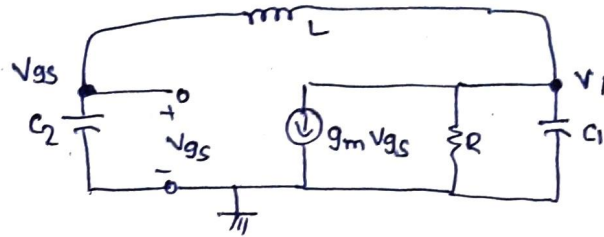
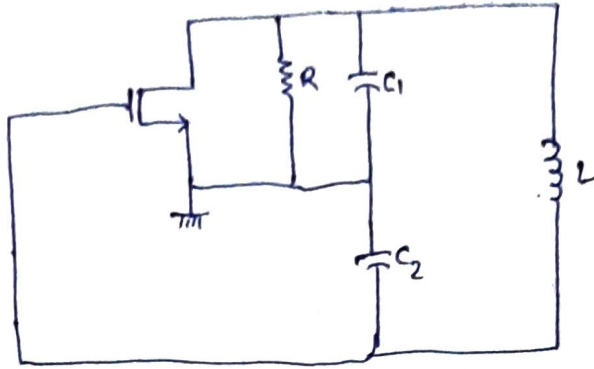


Colebit's Oscillator



$$\frac{V_1 - V_{gs}}{Ls}$$

$$\frac{V_1 - V_{gs}}{Ls} + g_m V_{gs} + \frac{V_1}{R} + V_1 C_1 s = 0$$

$$\frac{V_1 - V_{gs}}{Ls} = V_{gs} C_2 s$$

$$\Rightarrow \frac{V_1}{Ls} = V_{gs} \left(\frac{1}{Ls} + C_2 s \right)$$

$$V_1 = V_{gs} (1 + LC_2 s^2)$$

$$\frac{V_{gs} (1 + LC_2 s^2) - V_{gs}}{Ls} + g_m V_{gs} + \frac{V_{gs} (1 + LC_2 s^2)}{R} + V_{gs} C_1 s = 0$$

$$\text{as } V_{gs} \neq 0$$

$$C_2 s + g_m + (1 + LC_2 s^2) \left(\frac{1}{R} + C_1 s \right) = 0$$

$$s = j\omega$$

$$j\omega C_2 + g_m + (1 - LC_2 \omega^2) \left(\frac{1}{R} + j\omega C_1 \right) = 0$$

$$g_m + \frac{(1 - LC_2 \omega^2)}{R} + j \left(\omega C_2 + \omega C_1 (1 - LC_2 \omega^2) \right) = 0$$

making imaginary part = 0.

$$\omega C_2 = -\omega C_1 (1 - LC_2 \omega^2)$$

$$\omega_{osc} = \sqrt{\frac{C_1 + C_2}{LC_1 C_2}}$$

$$\omega C_2 + \omega C_1 - \omega^3 LC_1 C_2 = 0$$

$$\omega_0 = \sqrt{\frac{C_1 + C_2}{LC_1 C_2}}$$

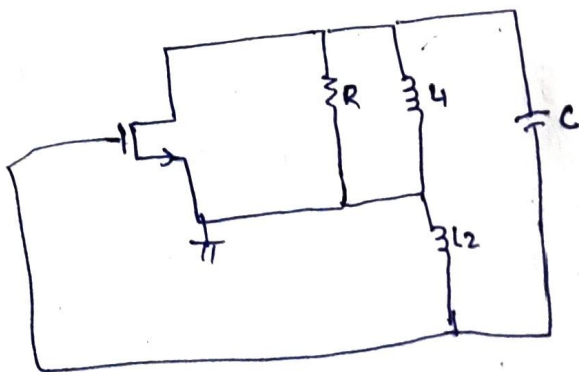
$$g_m + \frac{1 - LC_2 \left(\frac{C_1 C_2}{LC_1 C_2} \right)}{R} = 0$$

