EES Ver. 10.550: #1430: Mech. Engin., Engineering College in Aarhus, Aarhus, Denmark

Beregning af Phi ud fra målte temperaturer i systemet.

Dette bestemmes ud fra energibalancerne for kølemidlet og luften, over fordamperen:

 $q_{mR} \cdot (h_{R;4} - h_{R;1}) + \Phi_{0;R} = 0$  Energibalance for kølemidlet over fordamper

 $q_{mL} \cdot (h_{L;1} - h_{L;2}) - \Phi_{0;L} = 0$  Energibalance for luften over fordamper

----- Måledata indtastes her: -----

p<sub>R:f</sub> = (1,31 + 1) · 1 [bar] tryk i kølemiddel på fordampersiden

p<sub>R:k</sub> = (8,65 + 1) · 1 [bar] tryk i kølemiddel på kondensatorsiden

t<sub>R;3</sub> = 29,4 [C] temperatur i kølemiddel efter kondensator

t<sub>R;1</sub> = 1,82 [C] temperatur i kølemiddel efter fordamper

 $p_L = 1$  [bar] *luftens tryk* 

t<sub>L;1</sub> = 3,9 [C] luftens temperatur før fordamper

t<sub>L;2</sub> = 0,07 [C] luftens temperatur efter fordamper

rpm = 3977 · 
$$\left| 0.016666667 \cdot \frac{1/s}{1/min} \right|$$
 kompressors rpm

c<sub>L</sub> = 3 [m/s] strømningshastighed af luft over fordamper

 $A_f = \left[\frac{0.21}{2}\right]^2 \cdot \pi - 0.083^2$  Tværsnitsareal af luftens vej over fordamper

----- Alt herunder beregnes -----

-----Entalpier:----

Kølemiddel

der antages at entalpien er konstant over ekspansionventilen

 $h_{R;4} = h$  (R134a;  $T = t_{R;3}$ ;  $P = p_{R;k}$ ) Entalpi af kølemidlet før fordamper beregnet ud fra tryk og temp efter kondensator.  $h_{R;4} = h_{R;3}$ 

 $h_{R;1} = h (R134a; T = t_{R;1}; P = p_{R;f})$  Entalpi af kølemidlet efter fordamper

 $h_{L;1} = h (Air_{ha}; T = t_{L;1}; P = p_L)$  Entalpi af luft før fordamper

 $h_{L;2} = h (Air_{ha}; T = t_{L;2}; P = p_L)$  Entalpi af luft efter fordamper

----- massestrømme: -----

Luft

Luft

$$t_{L;m} = \frac{t_{L;1} + t_{L;2}}{2}$$
 luftens middeltemperatur

$$\rho_L = \rho \left( Air_{ha}; T = t_{L:m}; P = p_L \right)$$
 luftens densitet

$$q_{VL} = c_L \cdot A_f$$
 luftens volumenstrøm

$$q_{mL} = q_{VL} \cdot \rho_L$$
 luftens massestrøm

$$disp = 5.08 \cdot \left| 0.000001 \cdot \frac{m3}{cm3} \right|$$

## kølemiddel

$$q_{mR} = q_{vr} \cdot \rho_{r1}$$
 massestrøm af kølemiddel

$$q_{vr} = q_{vs} \cdot \eta_v$$
 volumenstrøm af kølemiddel

$$\eta_{v} = -0.01696 \cdot \frac{p_{R;k}}{p_{R;f}} + 0.79144$$
 volumetrisk virkningsgrad

$$\rho_{r1} = \rho \left( R134a ; T = t_{R;1}; P = p_{R;f} \right)$$
 densitet af kølemiddel før kompressor

$$t_{fordamp} = T_{sat} (R134a; P = p_{R;f})$$
 fordampningstemperatur

$$t_{kondens} = T_{sat} (R134a; P = p_{R;k})$$
 kondenseringstemperatur

overhedning = 
$$t_{R;1} - t_{fordamp}$$
 overhedning gennem fordamper

## usikkerheder

$$U_t = 1,397505$$
 [K]

$$U_p = 0.065765$$
 [bar]

