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Inventor(s)

TAKAHASHI; Motoki

### CONTROL APPARATUS FOR VEHICLE

#### Abstract

A control apparatus including a processor configured to control a drive power of a towed vehicle which has a drive power source which is towed through a coupler by a towing vehicle. When the towing vehicle is running while towing the towed vehicle, the processor is configured to limit the drive power of the towed vehicle such that the towed vehicle does not push the towing vehicle through the coupler. Preferably, the processor is configured to calculate, based on a drive power of the towing vehicle, an upper limit value of an allowable range of the drive power of the towed vehicle in which the towed vehicle does not push the towing vehicle, and to limit the drive power of the towed vehicle by the upper limit value.

**Inventors:** TAKAHASHI; Motoki (Susono-shi, JP)

**Applicant:** TOYOTA JIDOSHA KABUSHIKI KAISHA (Toyota-shi, JP)

**Family ID:** 1000008495676

**Assignee:** TOYOTA JIDOSHA KABUSHIKI KAISHA (Toyota-shi, JP)

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## Background/Summary

[0001] This application claims priority from Japanese Patent Application No. 2024-024104 filed on Feb. 20, 2024, the disclosure of which is herein incorporated by reference in its entirety.

### FIELD OF THE INVENTION

[0002] The present invention relates to a control apparatus for controlling a drive power of a towed vehicle.

### BACKGROUND OF THE INVENTION

[0003] There is well known a control apparatus that includes a drive control portion that controls a drive power of a towed vehicle which is towed by a towing vehicle through a coupler and which has a drive power source. For example, a control apparatus for an articulated vehicle described in Patent Document 1 is such a control apparatus. Patent Document 1 discloses a towing vehicle equipped with a first motor that can be driven by a first battery, and a towed vehicle equipped with a second motor that can be driven by a second battery.

### PRIOR ART DOCUMENT

Patent Document

[0004] [Patent Document 1] [0005] Japanese Patent Application Laid-Open No. 2013-184584

### SUMMARY OF THE INVENTION

[0006] A responsiveness of the drive power of the vehicle varies depending on the type or combination of the drive power sources, and varies among engine and electric vehicles. On the other hand, where the towed vehicle as well as the towing vehicle is adapted to generate the drive power, it is possible to increase an acceleration performance in a towing running state in which the towing vehicle runs the towed vehicle. However, if the responsiveness of the drive power varies among vehicles, a situation may occur in which the drive power of the towed vehicle is larger than necessary. Under such a situation, there is a concern that behavior of the towing vehicle may be disturbed or a driver of the towing vehicle may feel discomfort. If the drive power of the towed vehicle is greatly reduced, the above-described situation is unlikely to occur, but benefit of increasing the acceleration performance is unlikely to be obtained.

[0007] The present invention has been made in view of the above circumstances, and an object of the present invention is to provide a control apparatus capable of stabilizing behavior of a towing vehicle while enjoying an increase in acceleration performance by a drive power of a towed vehicle.

[0008] The present invention provides a control apparatus comprising a processor configured to control a drive power of a towed vehicle which has a drive power source which is towed through a coupler by a towing vehicle. When the towing vehicle is running while towing the towed vehicle, the processor is configured to limit the drive power of the towed vehicle such that the towed vehicle does not push the towing vehicle through the coupler.

[0009] In the control apparatus according to the present invention, when the towing vehicle is in the towing running state in which the towing vehicle is running while towing the towed vehicle, the drive power of the towed vehicle is limited such that the towed vehicle having the drive power source does not push the towing vehicle through the coupler. Thus, the towed vehicle generates the drive power, and thus, drive assistance in the towing running state can be performed. For example, improvement of acceleration performance and hill climbing performance, enlargement of towing capacity, extension of cruising distance and the like can be expected. Further, response of the drive power of the towed vehicle is controlled, and thus the towed vehicle is prevented or suppressed from pushing the towing vehicle. Therefore, it is possible to stabilize behavior of the towing

vehicle while enjoying the improvement of the acceleration performance by the drive power of the towed vehicle.

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## Description

### BRIEF DESCRIPTION OF THE DRAWINGS

[0010] FIG. 1 is a view showing a schematic configuration of a articulated vehicle to which the present invention is applied, and is a view showing control functions and main parts of a control system for various controls in the articulated vehicle.

[0011] FIGS. 2A and 2B are views showing an example of a towing running state in which a towing vehicle runs while towing a trailer as a towed vehicle.