$$g_m + \frac{1 - \frac{(C_1 + C_2)}{C_1}}{R} = 0$$

$$g_m R = \frac{C_2}{C_1}$$

$$g_m = \frac{(C_1 + C_2)}{R} = 0$$

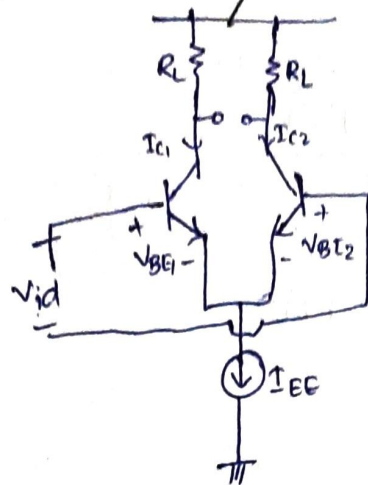
Hartley Oscillator



$$\omega_0 = \sqrt{\frac{1}{C(L_1 + L_2)}}$$

$$g_m R = \frac{L_1}{L_2}$$

Analog Multiplier / 2-Quadrant Multiplier



$$V_{id} - V_{BE1} + V_{BE2} = 0$$

$$I_{C1} = I_{S1} e^{\frac{2 V_{BE1}}{K T}}$$

$$I_{C2} = I_{S2} e^{\frac{2 V_{BE2}}{K T}}$$

As $Q_1 \equiv Q_2$ $I_{S1} = I_{S2}$

I_S = saturation current.

$$V_{id} = V_{BE1} - V_{BE2}$$

$$= \frac{K T}{2} \ln \frac{I_{C1}}{I_{S1}} - \frac{K T}{2} \ln \frac{I_{C2}}{I_{S2}}$$

$$V_{id} = V_T \ln \frac{I_{C1}}{I_{C2}}$$

$$\frac{K T}{2} = V_T = 26 \text{ mV}$$

↓
Thermal Voltage.

$$I_{C1} + I_{C2} = I_{EE}$$

$$I_{C2} e^{\frac{V_{id}}{V_T}} + I_{C2} = I_{EE}$$

$$I_{C2} \left(1 + e^{\frac{V_{id}}{V_T}} \right) = I_{EE}$$

$$I_{C2} = \frac{I_{EE}}{1 + e^{\frac{V_{id}}{V_T}}}$$

$$I_{C1} = \frac{I_{EE}}{1 + e^{-\frac{V_{id}}{V_T}}}$$

$$V_o = \Delta I_C R_L$$

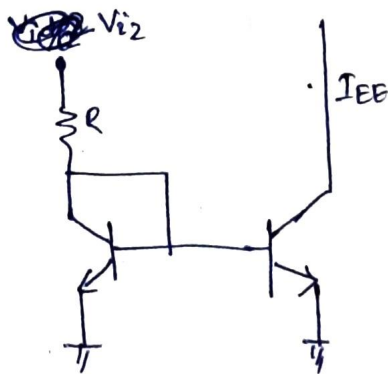
$$= \left(\frac{I_{EE}}{1 + e^{-\frac{V_{id}}{V_T}}} - \frac{I_{EE}}{1 + e^{\frac{V_{id}}{V_T}}} \right) R_L$$

$$I_{EE} \left\{ \frac{1 + e^{\frac{V_{id}}{V_T}} - 1 - e^{-\frac{V_{id}}{V_T}}}{\left(1 + e^{\frac{V_{id}}{V_T}}\right) \left(1 + e^{-\frac{V_{id}}{V_T}}\right)} \right\} R_L$$

$$= I_{EE} \left(\frac{e^{\frac{V_{id}}{V_T}} - e^{-\frac{V_{id}}{V_T}}}{2 + e^{\frac{V_{id}}{V_T}} + e^{-\frac{V_{id}}{V_T}}} \right) R_L$$

$$V_o = I_{EE} \left(\frac{\left(e^{\frac{V_{id}}{2V_T}}\right)^2 - \left(e^{-\frac{V_{id}}{2V_T}}\right)^2}{\left(e^{\frac{V_{id}}{2V_T}}\right)^2 + \left(e^{-\frac{V_{id}}{2V_T}}\right)^2 + 2e^{\frac{V_{id}}{2V_T}} e^{-\frac{V_{id}}{2V_T}}} \right) R_L$$

$$V_o = I_{EE} \frac{e^{\frac{V_{id}}{2V_T}} - e^{-\frac{V_{id}}{2V_T}}}{e^{\frac{V_{id}}{2V_T}} + e^{-\frac{V_{id}}{2V_T}}} \times R_L$$



