$ ), and thus a low level at the output of the comparator 2 as well.



• In the stable state, the flip-flop is in the `reset' state.

•  $\overline{Q}$  will be high and Q will be low. So, the output  $v_{O}$  will be close 0 V.



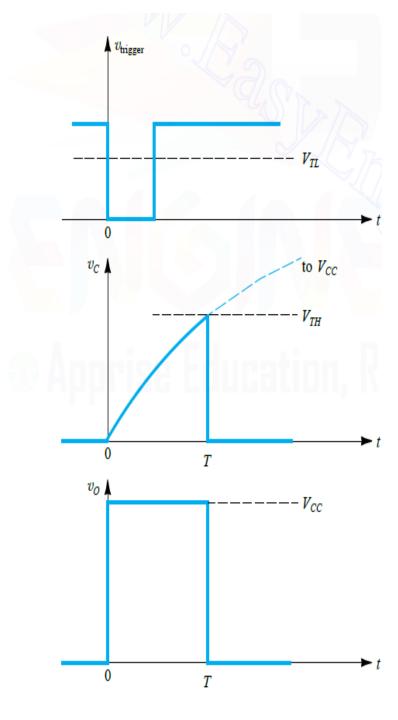
 To trigger the monostable multivibrator, a negative triggering pulse is applied to the 'Trigger' input terminal.

• 
$$v_{trigger} < V_{TL}$$

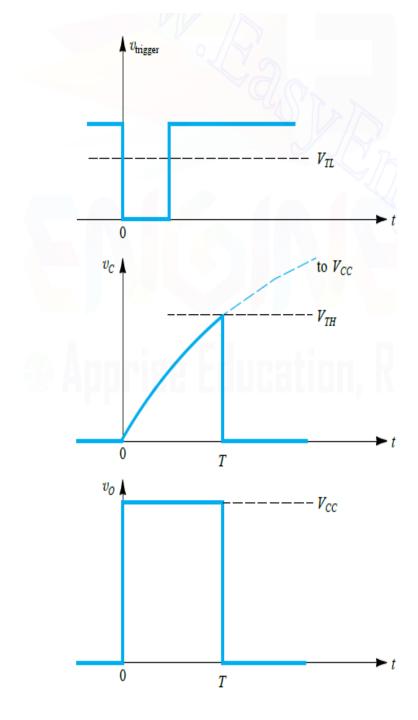
• The output of the comparator 2 goes to the high level.

The flip-flop is `set'. Q is high.

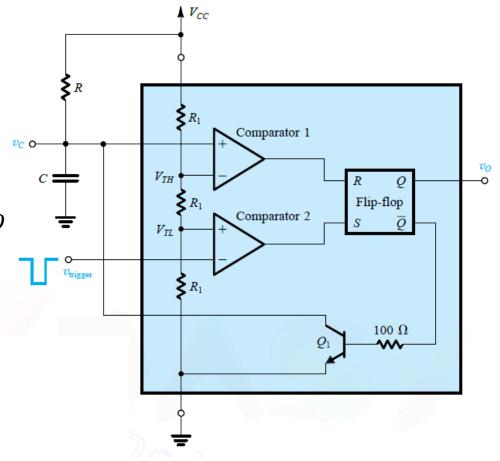
• So, the output  $v_O$  is high.



- The flip-flop is `set'.  $\overline{Q}$  is low.
- Will turn  $Q'_1$  transistor <u>off</u>.
- Capacitor begins to charge up through R.
- $v_C$  will rise up exponentially toward  $V_{CC}$ .
- The monostable multivibrator reaches the 'quasistable' state. The state prevails until  $v_{\it C}$  reaches  $V_{\it TH}$  and exceeds  $V_{\it TH}$ .



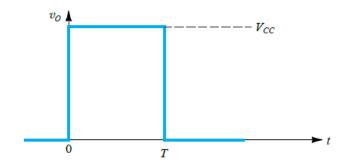
- The output of the comparator 1 will be high.
- The flip-flop will be 'reset' again.
- $\overline{Q}$  will be high and Q will be low. So, the output  $v_O$  will be close 0 V.
- The transistor will be switched on again.
- The capacitor will discharge to zero voltage level.
- The monostable multivibrator is back to the `stable' state.



# Lecture 35

# Determining the Pulse Width of 555 timer based Monostable Multivibrator

• The width of the pulse, *T* is the time the Monostable multivibrator spends in a 'quasistable' state.



