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Beregning af Phi ud fra målte temperaturer i systemet.

Dette bestemmes ud fra energibalancerne for kølemidlet og luften, over fordamperen:

 $q_{mR} \cdot (h_{R;4} - h_{R;1}) + \Phi_{0;R} = 0$  Energibalance for kølemidlet over fordamper

 $q_{mL}$  ·  $(h_{L;1}-h_{L;2})-\Phi_{0;L}$  = 0 Energibalance for luften over fordamper

----- Måledata indtastes her: -----

p<sub>R:f</sub> = (2,34 + 1) · 1 [bar] tryk i kølemiddel på fordampersiden

 $p_{R:k} = (10,3 + 1) \cdot 1$  [bar] tryk i kølemiddel på kondensatorsiden

t<sub>R:3</sub> = 34,7 [C] temperatur i kølemiddel efter kondensator

t<sub>R;1</sub> = 11,5 [C] temperatur i kølemiddel efter fordamper

 $p_L = 1$  [bar] luftens tryk

t<sub>L;1</sub> = 19,9 [C] *luftens temperatur før fordamper* 

t<sub>L;2</sub> = 13,9 [C] luftens temperatur efter fordamper

 $rpm = 4000 \cdot \left| 0.016666667 \cdot \frac{1/s}{1/min} \right| kompressors rpm$ 

c<sub>L</sub> = 3 [m/s] strømningshastighed af luft over fordamper

 $A_f = \left[\frac{0.21}{2}\right]^2 \cdot \pi - 0.083^2$  Tværsnitsareal af luftens vej over fordamper

----- Alt herunder beregnes -----

-----Entalpier:-----

Kølemiddel

der antages at entalpien er konstant over ekspansionventilen

 $h_{R;4} = h$  (R134a;  $T = t_{R;3}$ ;  $P = p_{R;k}$ ) Entalpi af kølemidlet før fordamper beregnet ud fra tryk og temp efter kondensator.

 $h_{R;1} = h (R134a; T = t_{R;1}; P = p_{R;t})$  Entalpi af kølemidlet efter fordamper

Luft

 $h_{L;1} = h (Air_{ha}; T = t_{L;1}; P = p_L)$  Entalpi af luft før fordamper

 $h_{L;2} = h (Air_{ha}; T = t_{L;2}; P = p_L)$  Entalpi af luft efter fordamper

----- massestrømme: -----

Luft

$$t_{L;m} = \frac{t_{L;1} + t_{L;2}}{2}$$
 luftens middeltemperatur

$$\rho_L = \rho \left( Air_{ha}; T = t_{L:m}; P = p_L \right)$$
 luftens densitet

$$q_{VL} = c_L \cdot A_f$$
 luftens volumenstrøm

$$q_{mL} = q_{VL} \cdot \rho_L$$
 luftens massestrøm

$$disp = 5.08 \cdot \left| 0.000001 \cdot \frac{m3}{cm3} \right|$$

## kølemiddel

$$q_{mR} = q_{vr} \cdot \rho_{r1}$$
 massestrøm af kølemiddel

$$q_{vr} = q_{vs} \cdot \eta_v$$
 volumenstrøm af kølemiddel

$$\eta_v = -0.01696 \cdot \frac{p_{R;k}}{p_{R;f}} + 0.79144$$
 volumetrisk virkningsgrad

$$\rho_{r1} = \rho \left( R134a ; T = t_{R;1}; P = p_{R;f} \right)$$
 densitet af kølemiddel før kompressor

$$t_{fordamp} = T_{sat} (R134a; P = p_{R;f})$$
 fordampningstemperatur

$$t_{kondens} = T_{sat} (R134a; P = p_{R;k})$$
 kondenseringstemperatur

overhedning = 
$$t_{R;1} - t_{fordamp}$$
 overhedning gennem fordamper

## usikkerheder

$$U_t = 1,397505$$
 [K]

$$U_p = 0.065765$$
 [bar]

