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United States Patent	12395177
Kind Code	B2
Date of Patent	August 19, 2025
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Reducing non-linearities of a phase rotator

Abstract

A transceiver includes a first transmit (Tx) component configured to connect to a second receive (Rx) component in a second transceiver; a first Rx component configured to connect to a second Tx component in the second transceiver; a single Phase-Locked Loop (PLL) circuit connected to both the first Tx component and the first Rx component; and a control circuit configured to continuously calibrate a first Look-Up Table (LUT) configured to feed operating codes to a first phase rotator connected to an output of the single PLL circuit and to one of the first Tx component and the first Rx component. In an embodiment, the control circuit is further configured to continuously calibrate a second LUT configured to feed operating codes to a second phase rotator connected to an output of a single PLL circuit in the second transceiver.

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Appl. No.: 18/732176

Filed: June 03, 2024

Prior Publication Data

Document Identifier	Publication Date
US 20240322829 A1	Sep. 26, 2024

Related U.S. Application Data

continuation parent-doc US 17944364 20220914 US 12034448 child-doc US 18732176
continuation parent-doc US 17318118 20210512 US 11463093 20221004 child-doc US 17944364

Publication Classification

Int. Cl.: **H03L7/081** (20060101); **H03L7/099** (20060101); **H03L7/197** (20060101); **H04L7/00** (20060101); **H04L7/033** (20060101)

U.S. Cl.:

CPC **H03L7/0814** (20130101); **H03L7/0994** (20130101); **H03L7/1976** (20130101); **H04L7/0037** (20130101); **H04L7/033** (20130101);

Field of Classification Search

CPC: H03L (7/081); H03L (7/0814); H04L (7/033); H04L (7/0337); H04L (7/00); H04L (7/0016); H04L (7/0033); H04L (7/0037)

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Attorney, Agent or Firm: Baratta Law PLLC

Background/Summary

CROSS-REFERENCE TO RELATED APPLICATION(S) (1) The present disclosure is a continuation of U.S. patent application Ser. No. 17/944,364, filed Sep. 14, 2022, which was a continuation of U.S. patent application Ser. No. 17/318,118, filed May 12, 2021, the contents of which are incorporated by reference in their entirety.

FIELD OF THE DISCLOSURE

(1) The present disclosure generally relates to phase rotators. More particularly, the present disclosure relates to systems and methods for improving the linearization of a phase rotator connected to an output of a Phase-Locked Loop (PLL) by continuously updating operating code stored in a Look-Up Table (LUT).

BACKGROUND OF THE DISCLOSURE

(2) Phase-Locked Loops (PLLs) are often used to reduce phase shift between an input and output within a system. A PLL normally includes a phase comparator, a filter (e.g., low pass filter), and a Voltage Controlled Oscillator (VCO) along a main path from an input to an output of the PLL. The output from the VCO is fed back to the phase comparator in a feedback loop to allow the phase comparator to detect any shift in phase and adjust the VCO accordingly to match the phases.

(3) A common solution for resolving clock reference drift between a transmitter and a receiver is to use separate PLLs for the transmitter and receiver and allowing each PLL to produce a frequency offset by adjusting the VCO frequency and/or by rotating a phase rotator inside the PLL feedback loop, allowing the PLL to attenuate any phase rotator induced jitter. However, with two PLLs in this case, the power and area requirements are greatly increased on a circuit board.

(4) A conventional solution to separate PLL phase ramping is to use a clock rate of a digital core as an update rate for the phase rotator. Phase rotators are not commonly used in a continuous ramp to implement frequency offsets without including them directly within the feedback loop. The location of the phase rotators within the feedback loop can filter non-linear responses so that the phase rotator induced jitter is less of an issue. For architectures using a single PLL, the out-of-loop response is typically important, such that minimizing jitter can be critical through all available methods. However, this may also be potentially problematic in cases where it is desirable to further reduce digital core frequency for reducing power.

(5) The conventional systems include various shortcomings. For example, the use of a second PLL greatly increases power and area requirements. Also, operating at the digital core rate can restrict

the update rate and can subject the update rate to affects from other system conditions (e.g., data rate, digital core power, etc.). If low rates are used due to power, this can add an artificial floor onto the jitter parameter.

(6) Furthermore, conventional solutions for linearizing phase rotators can be configured to reduce linearization errors by placing them within the feedback loop of a PLL. Calibration can be performed in the lab or by using special start-up circuits to perform a self-test. However, using the phase rotator within the feedback loop itself restricts the ability to generate multiple clock frequencies (e.g., so as to track jitter frequency errors). Thus, a separate PLL may be required in this case for each clock (e.g., such as a clock for each of the transmitter and receiver). Also, using start-up “foreground” calibration requires the design to maintain calibration over its operating lifetime, especially if it cannot be taken offline for recalibration. Thus, after putting a circuit in use, it may be impossible to change these initial calibration settings and compensate for certain types of changes (e.g., aging effects, effects from voltage shifts, temperature changes, etc.). Therefore, there is a need in the field of PLLs and phase rotation control circuitry to avoid the above-mentioned deficiencies and provide improved linearization of phase rotators.

BRIEF SUMMARY OF THE DISCLOSURE

(7) The present disclosure describes systems, circuits, and techniques for improving linearization of phase rotation systems. According to one embodiment, a circuit includes a single Phase-Locked Loop (PLL) circuit having a main path and a return path forming a feedback loop. The circuit also includes one or more phase rotators connected to an output of the single PLL circuit outside the feedback loop and one or more adaptable Look-Up Tables (LUTs) populated with operating code to be provided to the one or more phase rotators for defining operating characteristics of the one or more phase rotators. Furthermore, the circuit includes a control device configured to receive phase response characteristics from the one or more phase rotators. The control device is further configured to modify the operating code of the one or more adaptable LUTs based on the phase response characteristics to reduce non-linearities of the one or more phase rotators.

(8) According to additional embodiments, the one or more phase rotators of the circuit may include a first phase rotator associated with a transmitter component and a second phase rotator associated with a receiver component. The transmitter component and receiver component are configured to share the single PLL circuit. The circuit may also include a Clock and Data Recovery (CDR) circuit configured to receive output signals from the receiver component and provide input signals to one of the one or more adaptable LUTs and to the control device. The one or more phase rotators are configured for continuous operation, and wherein the control device is configured to iteratively modify the operating code of the one or more adaptable LUTs based on changeable phase response characteristics of the one or more phase rotators to allow the control device to improve linearization performance of the one or more phase rotators. Also, the control device may be configured to compensate for the changeable phase response characteristics caused by errors due to temperature changes, voltage shifts, and aging effects.

(9) In additional embodiments, the circuit may further include one or more linear ramps configured to shift the output frequency of the one or more phase rotators. The control device may be configured to modify the operating code of the one or more adaptable LUTs to improve the linearization of the one or more linear ramps. The one or more adaptable LUTs may be configured to correct phase errors in the one or more phase rotators. Also, the control device may include an Integrated Digital-to-Analog Converter (IDAC) coding component configured for background calibration of the one or more adaptable LUTs. The IDAC coding component may be configured to receive interpolation information from an interpolator, wherein the interpolator can include a clock configured to control an update rate at which the IDAC coding component modifies the operating code of the one or more adaptable LUTs. The clock may operate faster than a digital core rate associated with the one or more adaptable LUTs, wherein the IDAC coding component may be configured to interpolate intermediate code between the operating code associated with the digital

core rate.

(10) Furthermore, the circuit may also include one or more phase rotator controllers configured to receive the operating code from the one or more adaptable LUTs and apply the operating code to the one or more phase rotators. and one or more frequency dividers each connected to an output of the one or more phase rotators. Also, the circuit may include a spectrum analyzer configured to measure the phase response characteristics from the one or more phase rotators and forward the phase response characteristics to the control device. The control device may be configured to provide an incremental step to an accumulator associated with a digital core connected to the one or more phase rotator controllers. For example, the spectrum analyzer may be configured to perform a trial offset process, where the trial offset process may include applying different sets of test operating code to the one or more adaptable LUTs, monitoring non-linearities of the one or more phase rotators to determine a set of test operating code having the best results, and replacing the operating code with the set of test operating having the best results.

