EES Ver. 10.550: #1430: Mech. Engin., Engineering College in Aarhus, Aarhus, Denmark

Beregning af Phi ud fra målte temperaturer i systemet.

Dette bestemmes ud fra energibalancerne for kølemidlet og luften, over fordamperen:

 $q_{mR} \cdot (h_{R;4} - h_{R;1}) + \Phi_{0;R} = 0$ Energibalance for kølemidlet over fordamper

 $q_{mL} \cdot (h_{L;1} - h_{L;2}) - \Phi_{0;L} = 0$ Energibalance for luften over fordamper

----- Måledata indtastes her: -----

 $p_{R;f} = (1,46 + 1) \cdot 1$ [bar] tryk i kølemiddel på fordampersiden

 $p_{R;k} = (8,47 + 1) \cdot 1$ [bar] tryk i kølemiddel på kondensatorsiden

t_{R;3} = 26,5 [C] temperatur i kølemiddel efter kondensator

t_{R;1} = 2,21 [C] temperatur i kølemiddel efter fordamper

 $p_L = 1$ [bar] luftens tryk

t_{L;1} = 2,96 [C] luftens temperatur før fordamper

 $t_{L;2} = 0.2$ [C] luftens temperatur efter fordamper

rpm = 2800 ·
$$\left| 0.016666667 \cdot \frac{1/s}{1/min} \right|$$
 kompressors rpm

c_L = 3 [m/s] strømningshastighed af luft over fordamper

 $A_f = \left[\frac{0.21}{2}\right]^2 \cdot \pi - 0.083^2$ Tværsnitsareal af luftens vej over fordamper

----- Alt herunder beregnes -----

-----Entalpier:-----

Kølemiddel

der antages at entalpien er konstant over ekspansionventilen

 $h_{R;4} = h$ (R134a; $T = t_{R;3}$; $P = p_{R;k}$) Entalpi af kølemidlet før fordamper beregnet ud fra tryk og temp efter kondensator. $h_{R;4} = h_{R;3}$

 $h_{R;1} = h (R134a; T = t_{R;1}; P = p_{R;f})$ Entalpi af kølemidlet efter fordamper

 $h_{L;1} = h (Air_{ha}; T = t_{L;1}; P = p_L)$ Entalpi af luft før fordamper

 $h_{L;2} = h (Air_{ha}; T = t_{L;2}; P = p_L)$ Entalpi af luft efter fordamper

----- massestrømme: -----

Luft

Luft

$$t_{L;m} = \frac{t_{L;1} + t_{L;2}}{2}$$
 luftens middeltemperatur

$$\rho_L = \rho \left(Air_{ha}; T = t_{L:m}; P = p_L \right)$$
 luftens densitet

$$q_{VL} = c_L \cdot A_f$$
 luftens volumenstrøm

$$q_{mL} = q_{VL} \cdot \rho_L$$
 luftens massestrøm

$$disp = 5.08 \cdot \left| 0.000001 \cdot \frac{m3}{cm3} \right|$$

kølemiddel

$$q_{mR} = q_{vr} \cdot \rho_{r1}$$
 massestrøm af kølemiddel

$$q_{vr} = q_{vs} \cdot \eta_v$$
 volumenstrøm af kølemiddel

$$\eta_{v} = -0.01696 \cdot \frac{p_{R;k}}{p_{R;f}} + 0.79144$$
 volumetrisk virkningsgrad

$$\rho_{r1} = \rho \left(R134a ; T = t_{R;1}; P = p_{R;f} \right)$$
 densitet af kølemiddel før kompressor

$$t_{fordamp} = T_{sat} (R134a; P = p_{R;f})$$
 fordampningstemperatur

$$t_{kondens} = T_{sat} (R134a; P = p_{R;k})$$
 kondenseringstemperatur

overhedning =
$$t_{R;1} - t_{fordamp}$$
 overhedning gennem fordamper

usikkerheder

$$U_t = 1,397505$$
 [K]

$$U_p = 0.065765$$
 [bar]