[0012] FIG. 3 is a flowchart for explaining a main part of a control operation of a vehicle control apparatus, and is a flowchart for explaining a control operation for stabilizing behavior of the towing vehicle while enjoying an increase in acceleration performance by a drive power of the trailer.

[0013] FIG. 4 is a view showing an example of a time chart in a case where the control operation shown in the flowchart of FIG. 3 is executed.

[0014] FIG. 5 is a flowchart for explaining a main part of a control operation of the vehicle control apparatus, and is a flowchart for explaining a control operation for stabilizing behavior of the towing vehicle while enjoying an increase in acceleration performance by the drive power of the trailer, and is an embodiment different from FIG. 3.

[0015] FIG. 6 is a flowchart for explaining a main portion of a control operation of an electronic control device of the trailer, which is a flowchart for explaining a control operation for stabilizing behavior of the towing vehicle while enjoying an increase in acceleration performance by the drive power of the trailer, and is an embodiment different from FIGS. 3 and 5.

### DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

[0016] Hereinafter, embodiments of the present invention will be described in detail with reference to the drawings.

#### First Embodiment

[0017] FIG. 1 is a view showing a schematic configuration of a articulated vehicle to which the present invention is applied, and is a view showing control functions and main parts of a control system for various controls in the articulated vehicle 10. In FIG. 1, the articulated vehicle 10 is a combination of a towing vehicle 20 and a trailer 60.

[0018] The towing vehicle 20 is, for example, a known automobile, and includes an engine 22, a transmission 24, a differential gear device 26, a drive shaft 28 and drive wheels 30. The engine 22 functions as a drive power source of the towing vehicle 20. An engine torque  $T_e$ , which is a torque of the engine 22, is controlled by an electronic control device 50. In the towing vehicle 20, a power of the engine 22 is transmitted to the drive wheels 30 sequentially via the transmission 24, the differential gear device 26, the pair of drive shafts 28 and the like.

[0019] The trailer 60 is a towed vehicle towed by the towing vehicle 20. The trailer 60 includes an electric motor 62, a differential gear device 64, a drive shaft 66 and drive wheels 68. The electric motor 62 functions as a drive power source of the trailer 60. The electric motor 62 is controlled by an electronic control device 80, to generate an electric motor torque  $T_m$ . In the trailer 60, a power of the electric motor 62 is transmitted to the drive wheels 68 sequentially via the differential gear device 64, the pair of drive shafts 66 and the like. A regenerative torque, which is a negative torque of the electric motor torque  $T_m$ , may be transmitted to the drive wheels 68 as a braking torque.

[0020] FIGS. 2A and 2B are views showing an example of a towing running state of the articulated vehicle 10 in which the towing vehicle 20 is running while towing the trailer 60. FIG. 2A is a side view as viewed from a left side of the articulated vehicle 10. FIG. 2B is a plan view as viewed from

an upper side of articulated vehicle **10**. In FIGS. 2A and 2B, the trailer **60** is towed by the towing vehicle **20** through a coupler **90**. The coupler **90** includes, for example, a trailer hitch member **92** and a towing-vehicle hitch member **94**. The trailer hitch member **92** is attached to a front end portion of the trailer **60**. The towing-vehicle hitch member **94** is attached to a rear end portion of the towing vehicle **20**. The trailer hitch member **92** and the towing-vehicle hitch member **94** are connected through a coupling portion **96**. The coupling portion **96** is a coupling portion of the trailer **60** coupled to the towing vehicle **20**, and is a distal end portion of the trailer hitch member **92** on a side of the towing vehicle **20**. The coupling portion **96** corresponds to a coupling portion between the towing vehicle **20** and the trailer **60**. The trailer **60** is towed by the towing vehicle **20** such that the coupler **90** prevents the towing vehicle **20** and the trailer **60** from approaching and separating from each other by the coupling portion **96** being coupled to the towing-vehicle hitch member **94**.

[0021] Referring back to FIG. 1, the towing vehicle **20** further includes the electronic control device **50** as a controller related to controls of the engine **22** and the like. The electronic control device **50** includes a so-called microcomputer or processor including, for example, a CPU, a RAM, a ROM and an input/output interface. The CPU performs various controls of the towing vehicle **20** by performing signal processing according to a program stored in the ROM in advance while using a temporary storage function of the RAM, for example.

