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### (54) EXERCISE MACHINES HAVING DAMPENER FOR REDUCING ACTUATOR BACKLASH

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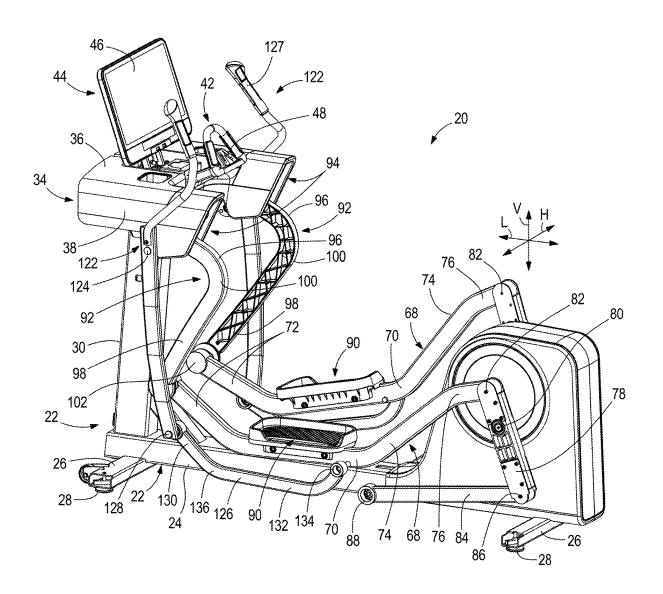
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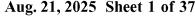
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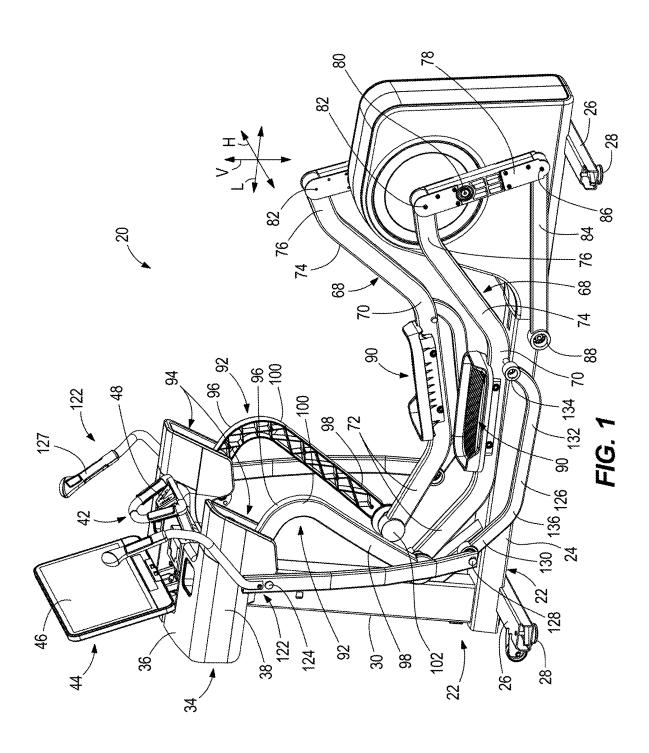
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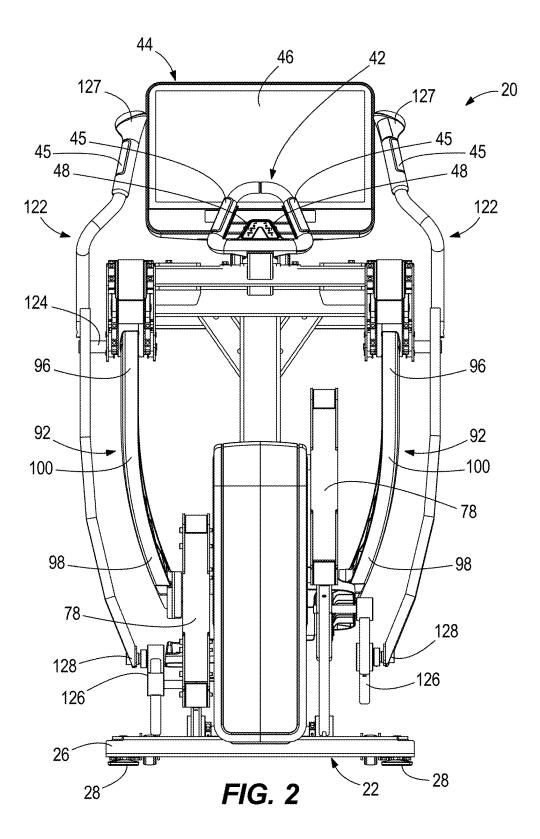
#### (57)ABSTRACT