- The pulse width, *T* is determined in the following way:
- Referring to the waveforms given here (associated with the

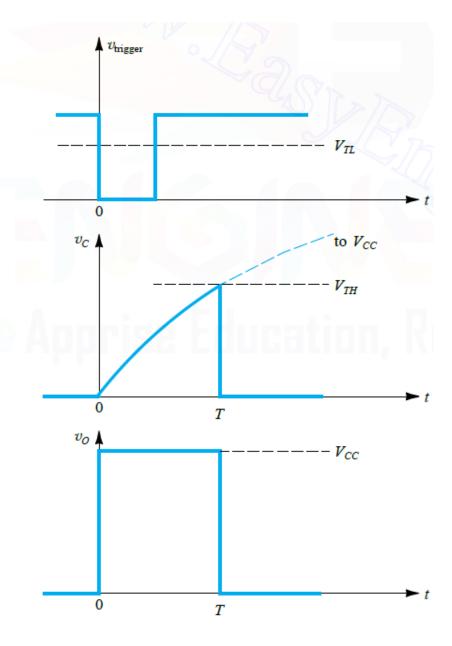
block diagram of 555 based monostable multivibrator),

$$v_C = V_{CC}(1 - e^{-t/CR})$$

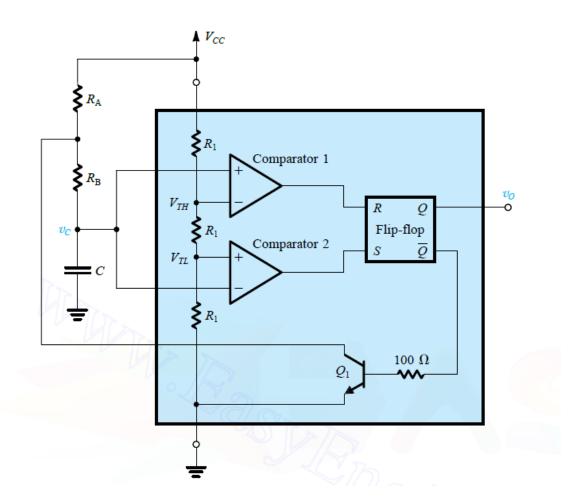
Substituting  $v_C = V_{TH} = \frac{2}{3}V_{CC}$  at t = T gives

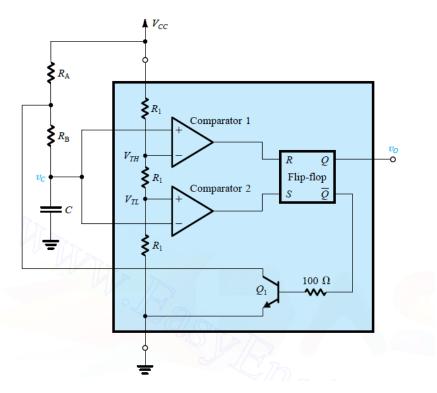
$$T = CR \ln 3 \approx 1.1 CR$$

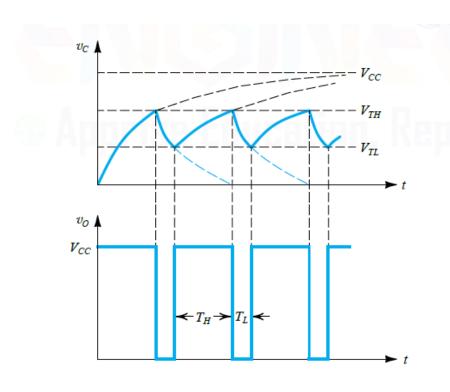
Thus the pulse width is determined by the external components C and R, which can be selected to have values as precise as desired.



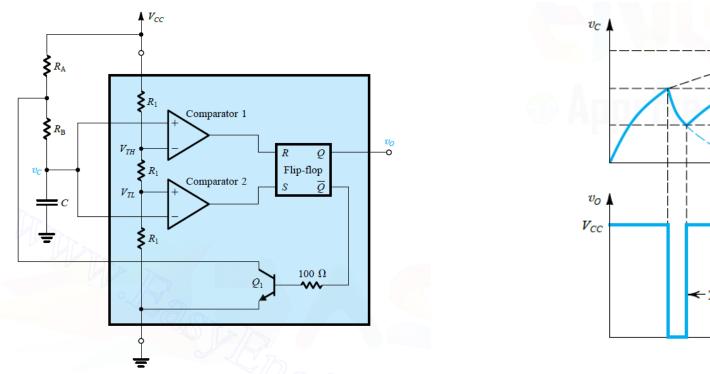
Two external resistors, and one external capacitor

