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### OPTICAL MODULATION DEVICE, OPTICAL MODULATOR, OPTICAL MODULATION MODULE, OPTICAL TRANSMISSION APPARATUS, AND OPTICAL TRANSMISSION SYSTEM

#### Abstract

An optical modulation device includes a substrate including a multilayer portion, an optical waveguide including a protruding portion extending on an optical waveguide layer in the multilayer portion, and a modulation electrode that is an electrode formed on the optical waveguide layer to control a light wave propagating through the optical waveguide and formed to be divided into a plurality of segments along a propagation direction of light of the optical waveguide, in which in all sections of the electrode or a section excluding a part of the sections, a clearance, measured in an extending direction of the optical waveguide, between gaps between adjacent segments is constant, and a refractive index  $n_1$  of a first support layer, a refractive index  $n_2$  of a second support layer, and a refractive index  $n_3$  of a third support layer have a relationship of  $n_2 > n_1$  and  $n_2 > n_3$ .

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## **Background/Summary**

### **CROSS-REFERENCE TO RELATED APPLICATIONS**

[0001] This application claims the benefit of Japanese Patent Application No. 2024-022425 filed Feb. 16, 2024, the disclosure of which is herein incorporated by reference in its entirety.

### **BACKGROUND OF THE INVENTION**

#### **Field of the Invention**

[0002] The present invention relates to an optical modulation device, an optical modulator, an optical modulation module, an optical transmission apparatus, and an optical transmission system.

#### **Description of Related Art**

[0003] In a high-frequency/high-capacity optical fiber communication system, an optical modulator incorporating an optical modulation device as an optical waveguide device including an optical waveguide formed on a semiconductor substrate of InP or the like or on a substrate of LiNbO<sub>3</sub> (hereinafter, referred to as LN) or the like having an electro-optic effect, and a control electrode for controlling a light wave propagating through the optical waveguide has been widely used.

Particularly, the optical modulation device using the LN substrate may implement optical modulation characteristics of a small optical loss and a wide bandwidth and thus, has been widely used in the high-frequency/high-capacity optical fiber communication system.

[0004] In recent years, in order to implement further low-voltage driving and high-frequency modulation while reducing a size of the optical modulator, an optical modulator using a rib optical waveguide or a ridge optical waveguide (hereinafter, collectively referred to as a protruding optical waveguide) configured by forming a strip-shaped protruding portion on a surface of an LN substrate formed as a thin film (or a thin plate) (for example, having a thickness of 20 μm or lower) to further strengthen interaction between a signal electric field and guided light in the substrate has also been used in practice.

[0005] In addition, in recent years, it has been suggested to use a so-called segmented electrode in which an electrode is divided into a plurality of segments along an optical propagation direction of the optical waveguide as a coplanar modulation electrode, in order to achieve impedance matching between the modulation electrode and a drive circuit and velocity matching between a high-frequency propagation velocity in the modulation electrode and an optical propagation velocity in the optical waveguide (Japanese Laid-open Patent Publication No. 2022-148652, Japanese Laid-open Patent Publication No. 2016-194544, and Japanese Laid-open Patent Publication No. 2020-181173).

### **SUMMARY OF THE INVENTION**

[0006] The inventors of the present invention have found that in the protruding optical waveguide provided with the segmented electrode as the modulation electrode, forming the protruding portion (that is, a rib or a ridge) constituting the optical waveguide with high accuracy in a wafer process still poses an issue of variation in optical characteristics such as a modulation extinction ratio. A factor or a solution of the issue has not been found for a long time.

[0007] An object of the present invention is to implement favorable optical characteristics in an optical modulation device using a protruding optical waveguide and a segmented electrode as a modulation electrode.

[0008] According to an aspect of the present invention, there is provided an optical modulation

device including a substrate including a multilayer portion including multiple layers, an optical waveguide including a protruding portion extending on an optical waveguide layer in the multilayer portion of the substrate, and a modulation electrode that is an electrode formed on the optical waveguide layer to control a light wave propagating through the optical waveguide and that is formed to be divided into a plurality of segments along a propagation direction of light of the optical waveguide, in which in all sections of the electrode or a section excluding a part of the sections of the electrode, a clearance  $L$ , measured in an extending direction of the optical waveguide, between gaps between adjacent segments is constant, the multilayer portion of the substrate includes the optical waveguide layer, a first support layer in contact with a lower surface of the optical waveguide layer, a second support layer in contact with a lower surface of the first support layer, and a third support layer in contact with a lower surface of the second support layer, and a refractive index  $n_1$  of the first support layer, a refractive index  $n_2$  of the second support layer, and a refractive index  $n_3$  of the third support layer have a relationship of  $n_2 > n_1$  and  $n_2 > n_3$ .

[0009] According to another aspect of the present invention, the modulation electrode may be formed to be divided into a plurality of segments having the same length, and with respect to a wavelength  $\lambda$  of the light wave propagating through the optical waveguide and the refractive index  $n_1$  of the first support layer, the clearance  $L$ , measured in the extending direction of the optical waveguide, between the gaps between the adjacent segments may have a relationship of  $L > 4 \times \lambda / n_1$ .

[0010] According to another aspect of the present invention, with respect to a wavelength  $\lambda$  of the light wave propagating through the optical waveguide and the refractive index  $n_1$  of the first support layer, a thickness  $t_1$  of the first support layer may have a relationship of  $t_1 < 10 \times \lambda / n_1$ .

[0011] According to another aspect of the present invention, with respect to a refractive index  $n_0$  and a thickness  $t_0$  of the optical waveguide layer, the refractive index  $n_2$  and a thickness  $t_2$  of the second support layer may have a relationship of  $t_2 < t_0$  and  $n_2 > n_0$ .

[0012] According to another aspect of the present invention, the refractive index  $n_1$  of the first support layer, the refractive index  $n_2$  of the second support layer, and the refractive index  $n_3$  of the third support layer may have a relationship of  $(n_2 - n_3) < (n_2 - n_1)$ .

[0013] According to another aspect of the present invention, a light absorbing material that absorbs light in a wavelength range of the light wave propagating through the optical waveguide may be disposed in at least a part of an end surface of the substrate.

[0014] According to another aspect of the present invention, the light absorbing material may be a carbon material, a black resin, or a metal filler.

[0015] According to another aspect of the present invention, the substrate may be formed by laminating a plurality of plate bodies, and each plate body may include one layer or two adjacent layers among the optical waveguide layer, the first support layer, the second support layer, and the third support layer.

[0016] According to another aspect of the present invention, there is provided an optical modulator including any of the optical modulation devices, a case for accommodating the optical modulation device, an optical fiber for inputting light into the optical modulation device, and an optical fiber for guiding light output from the optical modulation device to an outside of the case.

[0017] According to another aspect of the present invention, there is provided an optical modulation module including any of the optical modulation devices, a case for accommodating the optical modulation device, an optical fiber for inputting light into the optical modulation device, an optical fiber for guiding light output from the optical modulation device to an outside of the case, and a drive circuit for driving the optical modulation device.

[0018] According to another aspect of the present invention, there is provided an optical transmission apparatus including the optical modulator or the optical modulation module, and an electronic circuit for generating an electrical signal for causing the optical modulation device to perform a modulation operation.

[0019] According to another aspect of the present invention, there is provided an optical

transmission system including the optical transmission apparatus, and an optical fiber transmission channel through which output light of the optical modulation device is transmitted.

[0020] According to the present invention, favorable optical characteristics can be implemented in an optical modulation device using a protruding optical waveguide and a segmented electrode as a modulation electrode.