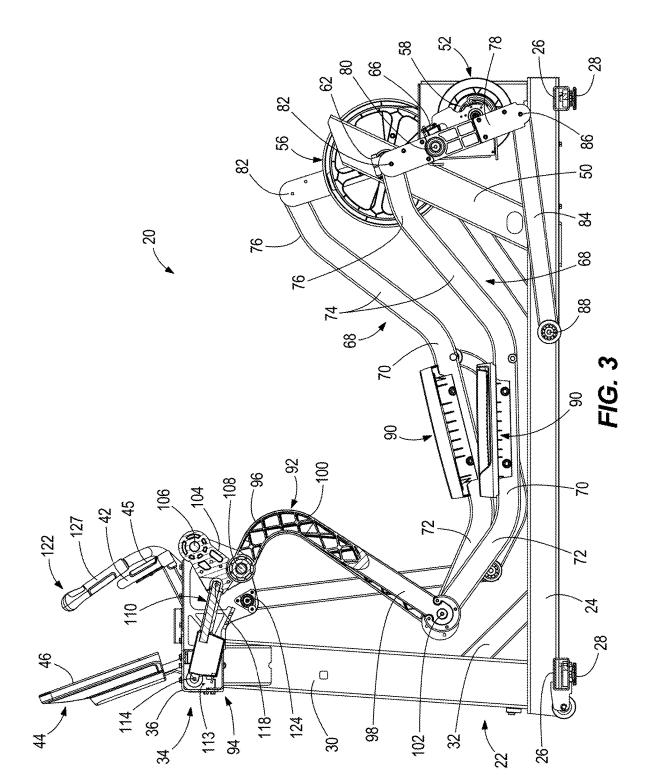
An exercise machine has a frame, a rocker arm operable to perform a striding exercise motion relative to the frame, an actuator coupling the rocker arm to the frame, the actuator being configured to adjust a position of the rocker arm relative to the frame to adjust an incline of the striding exercise motion, and a dampener configured to apply a preload force on the actuator to dampen reversing loads from the rocker arm and reduce backlash in the actuator.