[0022] Various signals and the like based on values detected by various sensors and the like provided in the towing vehicle **20** are supplied to the electronic control device **50**. The various sensors and the like provided in the towing vehicle **20** are, for example, an engine speed sensor **32**, a vehicle running-speed sensor **34**, an accelerator opening sensor **36**, a throttle-valve opening sensor **38**, a steering sensor **40** and the like. The various signals include, for example, an engine rotational speed  $N_e$ , a vehicle running speed  $V_v$ , an accelerator opening degree  $\theta_{acc}$ , a throttle-valve opening degree  $\theta_{th}$ , a steering angle  $\theta_{sw}$  and a steering direction  $D_{sw}$ . The engine rotational speed  $N_e$  is a rotational speed of the engine **22**. The vehicle running speed  $V_v$  is a running speed of the towing vehicle **20**. The accelerator opening degree  $\theta_{acc}$  is a signal corresponding to an acceleration request amount indicating a magnitude of an acceleration operation made by a driver of the towing vehicle **20**, and is an accelerator operation amount by the driver. The throttle-valve opening degree  $\theta_{th}$  is the opening degree of the electronic throttle valve. The steering angle  $\theta_{sw}$  is a steering angle of a steering wheel of the towing vehicle **20**. The steering direction  $D_{sw}$  is a steering direction of the steering wheel.

[0023] Various command signals and the like are outputted from the electronic control device **50** to various devices and the like provided in the towing vehicle **20**. The various devices provided in the towing vehicle **20** include the engine **22**, for example. The various command signals include an engine control command signal  $S_e$  for controlling the engine **22**, for example.

[0024] The trailer **60** further includes the electronic control device **80** as a controller related to control of the electric motor **62** and the like. The electronic control device **80** includes a so-called microcomputer or processor including, for example, a CPU, a RAM, a ROM and an input/output interface. The CPU executes various controls of the trailer **60** by performing signal processing in accordance with a program stored in the ROM in advance while using a temporary storage function of the RAM, for example.

[0025] Various signals and the like based on values detected by various sensors and the like provided in the trailer **60** are supplied to the electronic control device **80**. The various sensors and the like provided in the trailer **60** are, for example, an electric-motor speed sensor **70**, a vehicle running-speed sensor **72**, a load sensor **74** and the like. The load sensor **74** is a sensor provided in the coupler **90**, particularly, in the coupling portion **96** (see FIGS. 2A and 2B), and is, for example, a strain gauge. The various signals include an electric-motor rotational speed  $N_m$ , a trailer running speed  $V_t$  and a hitch load  $F_x$ . The electric-motor rotational speed  $N_m$  is a rotational speed of the electric motor **62**. The trailer running speed  $V_t$  is a running speed of the trailer **60**. The hitch load

$F_x$  is a load applied to the coupler **90**, particularly, to the coupling portion **96**, and corresponds to a difference between a vehicle drive power  $F_v$  and a trailer drive power  $F_t$  in consideration of, for example, the steering angle  $\theta_{sw}$ , a weight of the towing vehicle **20**, a weight of the trailer **60** and the like (see FIGS. 2A and 2B). The vehicle drive power  $F_v$  is a drive power of the towing vehicle **20**. The trailer drive power  $F_t$  is a drive power of the trailer **60**. The hitch load  $F_x$  corresponds to a magnitude obtained by subtracting the vehicle drive power  $F_v$  from the trailer drive power  $F_t$ . When the hitch load  $F_x$  is a positive value ( $F_x > 0$ ), a direction of the hitch load  $F_x$  is a direction in which the trailer **60** pushes the towing vehicle **20**. When the hitch load  $F_x$  is a negative value ( $F_x < 0$ ), the trailer **60** does not push the towing vehicle **20**, that is, the towing vehicle **20** pulls the trailer **60**.

[0026] Various command signals and the like are outputted from the electronic control device **80** to various devices and the like provided in the trailer **60**. The various devices provided in the trailer **60** include the electric motor **62**, for example. The various command signals include a motor control command signal  $S_m$  for controlling the electric motor **62**, for example.

[0027] The electronic control device **50** and the electronic control device **80** are connected to each other in a wired or wireless manner so as to be able to communicate with each other. The electronic control device **50** and the electronic control device **80** cooperate with each other to constitute a vehicle control apparatus **100** that performs a drive control, for example.