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## Description

### BRIEF DESCRIPTION OF THE DRAWINGS

[0021] FIG. 1 is a diagram illustrating a configuration of an optical modulator using an optical modulation device according to a first embodiment of the present invention.

[0022] FIG. 2 is a plan view of the optical modulation device according to the first embodiment.

[0023] FIG. 3 is a side view of the optical modulation device illustrated in FIG. 2.

[0024] FIG. 4 is a diagram illustrating a configuration of a modulation portion of the optical modulation device illustrated in FIG. 2.

[0025] FIG. 5 is a cross-sectional view taken along line V-V of the modulation portion illustrated in FIG. 4.

[0026] FIG. 6 is a cross-sectional view of an optical modulation device according to a first modification example of the first embodiment.

[0027] FIG. 7 is a side view of an optical modulation device according to a second modification example of the first embodiment.

[0028] FIG. 8 is a plan view of an optical modulation device according to a second embodiment.

[0029] FIG. 9 is a side view of the optical modulation device illustrated in FIG. 8.

[0030] FIG. 10 is a plan view of an optical modulation device according to a modification example of the second embodiment.

[0031] FIG. 11 is a diagram illustrating a configuration of an optical modulation module according to a third embodiment.

[0032] FIG. 12 is a diagram illustrating a configuration of an optical transmission apparatus according to a fourth embodiment.

[0033] FIG. 13 is a diagram illustrating a configuration of an optical transmission system according to a fifth embodiment.

[0034] FIG. 14 is a plan view illustrating an example of an optical modulation device of the prior art.

[0035] FIG. 15 is a cross-sectional view taken along line XV-XV of the optical modulation device of the prior art illustrated in FIG. 14.

[0036] FIG. 16 is a cross-sectional view taken along line XVI-XVI of the optical modulation device of the prior art illustrated in FIG. 14.

### DETAILED DESCRIPTION OF THE INVENTION

[0037] The inventors of the present invention have intensively studied variation in optical characteristics of a protruding optical waveguide provided with a segmented electrode as a modulation electrode, and have found that a factor of the variation is interference of a leaked light beam generated from the protruding optical waveguide at a position of each gap portion between segments (each portion of the electrode divided at constant clearances) constituting the segmented electrode.

[0038] FIGS. 14, 15, and 16 are descriptive diagrams for describing the factor of the variation in the optical characteristics in an optical modulation device of the prior art. FIG. 14 is a plan view of an optical modulation device including a protruding optical waveguide provided with a segmented electrode as a modulation electrode, and FIG. 15 is a cross-sectional view taken along line XV-XV of the optical modulation device illustrated in FIG. 14. FIG. 16 is a cross-sectional view taken

along line XVI-XVI in the optical modulation device illustrated in FIG. 14.

[0039] With reference to FIGS. 14, 15, and 16, an optical modulation device 90 of the prior art illustrated as an example includes a Mach-Zehnder type optical waveguide 92 that is formed on one principal surface (upper surface) of an optical substrate 91 which is an LN substrate having a thickness of several  $\mu\text{m}$  to several tens of  $\mu\text{m}$  and that includes a protruding optical waveguide, and modulation electrodes 93a and 93b for controlling a light wave propagating through each of two arm waveguides 92a and 92b of the Mach-Zehnder type optical waveguide 92. Another principal surface (lower surface) of the optical substrate 91 is bonded to a support substrate 94 (refer to FIGS. 15 and 16). For example, the support substrate 94 is generally a glass plate having a lower refractive index than the optical substrate 91.

[0040] The modulation electrode 93a includes a hot electrode 93a1 and a ground electrode 93a2 that face each other with the arm waveguide 92a interposed therebetween in the principal surface of the optical substrate 91. Similarly, the modulation electrode 93b has a hot electrode 93b1 and a ground electrode 93b2 that face each other with the arm waveguide 92b interposed therebetween in the principal surface of the optical substrate 91.

[0041] Each of the modulation electrodes 93a and 93b is configured as a segmented electrode divided into a plurality of portions along optical propagation directions of the arm waveguides 92a and 92b. Specifically, each of the hot electrode 93a1 and the ground electrode 93a2 constituting the modulation electrode 93a is divided into a plurality of portions (segments) having the same length along the optical propagation direction of the arm waveguide 92a. Each of the hot electrode 93b1 and the ground electrode 93b2 constituting the modulation electrode 93b is also divided into a plurality of segments having the same length along the optical propagation direction of the arm waveguide 92b, and gaps between the segments are configured to be arranged at constant clearances.

[0042] Each segment of the hot electrodes 93a1 and 93b1 is electrically connected to each other by a hot transmission channel 96a. In addition, each segment of the ground electrode 93a2 is electrically connected to each other by a ground transmission channel 96b, and each segment of the ground electrode 93b2 is electrically connected to each other by a ground transmission channel 96c. Accordingly, the hot electrodes 93a1 and 93b1 connected to each other by the hot transmission channel 96a, the ground electrode 93a2 connected to the ground transmission channel 96b, and the ground electrode 93b2 connected to the ground transmission channel 96c constitute a coplanar electrode as a whole.

[0043] As illustrated in the cross-sectional view taken along line XVI-XVI in FIG. 16, in the arm waveguide 92a, in a case where a high-frequency signal is transmitted to the modulation electrode 93a, for example, an electric field is applied to the arm waveguide 92a in a portion in which the segments of the hot electrode 93a1 and the segments of the ground electrode 93a2 face each other. Accordingly, a refractive index changes (for example, increases) by  $\Delta n$  from a refractive index  $n_a$  (substrate refractive index  $n_a$ ) of the optical substrate 91. In gap portions in which the segments do not face each other, an electric field is not applied to the arm waveguide 92a. Thus, the refractive index remains as the substrate refractive index  $n_a$ .

[0044] Each of portions of the unchanging refractive index that are arranged along the arm waveguide 92a and that occur at positions of the gap portions in which the segments of the modulation electrode 93a do not face each other has a point of discontinuity of the refractive index (disturbance in a change in the refractive index) of the arm waveguide 92a along the optical propagation direction, and is a factor that causes leaked lights beam from the arm waveguide 92a.

[0045] Leaked light beams generated from each of the portions of the unchanging refractive index arranged along the arm waveguide 92a leak to the support substrate 94 having a refractive index  $n_b$  lower than that of the optical substrate 91 and are repeatedly reflected between the principal surfaces of the support substrate 94 to be intensified while interfering with each other in the support substrate 94 and propagate in a left-right direction of the illustration.

[0046] Particularly, each segmented electrode as the modulation electrode **93a** is generally divided into several hundred to several thousand segments. Thus, the number of gaps between the segments is also several hundreds to several thousands. Consequently, in the arm waveguide **92a**, the number of leaked light beams generated from each gap arranged at equal clearances between the segments is several hundreds to several thousands, and these leaked light beams interfere with each other to be intensified in the support substrate **94**. Accordingly, leaked light beams having considerable intensity may be generated in the support substrate **94**.

[0047] The above phenomenon also occurs in the arm waveguide **92b** in which the modulation electrode **93b** is formed, and leaked light beams from the arm waveguide **92b** interfere with each other to be intensified in the support substrate **94**. Accordingly, the leaked light beams having considerable intensity are further increased in the support substrate **94**.