Description

BRIEF DESCRIPTION OF THE DRAWINGS

- (1) The present disclosure is illustrated and described herein with reference to the various drawings, in which like reference numbers are used to denote like system components/method steps, as appropriate, and in which:
- (2) FIG. 1 is a schematic diagram illustrating a dual Phase-Locked Loop (PLL) circuit, according to various embodiments.
- (3) FIG. 2 is a schematic diagram illustrating a single PLL circuit, according to various embodiments of the present disclosure.
- (4) FIG. 3 is a schematic diagram illustrating a phase rotation circuit connected to an output of a PLL, according to various embodiments of the present disclosure.
- (5) FIG. 4 is a graph showing phase responses using fast and slow sampling rates compared with an ideal phase response, according to various embodiments of the present disclosure.
- (6) FIG. 5 is a graph showing jitter of a phase rotator system based on update rate, according to various embodiments of the present disclosure.
- (7) FIG. 6 is a graph showing the effects of various phase rotator deficiencies on the overall noise of a system, according to various embodiments of the present disclosure.
- (8) FIGS. 7A-7F are schematic diagrams illustrating circuits and systems for controlling phase rotation, according to various embodiments of the present disclosure.
- (9) FIG. 8 is a schematic diagram illustrating another system for controlling phase rotation, according to various embodiments of the present disclosure.
- (10) FIG. 9 is a schematic diagram illustrating yet another system for controlling phase rotation, according to various embodiments of the present disclosure.
- (11) FIGS. 10A-10D are diagrams illustrating timing and coding signals with respect to an interpolator of a phase rotation controller, according to various embodiments of the present disclosure.
- (12) FIGS. 11A-11J are graphs showing phase noise simulation results using various interpolation modes, according to various embodiments of the present disclosure.
- (13) FIGS. 12A-12N are graphs showing phase error simulation results using various interpolation modes, according to various embodiments of the present disclosure.
- (14) FIG. 13 is a graph showing phase error with respect to frequency offset using various interpolation modes, according to various embodiments of the present disclosure.
- (15) FIG. 14 is a table showing jitter results using various interpolation modes, according to various embodiments of the present disclosure.

(16) FIGS. 15A-15C are graphs showing aspects of a test offset process for improving Look-Up Table (LUT) operating code, according to various embodiments of the present disclosure.

(17) FIGS. 16A and 16B are graphs showing jitter response to LUT value adjustments, according to various embodiments of the present disclosure.

(18) FIGS. 17A-17C are graphs showing results of another technique for testing LUT values using iterative mutations, according to various embodiments of the present disclosure.

DETAILED DESCRIPTION OF THE DISCLOSURE

(19) In various embodiments, the present disclosure relates to systems and methods for performing linearization techniques to reduce non-linearities of phase rotators or phase shifters. In particular, one or more phase rotators may be connected to an output of a Phase-Locked Loop (PLL) circuit, yet outside the perimeter of the feedback loop of the PLL. In some embodiments of the present disclosure, each of the phase rotators may receive phase modifying signals from a linear ramp. Ideally, the linear ramp provides signals with perfect linearity. However, in reality, these linear ramps may include non-linearities that prevent the phase rotators from operating at an optimal level. Thus, the embodiments of the present disclosure are configured to utilize a Look-Up Table (LUT) for each linear ramp, where the LUT can be updated continuously to provide operating code that can improve the linearity of the linear ramps and thus improve the operability of the phase rotators.

(20) Digital core processors may be configured to provide clock signals at a predetermined rate. However, to improve the operation of the phase rotators according to some embodiments, the LUTs can be updated at a rate that is higher than the clock rate of the digital core processor. This can be done by an up-sampling technique where more updated samples can be processed than would normally be possible at the regular clock speed. The up-sampling techniques of the present disclosure include an interpolation process for interpolating samples between the normal samples defined by the processor speed. The up-sampling circuit of the present disclosure can increase the effective digital core rate, making it partially independent of the core rate, while still allowing the phase rotator to be updated at a sufficiently fast rate. This keeps jitter low enough to allow for a phase rotator to be placed outside the feedback loop of the PLL and avoids the need for a second PLL.

(21) The present disclosure provides systems and methods that enable highly linear phase rotators. A linearity performance level of the present circuits and systems is sufficient to enable continuous rotation of the phase rotators outside of the PLL feedback loop, which allows two or more separate components (e.g., a transmitter (Tx) and a receiver (Rx)) to share the single PLL, while each using its own phase rotator. Calibration of the operating code information stored in the LUTs can run continuously while the phase rotators are in operation. Thus, the embodiments of the present disclosure are configured to compensate for errors that may appear, including temperature shifts, voltage shifts, effects caused by the aging of the phase rotators and other related components, among other issues.

(22) In order to compensate for offsets in frequency references, separate PLLs are typically required for transceiver systems so that the PLL can lock onto different frequencies. However, to save power and area on a circuit board, it is possible to use a single PLL with two or more separate phase rotators. As mentioned above, each phase rotator can be fed a linearly increasing signal from a linear ramp to create the required frequency shift.

(23) The embodiments of the present disclosure are configured to provide techniques for calibrating an LUT associated with the PLL and phase rotators to properly linearize the characteristics of the phase rotators. The systems and methods of the present disclosure have an advantage over conventional systems in that the present circuits do not use static time-based characterization and are able to minimize the amount of equipment needed. Also, since the present techniques are configured to operate the phase rotators in continuous rotation, the present circuits are able to account for transient effects by calibrating the LUTs during continuous use. The present

methods are configured to run while the phase rotators are in operation, allowing for continuous background calibration. In this context, “background calibration” refers to calibration conducted at a back-end of a system or circuit, after accumulation steps, applying operating code from an LUT, and interpolation steps. The background calibration may include phase rotation calibration of Integrated Digital-to-Analog (IDAC) coding, which may then be applied to the LUT for updating the operating code stored in the LUT.

(24) The present disclosure can be used on a continuous linear phase ramp associated with a phase rotator to shift the output frequency of a PLL. Also, the present embodiments can be used in a clock recovery circuit to reduce the power of a system. For example, by using a single PLL for shared Tx and Rx components, the system can save power. To track frequency drifts between Tx and Rx blocks of different modules, the phase rotator may be rotated to generate the needed frequency offset.

(25) FIG. 1 is a schematic diagram illustrating an embodiment of a dual Phase-Locked Loop (PLL) circuit **10**. The dual PLL circuit **10** includes a first PLL **12a** and a second PLL **12b**. A reference signal (REF) is applied to a phase frequency detector **14a**, **14b** of the PLLs **12a**, **12b**, respectively. Along a main path of the respective PLL **12a**, **12b**, the phase frequency detector **14a**, **14b** provides an output to a charge pump **16a**, **16b**, a filter **18a**, **18b** (e.g., low pass filters), and a Voltage Controlled Oscillator (VCO) **20a**, **20b**. The VCO **20a**, **20b** provides an output through a respective amplifier **22a**, **22b**. The output of the first PLL **12a** is an Analog-to-Digital Converter (ADC) clock signal (ADC CLK) and the output of the second PLL **12b** is a Digital-to-Analog Converter (DAC) clock signal (DAC CLK). For example, the ADC CLK may be fed to a Rx component and the DAC CLK may be fed to a Tx component.