[0028] The electronic control device **50** includes an engine control portion **52** that controls the engine **22** in order to realize various controls in the towing vehicle **20**. The engine control portion **52** calculates a requested vehicle drive amount  $Q_{vdem}$ , which is a requested drive amount for the towing vehicles **20**, by applying the accelerator operation amount  $\theta_{acc}$  and the vehicle running speed  $V_v$  to a requested vehicle drive amount map  $MAP_v$ , for example. The requested vehicle drive amount map  $MAP_v$  is a relationship for obtaining the requested vehicle drive amount  $Q_{vdem}$ , which is obtained and stored in advance, for example, experimentally or by design, that is, which is determined in advance. The requested vehicle drive amount  $Q_{vdem}$  is, for example, the vehicle drive power  $F_v$  requested for the towing vehicle **20**, that is, a requested vehicle drive power  $F_{vdem}$  in the drive wheels **30**. The engine control portion **52** calculates a requested engine torque  $T_{edem}$  that is a requested value of the engine torque  $T_e$  for realizing the requested vehicle drive amount  $Q_{vdem}$ , in consideration of, for example, a transmission loss, an auxiliary load, a gear ratio of the transmission **24** and the like. The engine control portion **52** outputs an engine control command signal  $S_e$  for controlling the engine **22** so as to obtain the requested engine torque  $T_{edem}$ .

[0029] The electronic control device **80** includes an electric-motor control portion **82** that controls the electric motor **62** in order to realize various controls in the trailer **60**. The electric-motor control portion **82** calculates a trailer drive request amount  $Q_{tdem}$ , which is a drive request amount for the trailer **60**, by applying the accelerator opening degree  $\theta_{acc}$  and the trailer running speed  $V_t$  to a requested trailer drive amount map  $MAP_t$ , for example. The requested trailer drive amount map  $MAP_t$  is a relationship for obtaining a predetermined trailer drive request amount  $Q_{tdem}$ , for example. The trailer drive request amount  $Q_{tdem}$  is, for example, a trailer drive power  $F_t$  requested for the trailer **60**, that is, a requested trailer drive power  $F_{tdem}$  in the drive wheel **68**. The motor control portion **82** calculates a requested motor torque  $T_{mdem}$ , which is a requested value of the motor torque  $T_m$  for realizing the trailer drive request amount  $Q_{tdem}$ , in consideration of, for example, a transmission loss. The electric-motor control portion **82** outputs an electric-motor control command signal  $S_m$  for controlling the electric motor **62** so as to obtain the requested motor torque  $T_{mdem}$ . In this way, the electric-motor control portion **82** functions as a drive control portion that controls the trailer drive power  $F_t$ .

[0030] By the way, in consideration of output characteristics of the engine **22** and the electric motor **62**, a responsiveness of the vehicle drive power  $F_v$  to the requested vehicle drive power  $F_{vdem}$  may be inferior to a responsiveness of the trailer drive power  $F_t$  to the requested trailer drive power  $F_{tdem}$ . Therefore, during acceleration such as when the accelerator is turned on or when the

accelerator is increased, the trailer drive power  $F_t$  temporarily becomes larger than the vehicle drive power  $F_v$ , and there is a possibility that the trailer **60** would push the towing vehicle **20** at one point from the connection portion **96** through the coupler **90**. In this case, there is a concern that behavior of the towing vehicle **20** could be disturbed. Unless otherwise specified, the vehicle drive power  $F_v$  is synonymous with an actual vehicle drive power  $F_{vr}$  which is an actual value of the vehicle drive power  $F_v$ , and the trailer drive power  $F_t$  is synonymous with an actual trailer drive power  $F_{tr}$  which is an actual value of the trailer drive power  $F_t$ .

[0031] Therefore, the electric-motor control portion **82** controls the response of the trailer drive power  $F_t$  in order to avoid the trailer **60** from pushing the towing vehicle **20** through the coupler **90**. For example, the electric-motor control portion **82** limits the trailer drive power  $F_t$  such that the trailer **60** does not push the towing vehicle through the coupler **90** when the towing vehicle **20** is in the towing running state in which the towing vehicle **20** is running while towing the trailer **60** through the coupler **90**.

[0032] FIG. **3** is a flowchart showing a main part of the control operation of the vehicle control apparatus **100**, and is a flowchart showing a control routine for stabilizing the behavior of the towing vehicle **20** while enjoying the improvement of the acceleration performance by the trailer drive power  $F_t$ . This control routine is repeatedly executed, for example.

