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Soft magnetic powder and inductor

Abstract

A soft magnetic powder includes soft magnetic particles each having a nucleus that contains a soft magnetic metal and an insulating film on the surface of the nucleus. The insulating film contains Si and a hydrocarbon group having a C8 or longer linear-chain moiety, and the ratio by weight of Si to C in the insulating film is 7.6 or more and 42.8 or less (i.e., from 7.6 to 42.8).

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Background/Summary

CROSS-REFERENCE TO RELATED APPLICATIONS

(1) This application claims benefit of priority to Japanese Patent Application No. 2020-168437, filed Oct. 5, 2020, to Japanese Patent Application No. 2020-168442, filed Oct. 5, 2020, to Japanese Patent Application No. 2020-168443, filed Oct. 5, 2020, to Japanese Patent Application No. 2020-168444, filed Oct. 5, 2020, to Japanese Patent Application No. 2020-168445, filed Oct. 5, 2020, to Japanese Patent Application No. 2020-168446, filed Oct. 5, 2020, to Japanese Patent Application No. 2020-168786, filed Oct. 5, 2020, to Japanese Patent Application No. 2020-168787, filed Oct. 5, 2020, to Japanese Patent Application No. 2020-199921, filed Dec. 1, 2020, and to Japanese Patent Application No. 2021-091229, filed May 31, 2021, the entire content of each is incorporated herein by reference.

BACKGROUND

Technical Field

(2) The present disclosure relates to a soft magnetic powder and an inductor made therewith.

Background Art

(3) Inductors (coil components) made with a magnetic metal material have been used in smartphones and many more kinds of electrical equipment. An example is chip inductors, which can be mounted on the surface of a circuit board. A known type of magnetic metal material used in chip inductors is a dust core, or body, formed by compression molding of a soft magnetic powder as a collection of particles of a soft magnetic metal with added resin.

(4) International Publication No. 2018/131536 describes magnetic particles composed of very small cores (nuclei) made of a magnetic material and an insulating coating on the surface of the cores. The insulating coating is the product of a sol-gel reaction between an organic phosphoric acid having a C5 or longer hydrocarbon group and a metal alkoxide. Such magnetic particles have improved lubricity when shaped into a magnetic metal material by compression molding, and therefore pack densely in the magnetic metal material. As a result, the finished magnetic metal material has increased magnetic permeability.

(5) Improving the lubricity of the magnetic particles, however, can affect the strength of the finished magnetic metal material because it means reducing the force of binding between the magnetic particles and the resin present therearound. This known type of magnetic particles, therefore, has room for improvement in terms of the balance between the magnetic permeability and mechanical strength of metal magnetic materials shaped therefrom.

SUMMARY

(6) Accordingly, the present disclosure provides a soft magnetic powder that gives a magnetic metal material having sufficient mechanical strength and high magnetic permeability when shaped by compression molding.

(7) According to preferred embodiments of the present disclosure, a soft magnetic powder includes soft magnetic particles each having a nucleus that contains a soft magnetic metal and an insulating film on a surface of the nucleus. The insulating film contains Si and a hydrocarbon group having a C8 or longer linear-chain moiety, and a ratio by weight of Si to C in the insulating film is 7.6 or more and 42.8 or less (i.e., from 7.6 to 42.8).

(8) With the soft magnetic powder according to preferred embodiments of the present disclosure, a magnetic metal material shaped therefrom by compression molding can have high magnetic permeability with a limited loss of mechanical strength.

(9) Other features, elements, characteristics and advantages of the present disclosure will become more apparent from the following detailed description of preferred embodiments of the present disclosure with reference to the attached drawings.

Description

BRIEF DESCRIPTION OF THE DRAWINGS

(1) FIG. 1 is a diagram schematically illustrating the structure of an inductor according to an embodiment of the present disclosure, presenting a perspective view of the top side of the inductor;

(2) FIG. 2 is a diagram schematically illustrating the structure of the same inductor, presenting a perspective view of the mount surface side of the inductor;

(3) FIG. 3 is a perspective view of the internal structure of the same inductor;

(4) FIG. 4 is a cross-sectional view of a wire used for a coil, illustrating a cross-section perpendicular to the length;

(5) FIG. 5 is an outline of the production of an inductor;

(6) FIG. 6 is a diagram illustrating the shaping of a body from tablets of powder mix;

(7) FIG. 7 is a schematic diagram illustrating the core of a shaped body;

- (8) FIG. 8 is a diagram illustrating the structure of first soft magnetic particles as a component of powder mix;
- (9) FIG. 9 presents electron microscope surface images of an oxide film on the nucleus for types of Cr-free first soft magnetic particles;
- (10) FIG. 10 is a graphical representation of how the oxygen content of first soft magnetic particles changes the withstand voltage of a shaped article;
- (11) FIG. 11 is a graphical representation of how the oxygen content of first soft magnetic particles changes the relative permeability and saturation flux density of a shaped article;
- (12) FIG. 12 is a graphical representation of how the oxygen content of first soft magnetic particles changes a magnetic performance factor of a shaped article;
- (13) FIG. 13 is a diagram illustrating the structure of second soft magnetic particles as a component of powder mix;
- (14) FIG. 14 is an image of near-coil flow of powder mix during shaping and curing;
- (15) FIG. 15 is an image of voids in the surface and middle regions of a first tablet during the shaping and curing of a body;
- (16) FIG. 16 is a diagram for the description of reference planes of an inductor;
- (17) FIG. 17 presents images of resin packing beneath sides of a body;
- (18) FIG. 18 is a summary of measured surface roughness of a body;
- (19) FIG. 19 is a diagram for the description of the distances between sides of a body and a coil;
- (20) FIG. 20 is a diagram for the description of the relationship between the resin content of powder mix and the density of a body.
- (21) FIGS. 21A and 21B are images of lower and upper loops, respectively, of a coil together with materials therearound;
- (22) FIG. 22 is a diagram provided for the description of pressure applied during the shaping of a body;
- (23) FIG. 23 presents simulated characteristic curves of a “powder-between-loops” structure;
- (24) FIG. 24 is an image of the vicinity of a wound section with an air gap that serves as a magnetic gap;
- (25) FIG. 25 presents simulated characteristic curves with and without air gaps;
- (26) FIG. 26 is a diagram schematically illustrating an example of a grinder used in the grinding of a body;
- (27) FIG. 27 is a diagram for the description of side gaps;
- (28) FIG. 28 is a diagram schematically illustrating an example of a film forming device used in the formation of a protective film;
- (29) FIG. 29 is a graphical representation of experimentally determined relationships between nanosilica content and the rate of drying;
- (30) FIG. 30 is a graphical representation of experimentally determined relationships between the average diameter of nanosilica particles and the incidence of “film sticking”;
- (31) FIG. 31 is an image of cracks in a protective film; and
- (32) FIG. 32 is a graphical representation of a “plating mark” count with varying thickness of a protective film.

DETAILED DESCRIPTION

(33) Overall Structure of the Inductor

(34) FIGS. 1 and 2 are diagrams schematically illustrating the structure of an inductor 1 according to an embodiment. FIG. 1 is a perspective view of the top surface 14 side of the inductor 1, and FIG. 2 is a perspective view of the mount surface 12 side of the inductor 1.

(35) Constructed as a surface-mount electronic component, the inductor 1 according to this embodiment has a substantially rectangular-parallelepiped body 10 and a pair of outer electrodes 20 on the surface of the body 10. One side of the body 10 is the mount surface 12 (FIG. 2), on which the body 10 is mounted on the surface of a circuit board (not illustrated). The body 10 is covered with a protective film 50 except where it has the outer electrodes 20 on.

(36) The side of the body 10 opposite the mount surface 12 is the top surface 14 (FIG. 1). Of the four sides other than the mount surface 12 and the top surface 14, the pair of sides on which the body 10 has extensions 34 (described later) of a coil 30 are the first side surfaces 16, and the other pair are the second side surfaces 18. The first and second side surfaces 16 and 18 can also be described as the sides of the body 10 located radially around the wound section 32 of the coil 30 (described later). The mount surface 12 and the top surface 14, opposite each other, are also referred to as the primary sides.

(37) As illustrated in FIG. 1, the distance from the mount surface 12 to the top surface 14 is defined as the thickness T of the body 10. The length of the short side of the top surface 14 is defined as the width W of the body 10, and the length of the long side of the top surface 14 is defined as the length L of the body 10.

(38) FIG. 3 is a perspective view of the internal structure of the inductor 1 according to this embodiment.

(39) The body 10 has a coil 30 and a core 40 in which the coil 30 is embedded; the body 10 is a magnetic component with a built-in coil, in which a coil 30 is built in a core 40.

(40) The coil 30 is an air-core coil component, i.e., simply a coil of wire 31.

(41) The core 40 is a substantially rectangular-parallelepiped article formed by shaping a mixture of soft magnetic powder and resins, or powder mix, by compression molding with the coil 30 therein.

(42) The coil 30 has a wound section 32 formed by a length of wound wire 31 and a pair of extensions 34 from the wound section 32. The wound section 32 is formed by winding a length of wire 31 substantially into a spiral shape in such a manner that the wire 31 will have both of its ends outside and be continuous inside. Inside the body 10, the coil 30 is embedded in the core 40 with the central axis K of its wound section 32 parallel with the thickness T of the body 10. The extensions 34 extend from the wound section 32 to the pair of first side surfaces 16, one extension 34 to one side 16.

(43) FIG. 4 is a cross-sectional view of the wire 31 forming the coil 30, illustrating a cross-section perpendicular to the length. The wire 31 forming the coil 30 is composed of copper wire 36 and an insulating coating 60 that covers the copper wire 36. The insulating coating 60 has an electrically insulating coating layer 61 and a fuser layer 62 on the coating layer 61. In the formation of the coil 30, the wire 31 is heated while it is wound. The fuser layer 62 melts, fastening together the portions of the wire 31 forming the wound section 32. The wound section 32 of the finished coil 30, therefore, will not lose their shape easily. In addition, the insulating coating layer 61 provides reliable electrical insulation between the coil 30 and the core 40.

(44) The pair of outer electrodes 20 are substantially L-shaped elements extending from the first side surfaces 16 of the body 10 to reach the mount surface 12, one electrode 20 from one side 16. Each of the outer electrodes 20 is coupled to one extension 34 of the coil 30 at one first side surface 16, and its portion 20A reaching the mount surface 12 (FIG. 2) is electrically coupled to wiring of a circuit board, for example by soldering.

(45) An example of an inductor 1 having such a structure is a power inductor and is used as a choke coil, for example in a high-current DC-DC converter or power-supply circuit, in PCs, DVD players, digital cameras, TV sets, cellular phones, smartphones, automotive electronics, medical and industrial machinery, and other types of electronic equipment. These, however, are not the only possible

applications of the inductor **1**; it can be used in tuned circuits, filter circuits, rectifier/smoothing circuits, etc.

(46) Overview of the Production of the Inductor

(47) FIG. **5** is an outline of the production of the inductor **1**.

(48) As illustrated, the production of the inductor **1** includes granulation (Step **100**), coil formation (Step **200**), shaping and curing (Step **300**), grinding (Step **400**), film formation (Step **500**), film removal (Step **600**), and electrode formation (Step **700**).

(49) First, a mixture of the soft magnetic powder and resins to be contained in the core **40** (hereinafter powder mix) is granulated (Step **100**). The soft magnetic powder is a collection of particles having a surface coated with an insulating film.

(50) Separately, a coil **30** is formed from a piece of wire **31** covered with an insulating coating **60**. To ensure the resulting coil **30** will have the aforementioned wound section **32** and pair of extensions **34**, the wire **31** is wound by the method called “ α winding,” a technique of winding in which the piece of wire **31**, which will serve as a conductor, is wound substantially into a two-tier spiral shape in such a manner that the resulting coil **30** will have its starting and ending extensions **34** outside. The number of turns in the coil **30** is not critical. For example, the coil **30** may have about 6.5 turns.

(51) Then an article that will later become the body **10** is shaped and cured.

(52) The material for the shaped article is the granulated powder mix.

(53) Prior to this, the powder mix is shaped into tablets (solids in a predetermined shape). Putting the tablets and the coil **30** into a cavity in a mold and pressing them with a punch while heating the cavity will give a shaped article with the coil **30** therein. The cured article is removed from the cavity and polished. Barrel polishing will give the article rounded corners.

(54) As illustrated in FIG. **6**, two types of tablets are used: a first tablet **70** in an appropriate shape (e.g., substantially E-shaped) having a groove **71** for putting the coil **30** in, and a second tablet **72** in an appropriate shape (e.g., substantially I-shaped or flat-plate) that covers the groove **71** in the first tablet **70**. In the compression molding, the first tablet **70** with the coil **30** slotted in the groove **71** and the second tablet **72** are stacked in the cavity **75** in the mold **74**. The first and second tablets **70** and **72** are then heated and at the same time pressed with a punch **76** in the direction of stacking from the first tablet **70** or/and second tablet **72** side (in the example in FIG. **6**, from the second tablet **72** side). This will combine the first tablet **70**, coil **30**, and second tablet **72** into a one-piece structure.

(55) Alternatively, the granulated powder mix may be put directly into the cavity and shaped by compression molding.

(56) Preferably, the pressure **P** for the compression molding is lower than usual so that the individual particles **80** forming the soft magnetic powder will not break but maintain their original shape in the shaped body **10** as illustrated in FIG. **7**. This will limit damage to the insulating film on the surface of the individual particles **80** forming the soft magnetic powder, thereby limiting the associated lowering of the insulating performance (i.e., voltage resistance) of the film.

(57) Preferably, the soft magnetic powder is a collection of two or more sets of particles **80** with different sizes as illustrated in FIG. **7** (in the example in FIG. **7**, first soft magnetic particles **81** having a relatively large average diameter, or “larger particles,” and second soft magnetic particles **82** having a relatively small average diameter, or “smaller particles”). Shaping such a soft magnetic powder by compression molding will give an article (body **10**) densely packed with particles **80** of the powder because the smaller, second soft magnetic particles **82** penetrate between the larger, first soft magnetic particles **81** together with resin **90** as illustrated in FIG. **7** during the compression molding. Embodiments of the first and second soft magnetic particles **81** and **82** as a component of the core **40** will be described later.

(58) Then the second side surfaces **18** of the article are scraped away (i.e., ground) with an abrasive to a predetermined width **W**.

(59) This will trim the body **10** to a predetermined width **W**. The trimming will reduce the distances between the coil **30** inside the body **10** and the second side surfaces **18** (also referred to as the side gaps), thereby increasing the occupancy of the body **10** by the coil **30** in the radial direction with respect to the wound section **32** of the coil **30**. Shaping (Step **300**) the body **10** by compression molding and then grinding (Step **400**) it to a predetermined size is advantageous over controlling the size of the body **10** by compression molding alone in terms of size variations between bodies **10**.

(60) Polishing (e.g., barrel polishing) may follow to round the corners of the second side surfaces **18** produced by the grinding.

(61) The entire surface of the body **10**, now ground to a predetermined size, is then covered with a protective film **50**.

(62) The material for the protective film **50** is a thermosetting resin, such as an epoxy, polyimide, or phenolic resin, or thermoplastic resin, such as a polyethylene or polyamide resin. A resin containing filler, such as silicon oxide or titanium oxide, may also be used.

(63) The material for the protective film **50** is applied to the entire surface of the body **10**, for example by coating or dipping, and the applied material is cured to form a protective film **50**.

(64) The body **10**, now entirely covered with the protective film **50**, is then irradiated with a laser to remove the protective film **50** from the areas in which the outer electrodes **20** will be formed (hereinafter also electrode areas; in this embodiment, predetermined areas of the first side surfaces **16** and mount surface **12**) and also to remove the insulating coating **60** on the extensions **34** of the coil **30** exposed in the electrode areas.

(65) After the laser-assisted removal of the insulating coating **60**, etching may follow to clean the surface of the electrode areas.

(66) Then outer electrodes **20** are formed (Step **200**) by plating the electrode areas, from which the protective film **50** has been removed. The formation of the outer electrodes **20** may precede the formation of the protective film **50**.

(67) The outer electrodes **20** are formed by plating the soft magnetic powder and extensions **34** of the coil **30** exposed on the surface of the body **10** with a layer of copper (Cu).

(68) On the copper (Cu) layer, nickel (Ni) and tin (Sn) plating layers may be stacked in this order. A layer of aluminum (Al), silver (Ag), gold (Au), or palladium (Pd) may be used instead of the layer of copper (Cu).

(69) Outer electrodes formed by sputtering or sheets of electrically conductive resin or copper, for example, may also be used. The outer electrodes **20**, furthermore, do not need to be substantially L-shaped as in the drawings; they may be so-called “five-side electrodes” or bottom electrodes.

(70) An inductor **1** produced as described above is highly reliable and achieves good voltage resistance, magnetic permeability, saturation flux density, and characteristics under applied DC current. Its core **40** is better than that of known inductors in terms of specific resistance, the percentage of soft magnetic metal, etc., but at the same time has mechanical strength comparable to that of the core of known inductors.

(71) The following describes embodiments and examples of inductors **1**.

(72) In each embodiment or example, the inductor **1** has dimensions of about 2.0 mm \pm about 0.2 mm in length **L**, about 1.2 mm \pm about 0.2 mm in width **W**, and about 0.7 mm \pm about 0.1 mm in thickness **T** and a withstand voltage of about 20 V unless specified otherwise.

(73) The inductor **1** can be constructed using any of the configurations described in each of the following chapters, A-1-1. First Soft Magnetic Particles, A-1-2. Second Soft Magnetic Particles, A-2. Resins, B. Coil, C. Magnetic Paths, D. Grinding, and E. Protective Film, and can be made as any combination of such configurations.

(74) A. Powder Mix

(75) The powder mix used to form the core **40** contains soft magnetic powder and resins.

(76) A-1. Soft Magnetic Powder

(77) The soft magnetic powder in the powder mix is a collection of particles of a soft magnetic metal. The soft magnetic powder includes, for example, first soft magnetic particles **81** (larger particles) and second soft magnetic particles **82** (smaller particles), which have a smaller average diameter than the first soft magnetic particles **81**. As mentioned herein, the average diameter of particles refers to the median diameter by volume.

(78) The average diameter of the first soft magnetic particles **81** and that of the second soft magnetic particles **82** can be measured using a particle size analyzer before the particles **81** and **82** are mixed together. If they are measured in the core **40** shaped from the powder mix by compression molding, the measurement can be performed by analyzing an electron microscope image of a cross-section of soft magnetic particles obtained by polishing the core **40**. For example, the equivalent circular diameter of the cross-section of each soft magnetic particle in the electron microscope image is determined, and then the volume of imaginary spheres having this equivalent circular diameter is determined. The median diameter in the distribution of volumes is the average diameter of the particles.