[0048] A part of the high-intensity leaked light beams generated by the interference may enter a part of the Mach-Zehnder type optical waveguide **92** other than the arm waveguides **92a** and **92b** to be coupled with signal light (or modulated light) propagating through the Mach-Zehnder type optical waveguide **92**. Such leaked light beams coupled with the signal light (or the modulated light) propagating through the Mach-Zehnder type optical waveguide **92** are noise light and deteriorate the optical characteristics such as an extinction ratio of an optical modulation operation in the Mach-Zehnder type optical waveguide **92**, thereby causing the variation in the optical characteristics.

[0049] The present invention is conceived based on the knowledge about the factor of the variation in the optical characteristics and particularly, reduces the variation in the optical characteristics in the optical modulation operation by suppressing the interference between the leaked light beams in the support substrate to suppress an increase in the intensity of the leaked light beams caused by the interference.

[0050] Hereinafter, embodiments of the present invention will be described with reference to the drawings.

## 1. First Embodiment

[0051] First, a first embodiment of the present invention will be described. FIG. **1** is a diagram illustrating a configuration of an optical modulator **2** using an optical modulation device **1a** according to the first embodiment of the present invention. The optical modulator **2** includes the optical modulation device **1a** and a relay substrate **4** in a case **3**. For example, the optical modulation device **1a** has a DPQPSK modulator configuration. The case **3** is finally sealed airtight by fixing a cover (not illustrated) that is a plate body to an opening portion of the case **3**.

[0052] The optical modulator **2** also includes a signal pin **5a** for inputting a high-frequency electrical signal used for modulation of the optical modulation device **1a**, and a signal pin **5b** for inputting an electrical signal used for adjustment or the like of an operating point of the optical modulation device **1a**.

[0053] The optical modulator **2** further includes an input optical fiber **6a** for inputting light into the case **3** and an output optical fiber **6b** for guiding light modulated by the optical modulation device **1a** to an outside of the case **3**, on the same surface of the case **3**.

[0054] The input optical fiber **6a** and the output optical fiber **6b** are fixed to the case **3** through supports **7a** and **7b**, respectively, which are fixing members. The light input from the input optical fiber **6a** is collimated by a lens **8a** disposed in the support **7a** and is then input into the optical modulation device **1a** through a lens **8b**. However, this is only an example, and light may be input into the optical modulation device **1a** by, for example, introducing the input optical fiber **6a** into the case **3** through the support **7a** and connecting an end surface of the introduced input optical fiber **6a** to an end surface of a substrate **20** (described later) of the optical modulation device **1a**, in accordance with the prior art.

[0055] The optical modulator **2** also includes an optical unit **9** that polarizes and combines two modulated light beams output from the optical modulation device **1a**. The light beam output from

the optical unit **9** after being polarized and condensed is condensed by a lens **8c** disposed in the support **7b** and is coupled to the output optical fiber **6b**.

[0056] The relay substrate **4** relays the high-frequency electrical signal input from the signal pin **5a** and the electrical signal for adjustment or the like of the operating point input from the signal pin **5b** to the optical modulation device **1a** based on a conductor pattern (not illustrated) formed on the relay substrate **4**. For example, the conductor pattern on the relay substrate **4** is connected to each of the electrodes of the optical modulation device **1a** by wire bonding or the like. The optical modulator **2** also includes a terminator **10** having predetermined impedance in the case **3**.

[0057] FIG. **2** is a plan view illustrating an example of a configuration of the optical modulation device **1a**. The optical modulation device **1a** includes the substrate **20** configured with multiple layers. For example, the substrate **20** is rectangular in plan view and has two sides **21a** and **21b** on the left and the right of the illustration that extend in an up-down direction of the illustration to face each other, and two sides **21c** and **21d** at the top and the bottom of the illustration that extend in the left-right direction of the illustration to face each other in FIG. **2**.

[0058] FIG. **3** is a side view of the optical modulation device **1a** illustrated in FIG. **2** from the side **21a**. The substrate **20** includes an optical waveguide layer **22** and a support layer **23**. In the present embodiment, the support layer **23** includes a first support layer **231** and a second support layer **232**. In the present embodiment, for example, the substrate **20** is formed by laminating a plurality of plate bodies. Specifically, the substrate **20** is configured by laminating an optical substrate **24** and a support substrate **25**. The optical substrate **24** includes the optical waveguide layer **22**, and the support substrate **25** includes the support layer **23** formed with the first support layer **231** and the second support layer **232**. For example, the optical substrate **24** is an X-cut LN substrate that has an electro-optic effect and that is processed to have a thickness of 20  $\mu\text{m}$  or lower (for example, 2  $\mu\text{m}$ ) to be formed as a thin film. For example, the support substrate **25** is a glass substrate including the first support layer **231** and the second support layer **232** that are configured with different substances or compositions of glass.

[0059] The substrate **20** is not necessarily configured with a plurality of plate bodies as described above. The substrate **20** may be configured with a film body formed to have a layer shape on an appropriate substrate. For example, the substrate **20** can be a substrate including the first support layer **231** and the optical waveguide layer **22** that are formed to have a layer shape through a film forming process such as sputtering, vapor deposition, and/or crystal growth on an appropriate plate body constituting the second support layer **232**.

[0060] The optical modulation device **1a** includes an optical waveguide **26** (the whole thick dotted line illustrated in FIG. **2**) formed on the optical waveguide layer **22** (in the present embodiment, on the optical substrate **24**) of the substrate **20**. The optical waveguide **26** is a protruding optical waveguide (for example, a rib optical waveguide or a ridge optical waveguide) configured with a protruding portion extending on the optical waveguide layer **22** and, for example, performs coherent multi-level modulation exceeding 100 GBaud.

[0061] With reference to FIG. **2**, the optical waveguide **26** includes an input waveguide **27** that receives input light (an arrow to the right of the illustration) from the input optical fiber **6a** on an upper side of the illustration of the side **21a** on the left of the illustration of the optical waveguide layer **22**, and a branched waveguide **28** that causes the input light to branch into two light beams having the same light quantity. The optical waveguide **26** also includes so-called nested Mach-Zehnder type optical waveguides **29a** and **29b** as two modulation portions for modulating each light beam caused to branch by the branched waveguide **28**.

[0062] The nested Mach-Zehnder type optical waveguides **29a** and **29b** have a propagation direction of light that is folded by 180 degrees in a folded region **30** of the optical waveguide layer **22** in a right portion of the illustration, and output light to the left of the illustration from the side **21a** of the optical waveguide layer **22** via output waveguides **31a** and **31b**.

[0063] The nested Mach-Zehnder type optical waveguides **29a** and **29b** include two Mach-Zehnder

type optical waveguides **32a** and **32b**, and two Mach-Zehnder type optical waveguides **32c** and **32d**, respectively, provided in two waveguide portions forming a pair of arm waveguides. Hereinafter, the Mach-Zehnder type optical waveguides **32a**, **32b**, **32c**, and **32d** will be collectively referred to as Mach-Zehnder type optical waveguides **32**. Each Mach-Zehnder type optical waveguide **32** includes two arm waveguides.

[0064] A bias electrode **33a** for adjusting operating points of the nested Mach-Zehnder type optical waveguides **29a** and **29b** is formed in an upper portion of the illustration of the optical waveguide layer **22** upstream of the folded region **30** along a propagation direction of a light wave of the optical waveguide **26**. The Mach-Zehnder type optical waveguides **32a**, **32b** and the Mach-Zehnder type optical waveguides **32c** and **32d** are also provided with bias electrodes **33b** and **33c**, respectively, for adjusting their operating points.