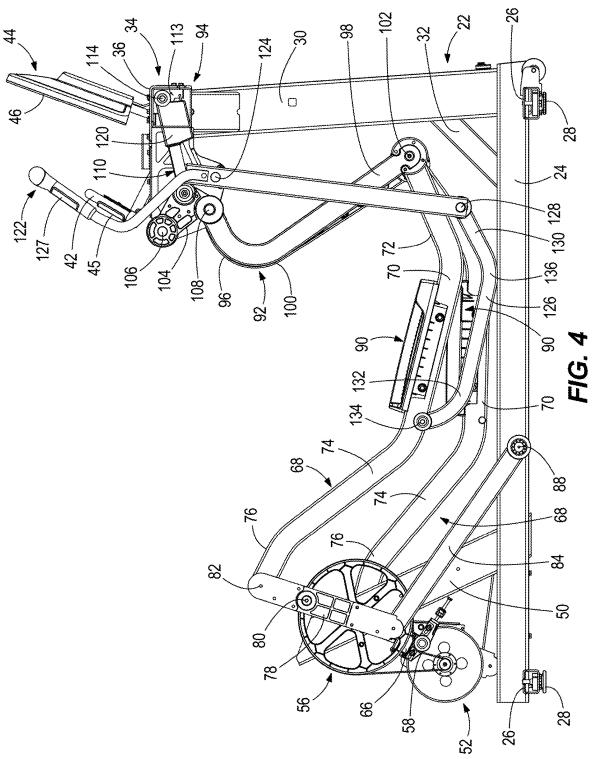


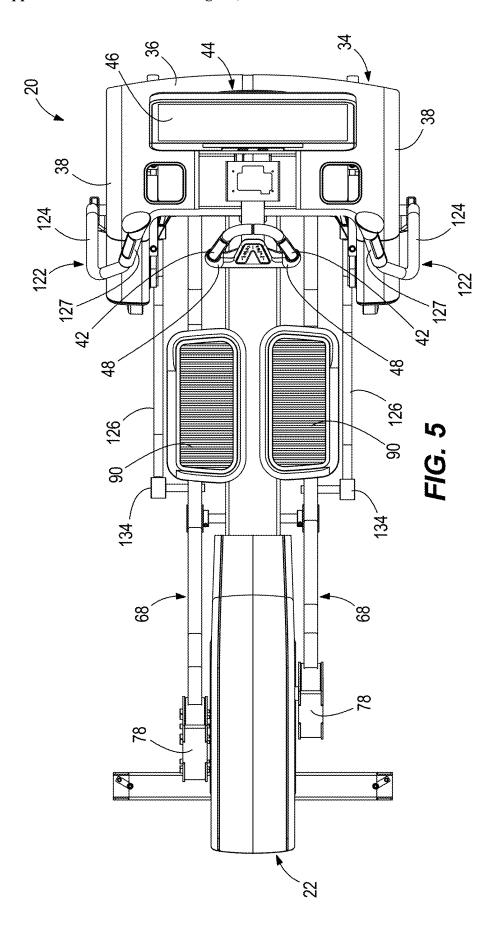


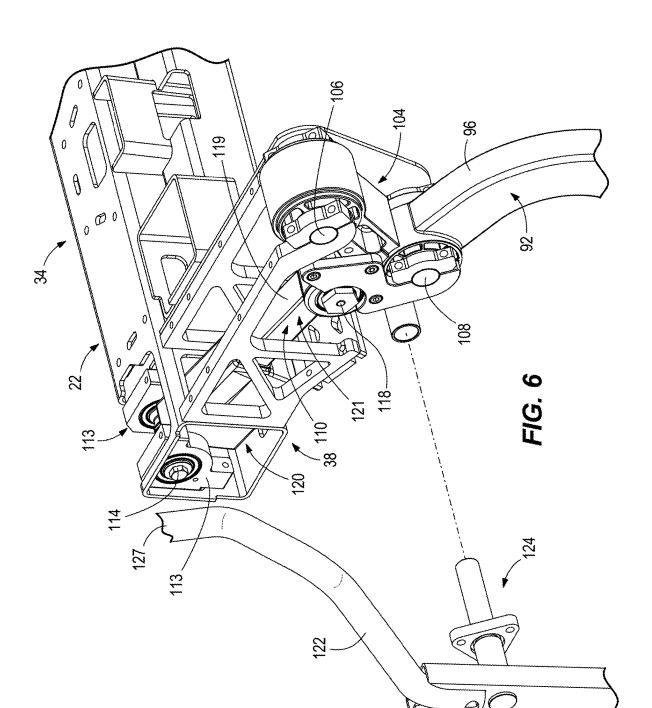