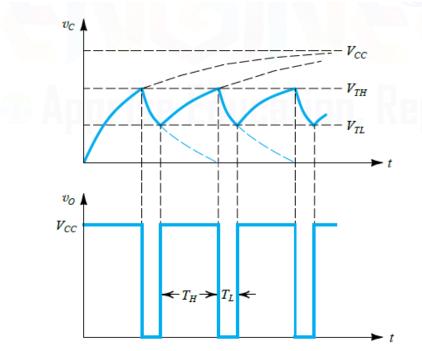




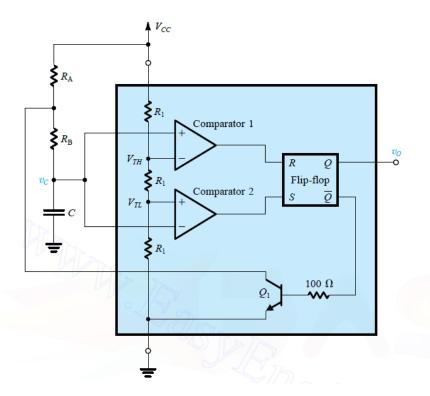


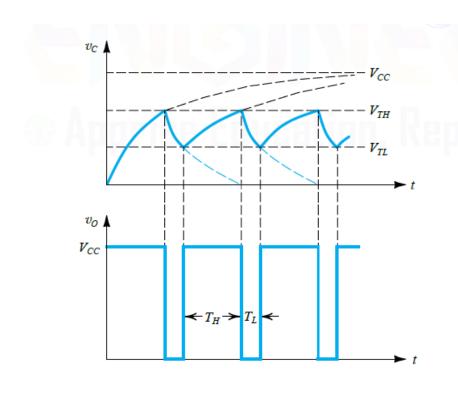
- Assume initially C is discharged.
- The flip-flop is `set'.
- Thus  $v_o$  is high, and  $Q_1$  is off.



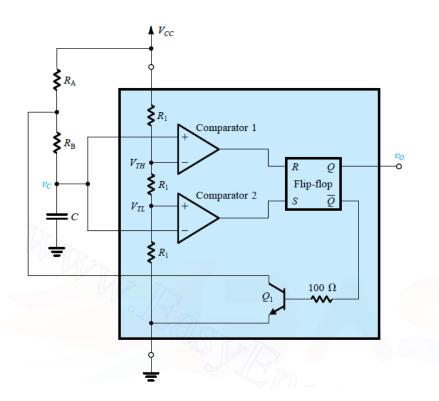


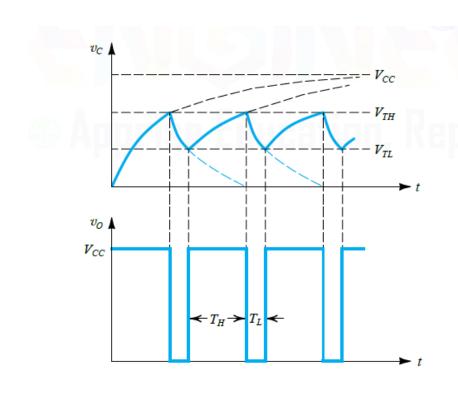
- C will charge up through the series combination of  $R_A$  and  $R_B$ .
- $v_C$  rises up exponentially toward  $V_{CC}$  with a time constant  $C(R_A + R_B)$ .
- When  $v_C$  crosses the level equal to  $V_{TL}$ , the output of the comparator 2 goes low.