[0065] Modulation electrodes for causing each of the four Mach-Zehnder type optical waveguides **32a**, **32b**, **32c**, and **32d** to perform a modulation operation are also formed in modulation portions **34a**, **34b**, **34c**, and **34d** illustrated in a lower portion of the illustration of the nested Mach-Zehnder type optical waveguides **29a** and **29b** folded in the folded region **30**. Hereinafter, the modulation portions **34a**, **34b**, **34c**, and **34d** will be collectively referred to as modulation portions **34**.

[0066] The high-frequency electrical signal for causing each Mach-Zehnder type optical waveguide **32** to perform the modulation operation is input from the relay substrate **4** through wire bonding **35** on the right of the illustration. The high-frequency electrical signal propagates through the modulation electrode formed in each modulation portion **34** and is terminated by a termination resistor (not illustrated) provided in the terminator **10** illustrated at the bottom of the illustration.

[0067] In order to avoid complication of the illustration to facilitate understanding, FIG. **2** does not illustrate details of the electrodes formed in the modulation portions **34a**, **34b**, **34c**, and **34d**. A segmented electrode formed to be divided into a plurality of segments along the propagation direction of light in the optical waveguide, as in the prior art illustrated in FIG. **13**, is formed in each modulation portion **34** as the modulation electrode.

[0068] For example, FIG. **4** illustrates a configuration of the modulation electrode in the modulation portion **34a**. The modulation electrodes of the other modulation portions **34b**, **34c**, and **34d** are also configured as in FIG. **4**.

[0069] In FIG. **4**, modulation electrodes **40a** and **40b** control light waves propagating through arm waveguides **36a1** and **36a2** of the Mach-Zehnder type optical waveguide **32a**, respectively.

[0070] The modulation electrode **40a** includes a hot electrode **40a1** and a ground electrode **40a2** facing each other with one arm waveguide **36a1** interposed therebetween in a surface of the optical waveguide layer **22**. Similarly, the modulation electrode **40b** includes a hot electrode **40b1** and a ground electrode **40b2** facing each other with the other arm waveguide **36a2** interposed therebetween in the surface of the optical waveguide layer **22**.

[0071] The modulation electrodes **40a** and **40b** are configured as segmented electrodes divided into a plurality of portions along optical propagation directions of the arm waveguides **36a1** and **36a2**, respectively. Specifically, each of the hot electrode **40a1** and the ground electrode **40a2** constituting the modulation electrode **40a** is divided into a plurality of portions (segments) having the same length along the optical propagation direction of the arm waveguide **36a1**, and gaps between the segments are arranged at constant clearances. Each of the hot electrode **40b1** and the ground electrode **40b2** constituting the modulation electrode **40b** is also divided into a plurality of segments having the same length along the optical propagation direction of the arm waveguide **36a2**, and gaps between the segments are arranged at constant clearances. For example, the number of segments of each of the hot electrodes **40a1** and **40b1** and the ground electrodes **40a2** and **40b2** is in the order of several thousands. However, the number of segments may be any number in accordance with optical modulation characteristics required for the optical modulation device **1a**.

[0072] Each segment of the hot electrodes **40a1** and **40b1** is electrically connected to each other by a hot transmission channel **41a**. In addition, each segment of the ground electrode **40a2** is



electrically connected to each other by a ground transmission channel **41b**, and each segment of the ground electrode **40b2** is electrically connected to each other by a ground transmission channel **41c**. Accordingly, the hot electrodes **40a1** and **40b1** connected to each other by the hot transmission channel **41a**, the ground electrode **40a2** connected to the ground transmission channel **41b**, and the ground electrode **40b2** connected to the ground transmission channel **41c** constitute a coplanar electrode as a whole.

[0073] FIG. 5 is a cross-sectional view taken along line V-V along the arm waveguide **36a1** in the modulation portion **34a** illustrated in FIG. 4. In FIG. 5, lower part (B) illustrates a configuration of the optical modulation device **1a** in a V-V cross section, and upper part (A) is a graph illustrating a change in a refractive index of the arm waveguide **36a1** along the optical propagation direction in the V-V cross section.

[0074] As illustrated in (A) of FIG. 5, in the arm waveguide **36a1**, as in the arm waveguide **92a** of the optical modulation device **90** according to the prior art illustrated in FIG. 16, in a case where a high-frequency signal is transmitted to the modulation electrode **40a**, an electric field is applied to the arm waveguide **36a1** in a portion in which the segments of the hot electrode **40a1** and the segments of the ground electrode **40a2** face each other. Accordingly, the refractive index changes (for example, increases) by  $\Delta n$  from a refractive index  $n_0$  (substrate refractive index  $n_0$ ) of the optical waveguide layer **22** (that is, the optical substrate **24**). In gap portions in which the segments do not face each other, an electric field is not applied to the arm waveguide **36a1**. Thus, the refractive index remains as the substrate refractive index  $n_0$ .

[0075] Each of portions of the unchanging refractive index (that is, portions in which the refractive index does not change from the substrate refractive index  $n_0$ ) that occur at positions of the gap portions in which the segments of the modulation electrode **40a** do not face each other in the arm waveguide **36a1** has disturbance in a change in the refractive index of the arm waveguide **36a1** along the optical propagation direction. In each of the portions having disturbance in the refractive index, leaked light beams may occur from the arm waveguide **36a1** formed on the optical waveguide layer **22**, as in the optical modulation device **90** according to the prior art.

[0076] However, in order not to cause the leaked light beams to spread into the substrate **20** and interfere with each other, in the present embodiment, particularly, the support layer **23** included in the substrate **20** is configured with three layers including the first support layer **231**, the second support layer **232**, and a third support layer **233** that have different refractive indices. The refractive index  $n_0$  of the optical waveguide layer **22** on which the optical waveguide **26** is formed, a refractive index  $n_1$  of the first support layer **231**, a refractive index  $n_2$  of the second support layer **232**, and a refractive index  $n_3$  of the third support layer **233** have the following relationship in Expression (1).

$$n_0 > n_1, n_2 > n_1, \text{ and } n_2 > n_3 \quad (1)$$

[0077] That is, the second support layer **232** having a high refractive index is present below the optical waveguide layer **22** on which the arm waveguide **36a1** is formed, with the first support layer **231** having a lower refractive index than the optical waveguide layer **22** interposed between the optical waveguide layer **22** and the second support layer **232**.

[0078] The second support layer **232** having a high refractive index is interposed between the first support layer **231** and the third support layer **233** that have low refractive indices. Thus, the second support layer **232** having a high refractive index is a layer having a light confinement effect between the first support layer **231** and the third support layer **233** having low refractive indices.

[0079] According to the above configuration, the leaked light beams generated from the arm waveguide **36a1** formed on the optical waveguide layer **22** easily pass through the first support layer **231** having a low refractive index, and a part of the leaked light beams may propagate through the second support layer **232** as light in a waveguide mode of the second support layer **232** having the light confinement effect. For example, this conversion into the waveguide mode may

randomly occur because of disturbance or the like in a boundary surface between the second support layer **232** and other support layers. Coherency of the “leaked light beams” is decreased through the propagation through the second support layer **232** and the random conversion into the waveguide mode.

[0080] Then, the “leaked light beams” converted into the waveguide mode of the second support layer **232** may reach an end portion of the substrate **20** and, for example, be output from the end portion of the substrate **20** depending on a degree of strength of the light confinement effect in the second support layer **232**. Accordingly, the “leaked light beams” may be guided to an outside of the substrate **20** without interfering with each other to be intensified. That is, intensification caused by the interference between the “leaked light beams” is suppressed (or prevented).