(79) The average diameter of the first soft magnetic particles **81** is about 20 μm or more and about 28 μm or less (i.e., from about 20 μm to about 28 μm), preferably about 21.4 μm or more and about 27.4 μm or less (i.e., from about 21.4 μm to about 27.4 μm). The average diameter of the second soft magnetic particles **82** is about 1 μm or more and about 6 μm or less (i.e., from about 1 μm to about 6 μm), preferably about 1.5 μm or more and about 1.8 μm or less (i.e., from about 1.5 μm to about 1.8 μm). Using such a powder mix containing first and second soft magnetic particles **81** and **82** with different average diameters helps improve relative permeability. The first soft magnetic particles **81**, having a larger average diameter, increases the saturation flux density, and therefore improves the characteristics under applied DC current, of the finished core **40**. The second soft magnetic particles **82**, which have a smaller average diameter, penetrate into the gaps between the first soft magnetic particles **81**, thereby improving the packing of soft magnetic particles in the core **40**.

(80) The amount of the second soft magnetic particles **82** in the powder mix is about 15% by weight or more and about 30% by weight or less (i.e., from about 15% by weight to about 30% by weight), preferably about 20% by weight or more and about 30% by weight or less (i.e., from about 20% by weight to about 30% by weight), of the total weight of soft magnetic particles in the powder mix. When the amount of the second soft magnetic particles **82** in the soft magnetic powder is in any of these ranges, the packing of soft magnetic particles in the core **40** shaped from the powder mix is further improved.

(81) The soft magnetic metal composition of the second soft magnetic particles **82** may be the same as that of the first soft magnetic particles **81**, but preferably, the two sets of soft magnetic particles have different compositions and substantially equal hardness. The hardness of the first and second soft magnetic particles **81** and **82** can be measured by nanoindentation. The hardness of the first soft magnetic particles **81** is, for example, about 600 HV (kgf/mm^{sup.2}) or more and about 1200 HV or less, desirably about 800 HV or more and about 1000 HV or less (i.e., from about 800 HV to about 1000 HV). The hardness of the second soft magnetic particles **82** is, for example, about 900 HV (kgf/mm^{sup.2}) or more and about 1400 HV or less, desirably about 900 HV or more and about 1100 HV or less (i.e., from about 900 HV to about 1100 HV).

(82) Desirably, the ratio of the hardness of the second soft magnetic particles **82** to that of the first soft magnetic particles **81** is about 0.7 or more and about 1.2 or less (i.e., from about 0.7 to about 1.2). This helps prevent the core **40** from losing its insulation resistance because this prevents the first or second soft magnetic particles **81**, or **82**, whichever has the lower hardness, from deforming when the powder mix is shaped into the core **40** by compression molding.

(83) A-1-1. First Soft Magnetic Particles

(84) A-1-1-1. Embodiment of the First Soft Magnetic Particles

(85) FIG. **8** is a diagram illustrating the structure of the first soft magnetic particles **81**. The first soft magnetic particles **81** are each composed of a nucleus **81A** made of a soft magnetic metal and an insulating film **81C** on the surface of the nucleus **81A**. The nucleus **81A** has an oxide film **81B** produced by the oxidation of the soft magnetic metal forming the nucleus **81A** on the surface of the nucleus **81A**.

(86) In order for the core **40** to withstand high voltages consistently, the insulating film **81C** needs to be adhering to the underlying oxide film **81B** firmly enough that it will not detach from the oxide film **81B**. Once the insulating film **81C** detaches from the oxide film **81B**, a decrease in the insulation resistance of the core **40** will affect the voltage resistance of the inductor. When the oxide film **81B** forms, however, the nucleus **81A** loses some amount of soft magnetic metal therein, and the core **40** will have reduced relative permeability because of the use of such nuclei **81A**. In view of relative permeability, therefore, it is preferred that the oxide film **81B** be as thin as possible.

(87) The inventors have found that when the nuclei **81A** are made of a Cr-containing soft magnetic metal, the oxide film **81B** that forms on their surface tend to be thin and smooth, and this can prevent the insulating film **81C** from adhering to the oxide film **81B** firmly enough. A possible solution reached is to limit the Cr content of the nuclei **81A** and at the same time select the thickness of the oxide film **81B** that forms on the surface of the nuclei **81A** within a particular range. This enables firm adhesion of the insulating film **81C** to the oxide film **81B** to be combined with limited loss of the relative permeability of the core **40** made using the nuclei **81A**.

(88) Specifically, an iron-based soft magnetic metal containing about 1.5% by weight or less Cr is used as the soft magnetic metal forming the nuclei **81A**. Setting the Cr content in this range helps strengthen the adhesion between the insulating film **81C** and the oxide film **81B**. In that case the nuclei **81A** have high relative permeability by virtue of high iron content, and also form uneven passivation film on their surface. The uneven passivation film makes the oxide film **81B** nonuniform, thereby increasing the area of contact between the oxide film **81B** and the insulating film **81C**.

(89) The nuclei **81A** may be particles of a Cr-free (containing no Cr) iron-based soft magnetic metal. As mentioned herein, being Cr-free means the material is substantially free of Cr; the material may contain Cr, but its amount is very small, as small as that of a potential contaminant from the environment in which the nuclei **81A** are produced (e.g., about 500 ppm or less).

(90) More specifically, the nuclei **81A** are particles of an Fe—Si—Cr alloy containing Cr in the above range or Fe—Si alloy in amorphous (non-crystalline) or crystalline magnetic metal form. The Fe—Si—Cr or Fe—Si alloy contains, for example, about 87% by weight or more Fe and about 3% by weight or more Si, optionally with B (boron).

(91) The nuclei **81A** of the first soft magnetic particles **81**, however, do not need to be particles of such an Fe—Si—Cr or Fe—Si alloy; they only need to be made with an iron-based soft magnetic metal. An example of another iron-based soft magnetic metal is an amorphous or crystalline Fe—Si—Cr—Al alloy containing Cr in the above range or an amorphous or crystalline Fe—Si—Al alloy.

(92) Using particles of a Cr-free alloy as the nuclei **81A** of the first soft magnetic particles **81** helps give the inductor better characteristics under applied DC current. The increased ratio by weight of Fe in the nuclei **81A** further increases the saturation flux density of the core **40** made using the nuclei **81A**.

(93) The oxide film **81B** can be formed through the oxidation of the soft magnetic metal present on the surface of the nuclei **81A** during the production of the nuclei **81A**. For example, the oxide film **81B** can be formed when the nuclei **81A** are exposed to water or an oxygen atmosphere during their production and/or by active oxidation, such as exposing the nuclei **81A** to a hot oxygen atmosphere.

(94) The oxide film **81B** becomes thicker as the soft magnetic metal on the surface of the nuclei **81A** is oxidized. The roughness of its surface increases at the same time, and the adhesion between the oxide film **81B** and the insulating film **81C** formed thereon becomes stronger accordingly. As the oxide film **81B** becomes thicker with advancing oxidation of the soft magnetic metal, however, the metal content of the nuclei **81A** decreases, affecting the relative permeability of the core **40** made using the nuclei **81A**. To ensure that the insulating film **81C** will adhere firmly with limited loss of relative permeability, it is desirable that the oxygen content of the nuclei **81A** be about 900 ppm or more and about 2800 ppm or less (i.e., from about 900 ppm to about 2800 ppm).

(95) The insulating film **81C** formed on the oxide film **81B** is, for example, an inorganic glass coating formed by mechanochemistry, such as a coating of phosphate glass, e.g., zinc phosphate or manganese phosphate, or a coating of glass. Alternatively, the insulating film **81C** may be an organic polymer coating, an organic-inorganic hybrid coating, or an inorganic electrically insulating coating. Such an insulating film **81C** can be formed by mechanochemistry, sol-gel reaction of a metal alkoxide, or any other process selected according to the material used.

(96) The thickness of the insulating film **81C** is about 10 nm or more and about 50 nm or less (i.e., from about 10 nm to about 50 nm). Setting the thickness of the insulating film **81C** about 10 nm or more helps increase the resistivity of the first soft magnetic particles **81**. Setting the thickness of the insulating film **81C** about 50 nm or less will ensure a high percentage of metal in the first soft magnetic particles **81**, thereby helping give good magnetic properties to the core **40** made using them.

(97) First soft magnetic particles **81** configured as described above allow the core **40** to withstand high voltages consistently by virtue of sufficiently firm adhesion of the insulating film **81C** formed on the oxide film **81B** on their nuclei **81A**, although the relative permeability of the core **40** remains high.

(98) A-1-1-2. Production of the First Soft Magnetic Particles

(99) The following describes the production of first soft magnetic particles **81** according to an embodiment of the present disclosure. The following is merely an example and is not the only method for producing first soft magnetic particles **81** according to an embodiment of the disclosure.

(100) The nuclei **81A** of the first soft magnetic particles **81** are obtained by, for example, gas atomization. That is, the metals from which the nuclei **81A** will be made are melted in an electric induction furnace, and the resulting molten metal is sprayed through a nozzle with a jet of inert argon gas to give fine particles of the metals. After being cooled in water and dried, these fine particles are used as the nuclei **81A** of the first soft magnetic particles **81**. The average diameter of the nuclei **81A** can be controlled by, for example, adjusting the velocity of the jet stream of argon gas and/or the diameter of the nozzle used to spray the molten metal in the gas atomization.

(101) If, for example, nuclei **81A** having an average diameter of about 20 μm or more are formed as particles of an amorphous metal, a possible option is the SWAP (spinning water atomization process), in which the fine particles of metals formed from molten metal are cooled rapidly in water spinning at a high speed.

(102) The nuclei **81A** are exposed to water and/or an oxygen atmosphere in the water cooling and the subsequent drying, forming an oxide film **81B** on their surface. The oxide film **81B** can be formed to a desired thickness by controlling the duration of the exposure to water or an oxygen atmosphere and/or the oxygen concentration of the environment in which the nuclei **81A** are produced. Exposing the dried nuclei **81A** to a hot oxygen atmosphere will further grow the oxide film **81B** on the surface of the nuclei **81A**. Here, it would be fair to assume that the formation of the oxide film **81B** will make no substantial change in the average diameter of the nuclei **81A**. The same also applies to the formation of the insulating film **81C**, which will be described later.

(103) The oxide film **81B** formed on the surface of the nuclei **81A**, furthermore, does not need to be uniform in terms of the distribution of metal oxide(s) therein. For example, if the metal or metals forming the nuclei **81A** can form multiple oxides, the distribution of the oxides inside the oxide film **81B** may be imbalanced, or the oxide film **81B** may be formed by multiple layers of different oxides.

(104) Then an insulating film **81C** is formed on the oxide film **81B** formed on the nuclei **81A**. The insulating film **81C** is, for example, a film of phosphate glass formed by mechanochemistry.

(105) A-1-1-3. Examples of First Soft Magnetic Particles

(106) Twenty-seven samples (samples A1-01 to A1-27) differing in the Cr content of the nuclei **81A** and the thickness of the oxide film **81B** on the surface of the nuclei **81A** were prepared and characterized. A summary of the particles of samples A1-01 to A1-27 is presented in Table 1 along with characterization results. Samples A1-03 to A1-08, A1-12 to A1-16, and A1-20 to A1-24 are examples of first soft magnetic particles **81** according to an embodiment of the present disclosure.

(107) The following describes the individual samples.

(108) Sample A1-01

(109) Production of Nuclei

(110) For use as the nuclei **81A**, fine particles of amorphous Fe—Si alloy containing no Cr (Cr-free) were prepared by the aforementioned SWAP. The Fe and Si contents of the nuclei **81A** were 93% by weight and 3.5% by weight, respectively. The nuclei **81A** also contained 3% by weight B, and the rest was C. The average thickness of the oxide film **81B**, produced by surface oxidation of the nuclei **81A**, was 5 nm. The hardness of the nuclei **81A** was 953 HV.

(111) The Fe and Si contents were measured by ICP-OES (spark optical emission spectrometry). The hardness of the nuclei **81A** was measured by nanoindentation.

(112) Formation of Insulating Film

(113) On the surface of the nuclei **81A** (with the oxide film **81B** thereon), an insulating film **81C** of zinc phosphate, which is a type of phosphate glass, was formed by mechanochemistry. The resulting soft magnetic particles covered with the insulating film **81C** were used as sample A1-01 of first soft magnetic particles **81**. The final thickness of the insulating film **81C** was 23 nm.

(114) The average (median) diameter of the first soft magnetic particles **81** was 25.3 μm .

(115) The average diameter was measured using a particle size analyzer.

(116) The average thickness of the oxide film **81B** was measured as follows. In a broad sense, the average thickness of the oxide film **81B** represents the average of the thickness of the oxide film **81B** measured at multiple points in a cross-section of the nuclei **81A**. In a narrow sense, it represents the value derived by the following procedure. First, one nucleus **81A** was sliced with a focused ion beam (FIB). The slice could be cut from any point of the nucleus **81A**. With an electron microscope (TEM) set to a magnification of $\times 100,000$, the cross-section of the nucleus **81A** was imaged at three regularly spaced points on the outer circumference for three fields of view. On each TEM image, the thickness of the oxide film **81B** was measured at four regularly spaced points. This was repeated for three nuclei **81A**, and the

average of all thickness measurements (three fields of view×four points×three nuclei=36 measurements) was reported as the average thickness. The thickness of the insulating film **81C** was also measured in the same way.

(117) Oxide Film Unevenness and Oxygen Content

(118) The difference between the largest and smallest thickness of the oxide film **81B** in a cross-section of the nuclei **81A** (hereinafter also referred to as the thickness gap of the oxide film **81B**) was determined as a measure of the unevenness of the oxide film **81B**. The difference between the largest and smallest thickness of the oxide film **81B** was measured as follows. First, one nucleus **81A** was sliced with a focused ion beam (FIB). The slice could be cut from any point of the nucleus **81A**. With an electron microscope (TEM) set to a magnification of ×100,000, the cross-section of the nucleus **81A** was observed along its outer circumference and imaged at three points where the oxide film **81B** looked thin and three points where the oxide film **81B** looked thick for three fields of view. On each TEM image, the largest and smallest thickness measurements were determined. The largest and smallest measurements across the three fields of view were reported as the largest thickness and the smallest thickness, respectively. The result is presented in Table 1.

(119) In addition, as a potential indicator of the amount of oxide film **81B** on the surface of the nuclei **81A** after the formation of the insulating film **81C**, the oxygen content of sample A1-01 was studied by measuring the amount of oxygen in one gram of the soft magnetic particles by inert gas fusion. The result is presented in Table 1.

(120) Strength of the Adhesion of the Insulating Film

(121) The strength of the adhesion of the insulating film **81C** on the soft magnetic particles was evaluated as follows using a powder resistivity meter (Hiresta). First, a 10-g powder as a collection of the soft magnetic particles was put into a measuring cylinder (having an electrically insulating wall and an earthed metal bottom) that came with the resistivity meter. The top of the powder in the cylinder was covered with a top plate, which was a metal plate having the same diameter as the cylinder. A voltage was applied across the bottom and top plates, and a load was applied to the top plate in the direction from it to the bottom plate. The electrical current that flowed between the top and bottom plates was monitored while the load was increased. The load at which the current exceeded a predetermined threshold (in the unit of MPa [megapascals]) was reported as a measure of the strength of the adhesion of the insulating film **81C**. The result was graded with ⊙, ○, or ×. If the reading was 60 MPa or more, the grade was ⊙. If the reading was 20 MPa or more and less than 60 MPa (i.e., from 20 MPa to less than 60 MPa, the grade was ○. If the reading was less than 20 MPa, the grade was ×. The result is presented in Table 1.

(122) Production of Test Specimens

(123) For the testing of the withstand voltage, relative permeability, and saturation flux density of articles shaped from the soft magnetic particles of sample A1-01, test specimens of sample A1-01 were produced. Ring-shaped test specimens were produced by compression molding of first soft magnetic particles **81** (sample A1-01), second soft magnetic particles **82**, and epoxy resins. The second soft magnetic particles **82** were particles of sample A2-05, which will be described later.

(124) The second soft magnetic particles **82** used to make the test specimens were ones having an average diameter of 3 μm obtained by forming a 2-nm-thick insulating film **82B** (described later) containing an alkyl group having a C16 linear-chain moiety on nuclei **82A** (described later) made of crystalline pure iron. In the test specimens, the ratio by weight between the first and second soft magnetic particles **81** and **82** was 75:25, and the ratio by weight between the first and second soft magnetic particles **81** and **82** combined and the epoxy resins was 100:3.1. As for shape, the test specimens were toroids measuring 8 mm in inner diameter, 13 mm in outer diameter, and 5 mm in thickness.

(125) Withstand Voltage

(126) A test specimen of sample A1-01 was tested for withstand voltage by measuring it using an AC/DC withstand voltage/insulation resistance tester. The result is presented in Table 1.

(127) Magnetic Permeability

(128) A test specimen of sample A1-01 was tested for relative permeability by measuring it using a BH analyzer and an impedance/material analyzer with a 1-MHz radiofrequency signal. The result is presented in Table 1.

(129) Saturation Flux Density

(130) A test specimen of sample A1-01 was tested for saturation flux density by measuring the change in its inductance under an applied DC current using an LCR meter and a DC power supply and determining the saturation flux density from the BH data obtained. The result is presented in Table 1.

(131) Samples A1-02 to A1-27

(132) Samples A1-02 to A1-27 were prepared and tested for the strength of adhesion, withstand voltage, relative permeability, and saturation flux density in the same way as sample A1-01. The Cr content of the nuclei **81A** was as in Table 1, and the Fe and Si contents and the oxygen content were also changed. The average thickness of the oxide film **81B**, produced by surface oxidation of the nuclei **81A**, increased with increasing oxygen content when the Cr content was constant.