(26) In addition, according to typical PLL architecture, the VCO **20a**, **20b** is configured to also provide the output back to the respective phase frequency detector **14a**, **14b** along feedback loops **24a**, **24b**. In this embodiment, the feedback loops **24a**, **24b** may also include an amplifier **24a**, **24b** and a frequency divider **28a**, **28b**, respectively. The signals that are fed back to the phase frequency detectors **14a**, **14b** along feedback paths **24a**, **24b** are configured to allow the phase frequency detectors **14a**, **14b** to compare the input and output phases and modify the VCO **20a**, **20b** to match the output phase with the input phase. However, as mentioned above, the dual PLL circuit **10**, which includes the two PLLs **12a**, **12b**, will use more power and take up more real estate on a circuit board compared to a system with only a single PLL.

(27) FIG. 2 is a schematic diagram illustrating an embodiment of a single PLL circuit **30**. In this embodiment, the single PLL circuit **30** includes a Phase Frequency Detector (PFD) **32**, a Charge Pump (CP) **34**, a filter **36** (e.g., low pass filter), and a VCO **38** along a main path from an input of the single PLL circuit **30** to an output thereof. Also, the VCO **38** is configured to provide a feedback signal along a return path **40**, whereby the main path and the return path **40** in combination form a feedback loop. In this embodiment, the return path **40** includes an amplifier **42** and a frequency divider (1/N) **44**, whereby feedback signals from the VCO **38** are fed to the PFD **32** for phase comparison purposes.

(28) Also, to enable the application of the PLL clock signals to two different components (e.g., a Tx component and a Rx component), the single PLL circuit **30** in this embodiment includes differential frequency components **46a**, **46b**. According to some embodiments, the VCO **38** and differential frequency components **46a**, **46b** may form a phase rotation circuit **48-1**. The first differential frequency component **46a** may be configured to supply output signals of an ADC CLK via a first amplifier **50a**, and the second differential frequency component **46b** may be configured to supply output signals of a DAC CLK via a second amplifier **50b**.

(29) FIG. 3 shows another embodiment of a phase rotation circuit **48-2**, which may be similar to the phase rotation circuit **48-1** shown in FIG. 2 and may be incorporated in the single PLL circuit **30** or other suitable PLL circuit for providing phase rotating functionality. More particularly, the phase rotation circuit **48-2** may be connected to an output of a PLL (e.g., at the output of the VCO

38) and positioned outside the feedback loop (e.g., outside the loop formed by the main path plus the return path **40** shown in FIG. 2). In this embodiment, the phase rotation circuit **48-2** includes the VCO **38** and an output **54** (of the PLL). The output **54** is fed to a first phase rotator **56a** and a second phase rotator **56b**. The phase rotation circuit **48-2** further includes a first linear ramp device **58a** that feeds a linearly increasing signal to the first phase rotator **56a** and a second linear ramp device **58b** that feeds a linearly increasing signal to the second phase rotator **56b**. Outputs **60a**, **60b** of the phase rotation circuit **48-2** are supplied by the first and second phase rotators **56a**, **56b**, respectively.

(30) It should be noted that the quality of a frequency shift of a PLL is sensitive to many different performance parameters of the phase rotators **56a**, **56b**. Maintaining a low noise clock signal from the PLL include tuning the phase rotators **56a**, **56b** to reduce non-linearities. While the phase rotators **56a**, **56b** may be designed specifically to minimize non-linearities, some non-linearities may still remain in the phase rotation circuit **48-2** (or other similar phase rotation circuits). In some cases, these non-linearities cannot be corrected by conventional systems. For examples, some non-linearities may be caused by natural non-linear transistor characteristics (e.g., process variations that affects a batch of chips, sample mismatch variations that affect performance, and other variations from one die to another) as well as variation caused by voltage shifts, temperature changes, and changes caused by the degradation or other effects of natural aging of the circuit components.

(31) According to various embodiments of the present disclosure, as described in more detail below, the phase rotators **56a**, **56b** and linear ramp devices **58a**, **58b** can be adjusted as needed to create outputs **60a**, **60b** with a more linear response, thereby improving the operational performance of the phase rotation circuit **48-2**. Thus, the systems and methods of the present disclosure are configured to compensate for the non-linearities of the phase rotation circuit **48-2**. For example, according to some implementations, a Look-Up Table (LUT) can be used to feed operating code to each respective pair of the phase rotators **56a**, **56b** and linear ramp devices **58a**, **58b**.

(32) The LUTs are configured to take input codes that represents a perfect, linear phase rotator response and add predetermined offsets so that the phase rotator creates the actual phase shift desired by the input code. If the phase rotators **56a**, **56b** are not perfectly compensated for by the LUTs, then the resulting phase errors will show up as clock spurs and jitter when the phase rotators **56a**, **56b** are rotated to create a frequency shift. To determine if the compensation is adequate, trial offsets can be made to the LUT and the jitter can be monitored. At first, small offsets (e.g., in both the positive and negative directions) can be made to multiple test values. If one of them leads to an improved response, additional steps can be taken in an attempt to continue to reduce jitter further. According to various implementations, the test values can be selected prudently. For example, if an offset is too long, then only broad non-linearities spanning many codes can be compensated for. If offset is too short, more jitter may be introduced thereby preventing the trial from determining if any improvement has been made. Once the best offsets are determined, they can be kept (e.g., stored in the LUT) and these steps can be repeated with an offset at a different location in the LUT.

(33) This technique may require high linearity in the phase rotators **56a**, **56b**. However, since the phase rotators **56a**, **56b** are located outside of the feedback path of the PLL, any error in their response would lead to phase jitter or spurs in the output waveforms. One way to improve the response is by increasing the update rate (e.g., up-sampling) of the phase rotator ramp (e.g., linear ramp devices **58a**, **58b**). If the phase rotator is updated very slowly, the ramp signal will be turned into a large step response as shown in FIG. 4.

(34) FIG. 4 is a graph **64** showing phase responses using fast and slow sampling rates compared with an ideal (linear) phase response. It should be noted that even if the phase rotator **56a**, **56b** has perfect linearity, the sampling rate of the respective linear ramp devices **58a**, **58b** can still lead to a poor output signal since the large steps will be turned into spurs.

(35) FIG. 5 is a graph 66 showing Root Mean Squared (RMS) clock jitter (in picoseconds (ps)) of a phase rotator system versus update rate. The update rate is based on a strobe frequency ($f_{\text{sub.strobe}}$) divided by a difference in frequency (Δf). The graph 66 shows simulated phase rotator systems and how update rate can limit phase rotator linearity. N is the number of bits. This diagram shows the jitter versus strobe frequency ratio (ratio of the strobe frequency to the operating frequency) with different number of bits in the control signal. So, N=5 represents a phase rotator with $2^5=32$ steps total. N=6 represents a phase rotator with 64 (2^6) steps, etc.

(36) As described in more detail below, an interpolator can be used in a phase rotation system when an update rate is increase (e.g., when up-sampling is enabled). For example, the interpolator may operate by linearly interpolating between successive phase rotator codes after an LUT correction. The interpolation may be performed by binary arithmetic (e.g., by adding two numbers, shifting bits to divide by 2) for minimal power cost. Since the codes interpolated intermediately have been corrected with the LUT, further non-linear correction may not be needed as long as the step size is small.

(37) Several interpolation modes may be possible according to various embodiments of the present disclosure. The interpolation modes may be indicated by a two-digit binary code, such as Mode 00, Mode 01, Mode 10, and Mode 11, described in more detail below with respect to FIG. 10. In this example, Mode 00 may be configured to disable interpolation completely, Mode 01 may be configured to interpolate at a $\times 2$ base clock rate (i.e., two times the clock rate of a digital core processor), Mode 10 may be configured to interpolate at a $\times 4$ rate, and Mode 11 may be configured to sample every other input code and sample at a rate of 8 times the divided down rate (e.g., four times the base clock rate).