[0081] The modulation electrode **40b** of the arm waveguide **36a2** and the modulation electrodes of the arm waveguides of the Mach-Zehnder type optical waveguides **32** in other modulation portions **34** are also configured in the same manner as the modulation electrode **40a** of the arm waveguide **36a1**. Even for the leaked light beams generated in these arm waveguides, intensification caused by the interference between the leaked light beams may also be suppressed because of the presence of the second support layer **232**, as described above.

[0082] Hereinafter, the arm waveguides of each Mach-Zehnder type optical waveguide **32** including the arm waveguides **36a1** and **36a2** of the Mach-Zehnder type optical waveguide **32a** will be collectively referred to as arm waveguides **36**. The modulation electrodes provided in the arm waveguides **36** in each modulation portion **34** including the modulation electrodes **40a** and **40b** provided in the arm waveguides **36a1** and **36a2** in the modulation portion **34a** will be collectively referred to as modulation electrodes **40**.

[0083] The above action suppresses intensification caused by the interference in the support layer **23** for the leaked light beams generated from the arm waveguides **36** formed on the optical waveguide layer **22**. Consequently, even in a case where the leaked light beams reach the optical waveguide layer **22** again to be combined with the signal light propagating through the optical waveguide **26**, an effect of the leaked light beams on the optical characteristics of the optical modulation device **1a** is suppressed to be low compared to that in the optical modulation device **90** of the prior art.

[0084] In order to effectively suppress the interference between the leaked light beams generated in the arm waveguides **36** of the Mach-Zehnder type optical waveguides **32** formed on the optical waveguide layer **22** using the above action, it may be important to suppress the interference between the leaked light beams in the first support layer **231** before the leaked light beams reach the second support layer **232**. Specifically, the interference between the leaked light beams in the first support layer **231** depends on a clearance **L** between the gaps arranged at constant clearances between each segment constituting the modulation electrodes **40** and/or a thickness **t1** of the first support layer **231**. The clearance **L** between the gaps refers to a distance between centers of each gap in a length direction along the corresponding arm waveguide **36**.

[0085] More specifically, in order to suppress the interference between the leaked light beams in the first support layer **231**, the clearance **L** between the gaps of the segments constituting the modulation electrodes **40** preferably satisfies Expression (2) illustrated below and more preferably satisfies Expression (3) with respect to a wavelength **A** of the light wave propagating through the optical waveguide **26** and the refractive index **n1** of the first support layer **231**.

[00001]  $L > 4 \times \lambda / n1$  (2)  $L > 10 \times \lambda / n1$  (3)

[0086] In order to suppress the interference between the leaked light beams in the first support layer **231**, the thickness **t1** of the first support layer **231** preferably satisfies Expression (4) illustrated below and more preferably satisfies Expression (5).

[00002]  $t1 < 10 \times \lambda / n1$  (4)  $t1 < 4 \times \lambda / n1$  (5)

[0087] A thickness **t2** of the second support layer **232** significantly affects line impedance of the

modulation electrodes **40** in a case where the thickness **t2** is set to be excessively large. Thus, the thickness **t2** is preferably smaller than a thickness **t0** of the optical waveguide layer **22** in the optical waveguide **26**. That is, the thickness **t2** of the second support layer **232** preferably has the following relationship in Expression (6) with respect to the thickness **t0** of the optical waveguide **26** in the optical waveguide layer **22**.

[00003]  $t2 < t0$  (6)

[0088] In order to actively guide the leaked light beams by securing light confinement in the second support layer **232** while configuring the second support layer **232** to be thin to satisfy Expression (6), the refractive index **n2** of the second support layer **232** is preferably larger than the refractive index **n0** of the optical waveguide layer **22**. That is, the refractive index **n2** of the second support layer **232** preferably has the following relationship in Expression (7) with respect to the refractive index **n0** of the optical waveguide layer **22**.

[00004]  $n2 > n0$  (7)

#### First Modification Example

[0089] As a first modification example of the optical modulation device **1a**, as illustrated in FIG. **6**, the substrate **20** can be configured to reduce the light confinement effect in the second support layer **232** so that the leaked light beams from the arm waveguides **36** are converted into the waveguide mode of the second support layer **232** and propagate through the second support layer **232**, and then leak to other support layers as a non-waveguide mode. For example, this configuration is suitable in various cases where a support layer having a high light confinement effect affects a high-frequency electric field or the like. FIG. **6** is a diagram illustrating a configuration of a modification example of the substrate **20** corresponding to FIG. **5** illustrating a configuration of the substrate **20** according to the first embodiment.

[0090] Even in this case, the coherency of the “leaked light beams” leaking to the third support layer **233** or the first support layer **231** from the second support layer **232** as the non-waveguide mode is decreased, as described above. Thus, intensification caused by interference between the leaked light beams in the third support layer **233** or the first support layer **231** is unlikely to occur. That is, even in this case, the intensification caused by the interference between the “leaked light beams” is suppressed by the presence of the second support layer **232**.

[0091] In a case where the substrate **20** is configured to reduce the light confinement effect in the second support layer **232** as illustrated in FIG. **6**, that is, in a case where the “leaked light beams” that have propagated through the second support layer **232** leak from the second support layer **232** again, a main direction in which the “leaked light beams” that have propagated leak is preferably a direction of the third support layer **233** farther from the signal light instead of a direction of the first support layer close to the signal light. Thus, the refractive index **n1** of the first support layer **231**, the refractive index **n2** of the second support layer **232**, and the refractive index **n3** of the third support layer **233** preferably have the following relationship in Expression (8).

[00005]  $(n2 - n3) < (n2 - n1)$  (8)

[0092] Accordingly, since the “leaked light beams” that have propagated through the second support layer **232** mainly leak in the direction of the third support layer **233**, leaking of the “leaked light beams” in the direction of the first support layer **231** and optical coupling of the “leaked light beams” with the optical waveguide **26** of the optical waveguide layer **22** can be suppressed. Consequently, an adverse effect of the leaked light beams on the optical characteristics of the optical modulation device **1a** can be suppressed.

[0093] Specifically, for example, the wavelength  $\lambda$  of the light wave propagating through the optical waveguide **26** is 1.55  $\mu\text{m}$ , and the clearance **L** between the gaps of the segments constituting the modulation electrodes **40** is 50  $\mu\text{m}$  or higher and 100  $\mu\text{m}$  or lower. The thickness **t0** of a portion of the optical waveguide layer **22** corresponding to the optical waveguide **26** is 1  $\mu\text{m}$  or higher and 2  $\mu\text{m}$  or lower, and the refractive index **n0** of the optical waveguide layer **22** in the wavelength  $\lambda$  is

2.2. For example, the first support layer **231** is formed of SiO.sub.2, has the thickness  $t_1$  of 3  $\mu\text{m}$ , and has the refractive index  $n_1$  of 1.48 in the wavelength  $\lambda$ . For example, the second support layer **232** may be formed of a high-refractive index material such as TiO.sub.2 or Ta.sub.2O.sub.5 or a semiconductor material such as Si or Ge. For example, the thickness  $t_2$  of the second support layer **232** is 0.2  $\mu\text{m}$  or higher and 3  $\mu\text{m}$  or lower. The refractive index  $n_2$  of the second support layer **232** in the wavelength  $\lambda$  is 2.35 in a case where the second support layer **232** is formed of TiO.sub.2, 2.1 in a case where the second support layer **232** is formed of Ta.sub.2O.sub.5 or the like, 3.4 in a case where the second support layer **232** is formed of Si, and 4.4 in a case where the second support layer **232** is formed of Ge. For example, the third support layer **233** is formed of glass, has the thickness  $t_3$  of 300  $\mu\text{m}$ , and has the refractive index  $n_3$  of 1.55 in the wavelength  $\lambda$  is.