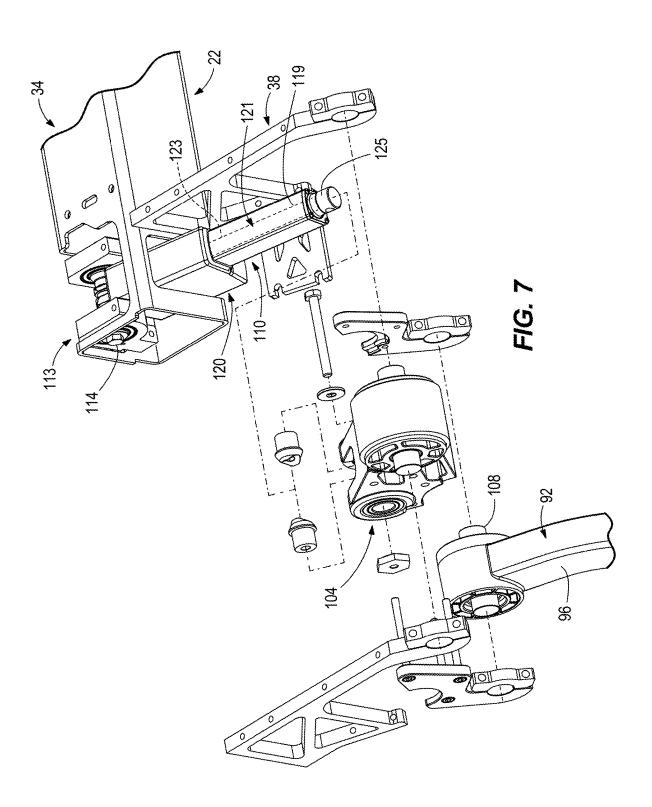


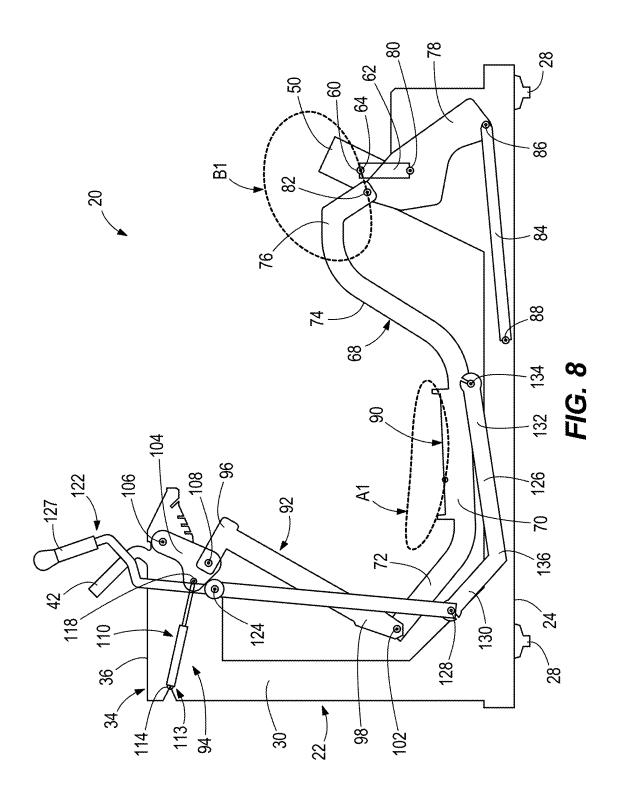


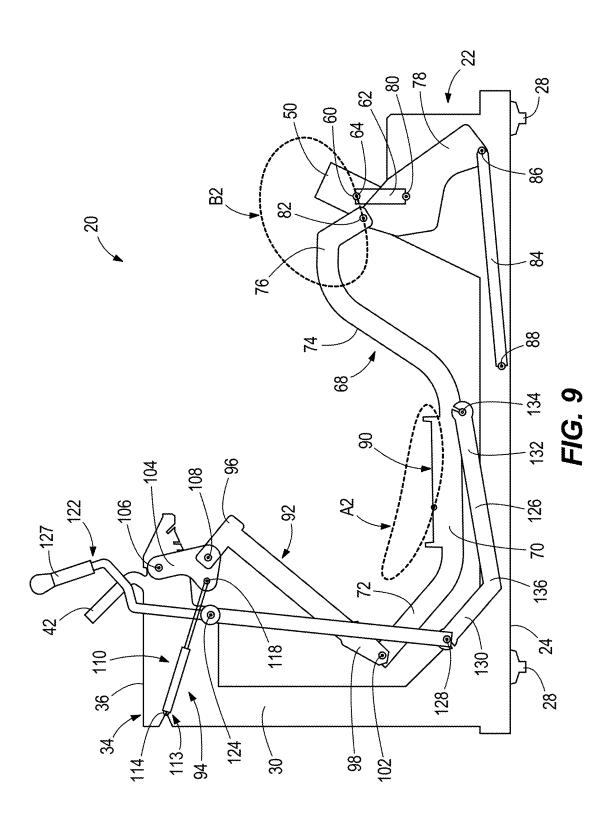