Replacing with current mirrors

Condition must satisfy

- i) $V_{i2} > V_{BE}$
- ii) $V_{id} \ll 2V_T$

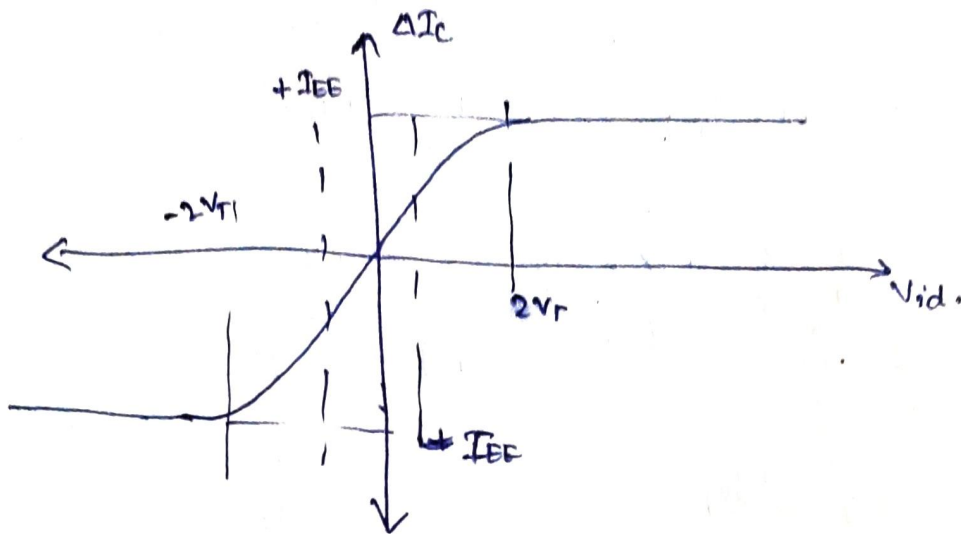
$$V_o = I_{EE} \tanh \left(\frac{V_{id}}{2V_T} \right) \times R_L$$

$$\approx I_{EE} \left(\frac{V_{id}}{2V_T} \right) \times R_L$$

$$V_o \approx \frac{V_{i2} - V_{EE}}{R} \times \frac{V_{id}}{2V_T} \times R_L$$

2-Quadrant Multiplier

V_{i2} has to be +ve
& V_{id} can be +ve or -ve.



Q. For the 2-quadrant multiplier, find the magnitude of dc differential voltage that is required to cause the slope of $(\Delta I_c \text{ vs } V_{id})$ to change by 1% from that of origin.

Soln:-

$$\frac{\partial \Delta I_c}{\partial V_{id}} = ??$$

$$\Delta I_c = I_{EE} \tanh \frac{V_{id}}{2V_T}$$

$$m_1 - m_0 = 0.01 m_0$$

$$\Delta I_c = I_{EE} \frac{e^{\frac{V_{id}}{2V_T}} - e^{-\frac{V_{id}}{2V_T}}}{e^{\frac{V_{id}}{2V_T}} + e^{-\frac{V_{id}}{2V_T}}}$$

$$= I_{EE} \frac{e^{\frac{V_{id}}{V_T}} - 1}{e^{\frac{V_{id}}{V_T}} + 1}$$

$$\frac{\partial \Delta I_c}{\partial V_{id}} = I_{EE} \frac{\partial}{\partial V_{id}} (e^{\frac{V_{id}}{V_T}} - 1) \times \frac{1}{(e^{\frac{V_{id}}{V_T}} + 1)} + I_{EE} \frac{\partial}{\partial V_{id}} \left(\frac{1}{e^{\frac{V_{id}}{V_T}} + 1} \right)$$

$$= I_{EE} \frac{\frac{1}{V_T} e^{\frac{V_{id}}{V_T}}}{(e^{\frac{V_{id}}{V_T}} + 1)} + I_{EE} \left(\frac{1}{e^{\frac{V_{id}}{V_T}} + 1} \right)^2 \times \frac{1}{V_T} \times (e^{\frac{V_{id}}{V_T}} - 1)$$