[0094] In the present embodiment and each embodiment described below, the clearance  $L$  between the gaps between the adjacent segments is not necessarily constant in all sections (that is, the whole) of each modulation electrode **40**. The clearance  $L$  between the gaps between the adjacent segments may be constant in all sections of the modulation electrode **40** or a section excluding a part of the sections of the modulation electrode **40**. Similarly, each segment does not necessarily have the same length in all sections of each modulation electrode **40**. Each segment may have a constant length in all sections of the modulation electrode **40** or a section excluding a part of the sections of the modulation electrode **40**. For example, in a case where the modulation electrode **40** is divided into several hundred to several thousand segments, the lengths of the segments and/or the clearance between the gaps between the adjacent segments in one section or a plurality of sections of the modulation electrode **40** may be different from the lengths of the segments and/or the clearance between the gaps between the adjacent segments in other sections.

#### Second Modification Example

[0095] While the whole substrate **20** is configured with multiple layers in the first embodiment, the whole substrate **20** is not necessarily configured with multiple layers. For example, the action and the effect of suppressing the interference between the leaked light beams can be achieved in a case where the substrate **20** is configured with multiple layers in at least a lower portion of the modulation portions **34** in which the modulation electrodes **40** which are the segmented electrodes are formed.

[0096] That is, the substrate **20** may include at least a multilayer portion configured with multiple layers, and the multilayer portion may include the optical waveguide layer **22**, the first support layer **231** in contact with a lower surface of the optical waveguide layer **22**, the second support layer **232** in contact with a lower surface of the first support layer **231**, and the third support layer **233** in contact with a lower surface of the second support layer **232**.

[0097] For example, as a second modification example, as illustrated in FIG. 7, the substrate **20** can include the optical waveguide layer **22**, the first support layer **231**, and the third support layer **233** in the whole substrate **20** in a layer structure seen from the side **21a**, and include the second support layer **232** in only the lower portion of the modulation portions **34** in which the modulation electrodes **40** are formed.

#### 2. Second Embodiment

[0098] Next, an optical modulation device **1b** according to a second embodiment of the present invention will be described. The optical modulation device **1b** has the same configuration as the optical modulation device **1a** except that a light absorbing material is disposed on the end surface of the substrate **20**. The optical modulation device **1b** may be used by mounting the optical modulation device **1b** on the optical modulator **2** instead of the optical modulation device **1a**.

[0099] FIG. 8 is a plan view of the optical modulation device **1b** and is a diagram corresponding to the plan view of the optical modulation device **1a** illustrated in FIG. 2. FIG. 9 is a side view of the optical modulation device **1b** seen from the side **21a** and is a diagram corresponding to the side view of the optical modulation device **1a** seen from the side **21a** illustrated in FIG. 3. In FIGS. 8 and 9, the same constituents as those in FIGS. 2 and 3 are designated using the same reference

numerals as those in FIGS. 2 and 3, and the description for FIGS. 2 and 3 is incorporated herein.

[0100] The optical modulation device **1b** has the same configuration as the optical modulation device **1a** except that a light absorbing material **43** that absorbs light in a wavelength range of the light wave propagating through the optical waveguide **26** is disposed on at least a part of the end surface of the substrate **20**. For example, a portion in which the light absorbing material **43** is disposed may be an end surface portion of the second support layer **232** through which the leaked light beams from the arm waveguides **36** provided with the modulation electrodes **40** which are the segmented electrodes may propagate in the end surface of the substrate **20**. In the present embodiment, the light absorbing material **43** is particularly disposed in the end surface portion of the second support layer **232** that may be reached by the leaked light beams. Specifically, the light absorbing material **43** is disposed in an end surface portion corresponding to a downstream position in the propagation direction of the light wave propagating through the arm waveguides **36** of the modulation portions **34** in the end surface of the second support layer **232**.

[0101] Accordingly, in the optical modulation device **1b**, the leaked light beams that are generated from the arm waveguides **36** of the optical waveguide layer **22** and that propagate through the second support layer **232** are absorbed by the light absorbing material **43** to be attenuated in a case where the leaked light beams reach the end surface of the second support layer **232**. Accordingly, the intensity of the leaked light beam reflected by the end surface among the leaked light beams propagating through the second support layer **232** is reduced, and the effect of the leaked light beams on the optical characteristics of the optical modulation device **1b** is further effectively suppressed compared to that in the optical modulation device **90** of the prior art.

[0102] While the light absorbing material **43** is disposed to extend over substantially the whole substrate **20** in a thickness direction in FIG. 9, the light absorbing material **43** may be disposed in at least the end surface portion of the second support layer **232**. However, by disposing the light absorbing material **43** to extend over substantially the whole substrate **20** in the thickness direction as illustrated in FIG. 9, the leaked light beams coming after propagating through the first support layer **231** and the third support layer **233** may also be absorbed by the light absorbing material **43**. Thus, the effect of the leaked light beams on the optical characteristics of the optical modulation device **1b** may be more effectively suppressed.

[0103] The end surface of the substrate **20** on which the light absorbing material **43** is disposed is a position at which an effect of a material disposed in the portion on electrical characteristics of the modulation electrodes **40** or waveguide characteristics of the optical waveguide **26** is low. Thus, various materials including a metal material may be selected as a material of the light absorbing material **43**.

[0104] For example, the light absorbing material **43** may be a carbon material of carbon black or the like, a black resin of a cashew oil or the like, or a metal filler of Ag or the like. For example, these types of the light absorbing material **43** may be applied to the end surface of the substrate **20** and cured to be disposed on the end surface using an appropriate resin as a binder.

#### Modification Example

[0105] As in the above configuration, the light absorbing material **43** is preferably disposed in the end surface portion corresponding to the downstream position in the propagation direction of the light wave propagating through the arm waveguides **36** of the modulation portions **34** in the end surface of the second support layer **232** through which the leaked light beams from the arm waveguides **36** may propagate.

[0106] Accordingly, for example, in a case where the modulation portions **34** are disposed in the optical waveguide layer **22** of the substrate **20** upstream of the folded region **30** along the propagation direction of the light wave in the optical waveguide **26** as illustrated in FIG. 10, the light absorbing material **43** is preferably disposed in the end surface portion of the second support layer **232** on the side **21b** positioned downstream in the propagation direction of the light wave propagating through the arm waveguides **36** of the modulation portions **34**.

### 3. Third Embodiment

[0107] Next, a third embodiment of the present invention will be described. In the present embodiment, the optical modulation device **1a** illustrated in the first embodiment is used in an optical modulation module **50**. FIG. **11** is a diagram illustrating a configuration of the optical modulation module **50** according to the present embodiment. In FIG. **11**, the same constituents as those of the optical modulator **2** according to the first embodiment illustrated in FIG. **1** are designated using the same reference numerals as the reference numerals illustrated in FIG. **1**, and their description in FIG. **1** is incorporated herein.

[0108] The optical modulation module **50** has the same configuration as the optical modulator **2** illustrated in FIG. **1** except for including a circuit substrate **51** instead of the relay substrate **4**. The circuit substrate **51** includes a drive circuit **52**. For example, the drive circuit **52** generates a high-frequency electrical signal for driving the optical modulation device **1a** based on a modulation signal supplied from the outside through the signal pin **5a** and outputs the generated high-frequency electrical signal to the optical modulation device **1a**.