(38) In some embodiments, a process may include a first step of re-timing the input data with the local clock. This may introduce possible timing margin issues since the phase relationship between the interpolation clock and the code from the digital core may be indeterminate. Thus, a phase selector can be added so the interpolation clock phase can be inverted instead. The re-timing clock can be divided down to reduce the resampling rate. In future iterations, variable dividers can be used (e.g., divide by 3 or 5) to match the mismatching interpolation clock and the digital core rate (e.g., matching a sampling frequency of 768 ps to a sampling frequency of 160 ps).

(39) The interpolation clock can also be divided down to generate intermediate clocks needed to control multiplexers and other logic blocks. Unused clock blocks can be gated to save power. A shift register may be configured to store a previous code, which can be fed into the averaging chain to create up to eight interpolated values between the two codes. As not all codes are used (depending on the Mode), the averaging blocks that are not needed can be disabled to save power. A mux can be configured to alternate between the interpolated values based on the intermediate clocks generated to output the interpolated codes in the correct order. A new strobe clock is generated and used to re-time the output code to maximize timing margin response.

(40) FIG. 6 shows a group of graphs 68 to demonstrate the effects of various phase rotator deficiencies on the overall noise of a system. The first column shows graphs of phase shifts with high Differential Non-Linearity (high DNL), high Integral Non-Linearity (high INL), and low resolution. The second column shows graphs of phase errors over time for the high DNL, high INL, and low resolution phase shifts. The last column shows a graph of the phase noise with respect to offset frequency and includes an accumulation of the phase errors shown in the second column.

The graphs 68 show how phase rotator impairments can affect jitter response. To improve the jitter response, the update rate of the phase rotator can be increased. Otherwise, as depicted in the graphs 68, the jitter will reach a floor and cannot be improved, even with a higher resolution phase rotator.

(41) Typically, the update rate will come from the digital core processor. Hence, the maximum rate is normally limited to what is desired for the core. The update rate may be based on certain factors, such as data rate, sample rate, power consumption, and logic performance. In conventional

systems, the phase rotator performance is not typically a priority, despite the impact that it can have on system performance. As such, the rate is typically much lower than what the phase rotator can support. The embodiments of the present disclosure are configured to increase the update rate (by interpolation) to provide better linearity of the phase rotators.

(42) The present disclosure increases the phase rotator effective update rate beyond the clock rate of the digital core processor by using a faster clock while determining the correct intermediate code between digital core clock samples. As the LUT of the phase rotator is essential in eliminating various process and mismatch variations, the interpolation circuit describe in the present disclosure can factor in and compensate for these variations, especially since the LUT rate can be limited. This can be done by interpolating after the LUT correction. In addition, avoiding unnecessary re-time stages may also be important, as the re-timing process may add delay and decrease the clock recovery bandwidth.

(43) FIGS. 7A-7F are schematic diagrams illustrating circuits and systems for controlling phase rotation according to various embodiments of the present disclosure. FIG. 7A shows an overall system **70** for controlling phase rotation. The system **70** includes a digital core **72** and an analog circuit **74**. The digital core **72** may be part of a processor, microprocessor, or other suitable processing device having a predetermined processor clock speed. In this embodiment, the digital core **72** includes an accumulator **76** and an LUT **78** and the analog circuit **74** includes an interpolator **80** and a phase rotator Integrated Digital-to-Analog Converter (IDAC) coding device **82**. In some embodiments, the phase rotator IDAC coding device **82** may be configured to provide updates that can be supplied to the LUT **78** for continuously updating the operating code of the LUT **78** for optimizing (or improving) the linearity of the phase rotation circuitry.

(44) The accumulator **76** and LUT **78** of the digital core **72** can be calibrated through lab characterization processes. The interpolator **80** can be calibrated using updated samples. The phase rotator IDAC coding device **82** can be calibrated using a background calibration process at an end location of the system **70**. According to conventional systems, it had been decided that this fourth stage of background calibration (e.g., at the phase rotator IDAC coding device **82**) does not have a large impact on the performance of various phase rotation systems (such as the system **70**). However, according to the embodiments of the present disclosure, this background calibration at the phase rotator IDAC coding device **82** can be performed in such a way to allow for calibration that indeed can have an impact on the system **70** and can optimize (or improve) the performance of the phase rotators **56a**, **56b** over the entire lifetime of the phase rotators **56a**, **56b**, even during the occurrence of different types of variations (e.g., temperature change, voltage shift, and aging effects, etc.).

(45) According to various embodiments of the present disclosure, the interpolator **80** can be used to interpolate between cycles or samples of the clock of the digital core **72**. This is an improvement over conventional designs, whereby phase rotator updates were limited to the rate of the digital core **72**. This allows the analog circuit **74**, configured as a macro for generating code generation, to operate at a much higher rate. As shown in FIG. 7A, 11 bits may be communicated simultaneously between each pair of components.

(46) Increasing the update rate of the interpolator **80** can reduce the non-linearity from phase rotation processes. In one example, the strobe or clock of the digital core **72** may have a rate of one cycle or sample every 640 fs (or one cycle/sample every 768 fs). The present disclosure allows the interpolator **80** to operate at one cycle every 160 fs. According to this example, the interpolator **80** can produce a speed of $4\times$ the digital core processor. "fs" here refers to system sampling frequency. So, for instance, if the system has a sampling frequency of 80 GHz, $\text{fs}/640$ is $80\text{ GHz}/640=125\text{ MHz}$.

(47) The LUT **78** is configured to operate at the digital core rate. The interpolator **80** interpolates codes linearly. After LUT conversion, however, the interpolator **80** can use a shift register to store successive values. This process can introduce a short delay path, which can be minimized by

reducing re-timing stages to a minimum.

(48) The accumulator **76** and the LUT **78** can be originally compensated for by in-lab tests, the interpolator **80** can be compensated for using a parts-based calibration, and the phase rotator IDAC coding **82** can be compensated for by background calibration. Calibration based on a Joint Calibration and Localization (JCL) process can be performed for the accumulator **76** and LUT **78**. This JCL-based calibration can be performed relatively easily. Also, JCL-based calibration may also be possible with the interpolator **80** (depending on various time constraints). However, JCL-based calibration would normally not be possible on the phase rotator IDAC coding device **82** without taking it off-line. The JCL-based calibration may only provide for static (initially predetermined) error correction, but it may be noted that transient effects would not be captured by this process. Thus, background calibration methods as described in the present disclosure are configured to populate the LUT **78** for utility in linearizing the phase rotation processes.

(49) FIG. 7B illustrates an embodiment of the analog circuit **74** shown in FIG. 7A, where the analog circuit **74** includes the interpolator **80** and the phase rotator IDAC coding device **82**. In this embodiment, the phase rotator IDAC coding device **82** includes first, second, third, and fourth phase rotators **86a**, **86b**, **86c**, **86d**. The first phase rotator **86a** includes a phase function $(\alpha + \beta \cos(\theta)) \cdot \sup{.2}$; the second phase rotator **86b** includes a phase function $(\alpha - \beta \cos(\theta)) \cdot \sup{.2}$; the third phase rotator **86c** includes a phase function $(\alpha + \beta \sin(\theta)) \cdot \sup{.2}$; and the fourth phase rotator **86d** includes a phase function $(\alpha - \beta \sin(\theta)) \cdot \sup{.2}$. The phase rotators **86a**, **86b**, **86c**, **86d** are configured to provide outputs to I DAC, Ib DAC, Q DAC, and Qb DAC, respectively. The phase rotator core has 4 differential pairs, each with an independent bias current. The 4 differential pairs each have different inputs and are named as such: I, Ib, Q and Qb. The codes I, Ib, Q, and Qb are the codes that are given to the current DACs that control the current bias to their respectively named differential pair. So the I code controls the current DAC for the I differential pair, and so on.