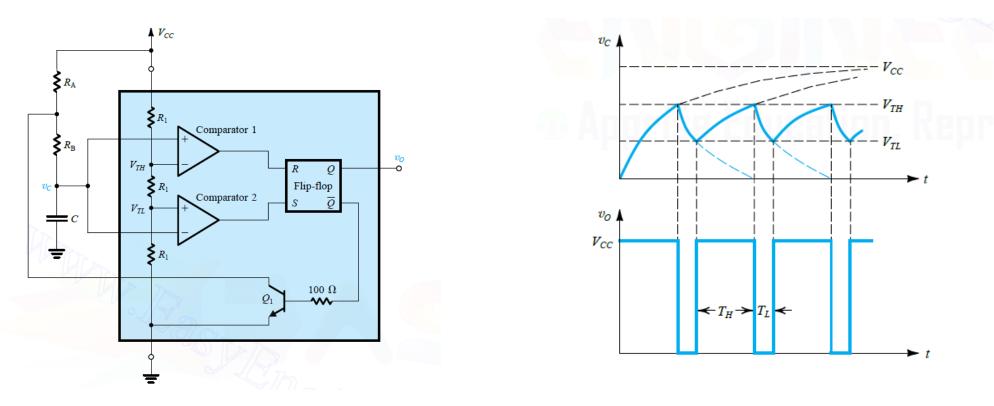


- But, the flip-flop remains `set'.
- ullet This state prevails until  $v_{\mathcal{C}}$  crosses the level equal to  $V_{TH}$
- The output of the comparator 1 goes high, the flip-flop is `reset'.

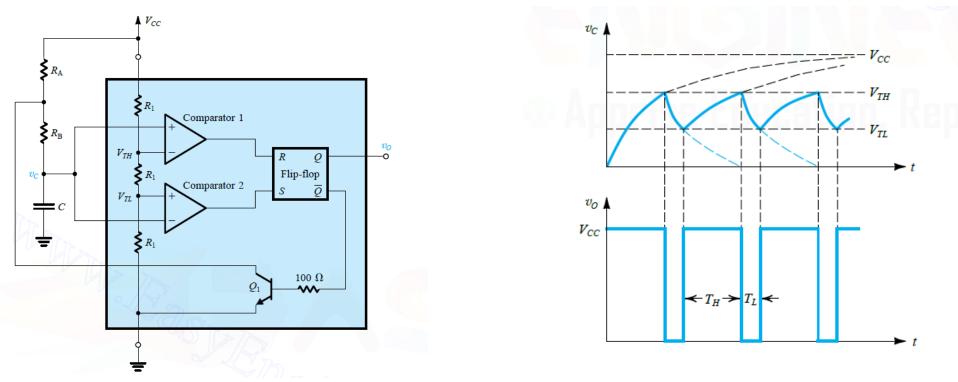




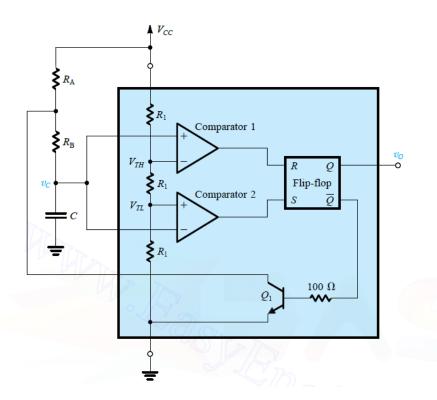
- Thus  $v_o$  goes low, and  $Q_1$  is turned on.
- The common node of  $R_A$  and  $R_B$  is almost at 0 V (approximately).
- Thus, C begins to discharge through  $R_B$  and the transistor.

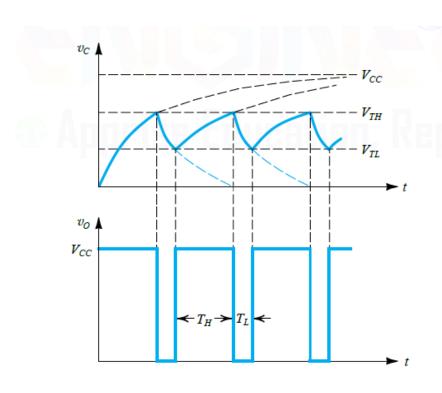


- $v_C$  decreases exponentially with a time constant  $CR_B$  toward 0 V.
- When  $v_C$  reaches  $V_{TL}$  , the output of the comparator 2 goes high.
- The flip-flop is `set'. Thus  $v_o$  is high, and  $Q_1$  is off.