Unit Settings: SI C bar J mass deg

Variable±Uncertainty	Partial derivative	% of uncertainty
overhedning = 6,941±1,567 [C]		
$p_{R,f} = 2,46\pm0,06577$ [bar]	∂ overhedning $/\partial p_{R,f} = -10,78$	20,47 %
$p_{R,k} = 9.47 \pm 0.06577$ [bar]	∂ overhedning $/\partial p_{R,k} = 0$	0,00 %
$t_{L,1} = 2,96\pm1,398$ [C]	∂ overhedning $/\partial t_{L,1} = 0$	0,00 %
$t_{L,2} = 0.2 \pm 1.398$ [C]	∂ overhedning $/\partial t_{L,2} = 0$	0,00 %
$t_{R,1} = 2.21 \pm 1.398$ [C]	∂ overhedning $/\partial t_{R,1} = 1$	79,53 %
$t_{R,3} = 26.5 \pm 1.398$ [C]	∂ overhedning $/\partial t_{R,3} = 0$	0,00 %
$\Phi_{0,L} = 293,2\pm209,9$ [W]		
$p_{R,f} = 2,46\pm0,06577$ [bar]	$\partial \Phi_{0,L}/\partial p_{R,f} = 0$	0,00 %
$p_{R,k} = 9,47\pm0,06577$ [bar]	$\partial \Phi_{0,L}/\partial p_{R,k} = 0$	0,00 %
$t_{L,1} = 2,96\pm1,398$ [C]	$\partial \Phi_{0,L} / \partial t_{L,1} = 105,7$	49,50 %
$t_{L,2} = 0.2 \pm 1.398$ [C]	$\partial \Phi_{0,L}/\partial t_{L,2} = -106,7$	50,50 %
t _{R,1} = 2,21±1,398 [C]	$\partial \Phi_{0,L}/\partial t_{R,1} = 0$	0,00 %
$t_{R,3} = 26.5 \pm 1.398$ [C]	$\partial \Phi_{0,L}/\partial t_{R,3} = 0$	0,00 %
$\Phi_{0,R} = 335,3\pm10,93$ [W]		
$p_{R,f} = 2,46\pm0,06577$ [bar]	$\partial \Phi_{0,R} / \partial p_{R,f} = 154,3$	86,19 %
$p_{R,k} = 9,47\pm0,06577$ [bar]	$\partial \Phi_{0,R} / \partial p_{R,k} = -3,188$	0,04 %
$t_{L,1} = 2,96\pm1,398$ [C]	$\partial \Phi_{0,R} / \partial t_{L,1} = 0$	0,00 %
$t_{L,2} = 0.2 \pm 1.398$ [C]	$\partial \Phi_{0,R} / \partial t_{L,2} = 0$	0,00 %
$t_{R,1} = 2,21\pm1,398$ [C]	$\partial \Phi_{0,R} / \partial t_{R,1} = 0,1639$	0,04 %

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 $t_{R,3} = 26,5\pm1,398$ [C]

 $\partial \Phi_{0,R} / \partial t_{R,3} = -2,899$

13,73 %

No unit problems were detected.

$$\begin{split} A_f &= 0,02775 \text{ [m}^2] \\ \eta_V &= 0,7262 \\ h_{R,1} &= 401869 \text{ [J/kg]} \\ \Phi_{0,L} &= 293,2 \text{ [W]} \\ p_{R,f} &= 2,46 \text{ [bar]} \\ q_{mR} &= 0,00203 \text{ [kg/s]} \\ q_{vs} &= 0,0002371 \text{ [m3/s]} \\ rpm &= 46,67 \text{ [1/s]} \\ t_{L,1} &= 2,96 \text{ [C]} \\ t_{R,1} &= 2,21 \text{ [C]} \\ U_p &= 0,06577 \text{ [bar]} \end{split}$$

 $\begin{array}{l} c_L = 3 \text{ [m/s]} \\ h_{L,1} = 276206 \text{ [J/kg]} \\ h_{R,4} = 236692 \text{ [J/kg]} \\ \Phi_{0,R} = 335,3 \text{ [W]} \\ p_{R,k} = 9,47 \text{ [bar]} \\ q_{VL} = 0,08324 \text{ [m3/s]} \\ \rho_L = 1,269 \text{ [kg/m}^3] \\ t_{fordamp} = -4,731 \text{ [C]} \\ t_{L,2} = 0,2 \text{ [C]} \\ t_{R,3} = 26,5 \text{ [C]} \\ U_t = 1,398 \text{ [K]} \end{array}$

disp = 0,00000508 [m³] $\begin{aligned} h_{L,2} &= 273431 \text{ [J/kg]} \\ \text{overhedning = 6,941 [C]} \\ p_L &= 1 \text{ [bar]} \\ q_{mL} &= 0,1056 \text{ [kg/s]} \\ q_{vr} &= 0,0001721 \text{ [m3/s]} \\ p_{r1} &= 11,79 \text{ [kg/m³]} \\ t_{kondens} &= 37,36 \text{ [C]} \\ t_{L,m} &= 1,58 \text{ [C]} \\ \text{underkøl = 10,86 [C]} \end{aligned}$

No unit problems were detected.

KEY VARIABLES

 $\Phi_{0,L}$ = 293,2 [W] kuldeydelse fra luft overhedning = 6,941 [C]

 $\Phi_{0,R} = 335,3 \text{ [W]}$ kuldeydelse fra kølemiddel