[0033] In FIG. **3**, first, at step **S10a** corresponding to function of the electronic control device **50**, information such as the accelerator opening degree  $\theta_{acc}$ , the steering angle  $\theta_{sw}$  and the steering direction  $D_{sw}$  is obtained. Next, at step **S20a** corresponding to functions of the engine control portion **52** and the motor control portion **82**, the requested vehicle drive power  $F_{vdm}$  and the requested trailer drive power  $F_{tdm}$  are calculated. Next, at step **S30a** corresponding to functions of the engine control portion **52** and the motor control portion **82**, an estimated value of the vehicle drive power  $F_v$  and an estimated value of the trailer drive power  $F_t$  are calculated. For example, the estimated value of the vehicle drive power  $F_v$  is calculated by a predetermined approximate expression in which a response delay with respect to the requested vehicle drive power  $F_{vdm}$  is taken into consideration. Alternatively, the estimated value of the vehicle drive power  $F_v$  is calculated based on the actual engine torque  $T_e$ . In this instance, the steering angle  $\theta_{sw}$ , the steering direction  $D_{sw}$ , the braking power by wheel brakes and the like may be considered. Further, for example, the estimated value of the trailer drive power  $F_t$  is calculated by a predetermined approximate expression in which a response delay with respect to the requested trailer drive power  $F_{tdm}$  is taken into consideration. Alternatively, the estimated value of the trailer drive power  $F_t$  is calculated based on the actual electric motor torque  $T_m$ . Next, at step **S40a** corresponding to function of the motor control portion **82**, a trailer drive power limit  $F_{tlim}$ , which is an upper limit value of the trailer drive power  $F_t$  at which the trailer **60** does not push the towing vehicle **20** through the coupler **90**, is calculated based on the estimated value of the vehicle drive power  $F_v$ . For example, the trailer drive power limit  $F_{tlim}$ , which is an upper limit value of an allowable range of the trailer drive power  $F_t$  in which the hitch load  $F_x$  becomes a negative value in calculation, is calculated based on the estimated value of the trailer drive power  $F_v$ . Next, at step **S50a** corresponding to function of the motor control portion **82**, the requested trailer drive power  $F_{tdm}$  is limited or upper-guarded to the trailer drive power limit  $F_{tlim}$ . That is, when the requested trailer drive power  $F_{tdm}$  exceeds the trailer drive power limit  $F_{tlim}$ , the requested trailer drive power  $F_{tdm}$  is set to the trailer drive power limit  $F_{tlim}$ . Next, at step **S60a** corresponding to function of the electric-motor control portion **82**, the electric motor **62** is controlled using the requested trailer drive power  $F_{tdm}$  whose upper limit is guarded by the trailer drive power limit  $F_{tlim}$ , and the trailer **60** is driven. That is, the requested trailer drive power  $F_{tdm}$ , whose upper limit is guarded by the trailer drive power limit  $F_{tlim}$ , is reflected in the trailer drive power  $F_t$ .

[0034] In this way, the electric-motor control portion **82** calculates the trailer drive power limit  $F_{tlim}$ , which is the upper limit of the allowable range of the trailer drive power  $F_t$  in which the trailer **60** does not push the towing vehicle **20**, based on the vehicle drive power  $F_v$ , and then limits

the trailer drive power  $F_t$  by the trailer drive power limit  $F_{tlim}$ . The trailer drive power limit  $F_{tlim}$  is the upper limit of the allowable range of the trailer drive power  $F_t$  in which the hitch load  $F_x$  is less than a load value by which the towing vehicle **20** is pushed by the trailer **60**, namely, in which the hitch load  $F_x$  does not act in a direction by which the towing vehicle **20** is pushed by the trailer **60**. That is, the trailer drive power limit  $F_{tlim}$  is determined such that the trailer **60** does not push the towing vehicle **20**.

[0035] FIG. **4** is a view showing an example of a time chart in a case where the control routine shown in the flowchart of FIG. **3** is executed. FIG. **4** shows an example of the case of starting or accelerating. In FIG. **4**, a time point  $t_1$  indicates a time point at which the accelerator is turned on or a time point at which the accelerator is operated to increase the acceleration. In a comparative example indicated by a broken line, the trailer drive power  $F_t$  is generated with better responsiveness than the vehicle drive power  $F_v$ . In such a situation, the trailer **60** pushes the towing vehicle **20**. In contrast, in the present embodiment indicated by two dot chain line, the trailer drive power  $F_t$  is limited by the trailer drive power limit  $F_{tlim}$ , and thus a situation in which the trailer **60** pushes the towing vehicle **20** is avoided or suppressed.