(133) TABLE-US-00001

TABLE 1	Thickness	Magnetic gap of the	Withstand	Saturation	performance	Sample	Cr	Fe	Si	Oxygen	oxide film																																																																																																																																																																																																																																																																																													
Strength of voltage	Relative flux density	factor No.	(wt %)	(wt %)	(wt %)	(ppm)	(nm)	adhesion (V/mm)	permeability (T)	(μ × BS)																																																																																																																																																																																																																																																																																														
A1-01	0	93	3.5	500	17	X	32	36.0	1.20	43.20	A1-02	0	93	3.5	800	18	X	35	35.0	1.21	42.35	A1-03	0	93	3.5	900	26	⊙	38	35.5	1.23	43.67	A1-04	0	93	3.5	1200	45	⊙	41	35.3	1.25	44.13	A1-05	0	93	3.5	1500	59	⊙	53	33.8	1.25	42.25	A1-06	0	93	3.5	2500	95	⊙	64	32.8	1.24	40.67	A1-07	0	93	3.5	2600	130	⊙	70	31.8	1.21	38.48	A1-08	0	93	3.5	2800	151	⊙	75	30.8	1.25	38.50	A1-09	0	93	3.5	3000	155	X	77	29.0	1.20	34.80	A1-10	0.5	92	3.5	500	12	X	30	36.7	1.05	38.54	A1-11	0.5	92	3.5	800	16	X	33	36.5	1.05	38.33	A1-12	0.5	92	3.5	900	19	○	36	36.2	1.05	38.01	A1-13	0.5	92	3.5	1200	33	○	39	36.0	1.06	38.16	A1-14	0.5	92	3.5	1500	45	○	50	34.5	1.09	37.61	A1-15	0.5	92	3.5	2600	90	○	61	33.5	1.08	36.18	A1-16	0.5	92	3.5	2800	114	○	67	32.4	1.10	35.64	A1-17	0.5	92	3.5	3000	133	X	71	31.4	1.14	35.80	A1-18	1.5	90	3.5	500	9	X	29	37.1	1.00	37.10	A1-19	1.5	90	3.5	800	14	X	32	37.5	1.00	37.50	A1-20	1.5	90	3.5	900	19	○	36	38.1	1.00	38.10	A1-21	1.5	90	3.5	1200	25	○	37	37.9	1.01	38.28	A1-22	1.5	90	3.5	1500	38	○	48	36.3	1.03	37.39	A1-23	1.5	90	3.5	2600	81	○	58	35.2	1.07	37.66	A1-24	1.5	90	3.5	2800	100	○	62	34.2	1.05	35.91	A1-25	1.5	90	3.5	3000	120	X	68	33.0	1.08	35.64	A1-26	2	89	5.2	500	4	X	30	36.0	0.95	34.20	A1-27	2.5	88	5.5	500	3	X	30	37.9	0.90	34.11

(134) FIG. 9 presents electron microscope images of the surface of types of nuclei **81A** that contained no Cr (Cr-free) and whose oxygen content was 500, 1200, 1500, 2500, or 2600 ppm, i.e., nuclei **81A** of samples A1-01, A1-04, A1-05, A1-06, and A1-07. As can be seen from the difference between samples in the surface condition of the nucleus **81A** shown in FIG. 9, undulations on the surface of the oxide film **81B** became deeper with increasing thickness of the oxide film **81B**, or with increasing oxygen content of the nuclei **81A** before the formation of the insulating film **81C**. A possible cause of this deepening of undulations on the oxide film **81B** with increasing thickness, the inventors believe, is that the increase in the thickness of the oxide film **81B** changed the status of contact between nuclei **81A**, making a difference in the dryness of the surface of the nuclei **81A** that resulted in variations in the tendency for oxidation of the Fe—Si alloy from place to place.

(135) When the oxygen content was 900 ppm or higher, the average thickness of the oxide film **81B** was large, and the thickness gap of the oxide film **81B** was large enough that the strength of the adhesion of the insulating film **81C** met its acceptance criteria. In view of the strength of the adhesion of the insulating film **81C**, therefore, it is desirable that the oxygen content of the first soft magnetic particles **81** be about 900 ppm or more.

(136) This strengthening of the adhesion of the insulating film **81C** with increasing thickness of the oxide film **81B**, the inventors believe, owes to an enhancement of anchoring effect as a result of the deepening of undulations on the surface of the oxide film **81B** with increasing thickness of the oxide film **81B**.

(137) When the strength of adhesion with samples A1-26 and A1-27 is compared with that with samples A1-03 to A1-08, A1-12 to A1-16, and A1-20 to A1-24 in Table 1, furthermore, it is found that this strengthening of adhesion owing to increasing surface roughness was observed when the Cr content was 1.5% by weight or less, and was significant with the Cr-free (containing no Cr) samples A1-03 to A1-08.

(138) FIG. **10** is a graphical representation of the dependence of withstand voltage on oxygen content for the Cr-free samples A1-01 to A1-09. FIG. **11** is a graphical representation of the dependence of relative permeability and saturation flux density on oxygen content for samples A1-01 to A1-09. FIG. **12** is a graphical representation of the dependence of a magnetic performance factor on oxygen content for samples A1-01 to A1-09.

(139) The withstand voltage, in FIG. **10**, increased with increasing oxygen content. The inventors believe this is because the adhesion of the insulating film **81C** became stronger with increasing thickness of the oxide film **81B**. As the strength of adhesion increased, the insulation resistance of the nuclei **81A** of the first soft magnetic particles **81** to the surroundings increased. The resistivity of the test specimen (shaped article) also rose accordingly.

(140) The relative permeability, in FIG. **11**, decreased with increasing oxygen content. The inventors believe this is because the percentage of the Fe—Si alloy in the nuclei **81A**, or the metal content of the soft magnetic particles, decreased with increasing oxygen content, or with increasing percentage of oxidized Fe—Si alloy in the nuclei **81A**. The data also indicate that limiting the oxygen content to about 2800 ppm or less will reduce the decrease in relative permeability associated with the increase in the thickness of the oxide film **81B** to approximately 15% of that at an oxygen content of about 500 ppm.

(141) The saturation flux density increased with oxygen content. The inventors believe this is also because the percentage of the oxidized form of the Fe—Si alloy, the soft magnetic metal forming the nuclei **81A**, increased. As the percentage of oxidized alloy increased, the cross-sectional area of the Fe—Si alloy moiety in the nuclei **81A** decreased, resulting in a decrease in the proportion of effective magnetic fluxes, or the magnetic fluxes that passed through the Fe—Si alloy moiety of the nuclei **81A**, to all magnetic fluxes through the test specimen. In FIG. **11**, the falls in saturation flux density observed at oxygen contents of 2500, 2600, and 3000 ppm are attributable to factors such as the measuring conditions and the quality of the test specimen. A subsequent investigation has identified the cause of these outliers, revealing that the calculated volume of the test specimen was wrong at 2500 ppm, the test specimen heated because of mistakenly selected measuring conditions at 2600 ppm, and the test specimen was in an abnormal condition at 3000 ppm.

(142) Based on these results, sufficiently strong adhesion of the insulating film **81C** and a practically high withstand voltage are combined without great loss of relative permeability when the oxygen content of the first soft magnetic particles **81** as a component of the core **40** is about 900 ppm or more and about 2800 ppm or less (i.e., from about 900 ppm to about 2800 ppm). It is desirable that the oxygen content of the first soft magnetic particles **81** be in this range.

(143) Overall, the soft magnetic powder in the powder mix used to form the core **40** contains first soft magnetic particles **81**. The first soft magnetic particles **81** are composed of nuclei **81A** containing a soft magnetic metal and an insulating film **81C** on the surface of the nuclei **81A**. The nuclei **81A** have an oxide film **81B** formed by oxide(s) of the soft magnetic metal under the insulating film **81C**. The nuclei **81A** contain no Cr or about 1.5% by weight or less Cr, and their oxygen content by weight is about 900 ppm or more and about 2800 ppm or less (i.e., from about 900 ppm to about 2800 ppm).

(144) This configuration ensures the core **40** can withstand high voltages consistently with limited loss of magnetic permeability when the powder mix, containing the first soft magnetic particles **81**, is shaped into the core **40** as a magnetic metal material by compression molding.

(145) The soft magnetic metal in the nuclei **81A** of the first soft magnetic particles **81** can be an iron-based soft magnetic metal containing Fe and Si. This arrangement makes it easier to form the oxide film **81B** on the surface of the nuclei **81A**.

(146) The iron-based soft magnetic metal can be crystalline. This arrangement makes the formation of the oxide film **81B** on the surface of the nuclei **81A** even easier.

(147) Besides the first soft magnetic particles **81**, the soft magnetic powder as a component of the powder mix can contain second soft magnetic particles **82** that contain a soft magnetic metal and have an average diameter smaller than that of the first soft magnetic particles **81**. Using second soft magnetic particles **82** as described below in addition to the first soft magnetic particles **81** helps achieve higher magnetic permeability as they improve the packing of soft magnetic particles in the core **40**.

(148) When a magnetic metal material shaped from soft magnetic powder containing first soft magnetic particles **81** according to any of the examples in this chapter is combined with a coil of wire **31**, an inductor **1** is given. An inductor configured as such can be small yet highly reliable by virtue of its high withstand voltage.

(149) A-1-2. Second Soft Magnetic Particles

(150) A-1-2-1. Embodiment of Second Soft Magnetic Particles

(151) FIG. **13** is a diagram illustrating the structure of the second soft magnetic particles **82**. The second soft magnetic particles **82** are each composed of a nucleus **82A** made of a soft magnetic metal and an insulating film **82B** on the surface of the nucleus **82A**. The soft magnetic metal forming the nucleus **82A** is, for example, crystalline or amorphous iron (Fe). Specifically, the second soft magnetic particles **82** are particles of powdered carbonyl iron in onion-skin structure containing about 95% by weight or more and about 99.8% by weight or less (i.e., from about 95% by weight to about 99.8% by weight) Fe, preferably about 97% by weight or more and about 99.8% by weight or less (i.e., from about 97% by weight to about 99.8% by weight) Fe. The powdered carbonyl iron can contain carbon (C), oxygen (O), nitrogen (N), and/or sulfur (S) as impurity(ies). The powdered carbonyl iron to be used as the nuclei **82A** may have an Fe oxide film on its surface. (152) Like that in the first soft magnetic particles **81**, the soft magnetic metal forming the nuclei **82A** of the second soft magnetic particles **82** does not need to be Fe; it can be an iron-based soft magnetic metal, which is Fe with other metal(s) contained therein.

(153) The insulating film **82B** on the second soft magnetic particles **82** is the product of a sol-gel reaction, for example involving silica, and contains a hydrocarbon group having a C8 or longer linear-chain moiety. Specific examples of hydrocarbon groups having a C8 or longer linear-chain moiety include alkyl groups, which are linear saturated hydrocarbon groups. The hydrocarbon group having a C8 or longer linear-chain moiety may be one or more hydrocarbon groups selected from the group consisting of the octyl, nonyl, decyl, undecyl, dodecyl, tridecyl, tetradecyl, pentadecyl, hexadecyl, heptadecyl, and octadecyl groups. Primary, secondary, and tertiary alkyl groups can all

be used.

(154) The long-chain hydrocarbon group can be formed as, for example, the product of a sol-gel reaction performed using a mixture of tetraethoxysilane (TEOS) and a silane coupling agent having the hydrocarbon group.

(155) Adding a hydrocarbon group having a C8 or longer linear-chain moiety to the insulating film **82B** on the second soft magnetic particles **82** can improve the packing of soft magnetic particles in the core **40** when the core **40** is shaped from the powder mix containing the first and second soft magnetic particles **81** and **82**.

(156) Without wishing to be bound by a particular theory, the inventors presume this improved packing of soft magnetic powder occurs through the following mechanism. As stated, the core **40** is formed by compression molding of powder mix that contains first soft magnetic particles **81**, second soft magnetic particles **82**, and epoxy resins (e.g., thermosetting resins). If the second soft magnetic particles **82** (smaller particles), for example, as one of the two sets of soft magnetic particles have a hydrocarbon group having a C8 or longer linear-chain moiety on their surface, the flowability (lubricity) of the second soft magnetic particles **82** during the compression molding can improve because the hydrocarbon group weakens the hydrogen bonds and/or bipolar interactions between the second soft magnetic particles **82** and the polar groups on the epoxy resins (e.g., epoxy and/or hydroxyl groups).

(157) The highly lubricated second soft magnetic particles **82**, as a result, are able to penetrate into the spaces between the first soft magnetic particles **81** (larger particles). The inventors believe such is a mechanism behind the improved packing of soft magnetic particles in the core **40** from that without a long-chain hydrocarbon group on the soft magnetic particles. Improved packing of soft magnetic particles leads to an increased density of soft magnetic powder in the core **40**, thereby helping increase the relative permeability of the core **40**.

(158) The lubricity of the second soft magnetic particles **82** can be measured using a direct shear testing machine as used in JIS Z8835. More specifically, it can be measured by the following procedure using a direct shear tester with a moving base (Nano Seeds Corporation NS-S500 powder bed shear stress analyzer). The inner diameter of the upper cell (ring) and that of the lower cell (base) are both set to 15 mm, and the ring-to-base distance (slit) is set to 0.2 mm. Before the powder is loaded, a lid is placed on the ring and base to define the zero point so that the thickness of the powder bed can be measured using a laser sensor. A 10-g sample powder of the second soft magnetic particles **82** is loaded into the two-part cell to fill the cell uniformly, the lid is placed gently, and an indentation load of 150 N is applied with a vertical servo motor. The applied 150-N indentation load will hold the position of the load cell of the vertical servo motor. The rate of indentation is set to 0.2 mm/sec. One hundred seconds after the holding of the load cell of the vertical servo motor, horizontal shear is induced; the delay of the start of horizontal shear is set to 100 seconds. After the horizontal servo motor starts inducing horizontal shear, the pressure is measured every 0.1 seconds. The rate of horizontal shear is set to 5 μm/sec. For each sample, the measurement is carried out at 50 or more points (N≥50) continuously during the operation of the horizontal servo motor and ended when the coefficient of variation (CV) of the measurements falls below 0.4%. The thickness of the powder bed at the end of consolidation (final thickness of the powder bed) is measured with a laser sensor.

(159) From the load on the load cell of the vertical servo motor measured when it is held (maximum load of indentation), the load on the load cell measured at the start of operation of the horizontal servo meter (indentation load at the start of horizontal shear), and the final thickness of the powder bed, the lubricity can be determined according to the equation below (for details, see, for example, Japanese Patent Application No. 2019-224678).

(160)

$$\text{Stress relaxation (\%)} = \frac{\text{Maximum load of indentation} - \text{Indentation load at the start of horizontal shear}}{\text{Maximum load of indentation}} \times 100$$
$$\text{Lubricity (\%/mm)} = \frac{\text{Stress relaxation (\%)}}{\text{Final thickness of the powder bed (mm)}} \quad [\text{Equation 1}]$$

(161) As stated, adding a hydrocarbon group having a C8 or longer linear-chain moiety to the surface of the second soft magnetic particles **82** will improve the packing of soft magnetic particles in the core **40** during the formation of the core **40** by lubricating the second soft magnetic particles **82**, thereby helping increase the magnetic permeability of the core **40**. Lubricating the second soft magnetic particles **82** by introducing a long-chain hydrocarbon group to their surface, however, can at the same time affect the mechanical strength of the core **40** because it means weakening the adhesion or binding between second soft magnetic particles **82** and the resin present therearound or other soft magnetic particles (the first soft magnetic particles **81** and/or another collection of second soft magnetic particles **82**).

(162) The inventors have found that the mechanical strength of the shaped core **40** can be improved by controlling the lubricity of the second soft magnetic particles **82** by reducing the number of long-chain hydrocarbon groups, or hydrocarbon groups having a C8 or longer linear chain-moiety, on the surface of their nuclei **82A**.

(163) An example of a way to control the number of long-chain hydrocarbon groups on the surface of the second soft magnetic particles **82** is to adjust the proportions of tetraethoxysilane and the silane coupling agent in the mixture for sol-gel reaction used when the insulating film **82B** is formed on the surface of the nuclei **82A**.

(164) The number of long-chain hydrocarbon groups on the surface of the second soft magnetic particles **82** can be evaluated based on the proportions of silicon (Si) and carbon (C) in the insulating film **82B**. If the nuclei **82A** of the second soft magnetic particles **82** are free of both Si and C, the number of long-chain hydrocarbon groups can be evaluated on the basis of the ratio by weight of Si to C (Si/C weight ratio) in the second soft magnetic particles **82** as a whole. To maintain high magnetic permeability with limited loss of the mechanical strength of the core **40**, it is desirable that the Si/C weight ratio of the second soft magnetic particles **82** be about 7.6 or more and about 42.8 or less (i.e., from about 7.6 to about 42.8).

(165) In this embodiment, of the first and second soft magnetic particles **81** and **82**, differing in average diameter, in the powder mix, the second soft magnetic particles **82**, which have the smaller average diameter, have a long-chain hydrocarbon group on the surface of their nuclei **82A**. The long-chain hydrocarbon group, however, does not need to be on the second soft magnetic particles **82**. For example, an insulating film **82B** containing a hydrocarbon group having a C8 or longer linear-chain moiety as described above may be formed on the surface of the first soft magnetic particles **81** or the surface of both the first and second soft magnetic particles **81** and **82** instead of the second soft magnetic particles **82**. This will lubricate the surface of the first soft magnetic particles **81** or the surface of both the first and second soft magnetic particles **81** and **82**. In this case, too, the core **40** will have high magnetic permeability with limited loss of mechanical strength.

(166) A-1-2-2. Production of the Second Soft Magnetic Particles

(167) The following describes the production of second soft magnetic particles **82** according to an embodiment of the present disclosure. The following is merely an example and is not the only method for producing second soft magnetic particles **82** according to an embodiment of the disclosure.

(168) Preparation of Nuclei of Soft Magnetic Metal

(169) First, fine particles of metal as a precursor to the nuclei **82A** of the second soft magnetic particles **82** are prepared. The details of the

second soft magnetic particles **82**, such as average diameter and the composition of the nuclei **82A**, are as described above. It would be fair to assume that the surface treatment, described below, will make no substantial change in the average diameter of the nuclei **82A**.

(170) Formation of Insulating Film on the Surface of the Nuclei

(171) Then an insulating film **82B** containing a hydrocarbon group having a C8 or longer linear-chain moiety is formed on the surface of the nuclei **82A**. The insulating film **82B** can be formed through, for example, a sol-gel reaction of a surface treatment agent that contains tetraethoxysilane, which is an alkoxide, and a silane coupling agent. This will produce, on the nuclei **82A**, an insulating film **82B** having a hydrocarbon group with a linear-chain moiety as the product of the sol-gel reaction.

(172) The alkoxide does not need to be tetraethoxysilane; any metal alkoxide represented by the chemical formula $M-(OR)_{sub.n}$ can be used. Preferably, the metal(s) M in the metal alkoxide is one or more selected from the group consisting of Li, Na, Mg, Al, Si, K, Ca, Ti, Cu, Sr, Y, Zr, Ba, Ce, Ta, and Bi. The alkoxy group(s) OR in the metal alkoxide can be of any kind, such as the methoxy, ethoxy, and/or propoxy groups.

(173) A silane coupling agent is represented by the chemical formula $R'-Si(OR)_{sub.3}$. R' represents a hydrocarbon group having a C8 or longer linear-chain moiety and may be one or more selected from the group consisting of, for example, the octyl, nonyl, decyl, undecyl, dodecyl, tridecyl, tetradecyl, pentadecyl, hexadecyl, heptadecyl, and octadecyl groups. OR represents an alkoxy group and preferably is a methoxy or ethoxy group. If, for example, the manufacturer wants to form a hydrocarbon group having a C16 or longer linear-chain moiety, hexadecyltrimethoxysilane can be used.

(174) The lubricated second soft magnetic particles **82** obtained in such a way help make the core **40** a magnetic material (magnetic core) of high relative permeability. When shaped into the core **40** by compression molding together with the first soft magnetic particles **81** and epoxy resins, the second soft magnetic particles **82** are not restricted by the epoxy resins excessively but fill the spaces between the first soft magnetic particles **81** efficiently by virtue of their imparted lubricity.

(175) Desirably, the formation of the insulating film **82B** on the nuclei **82A** includes forming a tetraethoxysilane film on the surface of the nuclei **82A** and forming a film containing a long-chain hydrocarbon group, or hydrocarbon group having a C8 or longer linear-chain moiety, on the tetraethoxysilane film through a sol-gel reaction between the tetraethoxysilane and a silane coupling agent. This helps reduce the amount of silane coupling agent used to form the insulating film **82B**; the long-chain hydrocarbon groups will be distributed on the surface of the insulating film **82B** effectively, with only a limited fraction of them buried inside the insulating film **82B**.