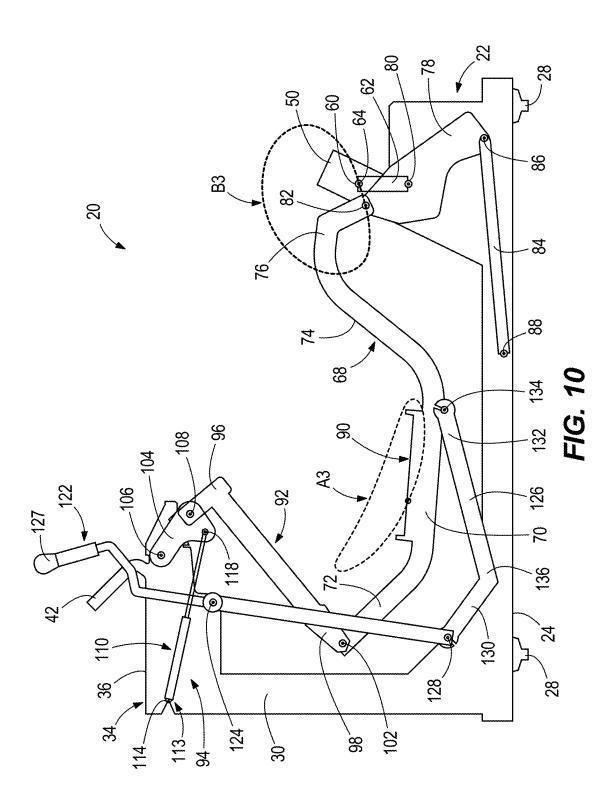


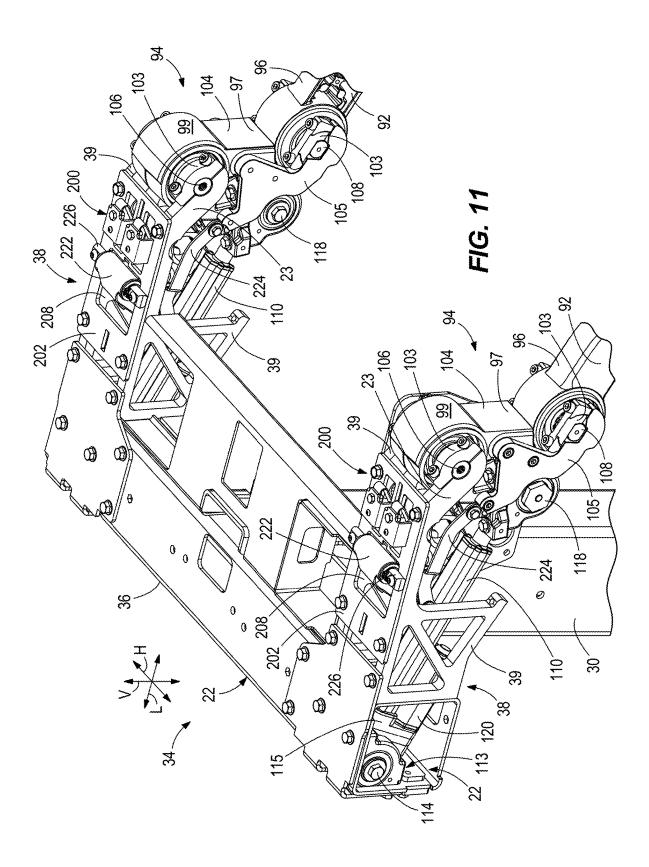


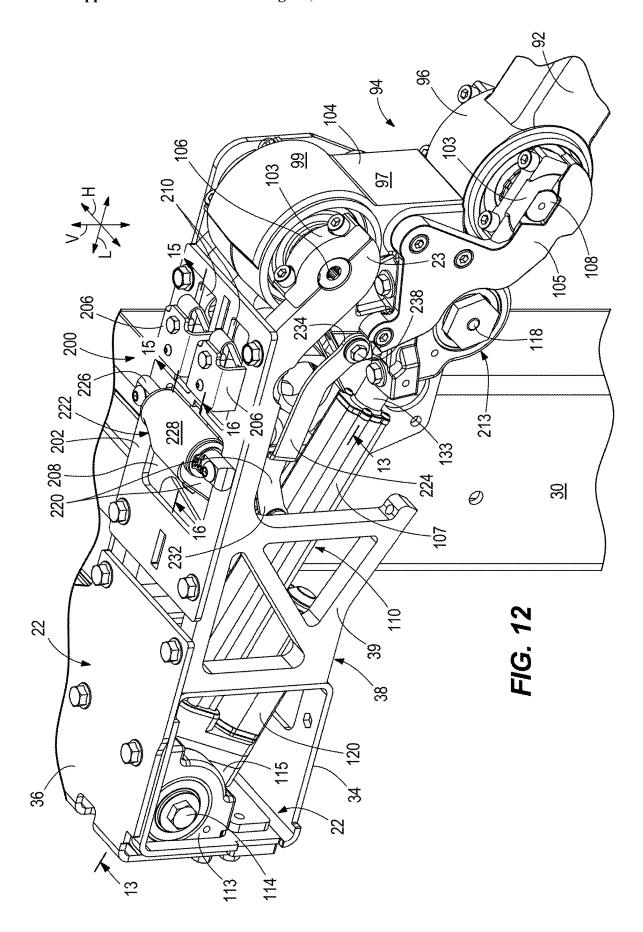