[0036] As described above, according to the present embodiment, the trailer **60** includes the electric motor **62** as the drive power source. Accordingly, the trailer **60** generates the trailer drive power  $F_t$ , and thus, drive assistance can be performed in the towing running state in which the towing vehicle **20** is running while towing the trailer **60**, and for example, improvement of acceleration performance or hill climbing performance, increase of towing capacity and extension of running distance can be expected. In addition, when the towing vehicle **20** is in the towing running state, the trailer drive power  $F_t$  is limited such that the trailer **60** does not push the towing vehicle through the coupler **90**. Accordingly, the response of the trailer drive power  $F_t$  is controlled, and thus the trailer **60** is prevented or suppressed from pushing the towing vehicle **20**. Therefore, it is possible to stabilize the behavior of the towing vehicle **20** while enjoying the improvement of the acceleration performance by the trailer drive power  $F_t$ .

[0037] Further, according to the present embodiment, the trailer drive power limit  $F_{tlim}$  is calculated based on the vehicle drive power  $F_v$ , and the trailer drive power  $F_t$  is limited by the trailer drive power limit  $F_{tlim}$ . The trailer drive power limit  $F_{tlim}$  is the upper limit of the allowable range of the trailer drive power  $F_t$  in which the hitch load  $F_x$  is less than a load value by which the towing vehicle **20** is pushed by the towed vehicle **60**, namely, in which the hitch load  $F_x$  does not act in a direction by which the towing vehicle **20** is pushed by the trailer **60**. Thus, the trailer drive power  $F_t$  is appropriately limited such that the trailer **60** does not push the towing vehicle **20** in the towing running state.

[0038] Next, other embodiments of the present invention will be described. In the following description, the same reference numerals are given to the same parts as those in the first embodiment, and the description thereof will be omitted.

## Second Embodiment

[0039] In the first embodiment, the trailer drive power  $F_t$  is limited by calculating the trailer drive power limit  $F_{tlim}$ . In this embodiment, the trailer drive power  $F_t$  is limited by the direction of the hitch load  $F_x$ .

[0040] FIG. **5** is a flowchart showing a main part of the control operation of the vehicle control device **100**, and is a flowchart showing a control routine for stabilizing the behavior of the towing vehicle **20** while enjoying the improvement of the acceleration performance by the trailer drive power  $F_t$ , and is repeatedly executed, for example. The flow chart of FIG. **5** shows the control routine, which is executed in this second embodiment and which is different from the control routine shown in the flowchart of FIG. **3**.

[0041] In FIG. **5**, steps **S10b**, **S20b** and **S30b** are the same as steps **S10a**, **S20a** and **S30a** in FIG. **3**, and therefore, the description thereof is omitted. Step **S30b** is followed by step **S40b** corresponding to function of the electric-motor control portion **82**, which is implemented to calculate the hitch

load  $F_x$  by using the steering angle  $\theta_{sw}$ , the steering direction  $D_{sw}$ , the estimated value of the vehicle drive power  $F_v$ , the estimated value of the trailer drive power  $F_t$  and the like, and to obtain the direction of the hitch load  $F_x$ . Then, it is determined whether or not the direction of the hitch load  $F_x$  corresponds to a direction in which the trailer **60** pushes the towing vehicle **20**. At this step **S40b**, a detection signal of the load sensor **74** indicative of the hitch load  $F_x$  may be used. When an affirmative determination is made at this step **S40b**, the requested trailer drive power  $F_{tdem}$  is subtracted or reduced at **S50b** corresponding to function of the electric-motor control portion **82**. For example, the requested trailer drive power  $F_{tdem}$  is reduced in a feedback control such that the hitch load  $F_x$  is less than a load value by which the towing vehicle **20** is pushed by the trailer **60**, namely, in which the hitch load  $F_x$  does not act in a direction by which the towing vehicle **20** is pushed by the trailer **60**. Alternatively, the requested trailer drive power  $F_{tdem}$  is subtracted or reduced depending on the hitch load  $F_x$  such that the requested trailer drive power  $F_{tdem}$  is reduced by a magnitude that is increased as the hitch load  $F_x$  is increased. When a negative determination is made at this step **S40b**, or after implementation of step **S50b**, step **S60b** corresponding to function of the motor control portion **82** is implemented to control the motor **62** by using the requested trailer drive power  $F_{tdem}$ , and to drive the trailer **60**. Further, at step **S60b**, the requested trailer drive power  $F_{tdem}$  calculated at step **S20b** is used as it is, and is reflected in the trailer drive power  $F_t$ . When an affirmative determination is made at step **S40b**, the requested trailer drive power  $F_{tdem}$  reduced at step **S50b** is used and is reflected in the trailer drive power  $F_t$ . [0042] In this way, the electric motor control portion **82** obtains the direction of the hitch load  $F_x$  and limits the trailer drive power  $F_t$  such that the direction of the hitch load  $F_x$  becomes a direction in which the trailer **60** does not push the towing vehicle **20**.