(50) The LUT **78** may be used to correct phase errors in the phase rotator response. The phase rotator IDAC coding device **82** may be configured to populate the LUT **78** for phase rotation to compensate for various issues. For example, populating the LUT **78** according to various implementations of the present disclosure may be performed to 1) compensate for remaining non-linearities that were previously uncompensated by non-linear code. This process may also be configured to 2) compensate for global process variations. Also, the process may also 3) compensate for sample mismatches and 4) compensate for effects from voltage shifts, temperature shifts, aging, etc.

(51) FIG. 7C is a schematic diagram illustrating an embodiment of the phase rotator IDAC coding device **82** shown in FIGS. 7A and 7B. Each of the phase rotators **86a**, **86b**, **86c**, **86d** includes first and second multiplexers **90a**, **90b** configured to receive a number of precalculated constants. An OR gate **92** is configured to receive a code Least Significant Bit (LSB) and a code Most Significant Bit (MSB) (representing polarity) at its inputs. An output of the OR gate **92** is supplied to a multiplier **94**, which also receives a coefficient ("coef") output from the first multiplexer **90a**. The output from the multiplier **94** is supplied to an adder **96**, which also receives an offset output from the second multiplexer **90b**.

(52) The output of the adder **96** is also the output of the respective phase rotator (e.g., phase rotator **86a**). This output, in addition to the outputs of the other adders of the other phase rotators (e.g., phase rotators **86b**, **86c**, **86d**) are supplied to each of four different multiplexers **98a**, **98b**, **98c**, **98d**. The multiplexers **98a**, **98b**, **98c**, **98d** receive selector signal "code MSB" for selecting one of the four inputs. The first multiplexer **98a** outputs Code I; the second multiplexer **98b** outputs Code Ib; the third multiplexer **98c** outputs Code Q; and the fourth multiplexer **98d** outputs Code Qb.

(53) FIG. 7D is a diagram illustrating an embodiment of four phase rotations based on the outputs of the multiplexers **98a**, **98b**, **98c**, **98d**. Analog codes are provided for representing different phase rotations. For example, Code I may represent a signal with no phase rotation; Code Ib may represent a signal with a 180° phase rotation (or phase shift); Code Q may represent a signal with a

90° phase rotation (or phase shift); and Code Qb may represent a signal with a 270° phase rotation (or phase shift). The MSB portions are designated by the character “A” and the LSB portions are designated by the character “D” (highlighted in FIG. 7D).

(54) FIG. 7E is a schematic diagram illustrating an embodiment of an interpolator **100**, which may represent the interpolator **80** shown in FIG. 7A. In this embodiment, the interpolator **100** includes a code input that is configured to receive CODE IN from the LUT **78** shown in FIG. 7A. The CODE IN is supplied to a first multiplexer **102a**, which provides a CODE OUT signal. A strobe (clock) input is configured to receive STROBE IN from the LUT **78**. The STROBE IN is supplied to a second multiplexer **102b**, which provides a STROBE OUT signal.

(55) The interpolator **100** also includes a clock generator and re-timer **104** configured to receive an interpolation clock (INTRPLTN CLK) from the LUT **78**. The clock generator and re-timer **104** supplies a first output to selector inputs of first and second flip-flops **106a**, **106b**. A second output is supplied to the second multiplexer **102b** and a third output is supplied to code selector logic **114**. The first flip-flop **106a** is also configured to receive the STROBE IN signal. The output of the first flip-flop **106a** is supplied to the second flip-flop **106b** and to an input of a code interpolator **108**. The second flip-flop **106b** also supplies an output to the code interpolator **108**. The code interpolator **108** may be configured to provide eight outputs to another multiplexer **110**. Mode selector logic **112** is configured to receive a mode select input and provide mode selections to each of the multiplexers **102a**, **102b**, the clock generator and re-timer **104**, and the code selector logic **114**. The code selector logic **114** is configured to select one of the inputs to the multiplexer **110** for output to the first multiplexer **102a**.

(56) FIG. 7F is a schematic diagram illustrating another embodiment of an interpolator **120**, which may also represent the interpolator **80** shown in FIG. 7A. In this embodiment, the interpolator **120** includes a multiplexer **122** for receiving, from the LUT **78**, a clock signal from the digital core **72** and an inverse of the digital core clock signal at its inputs. The multiplexer **122** provides an output to logic **124** configured to output four different clock signals. A first clock signal is the digital core clock signal $\times 0.5$ (CLK $\times 0.5$); a second clock signal is the digital core clock signal $\times 1$ (CLK $\times 1$); a third clock signal is the digital core clock signal $\times 2$ (CLK $\times 2$); and the fourth clock signal is the digital core clock signal $\times 4$ (CLK $\times 4$). These clock signals may be provided to various components of the interpolator **120**.

(57) First and second multiplexers **126a**, **126b** are configured to receive CODE IN and STROBE IN signals, respectively. A first flip-flop **128a** receives the STROBE IN signal and the CLK $\times 4$ as a selector input. The first flip-flop **128a** provides an output to a second flip-flop **128b**, which provides an output to a third flip-flop **128c**. Another multiplexer **130** receives the CLK $\times 1$ and CLK $\times 0.5$ clock signals and provides an output to the selector inputs of the second and third flip-flops **128b**, **128c**. The output of the second flip-flop **128b** is supplied as an input to a multiplexer **132**. A number of averaging circuits **134** are arranged between this output of the second flip-flop **128b** and an output of the third flip-flop **128c** to provide multiple outputs to the multiplexer **132**.

(58) The output of the multiplexer **132** is supplied to another flip-flop **136**. A multiplexer **138** receives CLK $\times 2$ and CLK $\times 4$ inputs and supplies an output to a selector input of the flip-flop **136** and to another input of the second multiplexer **126b**. The output of the flip-flop **136** is supplied to another input of the first multiplexer **126a**. Mode selector logic **140** is configured to receive a mode selection signal and provide a mode selection output to each of the first and second multiplexers **126a**, **126b**, the multiplexers **130** and **138**, and code select logic **142**. The code select logic receives the CLK $\times 1$, CLK $\times 2$, and CLK $\times 4$ clock signals and provides the selected output to a selector input of the multiplexer **132**.

(59) At any given time, one of each code blocks may be used. This can provide significant improvement over piecewise linear code block compared with other systems. Using the interpolators **100**, **120** described in the present disclosure, the system **70** is configured to compensate for sub-threshold region operation. These may be configured to as an improvement,

whereby other system may operate at the expense of slightly higher power and a reduction in gain. The system **70** of the present disclosure may be configured resolve linearity issues by making adjustments in the tuning and by sizing the interpolators **100**, **120** appropriately.

(60) FIG. **8** is a schematic diagram illustrating an embodiment of a control system **150** for controlling phase rotation. In this embodiment, the system **150** may include a phase rotation system **152** (e.g., the system **70** described above with respect to FIGS. 7A-7F). For example, the phase rotation system **152** may include a digital core **154** (e.g., the digital core **72**) and a clock slice device **156** (e.g., the analog circuit **74**). Also, the control system **150**, according to this embodiment, includes a spectrum analyzer **158** and a control device **160** (e.g., a control loop) used in a feedback loop configuration for providing linearization control of phase rotation devices.

(61) In some embodiments, the digital core **154** may include an accumulator **162** (e.g., the accumulator **76** shown in FIG. 7A) and an LUT **164** (e.g., the LUT **78**). The clock slice device **156** may include a phase rotator controller **166**, a Voltage-Controlled Oscillator (VCO) **168**, a phase rotator **170**, an amplifier **172**, a frequency divider (1/N) **174**, and a second amplifier **176**. The output of the second amplifier **176** is provided as a multiplexer output to the spectrum analyzer **158**. In response to phase rotation characteristics obtained by the spectrum analyzer **158**, the control device **160** is configured to update the LUT **164** as needed to optimizer (or improve) the operational code stored in the LUT **164** for creating a linearized phase rotator response. Also, the control device **160** is configured to provide an incremental step (inc_step) to the accumulator **162**.