(176) The surface treatment agent can be one that contains a surfactant during the formation of a tetraethoxysilane film. Adding a surfactant to the surface treatment agent will help lubricate the entire surface of the second soft magnetic particles **82**. The surfactant forms micelles, and the hydrophilic moiety of the micelles will form hydrogen bonds with silanol groups produced by the hydrolysis of the tetraethoxysilane. During the formation of a tetraethoxysilane, therefore, the micelles will be distributed on the surface of the soft magnetic metal nuclei **82A**, creating dense and sparse populations of tetraethoxysilane molecules on the surface of the nuclei **82A**. The subsequently formed long-chain, C8 or longer, hydrocarbon groups will be spaced apart from one another and, as a result, will disperse widely on the surface of the insulating film **82B**.

(177) A-1-2-3. Examples of Second Soft Magnetic Particles

(178) Twenty-seven samples of soft magnetic particles differing in the number of carbon atoms in the linear-chain moiety of the hydrocarbon group in the insulating film **82B** and the ratio by weight of Si to C (Si/C weight ratio) in the insulating film **82B** were prepared as samples A2-01 to A2-27 and characterized. A summary of samples A2-01 to A2-27 is presented in Table 2. Samples A2-01 to A2-09, A2-15 to A2-18, and A2-24 to A2-27 are examples of second soft magnetic particles **82** according to an embodiment of the present disclosure. Table 2 also presents data on the silane coupling agent used to produce the insulating film **82B** for each of samples A2-01 to A2-27.

(179) TABLE-US-00002 TABLE 2 Linear- Si/C weight Sample chain carbon ratio in the No. atoms insulating film Silane coupling agent
A2-01 16 6.5 Hexadecyltrimethoxysilane A2-02 16 7.6 Hexadecyltrimethoxysilane A2-03 16 8.1 Hexadecyltrimethoxysilane A2-04 16 9.7 Hexadecyltrimethoxysilane A2-05 16 10.7 Hexadecyltrimethoxysilane A2-06 16 13.4 Hexadecyltrimethoxysilane A2-07 16 17.8 Hexadecyltrimethoxysilane A2-08 16 42.8 Hexadecyltrimethoxysilane A2-09 16 81.1 Hexadecyltrimethoxysilane A2-10 0 7.6 Tetraethoxysilane A2-11 1 7.6 Methyltrimethoxysilane A2-12 2 7.6 Ethyltrimethoxysilane A2-13 3 7.6 n-propyltrimethoxysilane A2-14 6 7.6 Hexyltrimethoxysilane A2-15 8 7.6 Octyltrimethoxysilane A2-16 10 7.6 Decyltrimethoxysilane A2-17 12 7.6 Dodecyltrimethoxysilane A2-18 18 7.6 Octadecyltrimethoxysilane A2-19 0 42.8 Tetraethoxysilane A2-20 1 42.8 Methyltrimethoxysilane A2-21 2 42.8 Ethyltrimethoxysilane A2-22 3 42.8 n-propyltrimethoxysilane A2-23 6 42.8 Hexyltrimethoxysilane A2-24 8 43.8 Octyltrimethoxysilane A2-25 10 44.8 Decyltrimethoxysilane A2-26 12 45.8 Dodecyltrimethoxysilane A2-27 18 45.8 Octadecyltrimethoxysilane

(180) The following describes the individual samples.

(181) Sample A2-01

(182) Preparation of Nuclei

(183) For use as the nuclei **82A** of the second soft magnetic particles **82**, particles of powdered carbonyl iron containing 97% by weight or more and 99.8% by weight or less (i.e., from 97% by weight to 99.8% by weight) iron were selected. The hardness of the nuclei **82A** was 952 HV, substantially equal to that of the nuclei **81A** of the first soft magnetic particles **81** used in samples A1-01 to A1-08.

(184) Formation of Insulating Film Containing a Long-Chain Hydrocarbon Group

(185) On the surface of the nuclei **82A**, an insulating film **82B** containing an alkyl group having a C16 linear-chain moiety was formed. The surface treatment agent for the formation of the insulating film **82B** was a liquid mixture of tetraethoxysilane as an alkoxide, hexadecyltrimethoxysilane as a silane coupling agent, and a phosphate anionic surfactant as a surfactant.

(186) Specifically, the procedure was as follows. The tetraethoxysilane and hexadecyltrimethoxysilane were KBE04 (Shin-Etsu Chemical Co., Ltd.) and X-88-422 (Shin-Etsu Chemical Co., Ltd.), respectively. The phosphate anionic surfactant was PLYSURF AL (DKS Co., Ltd.).

(187) First, a tetraethoxysilane film was formed on the surface of the nuclei **82A**. Isopropyl alcohol, aqueous ammonia, and an aqueous solution of PLYSURF AL were mixed together and stirred (liquid dispersion 1). Isopropyl alcohol was added to a predetermined weight of the nuclei **82A**, and the powder of the nuclei **82A** was dispersed by sonication (liquid dispersion 2). Liquid dispersion 2 was stirred with liquid dispersion 1 using a stirrer (liquid dispersion 3).

(188) Then tetraethoxysilane was mixed into isopropyl alcohol (surface treatment solution 1). Surface treatment solution 1 was added to liquid dispersion 3 (reaction solution 1). Stirring reaction solution 1 with a stirrer produced a tetraethoxysilane film on the surface of the nuclei **82A**.

(189) On the surface of the resulting tetraethoxysilane film, a film containing an alkyl group having a C16 linear-chain moiety was formed. First, isopropyl alcohol, hexadecyltrimethoxysilane, and tetraethoxysilane were mixed together (surface treatment solution 2). Surface treatment solution 2 was added to reaction solution 1 (reaction solution 2). Stirring reaction solution 2 with a stirrer produced a film

containing an alkyl group having a C16 linear-chain moiety on the surface of the tetraethoxysilane film.

(190) Then reaction solution **2** was suction-filtered through a membrane filter to isolate particles covered with the insulating film **82B**. The isolated particles were washed with acetone as needed, air-dried at room temperature, and classified through a metal mesh sieve. The particles left on the sieve were used as sample A2-01 of second soft magnetic particles **82**.

(191) The average (median) diameter of the resulting second soft magnetic particles **82** was 1.7 μm . The average diameter was measured using a particle size analyzer.

(192) Si/C Weight Ratio of the Nuclei Covered with the Insulating Film

(193) As an indicator of the number of hydrocarbon groups having a C16 linear-chain moiety on the surface of the insulating film **82B**, the Si/C weight ratio of sample A2-01 was checked as follows after the formation of the insulating film **82B**.

(194) First, the second soft magnetic particles **82** covered with the insulating film **82B** was irradiated with x-rays using an x-ray photoelectron spectrometer, and information on the intensity of the peaks for the chemical elements contained in the insulating film **82B** was obtained by measuring what is called a wide-scan spectrum. Then the integrated intensity of the peaks for Si and C in the insulating film **82B** was determined by measuring what is called a narrow-scan spectrum. Normalizing the determined intensities based on the relative sensitivity factors of elemental orbitals gave the concentrations of the elements in atm % with the total as 100%. These atm % concentrations were multiplied by the atomic weight of the respective elements, and the products were used to calculate the ratio by weight between Si and C.

(195) Lubricity

(196) Sample A2-01 was tested for lubricity by analyzing 10 g of the soft magnetic particles of the sample using a direct shear tester with a moving base (Nano Seeds Corporation NS-S500 powder bed shear stress analyzer). The inner diameter of the upper cell (ring) and that of the lower cell (base) were both set to 15 mm, and the indentation load was set to 150 N. The result is presented in Table 3.

(197) Production of Test Specimens

(198) For the testing of articles shaped from the soft magnetic particles of sample A2-01, test specimens of sample A2-01 were produced. Ring-shaped test specimens were produced by compression molding of first soft magnetic particles **81**, second soft magnetic particles **82** (sample A2-01), and epoxy resins.

(199) The first soft magnetic particles **81** were particles of sample A1-04, which were particles of Cr-free amorphous Fe—Si alloy having an average diameter of 25.3 μm coated with a 5-nm-thick oxide film **81B** and a 23-nm-thick insulating film **81C**. The proportions (ratio by weight) of the first and second soft magnetic particles **81** and **82** were 75:25, and those of the first and second soft magnetic particles **81** and **92** combined and the epoxy resins were 100:3.1. As for shape, the test specimens were toroids measuring 8 mm in inner diameter, 13 mm in outer diameter, and 4 mm in thickness.

(200) Magnetic Permeability

(201) A test specimen of sample A2-01 was tested for relative permeability by measuring it using a BH analyzer and an impedance/material analyzer with a 1-MHz radiofrequency signal. The result was graded with \bigcirc or \times . If the reading was equal to or higher than the acceptance limit of 30, the grade was \bigcirc . If the reading was lower than the acceptance limit of 30, the grade was \times . The measured relative permeability and the grade are presented in Table 3.

(202) Radial Crushing Strength

(203) A test specimen of sample A2-01 was tested for radial crushing strength by applying a radial pressure to the toroidal test specimen and measuring the pressure at which the test specimen was broken. The result was graded with \bigcirc or \times . If the reading was equal to or higher than the acceptance limit of 85 N/mm^{sup.2}, the grade was \bigcirc . If the reading was lower than the acceptance limit of 85 N/mm^{sup.2}, the grade was \times . The measured radial crushing strength and the grade are presented in Table 3.

(204) Withstand Voltage

(205) A test specimen of sample A2-01 was tested for withstand voltage by measuring it using an AC/DC withstand voltage/insulation resistance tester. The result was graded with \bigcirc or \times . If the reading was equal to or higher than the acceptance limit of 50 V/mm, the grade was \bigcirc . If the reading was lower than the acceptance limit of 50 V/mm, the grade was \times . The grade is presented in Table 3.

(206) Samples A2-02 to A2-27

(207) Samples A2-02 to A2-27 were prepared and tested for lubricity in the same way as sample A2-01. The silane coupling agent specified in Table 2 was used, the number of carbon atoms in the linear-chain moiety of the hydrocarbon group in the insulating film **82B** was as in Table 2, and the Si/C weight ratio of the insulating film **82B** was as in Table 2. The procedure for the formation of the insulating film **82B** was the same as that for sample A2-01. For each of samples A2-02 to A2-27, test specimens similar to those of sample A2-01 were produced using the soft magnetic particles of the sample as second soft magnetic particles **82**. Using these test specimens, the samples were tested for relative permeability, radial crushing strength, and withstand voltage and graded in the same way as with sample A2-01.

(208) In the production of samples A2-01 to A2-27, the Si/C weight ratio was adjusted by changing the proportions of the tetraethoxysilane and the silane coupling agent used to form the insulating film **82B**.

(209) The test results for samples A2-01 to A2-09 are presented in Table 3, those for samples A2-10 to A2-18 are presented in Table 4, and those for samples A2-19 to A2-27 are presented in Table 5.

(210) TABLE-US-00003

Sample	carbon	insulating	Lubricity	Relative strength	voltage	permeability	strength	No. atoms	film (%/mm)	permeability (N/mm ^{sup.2})	grade	grade																																																																				
A2-01	16	6.5	3.0	35.3	82	\bigcirc	\bigcirc	X	A2-02	16	7.6	2.8	34.5	100	\bigcirc	\bigcirc	\bigcirc	A2-03	16	8.1	2.5	34.2	94	\bigcirc	\bigcirc	\bigcirc	A2-04	16	9.7	2.4	32.7	110	\bigcirc	\bigcirc	\bigcirc	A2-05	16	10.7	2.8	34.4	120	\bigcirc	\bigcirc	\bigcirc	A2-06	16	13.4	2.0	33.4	120	\bigcirc	\bigcirc	\bigcirc	A2-07	16	17.8	1.8	30.4	120	\bigcirc	\bigcirc	\bigcirc	A2-08	16	42.8	2.4	30.3	122	\bigcirc	\bigcirc	\bigcirc	A2-09	16	81.1	0.9	27.7	115	\bigcirc	X	\bigcirc

(211) TABLE-US-00004

Sample	carbon	insulating	Lubricity	Relative strength	voltage	permeability	strength	No. atoms	film (%/mm)	permeability (N/mm ^{sup.2})	grade	grade																																																																				
A2-10	0	7.6	1.5	22.6	120	X	X	\bigcirc	A2-11	1	7.6	1.6	23.2	120	X	X	\bigcirc	A2-12	2	7.6	2.1	23.8	120	\bigcirc	X	\bigcirc	A2-13	3	7.6	2.1	24.2	120	\bigcirc	X	\bigcirc	A2-14	6	7.6	2.2	25.4	120	\bigcirc	X	\bigcirc	A2-15	8	7.6	2.2	30.1	120	\bigcirc	\bigcirc	\bigcirc	A2-16	10	7.6	2.7	30.4	120	\bigcirc	\bigcirc	\bigcirc	A2-17	12	7.6	2.8	32.3	120	\bigcirc	\bigcirc	\bigcirc	A2-18	18	7.6	3.2	36.4	85	\bigcirc	\bigcirc	\bigcirc

(212) TABLE-US-00005

Sample	carbon	insulating	Lubricity	Relative strength	voltage	permeability	strength	No. atoms	film (%/mm)	permeability (N/mm ^{sup.2})	grade	grade																																																																				
A2-19	0	42.8	1.5	22.6	125	X	X	\bigcirc	A2-20	1	42.8	1.6	23.0	125	X	X	\bigcirc	A2-21	2	42.8	1.8	23.4	125	X	X	\bigcirc	A2-22	3	42.8	2.1	24.8	125	\bigcirc	X	\bigcirc	A2-23	6	42.8	2.1	25.4	125	\bigcirc	X	\bigcirc	A2-24	8	43.8	2.2	29.5	125	\bigcirc	X	\bigcirc	A2-25	10	44.8	2.2	29.6	125	\bigcirc	X	\bigcirc	A2-26	12	45.8	2.3	29.7	125	\bigcirc	X	\bigcirc	A2-27	18	45.8	2.5	32.0	84	\bigcirc	\bigcirc	X

(213) As can be seen from the measured lubricity and magnetic permeability grades in Tables 3 to 5, the presence of a hydrocarbon group having a C8 or longer linear-chain moiety in the insulating film **82B** on the surface of the nuclei **82A** improves the lubricity of the soft magnetic particles. The improved lubricity of the soft magnetic particles leads to improved density and, therefore, improved relative permeability of the shaped article (test specimen).

(214) For a given Si/C weight ratio, there is a trade-off between relative permeability and radial crushing strength. If the hydrocarbon group in the insulating film **82B** has a C8 or longer linear-chain moiety, the resulting core combines high relative permeability with practically high mechanical strength as long as the Si/C weight ratio is about 7.6 or more and about 42.8 or less (i.e., from about 7.6 to about 42.8); in that case the radial crushing strength is about 85 or more and the relative permeability is about 30 or more, despite the trade-off therebetween. In view of repeatability in production, it is more preferred that the Si/C weight ratio be about 9.7 or more and about 13.4 or less (i.e., from about 9.7 to about 13.4).

(215) Overall, the soft magnetic powder as a component of the powder mix contains second soft magnetic particles **82**. The second soft magnetic particles **82** are composed of nuclei **82A** containing a soft magnetic metal and an insulating film **82B** on the surface of the nuclei **82A**. The insulating film **82B** contains Si and also contains a hydrocarbon group having a C8 or longer linear-chain moiety. The ratio by weight of Si to C in the insulating film **82B** is about 7.6 or more and about 42.8 or less (i.e., from about 7.6 to about 42.8).

(216) This configuration ensures the core **40** will combine high mechanical strength and high magnetic permeability when the powder mix, containing the second soft magnetic particles **82**, is shaped into the core **40** as a magnetic metal material by compression molding. The source of Si is, for example, a silane coupling agent used to produce the insulating film **82B**.

(217) The hydrocarbon group in the insulating film **82B** on the second soft magnetic particles **82** can be alkyl group(s). This arrangement makes the formation of a hydrocarbon group having a C8 or longer linear-chain moiety on the surface of the nuclei **82A** easier.

(218) The nuclei **82A** of the second soft magnetic particles **82** can be particles of carbonyl iron. This arrangement will give the core **40** higher magnetic permeability when the powder mix is shaped into the core **40** as a magnetic metal material.

(219) Besides the second soft magnetic particles **82**, the soft magnetic powder as a component of the powder mix can contain first soft magnetic particles **81** that contain a soft magnetic metal and whose nuclei **81A** have an average diameter larger than that of the nuclei **82A** of the second soft magnetic particles **82**. This arrangement will improve the packing of soft magnetic particles in the core **40**, thereby helping achieve higher magnetic permeability.

(220) When a magnetic metal material shaped from soft magnetic powder containing second soft magnetic particles **82** according to any of the examples in this chapter is combined with a coil of wire **31**, an inductor **1** is given. An inductor configured as such can be small yet highly reliable.

(221) A-2. Resins

(222) The percentage of the resins is about 2.0% by weight or more and about 3.5% by weight or less (i.e., from about 2.0% by weight to about 3.5% by weight) of the total weight of the soft magnetic powder and resins. The resins include at least a bisphenol-A epoxy resin and a rubber-modified epoxy resin, optionally with a phenol-novolac epoxy resin.

(223) The inventors have identified proportions of the bisphenol-A and rubber-modified epoxy resins appropriate for the case when the powder mix contains no phenol-novolac epoxy resin (first resin formula; see the experimental test described later). The first resin formula is about 50% by weight or more and about 90% by weight or less (i.e., from about 50% by weight to about 90% by weight) bisphenol-A epoxy resin and about 10% by weight or more and about 50% by weight or less (i.e., from about 10% by weight to about 50% by weight) rubber-modified epoxy resin, both based on the total weight of resins in the powder mix.

(224) The bisphenol-A epoxy resin is the most abundant resin in the powder mix, but if it is the only resin in the powder mix, the resulting body **10** will often be brittle. Adding a rubber-modified epoxy resin to the powder mix helps reduce the brittleness of the body **10** as it will give the body **10** toughness. Selecting the proportions of the bisphenol-A and rubber-modified epoxy resins to all resins in the powder mix according to the first resin formula and shaping and curing (Step **300** in FIG. **5**) the powder mix into the body **10** with the coil **30** therein in the way as described above, furthermore, will give the inductor **1** improved body strength.

(225) The inventors have also identified proportions of the bisphenol-A, rubber-modified, and phenol-novolac epoxy resins appropriate for the case when the powder mix contains a phenol-novolac epoxy resin (second resin formula; see the experimental test described later). The second resin formula is about 40% by weight or more and about 80% by weight or less (i.e., from about 40% by weight to about 80% by weight) bisphenol-A epoxy resin, about 10% by weight or more and about 50% by weight or less (i.e., from 10% by weight to about 50% by weight) rubber-modified epoxy resin, and about 1% by weight or more and about 30% by weight or less (i.e., from about 1% by weight to about 30% by weight) phenol-novolac resin, all based on the total weight of resins in the powder mix.