$$= \frac{I_{EE}}{V_T} \left[\frac{1}{(1 + e^{\frac{v_{id}}{V_T}})} - \frac{(e^{\frac{v_{id}}{V_T}} - 1)}{(1 + e^{\frac{v_{id}}{V_T}})^2} \right] e^{\frac{v_{id}}{V_T}}$$

$$= \frac{I_{EE}}{V_T} e^{\frac{v_{id}}{V_T}} \left[\frac{1 + e^{\frac{v_{id}}{V_T}} - e^{\frac{-v_{id}}{V_T}} + 1}{(1 + e^{\frac{v_{id}}{V_T}})^2} \right]$$

$$\frac{\partial I_C}{\partial v_{id}} = \frac{I_{EE}}{V_T} \frac{2 e^{\frac{v_{id}}{V_T}}}{(1 + e^{\frac{v_{id}}{V_T}})^2} \bigg|_{v_{id}=0} = \frac{I_{EE}}{2V_T} \quad \downarrow m_0$$

$$m_1 - m_0 = -0.01 m_0$$

$$\frac{I_{EE}}{V_T} \frac{2 e^{\frac{v_{id}}{V_T}}}{(1 + e^{\frac{v_{id}}{V_T}})^2} = -1.01 \frac{I_{EE}}{2V_T}$$

$$e^{\frac{v_{id}}{V_T}} = x$$

$$\frac{4x}{(1+x)^2} = -1.01$$

$$x = 1.2$$

$$x = 0.8$$

$$0. - 4x = 1.01 (1+x)^2$$

$$1.01 x^2 + (2x)1.01 + 1.01 + 4x = 0$$

$$1.01 x^2 + (0.1) 2x + 1.01 = 0$$

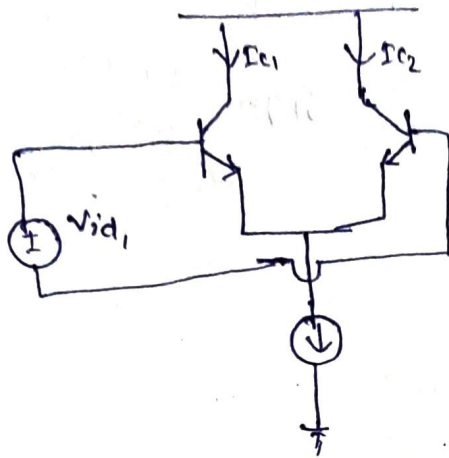
$$1.01 x^2 + 0.2 x + 1.01 = 0$$

$$1.01 x^2 + 0.2 x + 1.01 = 0 \quad x = \frac{-0.2 \pm \sqrt{0.04 - 4 \times 1.0201}}{2}$$

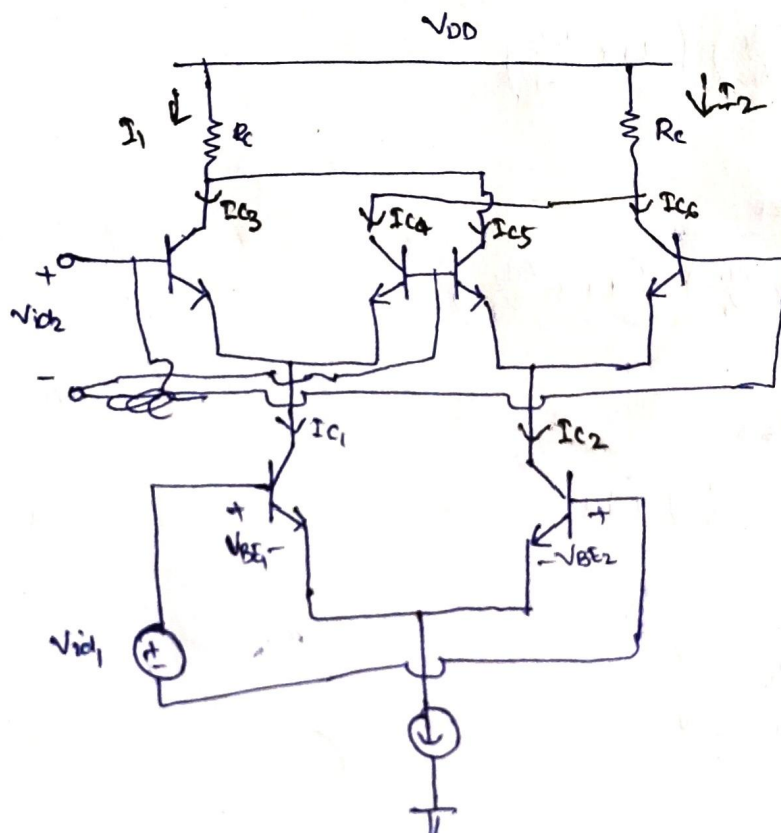
$$x = \frac{-0.2 \pm \sqrt{3.9204 - 4.0804}}{2} = \frac{-0.2 \pm 0.5 \sqrt{-4.0404}}{2}$$