(62) The control system **150** is arranged with the measurement setup as shown in FIG. **8** and may be configured to operate without Joint Calibration and Localization (JCL) phase rotator calibration hardware. Instead, the control system **150** may include a useful testbed for calibration testing by monitoring the integrated jitter and use the jitter to guide adjustments to the LUT **164**. Simulation results showing the input code and input clock signals provided to the interpolator (e.g., clock slice device **156**) and the output code and output clock signals supplied by the interpolator are shown with respect to FIGS. **10A-10D**, as described in more detail below.

(63) FIG. **9** is a schematic diagram illustrating an embodiment of another control system **180** for controlling phase rotation. The control system **180** may include the setup shown in FIG. **9** for conducting background calibration. In this embodiment, the control system **180** includes Card A and Card B. According to other embodiments, the control system **180** may be configured to any two separate components of a system where phase rotation can be performed for two or more components with a single Phase-Locked Loop (PLL).

(64) As shown, the control system **180** includes a control device **182** (e.g., control loop) used in a feedback loop control configuration for providing control to both Card A and Card B. Card A includes an oscillator **184** (e.g., VCO) representing an output of a PLL. Card A also includes first and second phase rotators **186a**, **186b** connected to the oscillator **184** and outside of the feedback loop of the associated PLL. In this embodiment, a Rx component **188** is arranged to receive the phase rotation output from the first phase rotator **186a** and a Tx component **190** is arranged to receive the phase rotation output from the second phase rotator **186b**. Card B include similar components. A Tx component **192** of Card B is configured to communicate data signals to the Rx component **188** of Card A along link **194**.

(65) The phase rotators **186a**, **186b** of Card A are configured to receive linear ramp signals from linear ramp devices **196a**, **196b**, respectively. LUTs **198a**, **198b** are configured to supply operating code to the linear ramp devices **196a**, **196b**, respectively, for controlling the operation and linearity of the linear ramp devices **196a**, **196b**. The first LUT **198a** is configured to receive control signals from the control device **182** and from a Clock and Data Recovery (CDR) device **200**. The CDR device **200** is also configured to receive phase response input from the Rx component **188** and provide signals indicative of the received phase response to the control device **182** for further analysis to enable recovery of clock and data signals. On the Tx side of Card A, the second LUT **198b** is configured to receive clock signals from a Tx CLK control device **202**. Again, Card B

includes a similar Tx CLK control device.

(66) The Rx component **188**, CDR device **200**, LUT **198a**, linear ramp device **196a**, and phase rotator **186a** form a feedback control loop for actively updating the LUT **198b** to optimize the linearity of the linear ramp device **196a** and phase rotator **186a**. Card B includes similar components and a similar feedback control loop with its Rx component. Another feedback loop involves the control device **182** that supplies control to the LUT **198b** and the associated LUT of Card B.

(67) The CDR **200** in the receiver loop is able to estimate and monitor the total clock jitter in the Tx and Rx paths. Trial adjustments in either the Rx LUT (e.g., LUT **198a**) or the Tx LUT (e.g., LUT **198b**) can be made and the total jitter monitored. Adjustments to the LUT **198a**, **198b** are made as needed. Since the jitter created by a small trial offset in the wrong direction is very small (e.g., approximately on the order of a few femtoseconds (fs)), the impact on the control system **180** is small. Long averages can be used in order to resolve these small differences. Over a long period of time, the LUTs **198a**, **198b** can be improved and slow effects, such as temperature or voltage drifts, aging effects, etc. can be compensated for.

(68) In operation, the control system **180** is configured to use the same control loop as used in other embodiments. However, according to some implementations, jitter may be measured using information from the CDR **200** regarding an amount of jitter. It is likely that only the LUT **198a** associated with the Rx loop needs to be modified (for simplicity). However, in some other embodiments, the control system **180** may be modified to potentially provide enhanced performance which may be possible by incorporating a CDR device with the Tx in another feedback loop to enable the modification of the LUT **198b** associated with the Tx side.

(69) As the LUT **198a** approaches an “ideal” value, the jitter issues (e.g., integrated spurs and phase noise) will improve. It may be noted that this arrangement might not be applicable on a single isolated point basis. For example, if a phase jump between consecutive points is too large, it may cause a phase jump that leads to spurs and increased jitter. In this case, it may be possible to use a search having smaller incremental steps over a larger range of LUT values so as to avoid any sudden jumps.

(70) FIGS. **10A-10D** are diagrams illustrating timing and coding signals with respect to an interpolator (e.g., interpolator **80**, **100**, **120**) of a phase rotation controller (e.g., control systems **150**, **180**). FIG. **10A** represents the timing and coding signals associated with Mode 00; FIG. **10B** represents the timing and coding signals associated with Mode 01; FIG. **10C** represents the timing and coding signals associated with Mode 10; and FIG. **10D** represents the timing and coding signals associated with Mode 11.

(71) In Mode 00 (no interpolation), the CLK IN and CLK OUT signals are the same and are not modified. Also, the CODE IN and CODE OUT signals are the same. In Mode 01 (CLK×2), the CLK IN is multiplied by 2 to arrive at the CLK OUT rate. Also, as is shown in FIG. **10B**, the CODE OUT signal includes twice as much granularity. In this respect, the CLK OUT includes interpolation (averaging) between the values (e.g., the average of values **2024** and **2040** in the CODE IN provides a value of 2032 in the intermediate clock signal on the CODE OUT). Similarly, Mode 10 (CLK×4) includes a CLK IN that is multiplied by 4 to arrive at the CLK OUT rate and the CODE OUT includes four times the granularity. In Mode 11 (CLK×8 at half the clock rate), the CLK OUT is equal to the CLK IN times 4, plus every other code in the CODE OUT is skipped to provide eight times the granularity.

(72) These simulation results show the phase error for a rotated output of the phase rotator at an offset of 96 parts per million (ppm) (e.g., used to calculate jitter) with all four interpolator modes exercised. The LUT is already populated and greatly reduces jitter from the phase rotator from 100-130 fs. The active interpolators of Modes 01, 10, and 11 (e.g., ×2, ×4, ×8) significantly improve the phase for higher offset values. This allows the performance at high offsets to be similar to that of lower offset values.

(73) Also, FIGS. **10A-10D** show interpolator improvements. Automatic or semi-automatic phase selection may include using a phase detector to determine relative phase between interpolation clock and strobe. Variable interpolation clock divider and strobe clock divider can be used to match different modes. Alternatively, the control systems (e.g., control systems **150**, **180**) can use different averaging blocks to create $3\times$ or $5\times$ interpolation in some cases. In addition, other interpolator improvement may include the ability to sample on the rising and falling edges to further increase rates by twofold (e.g., in Mode 11).

(74) Simulation results for phase rotation may include an extracted model of an entire clock generation core and current DACs (with an EM model for inductors). Schematic logic for phase rotator controllers may include long transient simulation with ramped input code to create different PPM offset. The phase rotator may have a clock of 250 MHz, rather than 125 MHz (e.g., sampling frequency of 640 samples per picosecond (ps)) or 104 MHz (e.g., sampling frequency of 768 samples per ps) clock used in some phase rotators. In some cases, a 24 ppm run may be conducted without LUT calibration for measuring jitter. The detected phase errors can be used to populate the LUT. Then, 12 ppm, 24 ppm, 48 ppm, 72 ppm, and 96 ppm offsets can be run. Then, the interpolations modes can be run.

(75) FIGS. **11A-11J** are graphs showing phase noise simulation results using various interpolation modes. FIGS. **12A-12N** are graphs showing phase error simulation results using various interpolation modes. FIG. **13** is a graph **210** showing phase error with respect to frequency offset using various interpolation modes. The graph **210** may represent transient extracted simulations of various digital core processors. It may be noted that the systems and methods of the present disclosure may be applicable to conventional phase rotator designs, but can also be applied to other (new) phase rotators.