[0043] As described above, according to the present second embodiment, similarly to the first embodiment described above, it is possible to achieve the behavior stabilization of the towing vehicle **20** while enjoying the improvement of the acceleration performance by the trailer drive power  $F_t$ .

[0044] Further, according to the present second embodiment, the direction of the hitch load  $F_x$  is obtained, and the trailer drive power  $F_t$  is limited such that the direction of the hitch load  $F_x$  becomes a direction in which the trailer **60** does not push the towing vehicle **20**. Thus, the trailer drive power  $F_t$  is appropriately limited such that the trailer **60** does not push the towing vehicle **20** in the towing running state.

### Third Embodiment

[0045] In the first and second embodiments, the electronic control device **50** and the electronic control device **80** cooperate with each other to constitute the vehicle control device **100** that performs the drive control of the articulated vehicle **10**. In the present third embodiment, the electronic control device **80** limits the trailer drive power  $F_t$  independently without cooperating with the electronic control device **50**. Therefore, in the present third embodiment, the trailer drive power  $F_t$  is limited by using the hitch load  $F_x$  which is the signal supplied from the load sensor **74**.

[0046] FIG. **6** is a flowchart showing a main part of the control operation of the electronic control device **80**, and is a flowchart showing a control routine for stabilizing the behavior of the towing vehicle **20** while enjoying the improvement of the acceleration performance by the trailer drive power  $F_t$ , and is repeatedly executed, for example. The flow chart of FIG. **6** shows the control routine, which is executed in this third embodiment and which is different from the control routines shown in the flowcharts of FIGS. **3** and **5**. The control routine shown in the flow chart of FIG. **6** can be completed only by the electronic control device **80**.

[0047] In FIG. **6**, each step of the control routine corresponds to function of the electric motor control portion **82**. At step **S10c**, the requested trailer drive power  $F_{tdem}$  is calculated. At this step **S10c**, the accelerator opening  $\theta_{acc}$  is not used, and the requested trailer drive power  $F_{tdem}$  for resisting a running resistance of the trailer **60** is calculated based on the trailer running speed  $V_t$ , for example. Next, at step **S20c**, information of the hitch load  $F_x$  which is the signal supplied from



the load sensor **74** is obtained. Next, at step **S30c**, it is determined whether or not the direction of the hitch load  $F_x$  is a direction in which the trailer **60** pushes the towing vehicle **20**. When an affirmative determination is made at step **S30c**, step **S40c** is implemented. Since this step **S40c** is the same as step **S50b** in FIG. 5, and therefore, the description thereof is omitted. When a negative determination is made at step **S30c**, or after implementation of step **S40c**, step **S50c** is implemented to control the electric motor **62** by using the requested trailer drive power  $F_{tdem}$ , and to drive the trailer **60**. Further, when the negative determination is made at step **S30c**, the requested trailer drive power  $F_{tdem}$  calculated at step **S10c** is used as it is, and is reflected in the trailer drive power  $F_t$ . When an affirmative determination is made at step **S30c**, the requested trailer drive power  $F_{tdem}$  reduced at step **S40c** is used and reflected in the trailer drive power  $F_t$ .

[0048] In this way, the electric-motor control portion **82** obtains the magnitude and the direction of the hitch load  $F_x$  by the load sensor **74**, and limits the trailer drive power  $F_t$  when the direction of the hitch load  $F_x$  is the direction in which the trailer **60** pushes the towing vehicle **20**. When limiting the trailer drive power  $F_t$ , the electric motor control portion **82** increases the magnitude of reduction in the trailer drive power  $F_t$  as the magnitude of the hitch load  $F_x$  is increased.

[0049] As described above, according to the present third embodiment, similarly to the first and second embodiments described above, it is possible to achieve the behavior stabilization of the towing vehicle **20** while enjoying the improvement of the acceleration performance by the trailer drive power  $F_t$ .

[0050] According to the present third embodiment, the magnitude and the direction of the hitch load  $F_x$  are obtained by the load sensor **74**, and the trailer drive power  $F_t$  is limited when the direction of the hitch load  $F_x$  is the direction in which the trailer **60** pushes the towing vehicle **20**. When the trailer drive power  $F_t$  is limited, the magnitude of reduction in the trailer drive power  $F_t$  is increased as the magnitude of the hitch load  $F_x$  is increased. Thus, the trailer drive power  $F_t$  is appropriately limited such that the trailer **60** does not push the towing vehicle **20** in the towing running state. Further, the trailer drive power  $F_t$  can be limited by the trailer **60** alone such that the trailer **60** does not push the towing vehicle **20**.