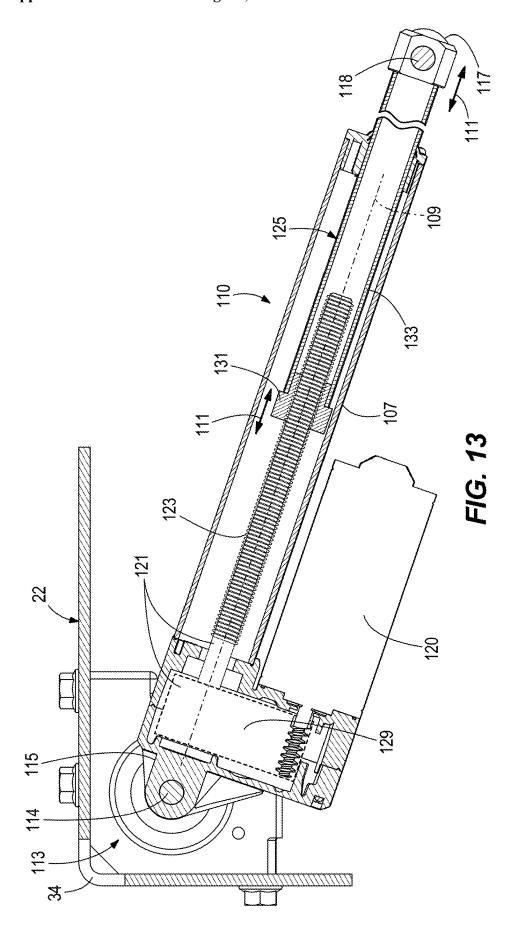


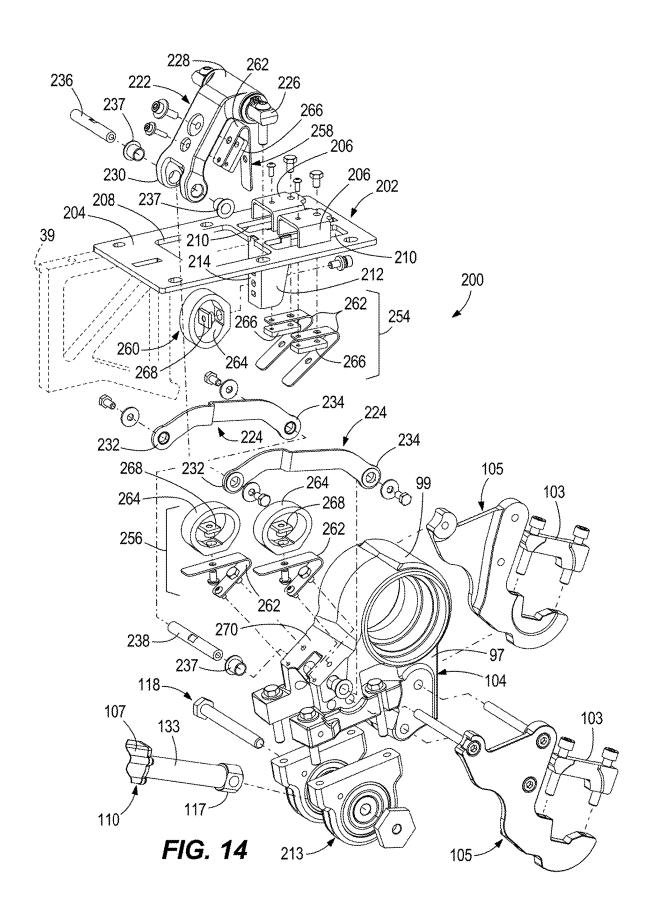


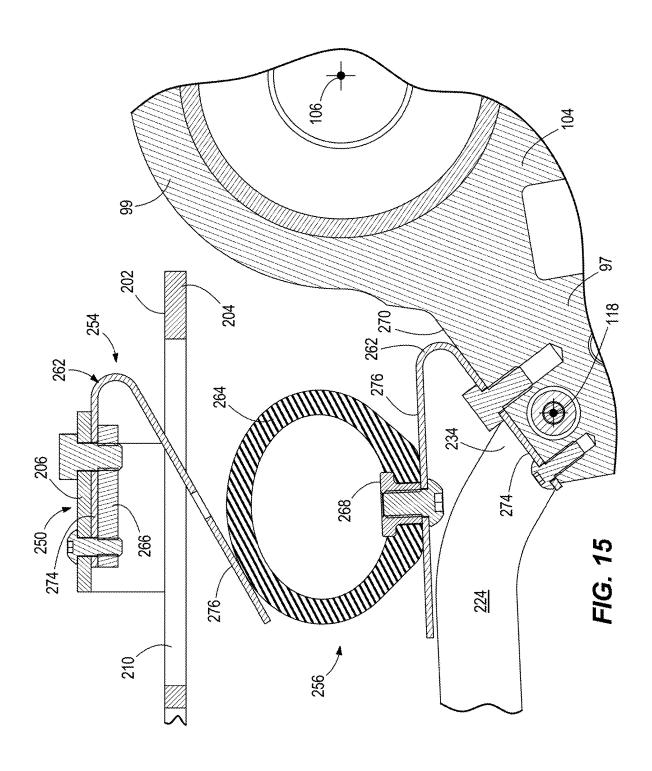


