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Stretchable liquid metal coaxial phase shifter

Abstract

A stretchable liquid metal coaxial phase shifter comprising opposingly located attachment disks which are attached to opposingly located shield interface rings which are open ended cylinders defining an interior space and exterior surface.

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Background/Summary

RELATED APPLICATIONS (1) This application claims priority to U.S. Provisional Application No. 63/237,999, filed on Aug. 27, 2021, which is incorporated herein in its entirety.

STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH & DEVELOPMENT

(1) Not applicable.

INCORPORATION BY REFERENCE OF MATERIAL SUBMITTED ON A COMPACT DISC

(2) Not applicable.

BACKGROUND OF THE INVENTION

(3) Liquid metals are not new to electronics with patents for reconfigurable liquid metal antennas dating back as far as 1942. However, the non-toxicity of gallium based liquid metals such as Galinstan and EGaIn have helped to drive a resurgence of studies for their applications in the last 10-15 years. A few of these applications consist of reconfigurable antennas, strain and pressure sensors, inductors, and phase shifters. In other designs, the design consisted of a liquid metal center conductor encased in an elastic polymer and surrounded by a shield consisting of five hand-woven liquid metal strands also encased in the elastic polymer. While the design was a good proof of concept, it suffered from transverse electromagnetic (TEM) breakdown at high frequencies. This caused increased transmission loss above 2 GHz.

BRIEF SUMMARY OF THE INVENTION

(4) In one aspect, the embodiments of the present invention reduce the high frequency transmission losses suffered by the prior designs by modifying the hand-woven shield to a hollow cylinder style shield that has a solid surface which is nonwoven with no gaps in the surface area. By using a solid shield rather than a mesh or woven shield, gaps in the shield are reduced or eliminated which in turn reduce the TEM breakdown at high frequencies and increase the operational frequencies of the phase shifter.

(5) In other embodiments, the present invention concerns a stretchable liquid metal coaxial phase shifter constructed of a liquid metal center conductor, a liquid metal shield in the shape of a hollow cylinder, and a stretchable rubber-based polymer (Ecoflex™ 00-30) which encases and insulates the liquid metal. Because the design of the shield consists of a hollow cylinder rather than woven strands, TEM breakdown at high frequencies is decreased, and the phase shifter improves its transmission and reflection coefficients at higher frequencies. Results show a transmission coefficient (S.sub.21) better than -1.8 dB and a reflection coefficient (S.sub.11) better than -10 dB with a 40 mm stretch (62%) and a frequency band of 1 GHz to 4 GHz.

Description

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWINGS

(1) In the drawings, which are not necessarily drawn to scale, like numerals may describe substantially similar components throughout the several views. Like numerals having different letter suffixes may represent different instances of substantially similar components. The drawings illustrate generally, by way of example, but not by way of limitation, a detailed description of certain embodiments discussed in the present document.

(2) FIG. 1 illustrates an embodiment of the present invention.

(3) FIG. 2 shows the phase angle of the transmission coefficient (S.sub.21) for the simulated phase shifter with delta varying from 0 mm to 65 mm. Additionally, it shows the phase shift over a 65 mm stretch at 1.5 GHz, 2.4 GHz, and 3.5 GHz.

(4) FIG. 3 illustrates another embodiment of the present invention.

(5) FIG. 4 illustrates the magnitude of the reflection coefficient (S.sub.11) for the constructed phase shifter with stretches varying from 0 mm to 65 mm. A maximum stretch of about 40 mm is found to maintain an S.sub.11 at -10 dB or better across the entire band.

(6) FIG. 5 shows the magnitude of the transmission coefficient (S.sub.21) for the constructed phase shifter with stretches varying from 0 mm to 65 mm. A stretch at 40 mm (the maximum stretch to maintain an S.sub.11 better than -10 dB) shows a maximum loss of 1.8 dB.

(7) FIG. 6 shows the phase angle for the transmission coefficient (S.sub.21) for the constructed phase shifter with stretches varying from 0 mm to 65 mm. Additionally, it shows the phase shift over 40 mm (the maximum stretch to maintain an S.sub.11 better than -10 dB) and 65 mm (100% stretch).

DETAILED DESCRIPTION OF THE INVENTION

(8) Detailed embodiments of the present invention are disclosed herein; however, it is to be understood that the disclosed embodiments are merely exemplary of the invention, which may be embodied in various forms.