[0051] Although the embodiments of the present invention have been described in detail with reference to the drawings, the present invention is also applicable to other aspects.

[0052] For example, in the first to third embodiments described above, the strain gauge is used as an example of the load sensor **74**, but the present invention is not limited to the detail. For example, the sensor provided in the coupling portion **96** may be a sensor capable of detecting the magnitude and the direction of the hitch load  $F_x$ , and may be a load cell, a displacement sensor or the like that are different from the strain gauge. The displacement sensor calculates the magnitude and the direction of the hitch load  $F_x$  by a displacement amount, for example. In the first and second embodiments described above, the trailer drive power  $F_t$  can be limited without using the hitch load  $F_x$  which is the detection signal of the load sensor **74**, and thus the load sensor **74** may not be provided.

[0053] In the first to third embodiments, for example, an electric motor may be used as the power source of the towing vehicle **20** instead of or in addition to the engine **22**. The transmission **24** is, for example, a known planetary gear type automatic transmission, a known belt type continuously variable transmission, a known synchronous meshing type parallel two shaft automatic transmission, a known electric continuously variable transmission, a known synchronous meshing type parallel two shaft manual transmission or the like. In a case where the power source included in the towing vehicle **20** is an electric motor, the towing vehicle **20** may not include the transmission **24**.

[0054] In the first to third embodiments, when the articulated vehicle **10** turns, an assist power from the trailer **60** is applied in a direction slightly deviated from a longitudinal direction of the towing vehicle **20**, and thus the assist power may act in an unintended direction (see FIG. 2B). Therefore, the present invention is particularly useful when the articulated vehicle **10** turns.

[0055] In the third embodiment, a way (degree) of being pulled in the towing running state may be estimated based on the trailer speed  $V_t$  with respect to the trailer drive power  $F_t$ , and the magnitude and the direction of the hitch load  $F_x$  may be estimated by the way of being pulled. In this case, the load sensor **74** may not be provided.

[0056] In the third embodiment, since the trailer **60** can limit the trailer drive power  $F_t$  by itself, the vehicle control apparatus **100** may include at least the electronic control device **80**. Further, the electronic control device **50** and the electronic control device **80** may not be connected to each other for communication with each other.

[0057] The above description is merely one embodiment, and the present invention can be implemented in a mode in which various modifications and improvements are added based on the knowledge of those skilled in the art.

#### NOMENCLATURE OF ELEMENTS

[0058] **20**: towing vehicle [0059] **50**: electronic control device [0060] **60**: trailer (towed vehicle)

[0061] **62**: electric motor (drive power source) [0062] **74**: load sensor (sensor) [0063] **80**: electronic

control device [0064] **82**: electric-motor control portion (drive control portion) [0065] **90**: coupler

[0066] **100**: vehicle control apparatus (control apparatus)

## Claims

1. A control apparatus comprising a processor configured to control a drive power of a towed vehicle which has a drive power source which is towed through a coupler by a towing vehicle, wherein, when the towing vehicle is running while towing the towed vehicle, the processor is configured to limit the drive power of the towed vehicle such that the towed vehicle does not push the towing vehicle through the coupler.
  2. The control apparatus according to claim 1, wherein the processor is configured to calculate, based on a drive power of the towing vehicle, an upper limit value of an allowable range of the drive power of the towed vehicle in which the towed vehicle does not push the towing vehicle, and to limit the drive power of the towed vehicle by the upper limit value.
  3. The control apparatus according to claim 2, wherein the allowable range of the drive power of the towed vehicle is a range in which a load applied to the coupler is less than a load value by which the towing vehicle is pushed by the towed vehicle.
  4. The control apparatus according to claim 1, wherein the processor is configured to obtain a direction of a load applied to the coupler, and to limit the drive power of the towed vehicle such that the direction of the load becomes a direction in which the towed vehicle does not push the towing vehicle.
  5. The control apparatus according to claim 1, wherein the processor is configured to obtain a magnitude and a direction of a load applied to the coupler, by a sensor provided in the coupler, and wherein the processor is configured, when the direction of the load is a direction in which the towed vehicle pushes the towing vehicle, to limit the drive power of the towed vehicle, and to reduce the drive power of the towed vehicle by a magnitude that is increased as the magnitude of the load applied to the coupler is increased.
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