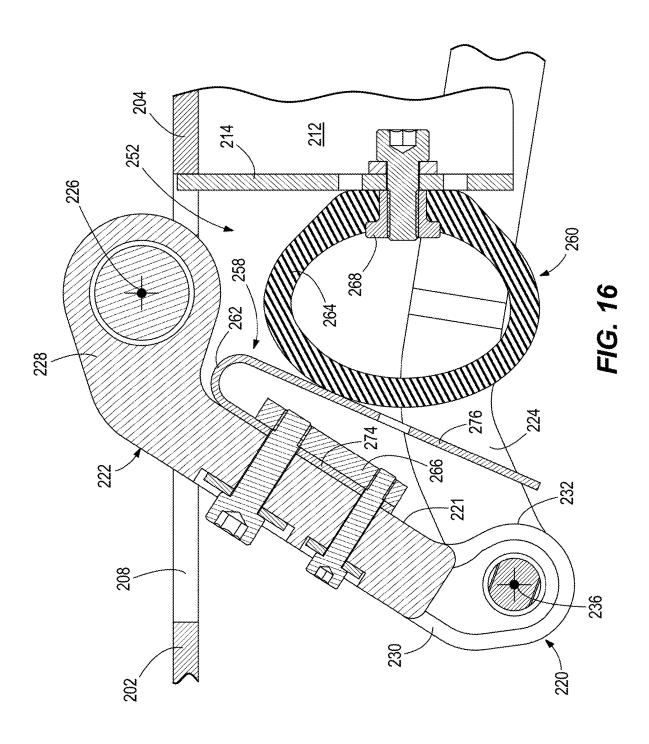


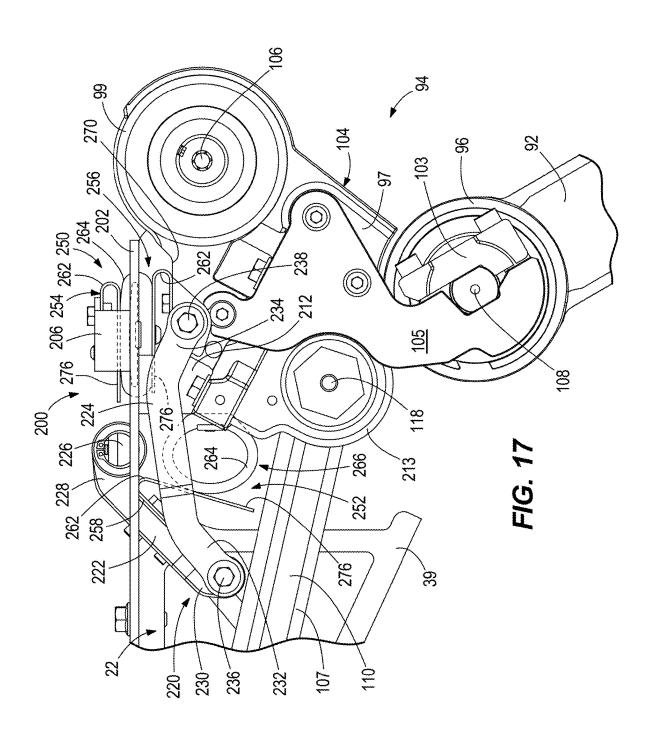


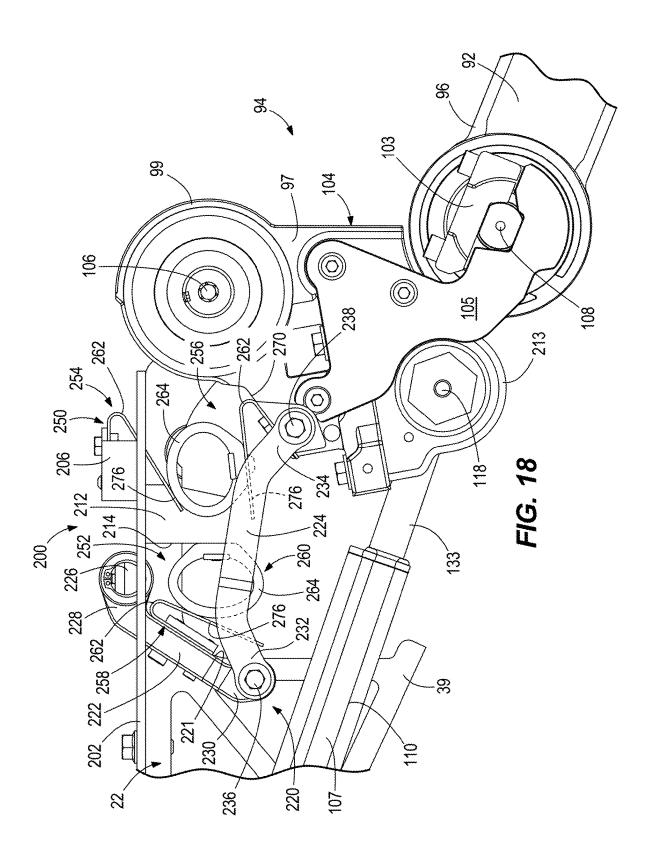