(9) Therefore, specific structural and functional details disclosed herein are not to be interpreted as limiting, but merely as a representative basis for teaching one skilled in the art to variously employ the present invention in virtually any appropriately detailed method, structure, or system. Further, the terms and phrases used herein are not intended to be limiting, but rather to provide an understandable description of the invention.

(10) Design Considerations

(11) When designing a coaxial transmission line for a specific characteristic impedance (Z_0), the factors for which one has control consist of the radius of the center conductor (a), the inner radius of the shield (b), and the permittivity (ϵ) and permeability (μ) of the dielectric material between the conductors, as shown in (1).

$$(12) \quad Z_0 = \sqrt{\frac{\ln(b/a)}{2}} \quad (1)$$

(13) If the relative permeability (U.sub.r) of the dielectric is 1, as in many dielectric insulators, then the factors of control reduce to the radii of the conductors (a and b) and the relative permittivity (ϵ .sub.r). Therefore, by selecting the radii of the conductors (a and b) for a given relative permittivity (ϵ .sub.r), one can design a 50Ω coaxial transmission line.

(14) Given that the dielectric material is the elastic polymer which encases both the center conductor and shield, it is important to understand the effect stretching has on the radii of the encased liquid metals and in turn, the characteristic impedance. As seen from (1), if the ratio (b/a) of the conductors' radii changes when stretched, the characteristic impedance will also change. Fortunately, for a coax design both the radius of the center conductor and the radius of the shield will change at the same percentage when stretched. This equates to the ratio of the two radii staying constant over the stretch and subsequently, a constant characteristic impedance. This effect is due to the Poisson ratio (ν) of the elastic polymer for both the center conductor and shield being the same.

(15) With the Poisson ratio [negative transverse strain ($-\epsilon$.sub.T) over the longitudinal strain (ϵ .sub.L) for the shield (ν .sub.b) and center conductor (ν .sub.a) being equal, the ratio of the radius of the stretched shield (b .sub.s) to the radius of the stretched center conductor (a .sub.s)) can be mathematically derived as equivalent to the ratio of the radius of the unstretched shield (b .sub.0)) to the radius of the unstretched center conductor (a .sub.0), as shown below where (L .sub.s) and (L .sub.0) are the stretched and unstretched lengths of the phase shifter. These ratios (b .sub.s/ a .sub.s and b .sub.0/ a .sub.0) being equal states, per (1), that the characteristic impedance will stay constant when the coaxial phase shifter is stretched.

$$(16) \quad \nu_a = \frac{-\epsilon_T}{\epsilon_L} = \frac{-(a_s - a_0)}{\frac{L_s - L_0}{L_0}} = \frac{-(b_s - b_0)}{\frac{L_s - L_0}{L_0}} = \nu_b \quad (2) \quad \frac{a_s - a_0}{a_0} = \frac{b_s - b_0}{b_0} \quad (3) \quad \frac{a_s}{a_0} - 1 = \frac{b_s}{b_0} - 1 \quad (4)$$

$$\frac{a_s}{a_0} = \frac{b_s}{b_0} \quad (5) \quad \frac{b_0}{a_0} = \frac{b_s}{a_s} \quad (6)$$

Construction

(17) FIGS. 1 and 3 illustrate an embodiment of the present invention. As shown, the present invention provides a stretchable liquid metal coaxial phase shifter **100** comprising opposingly located attachment disks **110** and **111** which are attached to opposingly located shield interface rings **120** and **121** which are open ended cylinders defining an interior space and exterior surface.

Located centrally inside rings **120** and **121** is center pin **130** having terminal ends connected to disks **110** and **111**. Liquid metal center conductor **140** is also centrally located inside rings **120** and **121**. Surrounding and enclosing center pin **130** and liquid metal center conductor **140** is stretchable, elastic polymer layer **150** which is also located inside rings **120** and **121**. Elastic polymer layer **150** defines a container in which center pin **130** and liquid metal center conductor **140** are located.

(18) Surrounding layer **150** and well as the outer surfaces of rings **120** and **121** is liquid metal shield **160**. Surrounding liquid metal shield **160** is stretchable, elastic polymer layer **170**. To function as a container for liquid metal shield **160**, layer **170** is located a spaced distance from layer **150** so as to define a cylindrical space between layer **150** and layer **170**. Liquid metal **160** is poured inside this space.