(76) FIG. **14** is a table **220** showing jitter results using various interpolation modes. It may be noted that the present embodiments provide significant improvement over conventional system (no interpolation), as seen for $\times 2$, $\times 4$, and $\times 8$ modes. This may be applicable to ppm jitter offsets greater than 24, which may cause minimal additional jitter, even up to 96 ppm. Due to extraction asymmetry, the simulations shown in the table **220** for no interpolation and $\times 2$ interpolation may possibly be optimistic. Therefore, improvement using the $\times 4$ and $\times 8$ modes may provide greater results.

(77) FIGS. **15A-15C** are screen shots showing an example of results of a test offset process for improving Look-Up Table (LUT) operating code. FIG. **15A** shows a plot of trial LUTs with different offsets from LUT locations 64 to 192. FIG. **15B** shows a plot of a magnified portion of the previous plot of FIG. **15A**. The magnified portion shows triangular trial offsets more clearly. Also, FIG. **15C** shows a plot of jitter vs trial offsets and illustrates jitter gradually approaching a minimum (e.g., about 1.9) near an “ideal” offset value.

(78) Also, FIG. **15A-15C** show a demonstration of the trial offsets for the LUT, whereby a series of trial LUT candidates can be evaluated. Each LUT candidate include a different offset value at location 128, ranging from -20 to $+20$. Continuity is retained by using a piecewise linear offset, starting from location 64 to location 192, shown in FIGS. **15A** and **15B** as LUT values vs LUT locations for seven different values of the trial LUT. Each of the trial LUTs is evaluated by writing it into the LUT and evaluating the phase rotator output jitter. FIG. **15C** shows the results in this regard, which includes the integrated jitter vs the peak offset value. In this case, the 0 value gave the best value and should therefore be used in the LUT. However, if a different value gives a lower jitter (or the lowest jitter of the group of values), then this value can be used instead by replacing the value location with the new value. Under normal circumstances, the full range of jitter vs offset does not necessarily need to be evaluated. The smaller numbers near 0 may be tested and the larger values can be tested only if the smaller ones showed improvement.

(79) According to a first technique or algorithm, a test control device may be configured to implement a search-like gradient descent (e.g., used to optimize neural network weights, among

other applications) using the integrated jitter as a “cost function.” At a given location, the test control device may be configured to find a gradient. That is, a derivative of a small change in the LUT with respect to the cost function may be calculated.

(80) This first technique can be done empirically using small changes to the LUT (e.g., by applying a small triangular offset (see FIG. 15B) at a given location) and seeing the effect on the jitter. If the jitter decreases, then this indicates the likelihood that the gradient descends in that direction. In this case, the technique may include continuing to make changes in that direction until the jitter no longer improves. After a number of iterations, the technique may include keeping only changes to the LUT that improve the jitter. This technique can be performed throughout the entire LUT (e.g., all data locations in the LUT). In some embodiments, it may be beneficial to leave one point untouched as a reference point. Therefore, this technique can start with offsets over a large portion and then gradually reduce the length of the test offset.

(81) FIGS. 16A and 16B are screen shots showing graphs of jitter responses to LUT value adjustments by utilizing another linearization optimization technique. In FIGS. 16A and 16B, an example test is shown where the results were obtained by an iteration method on a digital core processor under current development. FIG. 16A shows the measured jitter with small adjustments made to the LUT values at different values. The adjustments are piecewise linear triangular function 64 steps long, with a peak ranging from -2 to +2 in steps of 1 (i.e., -2, -1, 0, +1, and +2) and are added to the LUT, starting at locations 0, 32, 64, . . . , 960. At each different location, the five different offset values are individually tested and the best value is used before testing the next location. FIG. 16A shows the jitter progressively improving with each iteration. FIG. 16B shows the LUT offset values (i.e., the difference from a straight line from 0 to 1023) at the end of the calibration round. Before the run, each of the offset values may start at zero (0).

(82) This second technique for initial calibration may include many advantages. However, in some case, an issue with the second technique is that it may take a long time to reach the optimal state since only small steps are taken. However, this issue can be resolved by using a modified technique. The modified second technique may include a “genetic” algorithm to test many trial offsets simultaneously. The current LUT may be tested against many trial “strains,” which may include random offsets (e.g., “mutations”) of different strengths and sizes, and then the jitter for each strain can be tested. The strain with the best jitter value can be selected. Alternatively, multiple strains with the best jitter values can be taken and averaged. If the average LUT value is better than the base value against which the technique is being tested, it is kept and used as a new base value. Otherwise, the old base value is kept and continued to be used. In this case, further iterations can be performed done. In some embodiment, each iteration may be configured such that the strength of the mutations can be gradually diminished as the performance improves, until further improvements are no longer seen. Thus, the modified second technique has been observed as having a faster initial convergence than the first technique. Nevertheless, the first technique may be better suited for fine tuning of the LUT and can also be used more effectively in a background calibration situation.

(83) FIGS. 17A-17C are graphs showing results of the modified second technique for testing LUT values using iterative mutations. This technique may be based on “genetic” algorithm training and can create several test LUTs with random or pseudo random “mutations” (i.e., deviations from the current LUT values). In this example, a test can be conducted to measure jitter for each iteration. The test may include choosing the best X number of test strains and taking the average of them. Then this average can be kept if it is better than the current LUT. Otherwise, the mutations are rejected. The modified second technique may include continuing to iterate (e.g., by gradually reducing the strength and size of the mutations) until the LUT converges to optimal values. The initial convergence from a blind state may be performed faster than the first technique since the first technique tests small portions. However, the second technique may be unable to provide significant refinement as well as the first technique but may be better for initial calibration in a lab

setup. However, if JCL is not available, one or more of the techniques may not be viable for background calibration.

(84) Therefore, according to various embodiments of the present disclosure, a circuit (e.g., a phase rotation control system) may comprise a single Phase-Locked Loop (PLL) circuit having a main path and a return path forming a feedback loop. The circuit may also include one or more phase rotators connected to an output of the single PLL circuit outside the feedback loop. One or more adaptable Look-Up Tables (LUTs) may be populated with operating code to be provided to the one or more phase rotators for defining operating characteristics of the one or more phase rotators. The circuit may further include a control loop configured to receive phase response characteristics from the one or more phase rotators, the control loop further configured to modify the operating code of the one or more adaptable LUTs based on the phase response characteristics to reduce non-linearities of the one or more phase rotators.

(85) According to additional embodiments, the circuit may further be defined whereby the one or more phase rotators may include a first phase rotator associated with a transmitter component and a second phase rotator associated with a receiver component. The transmitter component and receiver component may be configured to share the single PLL circuit. The circuit may further include a Clock and Data Recovery (CDR) circuit configured to receive output signals from the receiver component and provide input signals to one of the one or more adaptable LUTs and to the control loop.

(86) Regarding this circuit, the one or more phase rotators may be configured for continuous operation, whereby the control loop may be configured to iteratively modify the operating code of the one or more adaptable LUTs based on changeable phase response characteristics of the one or more phase rotators to allow the control loop to improve linearization performance of the one or more phase rotators. The control loop may be configured to compensate for the changeable phase response characteristics caused by errors due to temperature changes, voltage shifts, and aging effects.

(87) Also, the circuit may comprise one or more linear ramps configured to shift the output frequency of the one or more phase rotators. The control loop may be configured to modify the operating code of the one or more adaptable LUTs to improve the linearization of the one or more linear ramps. For example, the one or more adaptable LUTs may be configured to correct phase errors in the one or more phase rotators. The control loop may include an Integrated Digital-to-Analog Converter (IDAC) coding component configured for background calibration of the one or more adaptable LUTs. The IDAC coding component may be configured to receive interpolation information from an interpolator, whereby the interpolator may include a clock configured to control an update rate at which the IDAC coding component modifies the operating code of the one or more adaptable LUTs. The clock may operate faster than a digital core rate associated with the one or more adaptable LUTs. Also, the IDAC coding component may be configured to interpolate intermediate code between the operating code associated with the digital core rate.