(226) The function of the phenol-novolac epoxy resin is to adjust the flow viscosity of the powder mix when it is shaped and cured into the body and to improve the strength of the body at elevated temperatures by adjusting the glass transition temperature of the body. Mixing in a phenol-novolac epoxy resin according to the second resin formula, therefore, will give the inductor **1** improved body strength.

(227) In addition, the inventors have noticed that shaping the body **10** as described above using a powder mix containing resins according to the first or second resin formula will give the inductor **1** specific configurations 1 to 3 below.

(228) Specific configuration 1: In a cross-section of the body **10**, the percentage of the area of voids to the total area of the soft magnetic particles (first and second soft magnetic particles) and resins is smaller in the region between about 1 μm and about 100 μm from the surface of the body **10** (surface region) than in the middle region of the body **10**; the body **10** is denser in the surface region than in the middle region.

(229) Specific configuration 2: Referring to FIGS. **1** to **3**, the resin content is smaller near the ridges between the primary sides **12** and **14** and the second side surfaces **18** than near the ridges between the primary sides **12** and **14** and the first side surfaces **16**.

(230) Specific configuration 3: Referring to FIGS. **1** to **3**, polished first or second soft magnetic particles are exposed out of the core **40**, but these exposed particles are covered with the protective film **50**. The roughness of the second side surfaces **18** is larger than that of the first side surfaces **16**. The narrower of the distances between the second side surfaces **18** and the wound section **32** of the coil **30** is greater than about one time and smaller than about four times the diameter of the first soft magnetic particles.

(231) The following describes the mechanism through which specific configurations 1 to 3 are obtained. As stated referring to FIG. **6**, the body **10** is formed by setting the coil **30** into a first tablet **70**, placing a second tablet **72** to sandwich the coil **30** with the first tablet **70**, and combining the three components into a one-piece structure. The first and second tablets **70** and **72** are heated and at the same time pressed in the direction in which they are stacked. This will cause the powder mix to flow, giving a core with an embedded coil **30** therein.

(232) FIG. **14** is an image from a coil **30** sandwiched between first and second tablets **70** and **72** as illustrated in FIG. **6**, presenting a close-up of a region Ar around the coil **30** while being pressed in the direction of stacking. FIG. **15** is a cross-sectional image of the first tablet **70**. As shown in FIG. **14**, spaces s1, s2, and s3 are left alongside the coil **30**. This indicates when the first and second tablets **70** and **72** are

pressed in the direction of stacking of the powder mix fills the spaces in the outer region of the core first.

(233) That is, outside the coil **30**, the powder mix moves smoothly, spaces are filled easily, and, therefore, the density of packing tends to be high. Inside the coil **30**, by contrast, the powder mix does not move smoothly, spaces are not filled easily, and, therefore, the density of packing tends to be low. The powder mix is therefore packed more densely in the outside **s10** to **s13** of the coil **30** than in the inside **s14** of the coil **30** as in FIG. **15**. As a result, the inductor **1** will have specific configuration 1.

(234) Voids in the surface region of the body will affect the moisture resistance of the inductor because water in the air can come into the body through them. The voids will also accelerate the degradation of the body because plating solution can penetrate into the body through them during the formation of the outer electrodes. Increasing the density in the surface region of the body by this specific configuration helps prevent these problems.

(235) FIG. **16** is a diagram for the description of the LT and WT planes, which are reference planes of the inductor **1**. FIG. **17** presents LT and WT cross-sectional images of an inductor **1** made as illustrated in FIG. **16**. As stated, the second side surfaces **18** of the body **10** are ground before the formation of the protective film. The first side surfaces **16**, however, are not. Near the ridges **s22** and **s23** between a primary side (mount surface of the inductor **1** in the image) **12** and the second side surfaces **18**, which are seen in the WT cross-sectional image, therefore, the soft magnetic powder is ground to be flush with the second side surfaces **18**. The soft magnetic powder near the ridges **s22** and **s23** therefore becomes exposed over a large area, making the resin content near the ridges **s22** and **s23** smaller than that near the ridges **s20** and **s21** between a primary side **12** and the first side surfaces **16**, which are seen in the LT cross-sectional image. As a result, the inductor **1** will have specific configuration 2. Specific configuration 2 helps prevent the inductor from losing its electrical insulation because of soft magnetic particles sticking out of the protective film; by virtue of the grinding (Step **400** in FIG. **5**), there will be few protruding particles near the ridges between the primary sides **12** and the second side surfaces **18**.

(236) FIG. **18** is a tabulated representation of electron microscope images of the LT and WT surfaces after the shaping and curing and those after the grinding, along with the maximum heights of the surfaces. Maximum height **Sz** is a measure of surface roughness.

(237) Greater Maximum Heights **Sz** Indicate Greater Surface Roughness.

(238) In the grinding, the LT surfaces are scraped. Some of the first or second soft magnetic particles there are eliminated at the same time, increasing the roughness of the surfaces. The maximum height **Sz** of the LT surfaces (**50 μm**), therefore, becomes larger than that of the WT surfaces (**43 μm**), which are not ground. Increasing the roughness of the LT surfaces helps improve the adhesion between the protecting film and the core on these surfaces. The surface roughness in this context was determined by measuring the maximum height (**Sz**) longitudinally in the middle of the LT and WT surfaces using a 3D laser scanning microscope (Keyence VK-X250).

(239) In addition to this, the narrower of the distances **SG1** and **SG2** between the second side surfaces **18** and the coil **30**, illustrated in FIG. **19**, is set greater than the equivalent of about one first soft magnetic particle **81** and smaller than the equivalent of about four first soft magnetic particles **81**. As a result, the inductor **1** will have specific configuration 3. Specific configuration 3 helps ensure the body is resistant to moisture even if small in size.

(240) A-2-1. Embodiment with Resins According to the First Resin Formula

(241) Sample bodies of inductors were prepared in the way as described above using a powder mix containing resins according to the first resin formula and tested. The shaping and curing were carried out at a temperature of **135° C.** and with a pressure of **10 MPa**.

(242) Body Strength

(243) Each sample was tested for strength by measuring load at failure in a three-point flexural test performed using a tester (Shimadzu AGS-5kNX universal precision tester). The sample was considered passing the test (Pass in tables) if the load at failure was **30 MPa** or more, and failing (Fail in tables) if the load at failure was less than **30 MPa**.

(244) Density

(245) The porosity of each sample was measured by detecting voids in a cross-sectional image and calculating the percentage of the total void area to the area of the cross-section.

(246) Specifically, the sample body was cut at half its length, and the cross-section was imaged with a scanning electron microscope (SEM) set to a magnification of **×1000** at four points (one point per side) between **1 μm** and **100 μm** from the surface of the body. Then the voids in the cross-sectional images were measured, and the measurements were averaged. The porosity in the middle region of the body was also measured in the same way, by imaging the same cross-section at four points in the middle of the body with an SEM set to a magnification of **×1000**, measuring the voids in the cross-sectional images, and averaging the measurements.

(247) Excluding samples **b4** to **b8**, **b22**, **b23**, and **b27** (see the tables below), all sample bodies had a small average porosity across a total of eight points in the surface and middle regions. These sample bodies, furthermore, were denser in the surface region than in the middle region; the percentage of the void area in the surface region was smaller than that in the middle region.

(248) Percentage of Resins in the Powder Mix

(249) FIG. **20** is a graphical representation of the relationship between the resin content of the powder mix and the density of the body, with the density of the body (**g/cm³**) on the vertical axis and the resin content (**% by weight**) of the powder mix on the horizontal axis. The body was shaped at a temperature of **180° C.**, with a pressure of **30 MPa**, and for a duration of **100 seconds**. In FIG. **20**, the body has a reduced density when the resin content is smaller than about **2.0%**. Presumably, the powder mix in this case was not packed densely when shaped into the body because of its low flowability.

(250) TABLE-US-00006 TABLE 6 Resins contained Test item Rubber- Phenol- Body Bisphenol-A modified novolac strength Sample epoxy resin epoxy resin epoxy resin (flexural No. (% by weight) (% by weight) (% by weight) strength) *b1 100 0 0 Fail b2 90 10 0 Pass b3 80 20 0 Pass b4 70 30 0 Pass b5 60 40 0 Pass b6 50 50 0 Pass *b7 40 60 0 Fail The asterisked samples, **b1** and **b7**, are comparative examples.

(251) Based on the test results in Table 6, the inductor will have improved body strength when the powder mix has the following resin formula: about **50% by weight** or more and about **90% by weight** or less (i.e., from about **50% by weight** to about **90% by weight**) bisphenol-A epoxy resin and about **10% by weight** or more and about **50% by weight** or less (i.e., from about **10% by weight** to about **50% by weight**) rubber-modified epoxy resin (first resin formula).

(252) A-2-2. Embodiment with Resins According to the Second Resin Formula

(253) Sample bodies of inductors were prepared and tested in the same way as in the embodiment described in A-2-1 but using a powder mix containing resins according to the second resin formula. As in the embodiment in A-2-1, the percentage of resins in the powder mix was **2.0% by weight** or more and **3.5% by weight** or less (i.e., from **2.0% by weight** to **3.5% by weight**) of the powder mix.

(254) TABLE-US-00007 TABLE 7 Resins contained Test item Rubber- Phenol- Body Bisphenol-A modified novolac strength Sample epoxy resin epoxy resin epoxy resin (flexural No. (% by weight) (% by weight) (% by weight) strength) *b8 90 9 1 Fail b9 80 19 1 Pass b10 80 15 5 Pass b11 80 10 10 Pass b12 70 29 1 Pass b13 70 25 5 Pass b14 70 10 20 Pass b15 60 29 1 Pass b16 60 30 10 Pass b17 60 10 30

Pass b18 50 49 1 Pass b19 50 40 10 20 Pass b20 50 30 20 Pass b21 50 20 30 Pass *b22 50 10 40 Fail *b23 40 59 1 Fail b24 40 50 10 Pass b25 40 40 20 Pass b26 40 30 30 Pass *b27 40 20 40 Fail The asterisked samples, b8, b22, b23, and b27, are comparative examples. (255) Based on the test results in Table 7, the inductor will have improved body strength when the powder mix has the following resin formula: about 40% by weight or more and about 80% by weight or less (i.e., from about 40% by weight to about 80% by weight) bisphenol-A epoxy resin, about 10% by weight or more and about 50% by weight or less (i.e., from about 10% by weight to about 50% by weight) rubber-modified epoxy resin, and about 1% by weight or more and about 30% by weight or less (i.e., from about 1% by weight to about 30% by weight) phenol-novolac epoxy resin (second resin formula).

(256) A-2-3. Embodiment Regarding Side Gaps

(257) To find the relationship between the distances (side gaps) SG1 and SG2 between the second side surfaces 18 and the coil 30, illustrated in FIG. 19, and the moisture resistance of the inductor 1, the samples listed in Tables 8 and 9 were prepared and tested for moisture resistance.

(258) Moisture Resistance

(259) Each sample was subjected to moisture resistance testing in a humidity chamber conditioned to a temperature of 85° C. and a humidity of 85%. The sample was considered passing the test (Pass in the tables) if the weight gain of the body associated with water absorption was 2% by weight or less, and failed (Fail in the tables) if the weight gain exceeded 2% by weight.

(260) Powder Mix Specifications

(261) The percentage of resins in the powder mix was 2.0% by weight or more and 3.5% by weight or less (i.e., from 2.0% by weight to 3.5% by weight), and the first resin formula was used. In the powder mix, the average diameter of the larger soft magnetic particles (first soft magnetic particles) was 21 μm (the samples in Table 8) or 28 μm (the samples in Table 9), and that of the smaller soft magnetic particles (second soft magnetic particles) was 2 μm.

(262) The following describes the testing of samples b51 to b60, the samples listed in Table 8. Samples b54 to b60 are examples of an embodiment of the present disclosure, and samples b51 to b53 are comparative examples.

(263) TABLE-US-00008 TABLE 8 Average diameter of the larger particles, 21 μm; Average diameter of the smaller particles, 2 μm
Narrower Wider Sample side gap side gap Inductance Moisture No. (μm) (μm) (μH) resistance *b51 0 110 0.412 Fail *b52 10 100 0.417 Fail *b53 18 92 0.420 Fail b54 25 85 0.423 Pass b55 29 81 0.424 Pass b56 33 77 0.425 Pass b57 40 70 0.427 Pass b58 45 65 0.428 Pass b59 50 60 0.429 Pass b60 55 55 0.429 Pass The asterisked samples, b51, b52, and b53, are comparative examples.

Example Set A-2-3-1

Example A-2-3-11 (Sample b54)

(264) A body was formed with a narrower side gap of 25 μm and a wider side gap of 85 μm. Test result: Passed the moisture resistance test.

Example A-2-3-12 (Sample b55)

(265) A body was formed with a narrower side gap of 29 μm and a wider side gap of 81 μm. Test result: Passed the moisture resistance test.

Example A-2-3-13 (Sample b56)

(266) A body was formed with a narrower side gap of 33 μm and a wider side gap of 77 μm. Test result: Passed the moisture resistance test.

Example A-2-3-14 (Sample b57)

(267) A body was formed with a narrower side gap of 40 μm and a wider side gap of 70 μm. Test result: Passed the moisture resistance test.

Example A-2-3-15 (Sample b58)

(268) A body was formed with a narrower side gap of 45 μm and a wider side gap of 65 μm. Test result: Passed the moisture resistance test.

Example A-2-3-16 (Sample b59)

(269) A body was formed with a narrower side gap of 50 μm and a wider side gap of 60 μm. Test result: Passed the moisture resistance test.

Example A-2-3-17 (Sample b60)

(270) A body was formed with equal side gaps of 55 μm. Test result: Passed the moisture resistance test.

Comparative Example Set A-2-3-1

Comparative Example A-2-3-11 (Sample b51)

(271) A body was formed with a narrower side gap of 0 μm and a wider side gap of 110 μm. Test result: Failed the moisture resistance test.

Comparative Example A-2-3-12 (Sample b52)

(272) A body was formed with a narrower side gap of 10 μm and a wider side gap of 100 μm. Test result: Failed the moisture resistance test.

Comparative Example A-2-3-13 (Sample b53)

(273) A body was formed with a narrower side gap of 18 μm and a wider side gap of 92 μm. Test result: Failed the moisture resistance test.

(274) Based on the test results in Table 8, with first soft magnetic particles having an average diameter of about 21 μm, the body is resistant to moisture when its smaller side gap is greater than the equivalent of about one first soft magnetic particle and smaller than the equivalent of about four first soft magnetic particles.

(275) The following describes the testing of samples b61 to b70, the samples listed in Table 9. Samples b65 to b70 are examples of an embodiment of the present disclosure, and samples b61 to b64 are comparative examples.

(276) TABLE-US-00009 TABLE 9 Average diameter of the larger particles, 28 μm; Average diameter of the smaller particles, 2 μm
Narrower Wider Sample side gap side gap Inductance Moisture No. (μm) (μm) (μH) resistance *b61 0 110 0.424 Fail *b62 10 100 0.430 Fail *b63 18 92 0.433 Fail *b64 25 85 0.436 Fail b65 29 81 0.437 Pass b66 33 77 0.439 Pass b67 40 70 0.440 Pass b68 45 65 0.441 Pass b69 50 60 0.442 Pass b70 55 55 0.442 Pass The asterisked samples, b61, b62, b63, and b64, are comparative examples.

Example Set A-2-3-2

Example A-2-3-21 (Sample b65)

(277) A body was formed with a narrower side gap of 29 μm and a wider side gap of 81 μm. Test result: Passed the moisture resistance test.

Example A-2-3-22 (Sample b66)

(278) A body was formed with a narrower side gap of 33 μm and a wider side gap of 77 μm. Test result: Passed the moisture resistance test.

Example A-2-3-23 (Sample b67)

(279) A body was formed with a narrower side gap of 40 μm and a wider side gap of 70 μm. Test result: Passed the moisture resistance test.

Example A-2-3-24 (Sample b68)

(280) A body was formed with a narrower side gap of 45 μm and a wider side gap of 65 μm. Test result: Passed the moisture resistance test.

Example A-2-3-25 (Sample b69)

(281) A body was formed with a narrower side gap of 50 μm and a wider side gap of 60 μm. Test result: Passed the moisture resistance test.

Example A-2-3-26 (Sample b70)

(282) A body was formed with equal side gaps of 55 μm . Test result: Passed the moisture resistance test.

Comparative Example Set A-2-3-2

Comparative Example A-2-3-21 (Sample b61)

(283) A body was formed with a narrower side gap of 0 μm and a wider side gap of 110 μm . Test result: Failed the moisture resistance test.

Comparative Example A-2-3-22 (Sample b62)

(284) A body was formed with a narrower side gap of 10 μm and a wider side gap of 100 μm . Test result: Failed the moisture resistance test.

Comparative Example A-2-3-23 (Sample b63)

(285) A body was formed with a narrower side gap of 18 μm and a wider side gap of 92 μm . Test result: Failed the moisture resistance test.

Comparative Example A-2-3-24 (Sample b64)

(286) A body was formed with a narrower side gap of 25 μm and a wider side gap of 85 μm . Test result: Failed the moisture resistance test.

(287) Based on the test results in Table 9, with first soft magnetic particles having an average diameter of about 28 μm , the body is resistant to moisture when its smaller side gap is greater than the equivalent of about one first soft magnetic particle and smaller than the equivalent of about four first soft magnetic particles.

(288) A-2-4. Other Considerations

(289) In the above embodiments, the resins contained in the powder mix are a bisphenol-A epoxy resin, a rubber-modified epoxy resin, and a phenol-novolac epoxy resin. The superordinate category of bisphenol-A epoxy resins is epoxy resins, and that of rubber-modified epoxy resins is flexible rubbers or resins.

(290) Examples of resins that may potentially be used as an alternative to the bisphenol-A epoxy resin include bisphenol-A, -F, and -S phenoxy resins. Examples of resins or rubbers that may potentially be used as an alternative to the rubber-modified epoxy resin include urethane-modified, NBR (acrylonitrile butadiene rubber)-modified, and CTBN (carboxyl-terminated butadiene acrylonitrile) rubber-modified epoxy resins and CTBN rubber. Examples of resins that may potentially be used as an alternative to the phenol-novolac epoxy resin include cresol, dicyclopentadiene, phenol aralkyl, biphenyl, naphthol, xylylene, triphenylmethane, and tetrakisphenolethane epoxy resins if only novolac resins are considered. As for non-novolac resins, naphthalene, biphenyl, and triazine epoxy resins can be used.

(291) B. Coil

(292) The following describes the coil **30** component of an inductor **1** having a core **40** shaped from the powder mix of soft magnetic particles and resins described in A. Powder Mix.

(293) Wire

(294) The wire **31** that forms the coil **30** of the inductor **1** may be substantially round or may be substantially rectangular (in FIG. 3, it is substantially rectangular). Substantially rectangular wire **31** is easier to wind without space between portions thereof when forming the wound section **32**.

(295) The number of turns in the wound section **32** is selected according to the characteristics the inductor **1** should have.

(296) Preferably, the wire **31** is copper wire **36**.

