Pin = Pe + Prad

=
$$\frac{1}{2}$$
 |Pin|² (Re + Read)

$$\frac{Q_p(\theta,\phi)}{Pin}$$

$$(40.0,0) = \frac{4\pi f^{2}(0)}{\int f^{2}(0) d^{32}}$$

$$\frac{4\pi \sin^2 0}{\int_{0.0}^{\pi} \int_{0.0}^{\pi} \sin^3 \theta \, d\theta \, d\phi} = \frac{4\pi \sin^2 \theta}{2\pi \times 4/3}$$
= 1.5 $\sin^2 \theta$

$$G_{\alpha}(\theta,\phi) = \frac{4\pi \frac{\cos^2(\pi_{\chi}\cos\theta)}{\sin^2\theta}}{\frac{2\pi}{\sin^2\theta}\frac{\pi}{\cos^2(\pi_{\chi}\cos\theta)\,d\theta\,d\phi}}$$

$$P_{r} = \frac{E^2 \lambda}{600 \, \text{Ti}^2}$$

$$P_{a \cdot g} = \frac{E^2}{2 \, \text{Ti}} = \frac{E^2}{200 \, \text{Ti}}$$

$$A_{e} = \frac{\lambda^{2}}{4\pi} D$$

Half-wave Dipole Antenna BED OFBET 0 4 0 4 211 Azs = 410 e - 1 BY cos (1/2 cos 0) ornie B anc Hos = 310 e-3 pr cos (1/21050) ; Eas = 7 Has. Pavg = $\frac{1}{2}\eta$ $\left[H\phi s\right]^2 a_r = \frac{\eta^{-1}o^2 \cos^2\left(\frac{\eta_2\cos\theta}{2\cos^2\left(\frac{\eta_2\cos\theta}{2\cos\theta}\right)}\right)}{8\eta^2 \eta^2 \sin^2\theta}$ Prad = | Parg ds Rad = 2 Prad = 73 52 Prad = 12 Rad Prad = 12 Prad = 12 Prad Prad = 36.56 Jo2 $|H\phi s| = \frac{T_0 \cos(\sqrt{\gamma_2}\cos\theta)}{2\pi \sin\theta}$ $|E\theta s| = \frac{\gamma_0 T_0 \cos(\sqrt{\gamma_2}\cos\theta)}{2\pi \sin\theta}$ Zin = Rin + j Xin Quarter - wave Monopole 7in: 3615+ j21.25 32 Prad = 18.28 102 Rrad = 2 Prad = 36.5 7. Small loop Antenna Ers p Eps= Hes = Hos =0 Hes = - Eos $|E\phi s| = \eta \frac{\pi \tau_0}{s} \frac{s}{J^2} \sin \theta$ $|H\phi s| = \frac{\pi \tau_0}{r} \frac{s}{J^2} \sin \theta$ 1762 ; For N-twon , S= Nn 62. For a single 4com, S: Read = $\frac{320 \, \text{n}^4 \, \text{s}^2}{4^4}$

Standing

Antenna

$$S = \frac{7 - 70}{7 + 70}$$

The standing in t

7km = 73 + 5 42.5

Zin = 36.5 +j 21.25 _ Quanter wave

Half wave

Slanding wave Tatio

$$V(\theta, \phi) = \tau^2 P_{avg} \cdot (w/s\tau)$$
 $P_{rad} = \oint_{S} P_{avg} \cdot ds = \oint_{S} P_{avg} \tau^2 \sin \theta \cdot d\theta \cdot d\phi$
 $P_{rad} = \int_{S} U(\theta, \phi) \sin \theta \cdot d\theta \cdot d\phi$
 $\int_{S} P_{avg} \cdot ds = \sin \theta \cdot d\theta \cdot d\phi$

in a particular - measure of concentration of the radiated Directive Gain

$$G_{d}(\theta,\phi) = \frac{U(\theta,\phi)}{Vavg} = \frac{A\pi U(\theta,\phi)}{Prod}$$

antenna pattern. The directive ad(0,0) depends on gain

Directivity

for Hentizian dipole,

For of dipole, ad (OIP) = TRIAN D: 1.64

Antenna

Hestzian Dipole

$$E_{\theta S} = \eta \frac{10 d!}{4\pi} \sin \theta \left[\frac{d\beta}{r} + \frac{1}{r^2} - \frac{j}{\beta r \theta} \right] e^{-j\beta r}$$

$$P_{\text{rad}} = \frac{T_0^2 \Pi \eta}{3} \left[\frac{d\ell}{A} \right]^2 = 40 \, \Pi^2 \left[\frac{d\ell}{A} \right]^2 J_0^2$$

$$R_{\text{rad}} = \frac{3 \, \text{rms}}{3} \, R_{\text{rad}}^2$$

Read =
$$80\pi^2 \left[\frac{dl}{d}\right]^2$$
.

lapl.

For Hentzian dipole,

Antenna friss equation Pr = Gar Gas (1)2 Ps adr - Difrective gain (Received) Received Directive gain ad1 = (Inaumitted) Pt = Pr [4nr] - Gar Gar. -total t-naw mitted power. $G_{at} = \frac{4\pi U}{P_a} = \frac{4\pi s^2 P_{avg}}{P_a}$ Pavg. = Gat Pt 41172 $P_r = P_{avg}$. Aer = $\frac{\lambda^2}{4\pi} Q_{or} P_{avg}$. Pr = $\frac{\lambda^2}{(4\pi r)^2}$ GD* GDF P2. Pr = Gar Gat (dails) 2 Pt. Triis transmission formule.

B HLBM.

Aem =
$$\frac{d^2}{4\pi}$$
 Do

 $P_r = P_{\ell}$ (a) (4) $\left(\frac{1}{4\pi R}\right)^2$.