(19) In a preferred embodiment, the components phase shifter **100** form a series of concentric cylinders nested within each other. For example, liquid metal center **140** is cylindrical in shape and is nested within the hollow center of cylindrical layer **150**. Cylindrical layer **150**, in turn is surround by the cylindrical metal shield **160**, which is in turn, surrounded by cylindrical layer **170**. In yet another embodiment, the present invention provides: a liquid metal center conductor which is surrounded and encased within a first stretchable polymer layer which insulates the liquid metal center conductor; a liquid metal shield which surrounds and encases the first stretchable polymer layer and a second stretchable polymer layer that surrounds and encases the liquid metal shield.

(20) In yet another embodiment, layer **160** is adapted to reduce transmission losses especially high frequency transmissions by having little or no gaps in the surface which are typically found with a mesh or woven surface. Instead, layer **160** may have a solid surface which is nonwoven with no gaps in the surface area. By using a solid shield rather than a mesh or woven shield, gaps in the outer surface of the shield are reduced or eliminated which in turn reduce the TEM breakdown at high frequencies and increase the operational frequencies of the phase shifter. As shown in FIGS. **5** and **6**, providing a solid layer **160** significantly improves performance. As shown, the present invention has only a 1 dB loss with 30 mm stretch and a 2.2 dB loss with 65 mm stretch at 2.4 GHz with a 321 degree phase shift.

(21) The main body of the phase shifter of the present invention may be constructed using a 3D printer to create molds for the layers **150** and **170** which serve as liquid metal containers, as shown in FIGS. **1** and **3**. Attachment disks **110** and **111** may be copper end-disks for attaching to the top and bottom may be cut from a 0.37 mm thick copper plate. The shield-to-ground interface rings **120** and **121** may be created by cutting a small rectangle from a 0.12 mm thick copper plate, wrapping it around a properly sized wooden cylinder, and soldering it together. Because the liquid metal dissolves solder joints, the solder joint on the copper ring was wrapped and protected with copper foil tape. SMA connectors **130A** and **130B** may be 17 mm center conductors to ease the assembly and to ensure proper contact to the liquid metal center conductor **140** during stretching.

(22) A single center pin makes maintaining an electrical contact during stretching problematic. Having opposing center pins **130A** and **130B** does not inhibit maintaining an electrical contact during stretching. When phase shifter **100** is stretched, center pin **130A** is pulled away from center pin **130B**. Nonetheless, both center pins maintain electrical contact with liquid metal center conductor **140** during stretching. Also, for this embodiment, center pins **130A** and **130B** extend through disks **110** and **111** and may be fastened to the disks by connector **199** which may be a metal plate having internal threads that mate with external threads on the pins (not shown). Affixing a one-piece center pin to the disks also inhibits stretching.

(23) An embodiment of the present invention is further adapted to stretch from a first length having a first phase to a second length having a second phase. The second length is longer than the first length and the first phase is different than the second phase. Also, center pins **130A** and **130B** during stretching, maintain contact with liquid metal center conductor **140** while moving from a first position to a second position inside liquid metal center conductor **140**. The pins are closer

together when in the first position than when in the said second position.

(24) Once the Ecoflex™ liquid metal containers were fully cured and removed from the molds, the liquid metal was dispensed into the containers with a pipette or syringe. The SMA connectors and shield-to-ground interface rings were also soldered onto the metal end-disks which may be copper. And lastly, superglue (cyanoacrylate ester) was used to glue everything in place and to prevent liquid metal from leaking out from the center conductor or shield. To construct the stretchable liquid metal phase shifter, a gallium-based alloy (68.5% Ga, 21.5% In, and 10% Sn), labeled as galinstan was purchased from Rotometals.

(25) TABLE-US-00001 TABLE 1 Phase shifter dimensions. Dimension Value Center conductor radius 1.5 mm Shield inner-radius 6.5 mm Ecoflex™ thickness 5 mm (between conductors) Shield thickness 3 mm Ecoflex™ thickness 3 mm (outer container) Ecoflex™ conductor length 61 mm Ecoflex™ cap thickness 2 mm Overall length 65 mm

(26) Medical AG with a low melting point of -19°C . (-2°F), but an in-house mixed alloy with a melting point closer to 11°C . (52°F) and a conductivity roughly $3.46 \times 10^6 \text{ S/m}$. The elastic polymer used as the stretchable container of the liquid metal was Ecoflex™ 00-30 from Smooth-On. Because of its high elasticity with an elongation at break of 900%, it was a preferred choice over other materials such as polydimethylsiloxane (PDMS). Although the manufacturer did not specify the Poisson ratio of Ecoflex™, the value 0.49 was used in the simulations as 0.47 to 0.4999 is common for silicone rubbers. The elastic modulus at 100% elongation is provided as 69 kPa by Smooth-On. Additionally, the permittivity was measured to be between 3.0 and 3.2, so 3.1 was used in the simulations.