## Unit Settings: SI C bar J mass deg

Variable±Uncertainty	Partial derivative	% of uncertainty
overhedning = 7,831±1,506 [C]		
$p_{R,f} = 3.34 \pm 0.06577$ [bar]	$\partial$ overhedning $/\partial p_{R,f} = -8,519$	13,85 %
$p_{R,k} = 11,3\pm0,06577$ [bar]	$\partial$ overhedning $/\partial p_{R,k} = 0$	0,00 %
$t_{L,1} = 19,9\pm1,398$ [C]	$\partial$ overhedning $/\partial t_{L,1} = 0$	0,00 %
$t_{L,2} = 13.9 \pm 1.398$ [C]	$\partial$ overhedning $/\partial t_{L,2} = 0$	0,00 %
t <sub>R,1</sub> = 11,5±1,398 [C]	$\partial$ overhedning $/\partial t_{R,1} = 1$	86,15 %
$t_{R,3} = 34.7 \pm 1.398$ [C]	$\partial$ overhedning $/\partial t_{R,3} = 0$	0,00 %
$\Phi_{0,L} = 603.7 \pm 198.9 \text{ [W]}$		
$p_{R,f} = 3.34 \pm 0.06577$ [bar]	$\partial \Phi_{0,L}/\partial p_{R,f} = 0$	0,00 %
$p_{R,k} = 11,3\pm0,06577$ [bar]	$\partial \Phi_{0,L}/\partial p_{R,k} = 0$	0,00 %
$t_{L,1} = 19,9\pm1,398$ [C]	$\partial \Phi_{0,L}/\partial t_{L,1} = 99,59$	48,97 %
$t_{L,2} = 13,9 \pm 1,398$ [C]	$\partial \Phi_{0,L}/\partial t_{L,2} = -101,7$	51,03 %
t <sub>R,1</sub> = 11,5±1,398 [C]	$\partial \Phi_{0,L}/\partial t_{R,1} = 0$	0,00 %
$t_{R,3} = 34.7 \pm 1.398$ [C]	$\partial \Phi_{0,L}/\partial t_{R,3} = 0$	0,00 %
$\Phi_{0,R} = 623,5\pm16,02$ [W]		
$p_{R,f} = 3.34 \pm 0.06577$ [bar]	$\partial \Phi_{0,R} / \partial p_{R,f} = 210,7$	74,77 %
$p_{R,k} = 11,3\pm0,06577$ [bar]	$\partial \Phi_{0,R} / \partial p_{R,k} = -4,279$	0,03 %
$t_{L,1} = 19,9\pm1,398$ [C]	$\partial \Phi_{0,R} / \partial t_{L,1} = 0$	0,00 %
$t_{L,2} = 13,9 \pm 1,398$ [C]	$\partial \Phi_{0,R} / \partial t_{L,2} = 0$	0,00 %
$t_{R,1} = 11,5\pm1,398$ [C]	$\partial \Phi_{0,R} / \partial t_{R,1} = 0,4818$	0,18 %

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 $t_{R,3} = 34,7\pm1,398$  [C]

 $\partial \Phi_{0,R} / \partial t_{R,3} = -5,736$ 

25,02 %

No unit problems were detected.

 $\begin{array}{lll} A_f = 0,02775 & [m^2] \\ \eta_V = 0,7341 & I \\ h_{R,1} = 407830 & [J/kg] & I \\ \Phi_{0,L} = 603,7 & [W] & I \\ p_{R,f} = 3,34 & [bar] & I \\ q_{mR} = 0,003915 & [kg/s] & I \\ q_{vs} = 0,0003387 & [m3/s] & I \\ rpm = 66,67 & [1/s] & I \\ t_{L,1} = 19,9 & [C] & I \\ t_{R,1} = 11,5 & [C] & I \\ U_p = 0,06577 & [bar] & I \\ \end{array}$ 

 $\begin{array}{l} c_L = 3 \text{ [m/s]} \\ h_{L,1} = 293246 \text{ [J/kg]} \\ h_{R,4} = 248542 \text{ [J/kg]} \\ \Phi_{0,R} = 623,5 \text{ [W]} \\ p_{R,k} = 11,3 \text{ [bar]} \\ q_{VL} = 0,08324 \text{ [m3/s]} \\ \rho_L = 1,202 \text{ [kg/m}^3] \\ t_{fordamp} = 3,669 \text{ [C]} \\ t_{L,2} = 13,9 \text{ [C]} \\ t_{R,3} = 34,7 \text{ [C]} \\ U_t = 1,398 \text{ [K]} \end{array}$ 

 $\begin{array}{l} \text{disp} &= 0,00000508 \text{ [m}^3] \\ \text{h}_{\text{L},2} &= 287210 \text{ [J/kg]} \\ \text{overhedning} &= 7,831 \text{ [C]} \\ \text{p}_{\text{L}} &= 1 \text{ [bar]} \\ \text{q}_{\text{mL}} &= 0,1 \text{ [kg/s]} \\ \text{q}_{\text{vr}} &= 0,0002486 \text{ [m}3/\text{s]} \\ \text{p}_{\text{r1}} &= 15,75 \text{ [kg/m}^3] \\ \text{t}_{\text{kondens}} &= 43,98 \text{ [C]} \\ \text{t}_{\text{L,m}} &= 16,9 \text{ [C]} \\ \text{underkøl} &= 9,276 \text{ [C]} \end{array}$ 

No unit problems were detected.

## **KEY VARIABLES**

 $\Phi_{0,L}$  = 603,7 [W] kuldeydelse fra luft overhedning = 7,831 [C]

 $\Phi_{0,R} = 623,5 \text{ [W]}$  kuldeydelse fra kølemiddel