(297) In an inductor **1** measuring, for example, about 2.0 mm \pm about 0.2 mm in length L, about 1.2 mm \pm about 0.2 mm in width W, and about 0.7 mm \pm about 0.1 mm in thickness T, the dimensions of the wound section **32** of the coil **30** are about 0.4 mm in height and about 1.17 mm in outer diameter and about 0.55 mm in inner diameter, both in the direction of width W.

(298) If the coil **30** is formed by substantially rectangular wire **31**, the shorter side of its cross-section can be, for example, about 0.118 mm or less. Preferably, the shorter side of the cross-section measures about 0.052 mm or more.

(299) The longer side of the cross-section of the substantially rectangular wire can be, for example, about 0.203 mm or less. Preferably, the longer side of the cross-section is about 0.141 mm or more.

(300) The aspect ratio (longer side/shorter side) of the cross-section of the substantially rectangular wire can be, for example, between about 1.3 and about 3.4.

(301) If the thickness T of an inductor **1** having the above dimensions is changed to about 0.55 mm \pm about 0.1 mm (or in a “low-profile” inductor **1**), the dimensions of the wound section **32** of the coil **30** are, for example, about 1.17 mm in outer diameter and about 0.48 mm in inner diameter, both in the direction of width W, and about 0.30 mm in height. Wire **31** forming the coil **30** having such a wound section **32** of preferred size would be substantially rectangular wire having an aspect ratio (longer side/shorter side) of, for example, about 1.3 and a cross-section measuring about 0.11 mm along the shorter side and about 0.14 mm along the longer side.

(302) Insulation Coating

(303) The material for the coating layer **61** of the insulation coating **60** is not critical. Examples include polyurethane, polyester, epoxy, and polyimide-amide resins. Preferably, the coating layer **61** is made of polyimide-amide resin.

(304) Preferably, the thickness of the coating layer **61** is about 4 μm .

(305) As for the fuser layer **62** of the insulation coating **60**, an example of a material is poly amide resin.

(306) Preferably, the thickness of the fuser layer **62** is about 1 μm or more and about 25 μm or less (i.e., from about 1 μm to about 25 μm), more preferably about 2 μm or more and about 25 μm or less (i.e., from about 2 μm to about 25 μm), even more preferably about 2 μm or more and about 4 μm or less (i.e., from about 2 μm to about 4 μm).

(307) Setting the thickness of the fuser layer **62** as such helps prevent shape defects in the coil **30**. In that case the wound section **32** of the coil **30** will not be too large, but the bonding will be strong enough to prevent the outermost loops of the wound section **32** from disintegrating because of the springing back of the wire **31**.

(308) As stated, in the formation of the coil **30**, the wire **31** is heated while it is wound. The fuser layer **62** melts, fastening together the portions of the wire **31** forming the wound section **32**. The material for the fuser layer **62**, therefore, can be selected so that the melting point of the layer will be, for example, about 180° C.

(309) Such a melting point is close to the soldering temperature used when the finished inductor **1** is mounted on a printed circuit board by reflow soldering. The fuser layer **62**, therefore, can melt during the reflow soldering again. The partial penetration into the body **10** and solidification there of the material for the fuser layer **62** that may usually be observed during the reflow soldering is not a problem. By virtue of its viscosity, the molten material for the fuser layer **62** will be confined to the vicinity of the coil **30**.

(310) If the side gaps Sg of the body **10** (distances between the coil **30** inside the body **10** and the second side surfaces **18**) are about 50 μm or less, however, the material for the fuser layer **62** that melts during the reflow soldering can leach out through the second side surfaces **18**.

(311) If the body **10** is formed with second side surfaces thinner than about 50 μm or less, therefore, it is important that the fuser layer **62** not only have a melting point as specified above but also be made of a material having higher melt viscosity.

(312) An example of such a material for the fuser layer **62** is one that contains multiple resins with different molecular weights. In general,

resins have lower melt viscosity with decreasing molecular weight. Making the fuser layer **62** from a material containing multiple resins with different molecular weights, therefore, helps prevent the material for the fuser layer **62** from leaching out of the body **10** during the reflow soldering. The manufacturer in that case can adjust the melt viscosity of the fuser layer **62** by customizing the ratio by weight between the resins.

(313) Such a material containing multiple resins with different molecular weights can be produced by, for example, mixing resins with different molecular weights together. Alternatively, it may be produced by polymerizing part of a resin of a low molecular weight in the presence of a catalyst or by depolymerizing a resin of a high molecular weight in the presence of a catalyst.

(314) In an embodiment, the fuser layer **62** is made of, for example, two polyamides with different molecular weights.

(315) C. Magnetic Paths

(316) The following describes the structural relationship between the wire **31** forming the coil **30** and the magnetic powder forming the core **40** in an inductor **1** having a core **40** shaped from the powder mix of soft magnetic particles and resins described in A. Powder Mix. The wire **31** is substantially rectangular one.

(317) C-1. Magnetic Powder Between Loops

(318) Made of a soft magnetic powder formed by magnetic metal particles, the inductor **1** achieves better characteristics under applied DC current than if made of ferrite or similar magnetic materials.

(319) FIG. **21A** is an image of the lower loops **32L** of the coil **30** together with the materials therearound, and FIG. **21B** is an image of the upper loops **32L** of the coil **30** together with the materials therearound. In FIGS. **21A** and **21B**, the vertical direction of the image corresponds to the direction of thickness of the body **10**, and the horizontal direction of the image corresponds to the radial direction with respect to the wound section **32**. The length CW represents the coil width of the wound section **32**.

(320) In this configuration, as in FIGS. **21A** and **21B**, a subset of the second soft magnetic particles **82**, which are the smaller particles, are between loops **32L**. The subset of the second soft magnetic particles **82** is in the region **10S** near the outside of the wound section **32**. The second soft magnetic particles **82** present in this region **10S** help prevent local saturation of magnetic flux density by creating magnetic paths near the loops **32L** along the flow of the magnetic flux. In this configuration, the second soft magnetic particles **82** in this configuration also penetrate near the inside of the wound section **32** (not seen in the images). Their presence, however, is not limited to near the outside or inside of the wound section **32**; the only requirement is that a subset of the second soft magnetic particles **82** be between loops **32L** as described below. This structure, having second soft magnetic particles **82** between loops **32L**, is hereinafter referred to as the powder-between-loops structure.

(321) The following describes the powder-between-loops structure.

(322) As in FIGS. **21A** and **21B**, the soft magnetic powder includes larger first soft magnetic particles **81** and smaller second soft magnetic particles **82**.

(323) The space between loops **32L** is narrow, allowing the smaller, second soft magnetic particles **82** to enter while not allowing the larger, first soft magnetic particles **81** to enter. The second soft magnetic particles **82** have been formed to an average diameter smaller than the thickness of the fuser layer **62** on the loops **32L**. By virtue of this, the second soft magnetic particles **82** can penetrate near the fuser layer **62** easily.

(324) In this configuration, the compression molding for shaping and curing the powder mix containing first and second soft magnetic particles **81** and **82** into the body **10** with the coil **30** therein is carried out with a pressure P higher than usual to encourage the second soft magnetic particles **82** to penetrate between the loops **32L**. The heating in the compression molding, furthermore, melts the fuser layer **62** in the insulation coating **60** on the surface of the loops **32L** so that the second soft magnetic particles **82** can penetrate easily.

(325) More specifically, when pressure P acts from above as illustrated in FIG. **22**, the wound section **32** of the coil **30** and its surroundings are exposed not only to the pressure P from above but also to pressure P from below and in the horizontal direction, for example because of the law of action and reaction. Pressure is therefore applied to the second soft magnetic particles **82** in the direction from the outside of the coil **30** to its loops **32L**, helping the second soft magnetic particles **82** fill the gaps between the loops **32L**.

(326) The pressure P parameters may include not only the pressure P itself but also the duration of compression and other relevant parameters. Selecting appropriate parameters helps the second soft magnetic particles **82** fill the gaps between the loops **32L** well. Other parameters, such as the heating conditions and the distance between the wound section **32** and the surrounding walls (the inner surfaces of the mold **74** and the punch **76**), may also be customized to further encourage the filling of the gaps between the loops **32L** with the second soft magnetic particles **82**.

(327) Introducing the second soft magnetic particles **82** between the loops **32L** as in FIGS. **21A** and **21B** helps improve characteristics under applied DC current as it will prevent local saturation of magnetic flux density near the wound section **32**.

(328) The following describes the length LS of the second soft magnetic particles **82** between the loops **32L**.

(329) This length LS corresponds to the length of contact between the portions of the coil **30** forming the loops **32L** and the second soft magnetic particles **82**.

(330) The inventors performed a study to determine the saturation current Isat with different lengths LS of the second soft magnetic particles **82** between the loops **32L** with the following parameters: the line width of the loops **32L** of the coil **30**, 95 μm ; the thickness of the loops **32L** of the coil **30**, 180 μm ; the thickness of the fuser layer **62** between the loops **32L** of the coil **30**, 6 μm ; the average diameter of the first soft magnetic particles **81**, 10 μm or more; the average diameter of the second soft magnetic particles **82**, 5 μm or less; pressure P, 300 kg/cm².

(331) The saturation current Isat is the electric current at which the inductance decreases by a certain percentage from the initial inductance, or the inductance with no applied current, and is a measure of the maximum current that can be passed while avoiding magnetic saturation. The saturation current Isat was defined as the electric current at which the inductance decreases by about 30% from the initial inductance. The results are presented in Table 10.

(332) TABLE-US-00010 TABLE 10 Length LS of second soft magnetic particles between loops Isat Comparative (no magnetic powder) 100 Example CK-1 Comparative 5% of the length of contact 100.07 Example CK-2 between wires Example C1-1 10% of the length of contact 100.14 between wires Example C1-2 50% of the length of contact 100.7 between wires Comparative 55% of the length of contact 100.77 Example CK-3 between wires

(333) Comparative Example CK-1 was an example in which the length LS of the second soft magnetic particles **82** between the loops **32L** was zero in a cross-section of the portions of the coil **30** forming the loops **32L** (e.g., the WT cross-section), i.e., there were no second soft magnetic particles **82** between the loops **32L**. Comparative Example CK-2 was an example in which the length LS was 5% of the length of contact between the loops **32L** in a cross-section of the coil, or, in other words, 5% of the length over which portions of the wire **31** forming the coil are in contact with each other in a cross-section of the coil. The proportion of the length LS of the second soft magnetic particles **82**

between the loops **32L** to the length of contact between the loops **32L** was defined as (the total length LS of the second soft magnetic particles **82** between all loops **32L**)/(the total length of contact between all loops **32L**) in an image of the WT cross-section of the body **10** at the midpoint of its length L.

(334) Example C1-1 represents a case in which the length LS is about 10% of the length of contact between the portions of the wire **31** in a cross-section of the coil. Example C1-2 represents a case in which the length LS is about 50% of the length of contact between the portions of the wire **31** in a cross-section of the coil. Comparative Example CK-3 represents a case in which the length LS is about 55% of the length of contact between the portions of the wire **31** in a cross-section of the coil. The saturation currents Isat in the table assume that the Isat in Comparative Example CK-1 is 100.

(335) In the study conducted by the inventors, the saturation current Isat was large compared with that with a zero length LS when the LS was 10% or more of the length of contact between portions of the wire **31** in a cross-section of the coil. It is, therefore, preferred that the length LS be about 10% or more of the length of contact between portions of the wire **31**. A length LS exceeding about 55% of the length of contact between portions of the wire **31** in a cross-section of the coil, however, can cause the loops **32L** to disintegrate easily because of cracks in the fuser layer **62** joining the loops **32L** together.

(336) In light of these, the inventors have concluded if the manufacturer aims at the control of magnetic saturation and the resulting improvement in the characteristics under applied DC current, it is preferred that the length LS be about 10% or more of the length of contact between portions of the wire **31** in a cross-section of the coil. If the separation of loops **32L** is also a concern, it is preferred that the length LS be about 10% or more and about 50% or less (i.e., from about 10% to about 50% or less) of the length of contact between portions of the wire **31** in a cross-section of the coil. Overall, it is preferred that the length LS be selected within the range of about 10% to about 50% of the length of contact between the portions of the wire **31** in a cross-section of the coil.

(337) FIG. 23 presents simulated characteristic curves of the powder-between-loops structure.

(338) In FIG. 23, the horizontal axis indicates electric current, and the vertical axis indicates inductance (L). In FIG. 23, Comparative Example CK-4 represents a case in which no powder-between-loops structure is formed; there are no second soft magnetic particles **82** between the upper and lower tiers of the two-tier wound section **32**, between the upper loops **32L**, and between the lower loops **32L**.

(339) Example C1-3 represents a case in which some second soft magnetic particles **82** are present between the upper and lower tiers of the wound section **32**, between the upper loops **32L**, and between the lower loops **32L**. The penetrating second soft magnetic particles **82** exist throughout the gaps in these regions.

(340) Example C1-4 represents a case in which the penetrating second soft magnetic particles **82** are confined to the space between the outermost loops of the upper and lower tiers of the wound section **32**, the upper half of the gaps between the upper loops **32L**, and the lower half of the gaps between the lower loops **32L**.

(341) Example C1-5 represents a case in which the penetrating second soft magnetic particles **82** are present in the upper half of the gaps between the upper loops **32L** and the lower half of the gaps between the lower loops **32L**.

(342) Example C1-6 represents a case in which the penetrating second soft magnetic particles **82** are present between the upper loops **32L** and between the lower loops **32L**, existing throughout the gaps in these regions.

(343) Table 11 presents simulated initial inductance (initial L) and saturation current Isat in Comparative Example CK-4 and Examples C1-3 to C1-6. The parameters such as the line width and thickness of the coil **30** and the thickness of the fuser layer **62** are the same as in Table 10.

(344) TABLE-US-00011 TABLE 11 Position of the magnetic powder Initial between loops L Isat Comparative (no magnetic powder) 0.21 5.28 Example CK-4 Example C1-3 All gaps between the upper and lower 0.21 5.44 tiers, between the upper loops, and between the lower loops Example C1-4 The space between the outermost loops 0.21 5.32 of the upper and lower tiers, the upper half of the gaps between the upper loops, and the lower half of the gaps between the lower loops Example C1-5 The upper half of the gaps between the 0.21 5.32 upper loops and the lower half of the gaps between the lower loops Example C1-6 All gaps between the upper loops and 0.21 5.44 between the lower loops

(345) As shown in FIG. 23, Examples C1-3 to C1-6 achieved high inductance compared with Comparative Example CK-4 in a broad range of electric currents, from 0 A to 10 A, indicating controlled magnetic saturation and the resulting improvement in the characteristics under applied DC current. As is clear from Table 11, furthermore, Examples C1-3 to C1-6 were superior to Comparative Example CK-4 in terms of saturation current Isat, too.

(346) Examples C1-3 and C1-6, furthermore, were equally good in terms of characteristics (inductance and saturation current Isat) and achieved even higher inductance than Examples C1-4 and C1-5. A similarity between Examples C1-3 and C1-6 is that the penetrating second soft magnetic particles **82** are present between the upper loops **32L** and between the lower loops **32L**; presumably, this is advantageous in the control of magnetic saturation and the resulting improvement in the characteristics under applied DC current.

(347) Overall, the core **40**, with an embedded coil **30** therein, contains larger first soft magnetic particles **81** and smaller second soft magnetic particles **82**, and a subset of the second soft magnetic particles **82** penetrate between the loops **32L** of the coil **30** to create magnetic paths near the loops **32L**. By virtue of this, local saturation of magnetic flux density is controlled even if the magnetic particles are ones that deliver good characteristics under applied DC current.

(348) Setting the length LS of the second soft magnetic particles **82** between the loops **32L** to about 10% or more of the length of contact between portions of the wire **31** in a cross-section of the coil, furthermore, will provide more effective control of the local saturation of magnetic flux density, or magnetic saturation, than when the length LS is less than about 10% of the length of contact between portions of the wire **31**.

(349) Setting the length LS of the second soft magnetic particles **82** between the loops **32L** to about 50% or less of the length of contact between portions of the wire **31** in a cross-section of the coil helps avoid the separation between loops **32L** caused by cracks in the fuser layer **62** joining the loops **32L** together.

(350) Adjacent loops **32L** are joined together by a fuser agent supplied from the fuser layer **62**, and the second soft magnetic particles **82** are formed to an average diameter smaller than the thickness of the fuser layer **62** so that a subset thereof will penetrate into the fuser layer **62** and create magnetic paths between the loops **32L**. This helps control magnetic saturation effectively because the creation of magnetic paths between the loops **32L** taking place simultaneously with the joining of adjacent loops **32L** contributes to efficiency.

(351) The penetration of a subset of the second soft magnetic particles **82** between the loops **32L**, furthermore, is achieved by adjusting at least the pressure P when the materials for the core **40** (such as first and second soft magnetic particles **81** and **82**) and the coil **30** are shaped into the body **10** by compression molding. It is therefore easy to create the magnetic paths between the loops **32L**.

(352) The customization of pressure P parameters, heating conditions, etc., is not the only possible way to make a subset of the second soft magnetic particles **82** penetrate between the loops **32L**. Approaches may be combined to encourage some second soft magnetic particles **82**

to penetrate the loops **32L**, such as adjusting the diameters of the first and second soft magnetic particles **81** and **82**, adjusting the lubricity of the surface layers between the particles **81** and **82**, and selecting appropriate resins.

(353) If the coil **30** has a multitiered wound section **32** (having two or more tiers) formed by one continuous length of wire **31**, it is preferred that there be a subset of the second soft magnetic particles **82** between the uppermost and/or lowermost loops **32L**. This is an easy way to create magnetic paths effective in controlling magnetic saturation.

(354) As long as a subset of the second soft magnetic particles **82** penetrate between the loops **32L**, the materials for the core **40** or their amounts may be changed, and the shape of the coil **30**, for example, may be changed. The penetration of a subset of second soft magnetic particles **82** between the loops **32L**, furthermore, does not need to take place during the shaping and curing; it may be induced whenever possible.

(355) The coil **30** does not need to be wound by α winding either. For example, the coil **30** may be wound edgewise. Even with edgewise or other winding techniques, effective control of magnetic saturation is easy to achieve as long as second soft magnetic particles **82** create magnetic paths between adjacent loops **32L** joined together by the fuser layer **62**.

(356) C-2. Magnetic Gap

(357) The inductor **1** may have a magnetic gap near the wound section **32** of the coil **30** to further control the saturation of the magnetic flux density near the wound section **32**.

(358) FIG. **24** is an image of the vicinity of the wound section **32** with an air gap **40K** that serves as a magnetic gap.

(359) The air gap **40K** extends along a row of loops **32L** and substantially perpendicular to the magnetic flux. The creation of the air gap **40K** takes place during the shaping and curing. To be more exact, air gaps **40K** like that in FIG. **24** are created around the wound section **32** of the coil **30** by utilizing the springing back of (repulsive force in) the materials for the core, such as the first and second soft magnetic particles **81** and **82**. In the shaping and curing, pressure **P** is applied horizontally and vertically to the coil **30** to compress the core materials, such as the first and second soft magnetic particles **81** and **82**, near the wound section **32** of the coil **30** as illustrated in FIG. **22**. Then the core materials are allowed to spring back, for example by quick retraction of the punch **76** quickly or removal of the body **10** from the mold before the core materials harden completely.