(27) Dimensions

(28) To create the phase shifter, a center conductor radius of 1.5 mm and shield inner radius (distance to the inside of the shield) of 6.5 mm was used. These values with an Ecoflex™ permittivity of 3.1 generate a characteristic impedance of 49.94 Ω . Additional dimensions for the simulation model and prototype are shown in TABLE 1.

(29) Simulations

(30) Simulations were completed in CST Microwave Studio using the parameter values from TABLE 1. A parameter named delta was used to represent the stretched amount. By defining the length in terms of the initial length+delta, the phase shifter achieved a simulated stretch by running a parametric sweep of delta from first length at 0 mm to second longer length which was 65 mm—representing a 100% stretch.

(31) Another addition to the model consisted of copper disks attached to the Ecoflex™ on the top and bottom of the phase shifter. These disks served two purposes: 1. an attachment point for stretching the phase shifter, and 2. a rigid surface for attaching components to interface the liquid metal to the outside world. These components consist of an SMA connector with a long 17 mm center pin to interface to the liquid metal center conductor and a thin walled 10 mm tall metal ring, which may be copper, to interface the ground to the liquid metal shield.

(32) The simulation results showed improvements at high frequency. Over the frequency range of 1 GHz to 4 GHz with a stretch varying up to 65 mm, simulation results show the transmission coefficient (S.sub.21) was better than -0.26 dB and the reflection coefficient (S.sub.11) was better than -15 dB . Also, the phase angle of the transmission coefficient (S.sub.21) for stretches in 10 mm increments is shown in FIG. 2. The plot demonstrates a feasible 334° phase shift at 2.4 GHz with a 65 mm stretch which equates to about $51.4^{\circ}/10 \text{ mm}$. Lastly, because of the constant Poisson ratio, the characteristic impedance stayed relatively constant at values between 48.8Ω and 48.9Ω .

(33) Measurements

(34) The constructed phase shifter was characterized by testing it with a network analyzer to measure the magnitude of the reflection coefficient (S.sub.11) and both the magnitude and phase of the transmission coefficient (S.sub.21). This was done over the frequency range of 1 GHz to 4 GHz with stretches every 10 mm up to 60 mm with an additional stretch at 65 mm to represent a 100%

stretch.

(35) From inspection of the reflection coefficient plot of FIG. 4, the maximum stretch while maintaining an S.sub.11 better than -10 dB, over the entire frequency, is found to be roughly 40 mm or about 62%. Inspection of the transmission coefficient plot of FIG. 5, shows the maximum loss of about 1.8 dB when limited to the 40 mm stretch to maintain the S.sub.11 at -10 dB or better. If the stretch increased to 65 mm (100% stretch), the maximum loss is still less than 2.8 dB. Lastly, the phase plot of FIG. 6 includes annotations for both phase shifts at 40 mm (S₁₁ of -10 dB or better) and also 65 mm (100% stretch). At 2.4 GHz, a 40 mm stretch provides a phase shift of 194° and a 65 mm stretch provides a phase shift of 321° . . . This equates to about $49.4^\circ/10$ mm which roughly matches the simulated value of $51.4^\circ/10$ mm.

(36) Other embodiments of the stretchable liquid metal coaxial phase shifter of the present invention demonstrates improvements in the high frequency response by modifying the shield from a woven mesh-style to a hollow cylinder-style. By such modifications, the reflection coefficient was improved from roughly -5 dB to -10 dB with the maximum frequency also increasing from 2.5 GHz to 4 GHz. This higher frequency of course enabled more phase shift but the high elasticity of the Ecoflex™ which allowed a greater stretch, and the improved reflection coefficient almost tripled the phase shift at 2 GHz from 74° to 203° (50 mm stretch, S₁₁ better than -10 dB). Additionally, the transmission coefficient was improved from -2.7 dB at 2 GHz to better than -1.8 dB up to 4 GHz (40 mm stretch, S₁₁ better than -10 dB). Additional improvements in the design and construction would likely further improve the results. Such improvements could be a) decreasing the thickness of the liquid metal shield to reduce sagging from the heavy liquid metal, b) improving the liquid metal injection technique for the shield to ensure no air gaps, and c) reducing the diameter of the phase shifter to also decrease weight and sagging.