$$= -0.1 \pm j$$

$$= -0.1 \pm 0.4$$



$$\Delta I_C = I_{EE} \tanh \frac{V_{id1}}{2V_T}$$



$$V_{id1} = V_{BE1} - V_{BE2}$$

$$V_{id2} = V_{BE3} - V_{BE4}$$

$$V_{id2} = V_{BE6} - V_{BE5}$$

$$I_{C1} = I_{C2} e^{\frac{V_{id}}{V_T}}$$

$$I_{C1} = \frac{I_{EE}}{1 + e^{-\frac{V_{id1}}{V_T}}}$$

$$I_{C2} = \frac{I_{EE}}{1 + e^{\frac{V_{id1}}{V_T}}}$$

$$I_{C3} = \frac{I_{C1}}{1 + e^{-\frac{V_{id2}}{V_T}}}$$

$$I_{C4} = \frac{I_{C1}}{1 + e^{\frac{V_{id2}}{V_T}}}$$

$$I_{C5} = \frac{I_{C2}}{1 + e^{\frac{V_{id2}}{V_T}}}$$

$$I_{C6} = \frac{I_{C2}}{1 + e^{-V_{id2}/2}}$$

Sign changes because

$$V_{id2} = V_{B6C} - V_{B5C}$$

$$I_{C3} = \frac{I_{EE}}{\left(1 + e^{\frac{V_{id1}}{V_T}}\right) \left(1 + e^{\frac{V_{id2}}{V_T}}\right)}$$

$$I_{C4} = \frac{I_{EE}}{\left(1 + e^{-\frac{V_{id1}}{V_T}}\right) \left(1 + e^{\frac{V_{id2}}{V_T}}\right)}$$

$$I_{C5} = \frac{I_{EE}}{\left(1 + e^{\frac{V_{id1}}{V_T}}\right) \left(1 + e^{-\frac{V_{id2}}{V_T}}\right)}$$

$$I_{C6} = \frac{I_{EE}}{\left(1 + e^{-\frac{V_{id1}}{V_T}}\right) \left(1 + e^{-\frac{V_{id2}}{V_T}}\right)}$$

$$V_{id1} = V_1$$

$$V_{id2} = V_2$$

$$I_1 = I_{C3} + I_{C5}$$

$$= I_{EE} \left[\frac{1}{\left(1 + e^{-V_1/V_T}\right) \left(1 + e^{-V_2/V_T}\right)} + \frac{1}{\left(1 + e^{V_1/V_T}\right) \left(1 + e^{V_2/V_T}\right)} \right]$$

$$I_1 = I_{EE} \frac{1}{\left(1 + e^{V_1/V_T}\right) \left(1 + e^{V_2/V_T}\right)} \times \left(e^{V_1/V_T} e^{V_2/V_T} + 1\right)$$

$$I_2 = I_{EE} \frac{1}{\left(1 + e^{-V_1/V_T}\right) \left(1 + e^{-V_2/V_T}\right)} \left(e^{-V_1/V_T} e^{-V_2/V_T} + 1\right)$$

$$\Delta I = I_1 - I_2 = I_{EE} \left(\tanh \frac{V_1}{2V_T} - \tanh \frac{V_2}{2V_T} \right)$$

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$$\Delta I \approx I_{EE} \left(\frac{V_1}{2V_T} - \frac{V_2}{2V_T} \right)$$