(360) The springing back includes at least the repulsion between first soft magnetic particles **81**, between second soft magnetic particles **82**, or between first and second soft magnetic particles **81** and **82**. Air gaps **40K** that will serve as magnetic gaps are created by utilizing one or more of these types of repulsion as needed. The springing back may include the repulsion between the coil **30** and the core **40** (first and second soft magnetic particles **81** and **82**).

(361) In other words, compression molding carried out with appropriate adjustments to parameters, such as the pressure **P**, the rate and duration of pressing, the speed of retraction of the punch **76**, and when the body **10** is removed, will create air gaps **40K** that extend around and along the rows of loops **32L**. Air gaps **40K** that will serve as magnetic gaps are therefore easy to create, and these air gaps **40K** help control the saturation of the magnetic flux density near the wound section **32** of the coil **30** and thereby improve the characteristics under applied DC current.

(362) The following describes the position, length, and width of the air gaps **40K**.

(363) The inventors performed a study to determine the saturation current I_{sat} with different positions, lengths, and widths of air gaps **40K** with the following parameters: the line width of the loops **32L** of the coil **30**, 95 μm ; the thickness of the loops **32L** of the coil **30**, 180 μm ; the thickness of the fuser layer **62** on the loops **32L** of the coil **30**, 4 μm ; the average diameter of the first soft magnetic particles **81**, 10 μm or more; the average diameter of the second soft magnetic particles **82**, 5 μm or less; pressure **P**, 300 kg/cm². The saturation current I_{sat} was defined as the electric current at which the inductance decreases by about 30% from the initial inductance.

(364) Table 12 presents the study results with regard to the position of the air gaps **40K**. The saturation currents I_{sat} in Table 12 assume that the I_{sat} is 100 when the air gaps **40K** are 11 μm away from the wound section **32**.

(365) TABLE-US-00012 TABLE 12 Position of the airgaps I_{sat} 0 μm from the wound section 67 1 μm from the wound section 70 2 μm from the wound section 73 3 μm from the wound section 76 4 μm from the wound section 79 5 μm from the wound section 82 6 μm from the wound section 85 7 μm from the wound section 88 8 μm from the wound section 91 9 μm from the wound section 94 10 μm from the wound section 97 (equivalent of the average diameter of the first soft magnetic particles) 11 μm from the wound section 100 15 μm from the wound section 113 20 μm from the wound section 130 (equivalent of double the average diameter of the first soft magnetic particles) 30 μm from the wound section 130 (equivalent of three times the average diameter of the first soft magnetic particles) 40 μm from the wound section 113 (equivalent of four times the average diameter of the first soft magnetic particles) 50 μm from the wound section 100 (equivalent of five times the average diameter of the first soft magnetic particles)

(366) As shown in Table 12, when the air gaps **40K** were 30 μm away from the wound section **32** or closer, the saturation current I_{sat} increased with increasing distance between the air gaps **40K** and the wound section **32**. When the air gaps **40** were more than 50 μm away, the I_{sat} was below 100. In the study conducted by the inventors, therefore, the air gaps **40K** were effective in controlling magnetic saturation when they were 50 μm away from the wound section **32** or closer. In other words, for the control of magnetic saturation, it is preferred that the distance between the air gaps **40K** and the wound section **32** be equal to or smaller than about five times the average diameter of the first soft magnetic particles **81**. More preferably, the air gaps **40K** are in the range of about 20 μm to about 30 μm away from the wound section **32**.

(367) Table 13 presents the study results with regard to the length **KL** (see FIG. **24**) of the air gaps **40K**. The saturation currents I_{sat} in Table 13 assume that the I_{sat} is 100 when the length **KL** of the air gaps **40K** is 10% of the coil width **CW** of the wound section **32** (FIG. **24**).

(368) TABLE-US-00013 TABLE 13 Length of the air gaps I_{sat} 10% of the coil width of the wound section 100 20% of the coil width of the wound section 102 30% of the coil width of the wound section 103 40% of the coil width of the wound section 105 50% of the coil width of the wound section 107 60% of the coil width of the wound section 109 70% of the coil width of the wound section 111 80% of the coil width of the wound section 113 90% of the coil width of the wound section 114 100% of the coil width of the wound section 116 110% of the coil width of the wound section 118

(369) As shown in Table 13, when the length **KL** of the air gaps **40K** was equal to or smaller than 110% of the coil width **CW** of the wound section **32**, the saturation current I_{sat} increased with longer air gaps **40K**. In the study conducted by the inventors, the air gaps **40K** were effective in controlling magnetic saturation when their length **KL** was equal to or larger than the width of a single loop **32L** (33% or more of the coil width **CW**).

(370) Air gaps **40K** whose length **KL** is much greater than the coil width **CW**, or, more specifically, exceeds about 110% of the coil width **CW**, can affect inductance.

(371) The inventors have therefore concluded it is preferred that the length **KL** of the air gaps **40K** be roughly equal to or larger than the

width of a single loop **32L** (about 33% or more of the coil width CW of the wound section **32**) and about 110% or less of the coil width CW of the wound section **32**. More preferably, the length of the air gaps **40K** is equal to or larger than about 1.5 times the width of a single loop **32L** (about 50% or more of the coil width CW of the wound section **32**) and roughly equal to or smaller than (about 100% or less of) the coil width CW of the wound section **32**.

(372) Table 14 presents the study results with regard to the width KW (see FIG. **24**) of the air gaps **40K**. The width KW corresponds to the length of the air gaps **40K** in the direction perpendicular to the rows of loops **32L**. The saturation currents Isat in Table 14 assume that the Isat is 100 when the width KW of the air gaps **40K** is less than 1 μm , which is smaller than the diameter of the smallest particles (defined as there being no air gap).

(373) TABLE-US-00014 TABLE 14 Width of the air gaps Isat Smaller than the smallest particles 100 1 μm 103 2 μm 107 3 μm 111 4 μm 114 5 μm 118 6 μm 122 7 μm 126 8 μm 131 9 μm 135 10 μm 140 11 μm 140

(374) As shown in Table 14, when the width KW of the air gaps **40K** was 10 μm or less, the saturation current Isat increased with increasing width KW. Widths KW of 10 μm and 11 μm resulted in equal Isat values. When the width KW of the air gaps **40K** exceeded about 11 μm , which means the width KW was larger than the average diameter of the first soft magnetic particles **81**, the body **10** easily cracked along the air gaps **40K** because of weakened adhesion of the resins to the first soft magnetic particles **81**.

(375) It is, therefore, preferred that the width KW of the air gaps **40K** be roughly equal to or larger than the average diameter of the second soft magnetic particles **82** (about 5 μm) and about 11 μm or less, more preferably as close to about 10 μm as can be without causing cracks in the body **10**.

(376) FIG. **25** presents simulated characteristic curves with and without air gaps **40K**. In FIG. **25**, the horizontal axis indicates electric current, and the vertical axis indicates inductance (L). Curve K1 is from a simulation without air gaps **40K**, and curve K2 is from a simulation with air gaps **40K** extending above and below and inside and outside the wound section **32** of the coil **30** both longitudinally and transversely with respect to the wound section **32**.

(377) Table 15 presents simulated initial inductance (initial L) and saturation current Isat for each of curves K1 and K2. The parameters such as the line width and thickness of the coil **30** and the thickness of the fuser layer **62** are the same as in Tables 10 and 11.

(378) TABLE-US-00015 TABLE 15 Air gaps (magnetic gaps) Initial L Isat Curve K1 No air gaps around the wound 0.49 5.06 (comparative example) section Curve K2 Air gaps present around the 0.43 5.92 (example) wound section

(379) As shown in FIG. **25** and Table 15, the simulation revealed magnetic saturation is controlled better with air gaps **40K** than without them, particularly when the electrical current is in a range of about 0 A to about 6 A.

(380) Overall, the body **10** has air gaps **40K** extending along the rows of loops **32L** of the coil **30** outside the wound section **32** of the coil **30** and within a distance of about five times the average diameter of the first soft magnetic particles **81** from the wound section **32**. By virtue of this, magnetic saturation is controlled even if the magnetic particles are ones that deliver good characteristics under applied DC current.

(381) The control of magnetic saturation provided by the air gaps **40K** is highly effective. This is because their length, or the dimension along the rows of loops **32L**, is roughly equal to or larger than the width of a single loop **32L** and roughly equal to or smaller than the coil width CW of the wound section **32**, and because their width, or the dimension in the radial direction with respect to the loops **32L**, is roughly equal to or larger than the average diameter of the second soft magnetic particles **82** and about 10 μm or less.

(382) The air gaps **40K**, furthermore, are easy to create. The air gaps **40K** are created by utilizing the springing back that occurs when the materials for the core **40** and the coil **30** are shaped into the body **10** by compression molding.

(383) As long as the air gaps **40K** can be created, the materials for the core **40** or their amounts may be changed, and the shape of the coil **30**, for example, may be changed. The air gaps **40K**, furthermore, do not need to be created during the shaping and curing of the body **10**; they may be created whenever possible.

(384) D. Grinding

(385) The following describes the grinding of the body **10** of an inductor **1** having a core **40** shaped from the powder mix of soft magnetic particles and resins described in A. Powder Mix.

(386) As stated, the body **10** of the inductor **1** is an article shaped from the powder mix by compression molding with an embedded coil **30** therein. The body **10** includes the coil **30** and a core **40**.

(387) As stated with reference to FIG. **5**, the body **10** shaped by compression molding is subjected to the grinding of its second side surfaces **18** (FIG. **1**) with an abrasive to a predetermined width W. This will trim the body **10** to a predetermined size, increasing the occupancy of the body **10** by the coil **30**. This approach of trimming the body **10** to a predetermined size by grinding is advantageous over controlling the size of the body **10** by adjusting the dimensions of the cavity in the mold in terms of size variations between bodies **10**.

Barrel polishing, for example, may follow to round the corners of the second side surfaces **18** produced by the grinding.

(388) Grinder

(389) FIG. **26** is a diagram schematically illustrating an example of a grinder **101** used in the grinding.

(390) The grinder **101** includes a receptacle **102** for keeping the body **10** to be ground (workpiece) in and upper and lower grindstones **103** and **104** for sandwiching the body **10** kept in the receptacle **102** between. The body **10** is put into the receptacle **102** with its second side surfaces **18**, or the surfaces to be ground, up and down.

(391) During the grinding, the grinder **101** presses its upper and lower grindstones **103** and **104** against the upper and lower second side surfaces **18**, respectively, with a predetermined load and moves the upper and lower grindstones **103** and **104** relative to the upper and lower second side surfaces **18** at the same time. An abrasive **105** on the upper and lower grindstones **103** and **104** grinds the upper and lower second side surfaces **18** simultaneously (double-side grinding).

(392) Grit Size

(393) The inventors have experimentally confirmed that the size of the abrasive **105** is proportional to the rate of grinding. As the abrasive **105** becomes larger, furthermore, the grinding eliminates more particles of the soft magnetic powder from the surfaces, and the ground surfaces will have greater roughness.

(394) To be more exact, grinding an article shaped from soft magnetic powder will cause a considerable number of particles of the powder to be eliminated by the abrasive **105**, which will leave hollows in the ground surfaces. If the soft magnetic powder contains larger and smaller particles, the grinding eliminates more of the larger particles than the smaller ones. As the size of the abrasive **105** increases, the grinding eliminates a greater number of larger particles, creating a greater number of relatively large hollows in the ground surfaces. As a result, the ground surfaces will have greater roughness.

(395) As for surface roughness, the inventors have experimentally confirmed that there is no correlation between surface roughness and load.

(396) In the examples described herein, surface roughness evaluations were based on arithmetic mean height. Specifically, multiple (e.g., three to four) measurement areas of a predetermined size (about 200 μm ×about 290 μm) were defined on the surface of interest, the maximum height in each area was measured using a laser microscope, and the average was reported as the arithmetic mean height. The laser microscope was Keyence Corporation's VK-X250.

(397) Grinding Speed

(398) The inventors have experimentally confirmed that as the grinding speed (velocity of the movement of the upper and lower grindstones **103** and **104**) increases, the grinding smoothens the exposed particles of the soft magnetic powder more effectively, and the ground surfaces will have smaller roughness. The grinding speed, furthermore, is proportional to the rate of grinding.

(399) Rate of Grinding

(400) A target rate of grinding is set, and the size of the abrasive **105** and the grinding speed are selected to achieve this target. As stated, the size of the abrasive **105** and the grinding speed are each related to the roughness of the ground surfaces. In the examples described herein, the size of the abrasive **105** and the grinding speed were selected to ensure that the grinding would increase the roughness of the second side surfaces **18** and make these sides rougher than the top surface **14** and the mount surface **12**, which were not to be ground.

(401) The increased surface roughness *S* brought by the grinding will strengthen the adhesion of the protective film **50** on the second side surfaces **18** of the body **10**. The body **10**, except where it has the outer electrodes **20** on, is covered with a protective film **50** that protects the body **10** from moisture and corrosion and provides good electrical insulation.

(402) Duration of Grinding

(403) The duration of grinding is defined as the length of time from the start of grinding *T*_s to the end of grinding *T*_e and is determined based on the difference between the initial and target widths *W* of the body **10** and the rate of grinding.

(404) During the grinding, a controller (not illustrated) controls the operation of the grinder **101** based on a load profile and the determined duration of grinding, ensuring that the body **10** shaped by compression molding will be ground to a predetermined width *W*.

(405) Side Gaps

(406) As illustrated in FIG. 27, a side gap *S*_g of the inductor **1** is defined as the thickness of the body **10** between the coil **30** therein and the closer second side surface **18**. If the body **10** is covered with a protective film **50**, the side gap *S*_g excludes the thickness of the protective film **50**.

(407) In the examples described herein, the side gaps *S*_g of the body **10** ground to a predetermined width *W* were wider than the equivalent of one larger particle of the soft magnetic powder and narrower than the equivalent of four larger particles of the soft magnetic powder. In other words, in the examples described herein, the target width of the body **10** in the grinding and/or the width *W*_{Lc} of the wound section **32** of the coil **30** (FIG. 27) were adjusted beforehand to ensure that the side gaps *S*_g of the body **10** ground to a predetermined width *W* would be such.

(408) Setting the side gaps *S*_g of the ground body **10** wider than the equivalent of about one larger particle of the soft magnetic powder will prevent the coil **30** from being exposed. Even if the grinding eliminates particles from the second side surfaces **18**, at least one large particle will remain between the second side surfaces **18** and the coil **30**.

(409) Limiting the side gaps *S*_g of the ground body **10** to narrower than the equivalent of about four larger particles of the soft magnetic powder will prevent loss of inductance. With such side gaps *S*_g, the body **10** is not too large, and, therefore, its occupancy by the coil **30** remains sufficiently high.

(410) Tables 16 and 17 present measured inductance and moisture resistance of inductors **1** with different combinations of the maximum and minimum side gaps *S*_g.

(411) The data in Table 16 are from inductors **1** made with a soft magnetic powder in which the average diameters of the larger and smaller particles were 21 μm and 2 μm , respectively. The data in Table 17 are from inductors **1** made with a soft magnetic powder in which the average diameters of the larger and smaller particles were 28 μm and 2 μm , respectively.

(412) The soft magnetic powders were made with particles of chromium-free Fe—Si amorphous alloy and crystalline pure iron. The particles of chromium-free Fe—Si amorphous alloy were the larger particles, whereas the particles of pure iron were the smaller. The surface of the larger particles was covered with a SiO—Fe.sub.2SiO.sub.4 bilayer oxide film, and that of the smaller particles was covered with an Fe oxide film. By virtue of the oxide films, each individual particle was electrically insulated.

(413) Powder mix of this soft magnetic powder and epoxy resins was shaped by compression molding to give bodies **10** for the inductors **1**.

(414) Actually, the larger particles were sample A1-04, a sample of first soft magnetic particles described above, and the smaller particles were any of samples A2-02 to -08, samples of second soft magnetic particles described above. The bodies **10**, therefore, had resins, Fe or Fe oxide(s), phosphate glass, SiO.sub.2, and an alkyl group having a C16 chain on their surface.

(415) The inductance was measured using an LCR meter, and the moisture resistance was examined by exposing the inductors **1** to an environment at a temperature of 85° C. and a humidity of 85%. For moisture resistance, “Fail” means the inductor **1** failed to meet predetermined quality criteria.

(416) TABLE-US-00016
TABLE 16 Side gaps Inductance Moisture Minimum Maximum (μH) resistance
0 110 0.412 Fail 10 100 0.417
Fail 18 92 0.420 Fail 25 85 0.423 Pass 29 81 0.424 Pass 33 77 0.425 Pass 40 70 0.427 Pass 45 65 0.428 Pass 50 60 0.429 Pass 55 55 0.429
Pass

(417) TABLE-US-00017
TABLE 17 Side gaps Inductance Moisture Minimum Maximum (μH) resistance
0 110 0.424 Fail 10 100 0.430
Fail 18 92 0.433 Fail 25 85 0.436 Fail 29 81 0.437 Pass 33 77 0.439 Pass 40 70 0.440 Pass 45 65 0.441 Pass 50 60 0.442 Pass 55 55 0.442
Pass

(418) As shown in Tables 16 and 17, the body **10** is sufficiently resistant to moisture when its minimum side gap *S*_g is wider than the equivalent of about one larger particle. The inductance, furthermore, decreases with increasing maximum side gap *S*_g.

(419) The data also indicate that the inductor **1** performs well in both moisture resistance and inductance when both side gaps *S*_g are roughly equal (about 1:1) and wider than the equivalent of about one larger particle and narrower than the equivalent of about four larger particles.

(420) Overall, an inductor **1** according to an embodiment of the present disclosure is composed of a substantially plate-shaped body **10** with an embedded coil **30** therein and a pair of outer electrodes **20** on the body **10**. The body **10** has been shaped from powder mix of soft magnetic powder containing two sets of particles with different average diameters, namely larger and smaller particles, and resins. The body **10** has second side surfaces **18** in the radial direction with respect to the coil **30**, and the side gaps *S*_g of the body **10**, which are the thickness dimensions between the second side surfaces **18** and the coil **30**, are wider than the equivalent of about one larger particle and narrower than the equivalent of about four larger particles.