(37) While the foregoing written description enables one of ordinary skill to make and use what is considered presently to be the best mode thereof, those of ordinary skill will understand and appreciate the existence of variations, combinations, and equivalents of the specific embodiment, method, and examples herein. The disclosure should therefore not be limited by the above-described embodiments, methods, and examples, but by all embodiments and methods within the scope and spirit of the disclosure.

Claims

1. A stretchable liquid metal coaxial phase shifter comprising: a liquid metal center conductor, said liquid metal center conductor encased within a first stretchable polymer layer which insulates said a liquid metal center conductor; a liquid metal shield, said a liquid metal shield encases said first stretchable polymer layer; a second stretchable polymer layer, said second stretchable polymer layer surrounds and encases said liquid metal shield; and wherein said phase shifter is adapted to stretch from a first length having a first phase to a second length having a second phase, said second length is longer than said first length and said first phase is different than said second phase.
2. The stretchable liquid metal coaxial phase shifter of claim 1 wherein said phase shifter is adapted to stretch from a first length to a second length, said second length is longer than said first length.
3. The stretchable liquid metal coaxial phase shifter of claim 1 further comprising disks attached to at least one of said stretchable polymer layers at the top and bottom of the phase shifter; said disks configured to function as attachment points for stretching the phase shifter, and to provide a rigid surface for attaching components to externally interface with said liquid metal center conductor.
4. The stretchable liquid metal coaxial phase shifter of claim 3 wherein said disks are metal.
5. The stretchable liquid metal coaxial phase shifter of claim 4 further comprising opposing located center pins, said center pins maintain an electrical connection with said liquid metal center conductor while moving from a first position to a second position inside said liquid metal center conductor.

6. The stretchable liquid metal coaxial phase shifter of claim 5 wherein said pins are closer together when in said first position than when in said second position.
 7. The stretchable liquid metal coaxial phase shifter of claim 6 wherein said center pins extend through said disks.
 8. The stretchable liquid metal coaxial phase shifter of claim 6 wherein said center pins extend through and are attached to said disks.
 9. The stretchable liquid metal coaxial phase shifter of claim 6 wherein said center pins extend through and are attached to said disks by a connector.
 10. The stretchable liquid metal coaxial phase shifter of claim 6 wherein said phase shifter has a 1 dB loss with 30 mm stretch.
 11. The stretchable liquid metal coaxial phase shifter of claim 6 wherein said phase shifter has a 2.2 dB loss with 65 mm stretch at 2.4 GHz.
 12. The stretchable liquid metal coaxial phase shifter of claim 6 wherein said phase shifter has a 2.2 dB loss with 65 mm stretch at 2.4 GHz with a 321 degree phase shift.
 13. A stretchable liquid metal coaxial phase shifter comprising: a liquid metal center conductor, said liquid metal center conductor encased within a first stretchable polymer layer which insulates said a liquid metal center conductor; a liquid metal shield, said a liquid metal shield encases said first stretchable polymer layer; a second stretchable polymer layer, said second stretchable polymer layer surrounds and encases said liquid metal shield; and wherein said phase shifter is adapted to be compressed.
 14. The stretchable liquid metal coaxial phase shifter of claim 13 wherein said phase shifter is adapted to be elongated.
 15. The stretchable liquid metal coaxial phase shifter of claim 14 further comprising opposing located center pins, said center pins maintain an electrical connection with said liquid metal center conductor and move towards one another when said phase shifter is compressed.
 16. The stretchable liquid metal coaxial phase shifter of claim 14 further comprising opposing located center pins, said center pins maintain an electrical connection with said liquid metal center conductor and move away from one another when said phase shifter is elongated.
 17. The stretchable liquid metal coaxial phase shifter of claim 13 further comprising metal disks attached to at least one of said stretchable polymer layers at the top and bottom of the phase shifter; said disks configured to function as attachment points for stretching the phase shifter, and to provide a rigid surface for attaching components to externally interface with said liquid metal center conductor.
 18. The stretchable liquid metal coaxial phase shifter of claim 17 wherein said center pins extend through said disks.
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