[0109] Since the optical modulation module **50** having the above configuration includes the optical modulation device **1a** like the optical modulator **2** according to the first embodiment, the optical modulation module **50** can implement a favorable optical modulation operation by reducing the effect of the leaked light beams from the arm waveguides **36** provided with the modulation electrodes **40**, which are the segmented electrodes, on the optical characteristics of the optical modulation device **1a**, like the optical modulator **2**.

[0110] While the optical modulation module **50** includes, for example, the optical modulation device **1a** in the present embodiment, the optical modulation module **50** may include the optical modulation device **1b** according to the second embodiment or the optical modulation device according to the modification example of the first embodiment or the modification example of the second embodiment.

### 4. Fourth Embodiment

[0111] Next, a fourth embodiment of the present invention will be described. In the present embodiment, the optical modulator **2** according to the first embodiment is mounted on an optical transmission apparatus **55**. FIG. **12** is a diagram illustrating a configuration of the optical transmission apparatus **55** according to the present embodiment. The optical transmission apparatus **55** includes the optical modulator **2**, a light source **56** that inputs light into the optical modulator **2**, a modulator drive unit **57**, and a modulation signal generation part **58**. The optical modulation module **50** according to the third embodiment can be used instead of the optical modulator **2** and the modulator drive unit **57**. The optical modulator **2** may include the optical modulation device **1b** according to the second embodiment or the optical modulation device according to the modification example of the first embodiment or the modification example of the second embodiment, instead of the optical modulation device **1a**.

[0112] The modulation signal generation part **58** is an electronic circuit for generating an electrical signal for causing the optical modulator **2** to perform the modulation operation, and generates a modulation signal that is a high-frequency signal for causing the optical modulator **2** to perform an optical modulation operation in accordance with corresponding modulation data, based on transmission data provided from the outside and outputs the modulation signal to the modulator drive unit **57**.

[0113] The modulator drive unit **57** amplifies the modulation signal input from the modulation signal generation part **58** to output four sets of high-frequency electrical signals for driving each modulation electrode **40** provided in the four Mach-Zehnder type optical waveguides **32** of the optical modulation device **1a** included in the optical modulator **2**.

[0114] These high-frequency electrical signals are input into the signal pin **5a** of the optical modulator **2** to drive the optical modulation device **1a**. Accordingly, for example, the light output from the light source **56** is subjected to DP-QPSK modulation by the optical modulator **2** and is

output from the optical transmission apparatus 55 as modulated light.

[0115] In the optical transmission apparatus 55, since the optical modulator 2 or the optical modulation module 50 including the optical modulation device 1a, 1b, or 1c is used, favorable optical transmission can be performed by implementing favorable modulation characteristics.

## 5. Fifth Embodiment

[0116] Next, a fifth embodiment of the present invention will be described. In the present embodiment, the optical transmission apparatus 55 according to the fourth embodiment is used in an optical transmission system 60. FIG. 13 is a diagram illustrating a configuration of the optical transmission system 60 according to the present embodiment. The optical transmission system 60 includes the optical transmission apparatus 55 according to the fourth embodiment, an optical fiber transmission channel 61 for transmitting a modulated optical signal that is output light of the optical modulator 2 or the optical modulation module 50 included in the optical transmission apparatus 55, and an optical reception apparatus 62 that receives the optical signal transmitted by the optical fiber transmission channel 61. The optical transmission system 60 transmits the optical signal via the optical transmission apparatus 55 using the optical modulator 2 or the optical modulation module 50 including the optical modulation device 1a or 1b or the optical modulation device according to their modification example. Thus, the optical transmission system 60 has favorable optical transmission performance.

## 6. Other Embodiments

[0117] While the optical waveguide layer 22 on which the optical waveguide 26 is formed is included in the optical substrate 24 which is the LN substrate in the first to third embodiments, the optical waveguide layer 22 is not necessarily formed of LN. The optical waveguide layer 22 may be formed of a semiconductor material such as InP.

[0118] In the embodiments, the substrate 20 configured with multiple layers is configured by laminating a plurality of plate bodies. However, this is only an example, and the substrate 20 may be configured with a film body formed to have a layer shape on an appropriate substrate, as described above.

[0119] In the embodiments, the optical substrate 24 as a plate body constituting the optical waveguide layer 22 and the support substrate 25 as a plate body constituting the first support layer 231 and the second support layer 232 are laminated in the substrate 20. However, the optical substrate 24 and the support substrate 25 are examples of plate bodies constituting the substrate 20, and any distribution of the layers included in each of the plurality of plate bodies may be used. That is, in a case where the substrate 20 is formed by laminating a plurality of plate bodies, each plate body may include one layer or a plurality of layers of any number among the optical waveguide layer 22 and a plurality of support layers such as the first support layer 231.

[0120] The present invention is not limited to the configurations of the embodiments and can be embodied in various aspects without departing from its gist.

## 7. Configurations Supported by Embodiments

[0121] The embodiments and their modification examples support the following configurations.

[0122] (Configuration 1) An optical modulation device includes a substrate including a multilayer portion including multiple layers, an optical waveguide including a protruding portion extending on an optical waveguide layer in the multilayer portion of the substrate, and a modulation electrode that is an electrode formed on the optical waveguide layer to control a light wave propagating through the optical waveguide and that is formed to be divided into a plurality of segments along a propagation direction of light of the optical waveguide, in which in all sections of the electrode or a section excluding a part of the sections of the electrode, a clearance L, measured in an extending direction of the optical waveguide, between gaps between adjacent segments is constant, the multilayer portion of the substrate includes the optical waveguide layer, a first support layer in contact with a lower surface of the optical waveguide layer, a second support layer in contact with a lower surface of the first support layer, and a third support layer in contact with a lower surface of

the second support layer, and a refractive index  $n_1$  of the first support layer, a refractive index  $n_2$  of the second support layer, and a refractive index  $n_3$  of the third support layer have a relationship of  $n_2 > n_1$  and  $n_2 > n_3$ .

[0123] According to the optical modulation device of Configuration 1, intensification caused by interference can be suppressed by guiding leaked light beams from the optical waveguide caused by the gaps between the segments of the optical modulation electrode which is a segmented electrode formed to be divided into a plurality of segments along the propagation direction of the light of the optical waveguide, to the second support layer. Accordingly, in the optical modulation device of Configuration 1, favorable optical characteristics can be implemented by reducing an effect of the leaked light beams on optical characteristics of the optical modulation device.

[0124] (Configuration 2) In the optical modulation device according to Configuration 1, the modulation electrode is formed to be divided into a plurality of segments having the same length, and with respect to a wavelength  $\lambda$  of the light wave propagating through the optical waveguide and the refractive index  $n_1$  of the first support layer, the clearance  $L$ , measured in the extending direction of the optical waveguide, between the gaps between the adjacent segments has a relationship of  $L > 4 \times \lambda / n_1$ .

[0125] According to the optical modulation device of Configuration 2, more favorable optical characteristics can be implemented by further suppressing the intensification caused by the interference between the leaked light beams.

[0126] (Configuration 3) In the optical modulation device according to Configuration 1 or 2, with respect to a wavelength  $\lambda$  of the light wave propagating through the optical waveguide and the refractive index  $n_1$  of the first support layer, a thickness  $t_1$  of the first support layer has a relationship of  $t_1 < 10 \times \lambda / n_1$ .

[0127] According to the optical modulation device of Configuration 3, more favorable optical characteristics can be implemented by suppressing the intensification caused by the interference between the leaked light beams in the first support layer.

[0128] (Configuration 4) In the optical modulation device according to any one of Configurations 1 to 3, with respect to a refractive index  $n_0$  and a thickness  $t_0$  of the optical waveguide layer, the refractive index  $n_2$  and a thickness  $t_2$  of the second support layer have a relationship of  $t_2 < t_0$  and  $n_2 > n_0$ .