(421) By virtue of the side gaps *S*_g of the body **10** set wider than the equivalent of about one larger particle of the soft magnetic powder, the

coil **30** is prevented from being exposed because there is at least one large particle between the second side surfaces **18** and the coil **30**.
(422) By virtue of the side gaps Sg of the body **10** limited to narrower than the equivalent of about four larger particles of the soft magnetic powder, loss of inductance is prevented because with such side gaps Sg, the body **10** is not too large, and, therefore, its occupancy by the coil **30** remains sufficiently high. Although small in size, the resulting inductor **1** is practical in terms of DC resistance and saturation flux density.
(423) In this embodiment, the second side surfaces **18** of the body **10** of the inductor **1** are covered with a protective film **50** and are rougher than at least one of the other sides (the mount surface **12** and the top surface **14**).
(424) By virtue of this, the second side surfaces **18** and the protective film **50** adhere firmly to each other.
(425) In this embodiment, the surface of the body **10** of the inductor **1** is covered with a protective film **50** except where it has the outer electrodes **20** on.
(426) The protective film **50** protects the body **10** from moisture and corrosion and provides good electrical insulation, making the inductor **1** a quality one.
(427) E. Protective Film
(428) The following describes the protective film **50** formed on the surface of the body **10** of an inductor **1** having a core **40** shaped from the powder mix of soft magnetic particles and resins described in A. Powder Mix.
(429) As stated, the body **10** of the inductor **1** is an article shaped from the powder mix by compression molding with an embedded coil **30** therein. The body **10** includes the coil **30** and a core **40**.
(430) The protective film **50** covers the entire surface of the body **10** excluding where it has the outer electrodes **20** on. The protective film **50** provides electrical insulation and protects the body **10** from moisture and corrosion. Even if the grinding eliminates larger particles of the soft magnetic powder from the ground surfaces (second side surfaces **18**), covering the ground surfaces with the protective film **50** will compensate for the associated loss of electrical insulation and resistance to moisture and corrosion.
(431) Formation of the Protective Film and the Device for it
(432) As described with reference to FIG. 5, the protective film **50** is formed by applying a material containing a thermosetting resin to the entire surface of the body **10**, for example by spraying or dipping.
(433) FIG. 28 is a diagram schematically illustrating an example of a film forming device **201** used in the film formation (Step **500** in FIG. 5).
(434) The film forming device **201** forms the protective film **50** on the surface of many bodies **10** (workpieces **208**) by spraying the material thereonto. As illustrated in the drawing, the film forming device **201** includes an enclosure **202**, a rotary drum **203** therein for putting the bodies **10** (workpieces **208**) in, a heater **204** for heating the drum **203**, a duct **205** as an exhaust for the drum **203**, and a spray nozzle **206** inside the drum **203**.
(435) To carry out the film formation, the film forming device **201** first preheats the drum **203** with the bodies **10** therein. Using the heater **204**, the drum **203** is heated to a temperature at which the material for the protective film **50** does not cure (e.g., about 30° C. to about 70° C.).
(436) Then the film forming device **201** forms the protective film **50** on the surface of the bodies **10** by spraying the material for the protective film **50** onto the bodies **10** through the spray nozzle **206** and at the same time blowing hot air **207** onto the bodies **10** through an air nozzle (not illustrated) while rolling (barreling) the drum **203** to tumble the bodies **10**. The tumbling of the bodies **10** and the blowing of hot air **207** onto the bodies **10** are continued until the protective film **50** on the bodies **10** dries to an appropriate degree. After the drying of the protective film **50**, the bodies **10** are removed from the drum **203**.
(437) Insufficient drying will cause the protective film **50** to have pores (small holes) and/or swellings and will also affect the adhesion of the protective film **50** to the bodies **10**. Excessive drying will make the protective film **50** a “discontinuous” film and will also affect the adhesion of the protective film **50** to the bodies **10**. Preferably, the protective film **50** is dried to such a degree that it will be a “continuous” film and adhere to the bodies **10** well.
(438) Material for the Protective Film
(439) The material for the protective film **50** is a liquid mixture of a resin component as the base, a solvent component as a diluent for the resin component, and a filler component as an additive.
(440) Resin Component
(441) An example of a suitable resin component is an epoxy resin as the primary ingredient with added phenoxy and/or novolac resins. Adding a phenoxy resin will toughen the protective film **50**. Adding a novolac resin will make the protective film **50** more resistant to heat.
(442) Preferably, a resin in the resin component contains a pigment.
(443) During the film removal (Step **600**) and electrode formation (Step **700**), described with reference to FIG. 5, a pigmented resin improves the workability of the bodies **10** when their surface is irradiated with a laser for the removal of the protective film **50** and when the outer electrodes **20** are formed. An example of a suitable pigment is carbon black.
(444) Solvent Component
(445) The solvent component includes solvent(s) that can be sprayed in mist form together with the resin component and then dries to an appropriate degree. An example of a suitable solvent component is one that contains methyl ethyl ketone (MEK), which is used as a diluent for resin paste.
(446) Filler Component
(447) The filler component includes filler(s) that reduces the gloss of the protective film **50**, improves the quality of the protective film **50**, and disperses in the solvent(s).
(448) Reducing the gloss of the protective film **50** helps prevent errors caused by washed-out color when the inductors **1** are visually inspected with a camera. An example of a suitable filler is powdered silica (SiO₂).
(449) As for the particle size, the smaller, the better. Small filler particles help prevent the spray nozzle **206**, through which the material for the protective film **50** is sprayed, from clogging and reduce the damage to the surface of the bodies **10** from the barreling of the drum **203**. If the filler is powdered silica, it is preferred to use nanosilica.
(450) Nanosilica
(451) The inventors have experimentally found that when the filler is nanosilica, there is a correlation between the rate of drying and the nanosilica content.
(452) FIG. 29 is a graphical representation of relationships between the nanosilica content and the rate of drying determined through an experiment.
(453) In this experiment, sample materials for the protective film **50** were prepared with an epoxy resin as the resin component, MEK as the

solvent component, and nanosilica as the filler component. Inductors **1** were constructed by forming a protective film **50** on bodies **10** using these samples and forming outer electrodes **20** on the bodies **10**. During the drying of the protective film **50**, the relationship between the duration of drying, i.e., the length of time for which the bodies **10** were left, and the solids content of the protective film **50** was investigated.

(454) Four sample materials for the protective film **50** were prepared with different amounts of nanosilica: 0 (containing no nanosilica), 50 phr, 100 phr, and 200 phr. In all samples, the average diameter of particles of the nanosilica was 45 nm.

(455) The average diameter of the silica particles was measured as follows. The body **10** was cut in parallel with its second side surfaces **18** at the intersection of the diagonals of the top surface **14** of the inductor **1**. On the upper and lower primary sides of the body **10**, the cross-section of the protective film **50** was imaged with a transmission electron microscope (TEM) at each quarter of the length L of the body **10** at a magnification of $\times 300,000$. The average diameter was determined by observing silica particles in the TEM images. The TEM was a field-emission transmission electron microscope (FE-TEM), more specifically JEOL Ltd.'s multipurpose electron microscope (JEM-F200) combined with an energy-dispersive x-ray microanalysis (EDX) system (Thermo Fischer Scientific Inc. NORAN System 7).

(456) As can be seen from FIG. **29**, the solids content increases with increasing nanosilica content, and even short drying results in a high solids content when the nanosilica content is high. Increasing the nanosilica content of the material for the protective film **50**, therefore, will accelerate the drying, and therefore helps shorten the duration of drying, of the protective film **50**.

(457) In addition, observations in this experiment revealed that the "sticking," described below, of the protective film **50** occurs when the solids content upon drying is about 80% or less. When the solids content upon drying is about 90%, the protective film **50** is of good quality but has cracks in its surface.

(458) It is therefore preferred that the protective film **50** be dried to a solids content of about 80% to about 90%.

(459) Film Sticking

(460) When the bodies are sprayed in the drum **203**, the protective film **50** may stick between bodies **10**. This can affect the quality of the protective film **50** and herein is referred to as "film sticking." The inventors have experimentally found that when the filler is nanosilica, the film sticking can be reduced by changing the diameter of particles of the nanosilica.

(461) FIG. **30** is a graphical representation of relationships between the average diameter of particles of nanosilica and the incidence of film sticking determined through an experiment.

(462) In this experiment, two sample materials for the protective film **50**, samples 1 and 2, were prepared.

(463) Sample 1 was made with an epoxy resin as the resin component, PGM as the solvent component, and nanosilica as the filler component. Sample 2 was made with an epoxy resin as the resin component, MEK as the solvent component, and nanosilica as the filler component. The nanosilica content of both samples 1 and 2 was 200 phr.

(464) A protective film **50** was formed on bodies **10** using samples 1 and 2 as described above, and then the bodies **10** were removed from the drum **203**. The incidence of film sticking was determined from the number of sticking bodies **10**.

(465) As can be seen from FIG. **30**, the incidence of film sticking decreases with decreasing average diameter of the silica particles.

(466) When sample 1, made with PGM as the solvent component, and sample 2, made with MEK as the solvent component, were compared, the incidence of film sticking was lower with sample 2 for a given average diameter of silica particles.

(467) For sample 2, furthermore, the incidence of film sticking was markedly low when the average diameter of the silica particles was 45 nm or less.

(468) For both samples 1 and 2, the incidence of film sticking was reduced to near zero as the average diameter of the silica particles decreased to about 12 nm.

(469) When the average diameter of the silica particles was 12 nm, however, the protective film **50** cracked as in FIG. **31** with both samples 1 and 2, although the cracking was successfully reduced by increasing the average diameter of the silica particles to 15 nm. It is, therefore, preferred that the average diameter of the silica particles be more than about 12 nm, more preferably about 15 nm or more as this makes it more certain that the protective film **50** will not crack.

(470) In the experiment, furthermore, the filler settled down in the material for the protective film **50** when the average diameter of silica particles exceeded 75 nm, and did not when the average diameter of silica particles was 75 nm. A protective film **50** formed from a material in which filler has settled down would be nonuniform, even though it might not stick. It is, therefore, preferred that the average diameter of the silica particles be about 75 nm or less.

(471) In addition, if the material for the protective film **50** contains silica particles (powdered silica) with an average diameter of about 15 nm to about 75 nm and if the amount of the silica particles is such that the material dries sufficiently fast (between about 150 phr and about 250 phr), the percentage by weight of silica particles to resin in the resulting protective film **50** is between about 150% and about 250%.

(472) In other words, a protective film **50** formed with such a silica-to-resin weight percentage dries quickly and does not stick; the protective film **50** in this case is of high quality.

(473) Plating Marks

(474) FIG. **32** is a graphical representation of the number of plating marks with varying thickness of the protective film **50**.

(475) The protective film **50** can leave areas of the body **10** exposed, and these areas may be unwantedly plated during the electrode formation. Deposits of this unwanted plating are herein referred to as "plating marks." An example of a cause of plating marks is the elimination of larger particles of the soft magnetic powder associated with grinding. The material for the protective film **50** can fail to fill the relatively large hollows left in the surface of the body **10**, and in the unfilled hollows plating marks can occur.

(476) In this measurement, the body **10** was examined for plating marks at predetermined intervals along the full length of the ridges between the top surface **14** and mount surface **12** and the first and second side surfaces **16** and **18**, and the plating marks were counted.

(477) As can be seen from the graph, many plating marks were observed when the protective film **50** was thin. When the thickness of the protective film **50** was 5 μm or more, however, the number of plating marks decreased markedly. When the thickness of the protective film **50** was 10 μm or more, few plating marks were observed.

(478) It is, therefore, preferred that the thickness of the protective film **50** be about 10 μm or more. With such a thickness, the protective film **50** certainly protects the entire surface of the body **10** and prevents plating marks.

(479) If the body **10** of the inductor **1** has a specified size, however, thickening of the protective film **50** will affect the performance of the inductor **1** because it means reducing the size of the body **10** excluding the protective film **50** and therefore the size of the coil **30** accordingly.

(480) The protective film **50**, furthermore, is then removed, and outer electrodes **20** are formed as described above in the areas of the inductor **1** from which the protective film **50** has been removed. If the protective film **50** is thicker than the outer electrodes **20**, the contact between the outer electrodes **20** and the circuit board will be poor because the surface of the outer electrodes **20** is lower than that of the

protective film **50**.

(481) It is, therefore, preferred that the thickness of the protective film **50** be smaller than, or at least roughly equal to, that of the outer electrodes **20**.

(482) More preferably, to give the inductor **1** high performance, the thickness of the protective film **50** is about 30 μm or less besides being smaller than or roughly equal to that of the outer electrodes **20**.

(483) The thickness of the outer electrodes **20** was measured as follows. That is, the body **10** was cut in parallel with its second side surfaces **18** at the intersection of the diagonals of the top surface **14** of the inductor **1**. The thickness of the outer electrodes **20** on the mount surface **12** of the body **10** was measured at each quarter of the length L of the electrodes **20** using a microscope at a magnification of $\times 1000$ and averaged (first measurement). The average first measurement of ten inductors **1** was reported as the thickness of the outer electrodes **20**. The microscope was Keyence Corporation's VHX-7000.

(484) Countermeasures Against the Elimination of Particles

(485) As stated, since the body **10** is an article shaped from soft magnetic powder, grinding its surface involves eliminating a considerable number of particles of the powder. In the embodiments and examples described herein, the soft magnetic powder contains larger particles, which have a larger average diameter, and smaller particles, which have a smaller average diameter. The grinding, therefore, leaves relatively deep hollows in the ground surfaces (second side surfaces **18**) as a result of the elimination of larger particles.

(486) Table 18 presents data from an experiment on the thickness of the protective film **50**, the depth of hollows resulting from the elimination of particles, and corrosion resistance.

(487) This experiment was performed using the same sample materials for the protective film **50** as in the experiment in FIG. **30**. The bodies **10** were shaped from soft magnetic powders in which the average diameter of the larger particles was between 21 μm and 28 μm .

(488) The thickness of the protective film **50** was measured as follows. That is, the body **10** was cut in parallel with its second side surfaces **18** at the intersection of the diagonals of the top surface **14** of the inductor **1**. The thickness of the protective film **50** on the upper and lower primary sides of the body **10** was measured at each quarter of the length L of the body **10** using a microscope at a magnification of $\times 1000$ and averaged (second measurement). The average second measurement of ten inductors **1** was reported as measured thickness (average thickness). The microscope was Keyence Corporation's VHX-7000.

(489) For corrosion resistance, "Fail" means the inductors **1** failed to meet predetermined quality criteria for corrosion resistance, and "Pass" means the inductors **1** met the quality criteria.

(490) TABLE-US-00018 TABLE 18 Average Depths Average thickness of hollows thickness/depth Corrosion [μm] [μm] of hollows resistance

(491) As can be seen from Table 18, the protective film **50** is prone to corrosion, and therefore is not of high quality enough, when it is thin for the depth of hollows resulting from the elimination of particles. The corrosion resistance is sufficiently high when the ratio of the thickness of the protective film **50** to the depth of the hollows is about 0.4 or more. Since the depth of the hollows is roughly equal to the average diameter of the larger particles, the protective film **50** is of high quality enough when its thickness is equal to or more than about 0.4 times the average diameter of the larger particles, even if particles have been eliminated from the surfaces therebeneath.

(492) Overall, an inductor **1** according to an embodiment of the present disclosure has a body **10** containing soft magnetic powder and resins, a coil **30** embedded in the body **10**, and outer electrodes **20** on the body **10** and also has a protective film **50** on the surface of the body **10**. The protective film **50** has a thickness of about 10 μm or more and contains silica particles and resin. The silica particles have an average diameter between about 15 nm and about 75 nm, and the percentage by weight of the silica particles to the resin is between about 150% and about 250%.

(493) The protective film **50** certainly protects the entire surface of the body **10** and prevents "plating marks" by virtue of having a thickness of about 10 μm or more.

(494) The protective film **50** also helps prevent errors that can occur when the inductor **1** is visually inspected by optical testing as its gloss has been reduced by the silica particles therein.

(495) The protective film **50**, moreover, is of high quality without being damaged by "sticking." This is because the average diameter of the silica particles therein is between about 15 nm and about 75 nm and because the percentage by weight of the silica particles to the resin being between about 150% and about 250%.

(496) In this embodiment, the thickness of the protective film **50** is smaller than or roughly equal to that of the outer electrodes **20**.

(497) This ensures the outer electrodes **20** will not be interfered with by the thickness of the protective film **50** when coming into contact with a circuit on a circuit board.

(498) In this embodiment, the protective film **50** contains carbon black.

(499) This improves the workability of the body **10** when the protective film **50** is removed by irradiation with a laser for the formation of the outer electrodes **20**.

(500) In this embodiment, the protective film **50** contains a phenoxy resin. This toughens the body **10**.

(501) In this embodiment, the protective film **50** contains a novolac resin. This makes the body **10** more resistant to heat.

(502) In this embodiment, the thickness of the protective film **50** is equal to or more than about 0.4 times the average diameter of the larger particles. This ensures the protective film **50** is of high quality enough, even if particles have been eliminated from the surfaces therebeneath.

(503) In this embodiment, the filler component may be titanium oxide, zirconium oxide, or aluminum oxide.

(504) While preferred embodiments of the disclosure have been described above, it is to be understood that variations and modifications will be apparent to those skilled in the art without departing from the scope and spirit of the disclosure. The scope of the disclosure, therefore, is to be determined solely by the following claims.

Claims

1. A soft magnetic powder comprising: first soft magnetic particles, each having a first nucleus that contains a soft magnetic metal and an insulating film on a surface of the first nucleus, wherein: the insulating film contains Si and a hydrocarbon group having a C8 or longer linear-chain moiety; and a ratio by weight of Si to C in the insulating film is from 7.6 to 42.8.
2. The soft magnetic powder according to claim 1, wherein the hydrocarbon group is an alkyl group.
3. The soft magnetic powder according to claim 2, wherein the first nucleus is made of carbonyl iron.
4. The soft magnetic powder according to claim 3, further comprising: second soft magnetic particles, each having a second nucleus that contains a soft magnetic metal, the second nucleus having an average diameter larger than the first nucleus.

5. An inductor comprising: a magnetic metal material made from the soft magnetic powder according to claim 3; and a coil of wire.
 6. An inductor comprising: a magnetic metal material made from the soft magnetic powder according to claim 4; and a coil of wire.
 7. The soft magnetic powder according to claim 2, further comprising: second soft magnetic particles, each having a second nucleus that contains a soft magnetic metal, the second nucleus having an average diameter larger than the first nucleus.
 8. An inductor comprising: a magnetic metal material made from the soft magnetic powder according to claim 7; and a coil of wire.
 9. An inductor comprising: a magnetic metal material made from the soft magnetic powder according to claim 2; and a coil of wire.
 10. The soft magnetic powder according to claim 1, wherein the first nucleus is made of carbonyl iron.
 11. The soft magnetic powder according to claim 10, further comprising: second soft magnetic particles, each having a second nucleus that contains a soft magnetic metal, the second nucleus having an average diameter larger than the first nucleus.
 12. An inductor comprising: a magnetic metal material made from the soft magnetic powder according to claim 11; and a coil of wire.
 13. An inductor comprising: a magnetic metal material made from the soft magnetic powder according to claim 10; and a coil of wire.
 14. The soft magnetic powder according to claim 1, further comprising: second soft magnetic particles, each having a second nucleus that contains a soft magnetic metal, the second nucleus having an average diameter larger than the first nucleus.
 15. An inductor comprising: a magnetic metal material made from the soft magnetic powder according to claim 14; and a coil of wire.
 16. An inductor comprising: a magnetic metal material made from the soft magnetic powder according to claim 1; and a coil of wire.
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