(88) According to some embodiments, the circuit may further comprise one or more phase rotator controllers configured to receive the operating code from the one or more adaptable LUTs and apply the operating code to the one or more phase rotators. The circuit may also include one or more frequency dividers each connected to an output of the one or more phase rotators.

Furthermore, the circuit may include a spectrum analyzer configured to measure the phase response characteristics from the one or more phase rotators and forward the phase response characteristics to the control loop. The control loop may be further configured to provide an incremental step to an accumulator associated with a digital core connected to the one or more phase rotator controllers. The spectrum analyzer may be configured to perform a trial offset process, whereby the trial offset process may include applying different sets of test operating code to the one or more adaptable LUTs, monitoring non-linearities of the one or more phase rotators to determine a set of test operating code having the best results, and replacing the operating code with the set of test

operating having the best results.

(89) Therefore, the systems and methods of the present disclosure may include various points of novelty with respect to conventional systems. For example, one aspect is that the present disclosure is configured use of a clock up-sampling circuit for phase rotator code interpolation to improve update rate for linearity improvement under continuous phase ramping, which is not available in conventional systems. Also, the present circuits may take advantage of slower rate non-linearity correction through the use of a LUT in order to minimize delay to improve the bandwidth. Variable code rate selection is also available with respect to the systems of the present disclosure to control the up-sampling rate and to handle different digital core rates. The embodiments described herein demonstrate the use of iterative adaptation (e.g., similar to that used in machine learning) to improve phase rotator linearization performance. Thus, the present embodiments are capable of application to background calibration, which appears to be absent from conventional systems, to calibrate out long term and gradual effects that cannot be predetermined.

(90) It will be appreciated that some embodiments described herein may include or utilize one or more generic or specialized processors (“one or more processors”) such as microprocessors; Central Processing Units (CPUs); Digital Signal Processors (DSPs); customized processors such as Network Processors (NPs) or Network Processing Units (NPUs), Graphics Processing Units (GPUs), or the like; Field-Programmable Gate Arrays (FPGAs); and the like along with unique stored program instructions (including both software and firmware) for control thereof to implement, in conjunction with certain non-processor circuits, some, most, or all of the functions of the methods and/or systems described herein. Alternatively, some or all functions may be implemented by a state machine that has no stored program instructions, or in one or more Application-Specific Integrated Circuits (ASICs), in which each function or some combinations of certain of the functions are implemented as custom logic or circuitry. Of course, a combination of the aforementioned approaches may be used. For some of the embodiments described herein, a corresponding device in hardware and optionally with software, firmware, and a combination thereof can be referred to as “circuitry configured to,” “logic configured to,” etc. perform a set of operations, steps, methods, processes, algorithms, functions, techniques, etc. on digital and/or analog signals as described herein for the various embodiments.

(91) Moreover, some embodiments may include a non-transitory computer-readable medium having instructions stored thereon for programming a computer, server, appliance, device, one or more processors, circuit, etc. to perform functions as described and claimed herein. Examples of such non-transitory computer-readable medium include, but are not limited to, a hard disk, an optical storage device, a magnetic storage device, a Read-Only Memory (ROM), a Programmable ROM (PROM), an Erasable PROM (EPROM), an Electrically EPROM (EEPROM), Flash memory, and the like. When stored in the non-transitory computer-readable medium, software can include instructions executable by one or more processors (e.g., any type of programmable circuitry or logic) that, in response to such execution, cause the one or more processors to perform a set of operations, steps, methods, processes, algorithms, functions, techniques, etc. as described herein for the various embodiments.

(92) Although the present disclosure has been illustrated and described herein with reference to preferred embodiments and specific examples thereof, it will be readily apparent to those of ordinary skill in the art that other embodiments and examples may perform similar functions and/or achieve like results. All such equivalent embodiments and examples are within the spirit and scope of the present disclosure, are contemplated thereby, and are intended to be covered by the following claims. Moreover, it is noted that the various elements, operations, steps, methods, processes, algorithms, functions, techniques, etc. described herein can be used in any and all combinations with each other.

Claims

1. A transceiver comprising: a first transmit (Tx) component configured to connect to a second receive (Rx) component in a second transceiver; a first Rx component configured to connect to a second Tx component in the second transceiver; a single Phase-Locked Loop (PLL) circuit connected to both the first Tx component and the first Rx component; and a control circuit configured to continuously calibrate a first Look-Up Table (LUT) configured to feed operating codes to a first phase rotator connected to an output of the single PLL circuit and to one of the first Tx component and the first Rx component.
2. The transceiver of claim 1, wherein the control circuit is further configured to continuously calibrate a second LUT configured to feed operating codes to a second phase rotator connected to an output of a single PLL circuit in the second transceiver.
3. The transceiver of claim 1, wherein the control circuit is further configured to continuously calibrate a second LUT configured to feed operating codes to a second phase rotator connected to an output of the single PLL circuit and the other of the first Tx component and the first Rx component.
4. The transceiver of claim 1, further comprising a Clock and Data Recovery (CDR) circuit configured to estimate and monitor clock jitter associated with both the first Tx component and the first Rx component, wherein the control circuit is configured to utilize the estimated clock jitter to continuously calibrate the first LUT.
5. The transceiver of claim 3, wherein the first LUT is adjusted by incremental steps where the CDR is used to provide the estimated clock jitter after each incremental step and to determine a next incremental step.
6. The transceiver of claim 1, wherein the first LUT is continuously calibrated via incremental steps that are less than an overall range, such that any wrong incremental step has small impact.
7. The transceiver of claim 5, wherein the incremental steps are on an order of a few femtoseconds.
8. The transceiver of claim 1, wherein the first LUT is continuously calibrated via a gradient descent-like search.
9. The transceiver of claim 1, wherein the first LUT is continuously calibrated via a genetic algorithm that tests multiple values in the first LUT simultaneously.
10. The transceiver of claim 1, wherein the first LUT is continuously calibrated while the single PLL circuit is in operation.
11. The transceiver of claim 1, wherein the first LUT is continuously calibrated thereby compensating any of temperature shifts, voltage shifts, and aging effects.
12. A method comprising steps of: in a transceiver comprising a first transmit (Tx) component configured to connect to a second receive (Rx) component in a second transceiver, a first Rx component configured to connect to a second Tx component in the second transceiver, and a single Phase-Locked Loop (PLL) circuit connected to both the first Tx component and the first Rx component, continuously calibrating a first Look-Up Table (LUT) configured to feed operating codes to a first phase rotator connected to an output of the single PLL circuit and to one of the first Tx component and the first Rx component.
13. The method of claim 11, wherein the steps further include continuously calibrating a second LUT configured to feed operating codes to a second phase rotator connected to an output of a single PLL circuit in the second transceiver.
14. The method of claim 11, wherein the steps further include continuously calibrating a second LUT configured to feed operating codes to a second phase rotator connected to an output of the single PLL circuit and the other of the first Tx component and the first Rx component.
15. The method of claim 11, wherein the steps further include monitoring and estimating clock jitter associated with both the first Tx component and the first Rx component with a Clock and

Data Recovery (CDR), wherein the estimated clock jitter is utilized to continuously calibrate the first LUT.

16. The method of claim 13, wherein the first LUT is adjusted by incremental steps where the CDR is used to provide the estimated clock jitter after each incremental step and to determine a next incremental step.

17. The method of claim 11, wherein the first LUT is continuously calibrated via incremental steps that are less than an overall range, such that any wrong incremental step has small impact.

18. The method of claim 15, wherein the incremental steps are on an order of a few femtoseconds.

19. The method of claim 11, wherein the continuously calibrating is via a gradient descent-like search.

20. The method of claim 11, wherein the continuously calibrating is via a genetic algorithm that tests multiple values in the first LUT simultaneously.