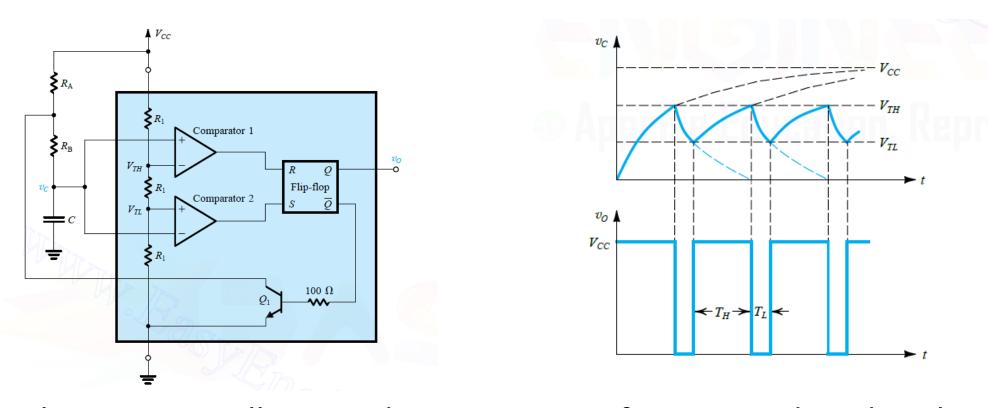


- C will again charge up through the series combination of  $R_A$  and  $R_B$ .
- $v_C$  rises up exponentially toward  $V_{CC}$  with a time constant  $C(R_A + R_B)$ .
- When  $v_{\mathcal{C}}$  crosses the level equal to  $V_{TH}$ , the output of the comparator 1 goes high, the flip-flop is `reset'.





- Thus  $v_o$  goes low, and  $Q_1$  is turned on.
- Thus, C begins to discharge through  $R_B$  and the transistor.
- And, the cycle continues.



The circuit oscillates and a square waveform is produced at the output.

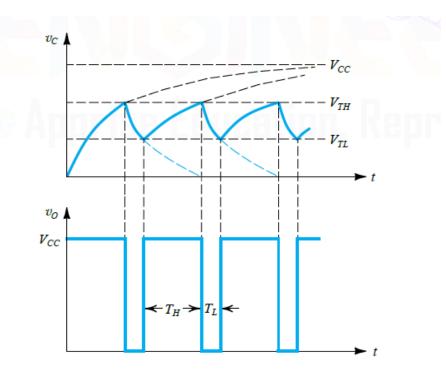
# $v_{C}$ $v_{CC}$ $v_{TH}$ $v_{TL}$ $v_{CC}$ $v_{TH}$ $v_{TL}$ $v_{TL}$

Reference to the fig.-s indicates that the output will be high during the interval  $T_H$ , in which  $v_C$  rises from  $V_{TL}$  to  $V_{TH}$ . The exponential rise of  $v_C$  can be described by

$$v_C = V_{CC} - (V_{CC} - V_{TL})e^{-t/C(R_A + R_B)}$$

where t=0 is the instant at which the interval  $T_H$  begins. Substituting  $v_C=V_{TH}=\frac{2}{3}\,V_{CC}$  at  $t=T_H$  and  $V_{TL}=\frac{1}{3}\,V_{CC}$  results in

$$T_H = C(R_A + R_B) \ln 2 \approx 0.69 C(R_A + R_B)$$

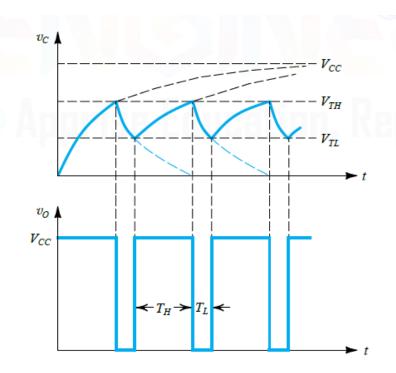


We also note from the fig.-s that  $v_O$  will be low during the interval  $T_L$ , in which  $v_C$  falls from  $V_{TL}$  to  $V_{TL}$ . The exponential fall of  $v_C$  can be described by

$$v_C = V_{TH} e^{-t/CR_B}$$

where we have taken t=0 as the beginning of the interval  $T_L$ . Substituting  $v_C=V_{TL}=\frac{1}{3}V_{CC}$  at  $t=T_L$  and  $V_{TH}=\frac{2}{3}V_{CC}$  results in

$$T_L = CR_B \ln 2 \simeq 0.69 CR_B$$



Equations given before can be combined to obtain the period *T* of the output square wave as

$$T = T_H + T_L = 0.69 \ C(R_A + 2R_B)$$

Also, the duty cycle of the output square wave can be found from Eqs given above

Duty cycle = 
$$\frac{T_H}{T_H + T_L} = \frac{R_A + R_B}{R_A + 2R_B}$$

Note that the duty cycle will always be greater than 0.5 (50%); it approaches 0.5 if  $R_A$  is selected to be much smaller than  $R_B$  (unfortunately, at the expense of supply current).