## Unit Settings: SI C bar J mass deg

Variable±Uncertainty	Partial derivative	% of uncertainty
overhedning = 8,207±1,583 [C]		
$p_{R,f} = 2.31 \pm 0.06577$ [bar]	$\partial$ overhedning $/\partial p_{R,f} = -11,32$	22,09 %
$p_{R,k} = 9.65 \pm 0.06577$ [bar]	$\partial$ overhedning $/\partial p_{R,k} = 0$	0,00 %
$t_{L,1} = 3.9 \pm 1.398$ [C]	$\partial$ overhedning $/\partial t_{L,1} = 0$	0,00 %
$t_{L,2} = 0.07 \pm 1.398$ [C]	$\partial$ overhedning $/\partial t_{L,2} = 0$	0,00 %
t <sub>R,1</sub> = 1,82±1,398 [C]	$\partial$ overhedning $/\partial t_{R,1} = 1$	77,91 %
$t_{R,3} = 29.4 \pm 1.398$ [C]	$\partial$ overhedning $/\partial t_{R,3} = 0$	0,00 %
$\Phi_{0,L} = 406,2\pm209,6$ [W]		
$p_{R,f} = 2.31 \pm 0.06577$ [bar]	$\partial \Phi_{0,L}/\partial p_{R,f} = 0$	0,00 %
$p_{R,k} = 9,65\pm0,06577$ [bar]	$\partial \Phi_{0,L}/\partial p_{R,k} = 0$	0,00 %
$t_{L,1} = 3.9 \pm 1.398$ [C]	$\partial \Phi_{0,L}/\partial t_{L,1} = 105,3$	49,30 %
$t_{L,2} = 0.07 \pm 1.398$ [C]	$\partial \Phi_{0,L}/\partial t_{L,2} = -106,8$	50,70 %
t <sub>R,1</sub> = 1,82±1,398 [C]	$\partial \Phi_{0,L}/\partial t_{R,1} = 0$	0,00 %
$t_{R,3} = 29.4 \pm 1.398$ [C]	$\partial \Phi_{0,L}/\partial t_{R,3} = 0$	0,00 %
$\Phi_{0,R} = 431,5\pm14,98$ [W]		
$p_{R,f} = 2.31 \pm 0.06577$ [bar]	$\partial \Phi_{0,R} / \partial p_{R,f} = 212,3$	86,92 %
$p_{R,k} = 9,65\pm0,06577$ [bar]	$\partial \Phi_{0,R} / \partial p_{R,k} = -4,392$	0,04 %
$t_{L,1} = 3.9 \pm 1.398$ [C]	$\partial \Phi_{0,R} / \partial t_{L,1} = 0$	0,00 %
$t_{L,2} = 0.07 \pm 1.398$ [C]	$\partial \Phi_{0,R} / \partial t_{L,2} = 0$	0,00 %
$t_{R,1} = 1.82 \pm 1.398$ [C]	$\partial \Phi_{0,R} / \partial t_{R,1} = 0.2843$	0,07 %

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 $t_{R,3} = 29,4\pm1,398$  [C]

 $\partial \Phi_{0,R} / \partial t_{R,3} = -3,86$ 

12,97 %

No unit problems were detected.

$$\begin{split} &A_f = 0,02775 \text{ [m}^2] \\ &\eta_V = 0,7206 \\ &h_{R,1} = 401932 \text{ [J/kg]} \\ &\Phi_{0,L} = 406,2 \text{ [W]} \\ &p_{R,f} = 2,31 \text{ [bar]} \\ &q_{mR} = 0,002679 \text{ [kg/s]} \\ &q_{vs} = 0,0003367 \text{ [m3/s]} \\ &rpm = 66,28 \text{ [1/s]} \\ &t_{L,1} = 3,9 \text{ [C]} \\ &t_{R,1} = 1,82 \text{ [C]} \\ &U_p = 0,06577 \text{ [bar]} \end{split}$$

 $\begin{array}{l} c_L = 3 \text{ [m/s]} \\ h_{L,1} = 277152 \text{ [J/kg]} \\ h_{R,4} = 240851 \text{ [J/kg]} \\ \Phi_{0,R} = 431,5 \text{ [W]} \\ p_{R,k} = 9,65 \text{ [bar]} \\ q_{VL} = 0,08324 \text{ [m3/s]} \\ p_L = 1,267 \text{ [kg/m}^3] \\ t_{fordamp} = -6,387 \text{ [C]} \\ t_{L,2} = 0,07 \text{ [C]} \\ t_{R,3} = 29,4 \text{ [C]} \\ U_t = 1,398 \text{ [K]} \end{array}$ 

 $\begin{array}{l} \text{disp} &= 0,00000508 \text{ [m}^3] \\ \text{h}_{\text{L},2} &= 273300 \text{ [J/kg]} \\ \text{overhedning} &= 8,207 \text{ [C]} \\ \text{p}_{\text{L}} &= 1 \text{ [bar]} \\ \text{q}_{\text{mL}} &= 0,1055 \text{ [kg/s]} \\ \text{q}_{\text{vr}} &= 0,0002426 \text{ [m3/s]} \\ \text{p}_{\text{r1}} &= 11,04 \text{ [kg/m}^3] \\ \text{t}_{\text{kondens}} &= 38,05 \text{ [C]} \\ \text{t}_{\text{L,m}} &= 1,985 \text{ [C]} \\ \text{underkøl} &= 8,651 \text{ [C]} \end{array}$ 

No unit problems were detected.

## **KEY VARIABLES**

 $\Phi_{0,L}$  = 406,2 [W] kuldeydelse fra luft overhedning = 8,207 [C]

 $\Phi_{0,R} = 431,5 [W]$  kuldeydelse fra kølemiddel