[0129] According to the optical modulation device of Configuration 4, the leaked light beams from the optical waveguide can be effectively guided to the second support layer while an effect of a material used in the second support layer on electrical characteristics of the electrode formed on the optical waveguide layer is prevented.

[0130] (Configuration 5) In the optical modulation device according to any one of Configurations 1 to 4, the refractive index  $n_1$  of the first support layer, the refractive index  $n_2$  of the second support layer, and the refractive index  $n_3$  of the third support layer have a relationship of  $(n_2 - n_3) < (n_2 - n_1)$ .

[0131] According to the optical modulation device of Configuration 5, coupling of the leaked light beams with the optical waveguide again can be suppressed by guiding the leaked light beams guided to the second support layer from the optical waveguide to the third support layer.

[0132] (Configuration 6) In the optical modulation device according to any one of Configurations 1 to 5, a light absorbing material that absorbs light in a wavelength range of the light wave propagating through the optical waveguide is disposed in at least a part of an end surface of the substrate.

[0133] According to the optical modulation device of Configuration 6, further favorable optical characteristics can be implemented by reducing intensity of the leaked light beams that have reached the end surface of the substrate via the light absorbing material disposed on the end surface to effectively reduce the effect of the leaked light beams on the optical characteristics of the optical modulation device.

[0134] (Configuration 7) In the optical modulation device according to Configuration 6, the light



absorbing material is a carbon material, a black resin, or a metal filler.

[0135] According to the optical modulation device of Configuration 7, further favorable optical characteristics of the optical modulation device can be implemented by effectively reducing the intensity of the leaked light beams that have reached the end surface of the substrate.

[0136] (Configuration 8) In the optical modulation device according to any one of Configurations 1 to 6, the substrate is formed by laminating a plurality of plate bodies, and each plate body includes one layer or two adjacent layers among the optical waveguide layer, the first support layer, the second support layer, and the third support layer.

[0137] According to the optical modulation device of Configuration 8, a substrate including a plurality of support layers and an optical waveguide layer on which an optical waveguide is formed can be easily configured.

[0138] (Configuration 9) An optical modulator includes the optical modulation device according to any one of Configurations 1 to 8, a case for accommodating the optical modulation device, an optical fiber for inputting light into the optical modulation device, and an optical fiber for guiding light output from the optical modulation device to an outside of the case.

[0139] According to the optical modulator of Configuration 9, since the optical modulation device of any one of Configurations 1 to 8 is used, an optical modulator having favorable optical characteristics may be implemented.

[0140] (Configuration 10) An optical modulation module includes the optical modulation device according to any one of Configurations 1 to 8, and a drive circuit for driving the optical modulation device.

[0141] According to the optical modulation module of Configuration 10, since the optical modulation device of any one of Configurations 1 to 8 is used, an optical modulation module having favorable optical characteristics may be implemented.

[0142] (Configuration 11) An optical transmission apparatus includes the optical modulator according to Configuration 9 or the optical modulation module according to Configuration 10, and an electronic circuit for generating an electrical signal for causing the optical modulation device to perform a modulation operation.

[0143] According to the optical transmission apparatus of Configuration 11, since the optical modulator or the optical modulation module using the optical modulation device of any one of Configurations 1 to 8 is used, favorable optical transmission characteristics can be implemented.

[0144] (Configuration 12) An optical transmission system includes the optical transmission apparatus according to Configuration 11, and an optical fiber transmission channel through which output light of the optical modulation device propagates.

[0145] According to the optical transmission system of Configuration 12, since the optical transmission apparatus using the optical modulation device of any one of Configurations 1 to 7 is used, favorable optical transmission characteristics can be implemented.

## Claims

1. An optical modulation device comprising: a substrate including a multilayer portion including multiple layers; an optical waveguide including a protruding portion extending on an optical waveguide layer in the multilayer portion of the substrate; and a modulation electrode that is an electrode formed on the optical waveguide layer to control a light wave propagating through the optical waveguide and that is formed to be divided into a plurality of segments along a propagation direction of light of the optical waveguide, wherein in all sections of the electrode or a section excluding a part of the sections of the electrode, a clearance L, measured in an extending direction of the optical waveguide, between gaps between adjacent segments is constant, the multilayer portion of the substrate includes the optical waveguide layer, a first support layer in contact with a lower surface of the optical waveguide layer, a second support layer in contact with a lower surface

- of the first support layer, and a third support layer in contact with a lower surface of the second support layer, and a refractive index  $n_1$  of the first support layer, a refractive index  $n_2$  of the second support layer, and a refractive index  $n_3$  of the third support layer have a relationship of  $n_2 > n_1$  and  $n_2 > n_3$ .
2. The optical modulation device according to claim 1, wherein the modulation electrode is formed to be divided into a plurality of segments having the same length, and with respect to a wavelength  $\lambda$  of the light wave propagating through the optical waveguide and the refractive index  $n_1$  of the first support layer, the clearance  $L$ , measured in the extending direction of the optical waveguide, between the gaps between the adjacent segments has a relationship of  $L > 4 \times \lambda / n_1$ .
  3. The optical modulation device according to claim 1, wherein, with respect to a wavelength  $\lambda$  of the light wave propagating through the optical waveguide and the refractive index  $n_1$  of the first support layer, a thickness  $t_1$  of the first support layer has a relationship of  $t_1 < 10 \times \lambda / n_1$ .
  4. The optical modulation device according to claim 1, wherein, with respect to a refractive index  $n_0$  and a thickness  $t_0$  of the optical waveguide layer, the refractive index  $n_2$  and a thickness  $t_2$  of the second support layer have a relationship of  $t_2 < t_0$  and  $n_2 > n_0$ .
  5. The optical modulation device according to claim 1, wherein the refractive index  $n_1$  of the first support layer, the refractive index  $n_2$  of the second support layer, and the refractive index  $n_3$  of the third support layer have a relationship of  $(n_2 - n_3) < (n_2 - n_1)$ .
  6. The optical modulation device according to claim 1, wherein a light absorbing material that absorbs light in a wavelength range of the light wave propagating through the optical waveguide is disposed in at least a part of an end surface of the substrate.
  7. The optical modulation device according to claim 6, wherein the light absorbing material is a carbon material, a black resin, or a metal filler.
  8. The optical modulation device according to claim 1, wherein the substrate is formed by laminating a plurality of plate bodies, and each plate body includes one layer or two adjacent layers among the optical waveguide layer, the first support layer, the second support layer, and the third support layer.
  9. An optical modulator comprising: the optical modulation device according to claim 1; a case for accommodating the optical modulation device; an optical fiber for inputting light into the optical modulation device; and an optical fiber for guiding light output from the optical modulation device to an outside of the case.
  10. An optical modulation module comprising: the optical modulation device according to claim 1; and a drive circuit for driving the optical modulation device.
  11. An optical transmission apparatus comprising: the optical modulator according to claim 9; and an electronic circuit for generating an electrical signal for causing the optical modulation device to perform a modulation operation.
  12. An optical transmission system comprising: the optical transmission apparatus according to claim 11; and an optical fiber transmission channel through which output light of the optical modulation device propagates.
  13. An optical transmission apparatus comprising: the optical modulation module according to claim 10; and an electronic circuit for generating an electrical signal for causing the optical modulation device to perform a modulation operation.
  14. An optical transmission system comprising: the optical transmission apparatus according to claim 13; and an optical fiber transmission channel through which output light of the optical modulation device propagates.
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