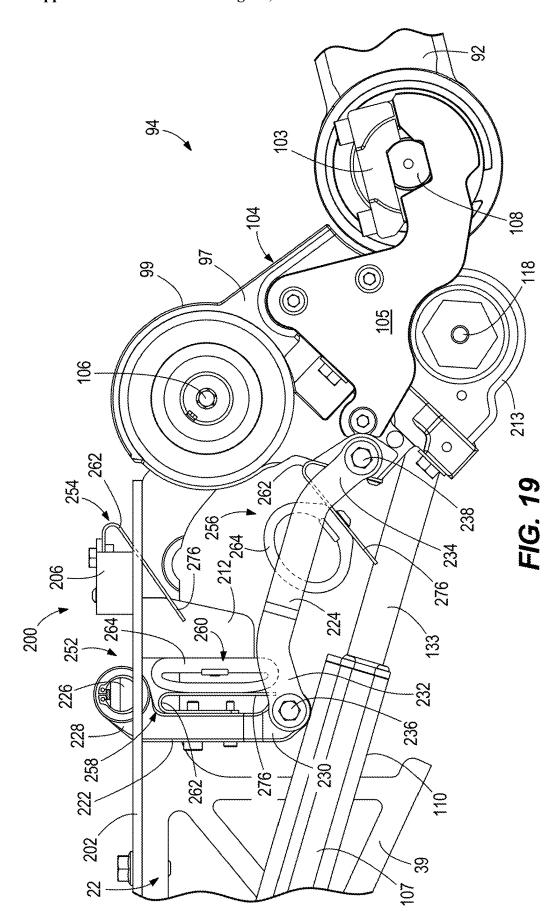


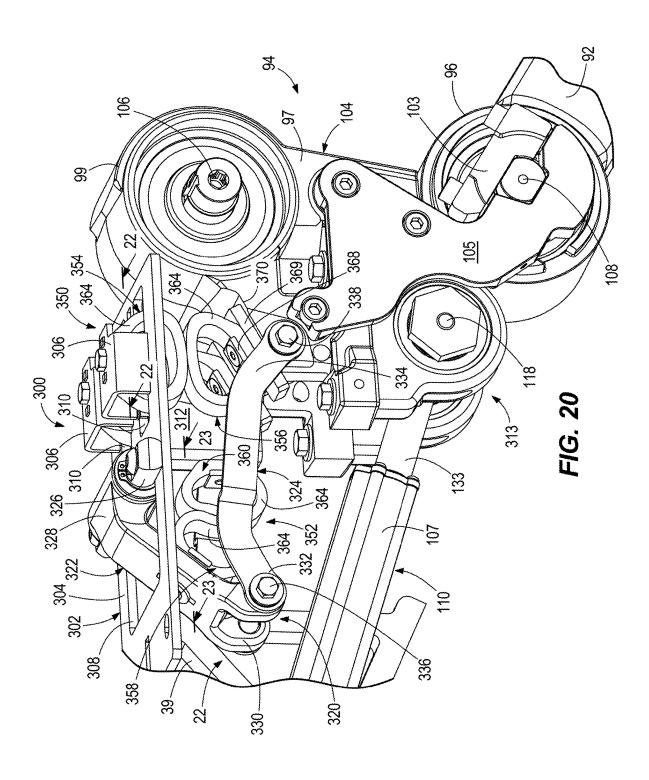


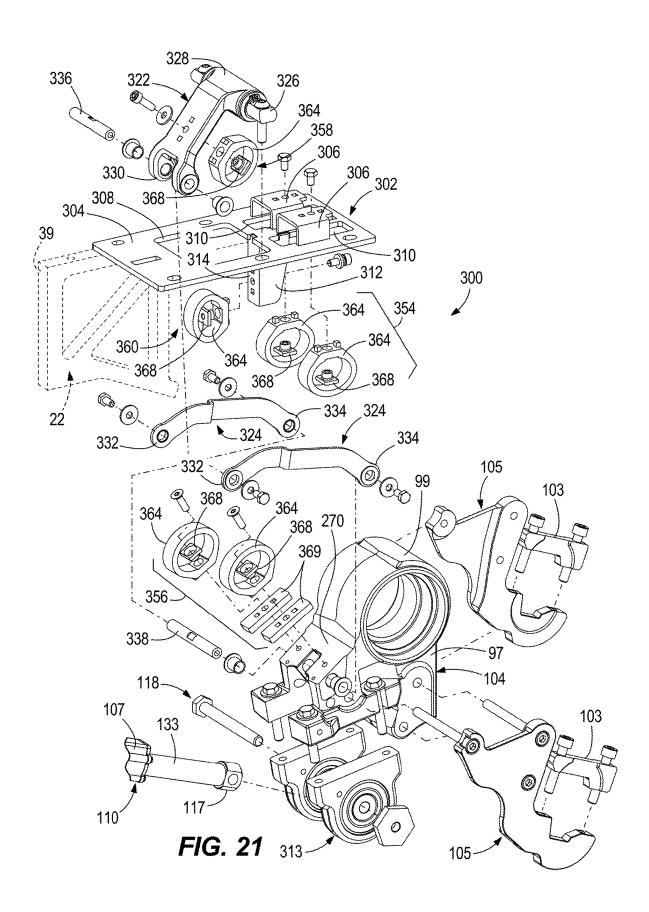


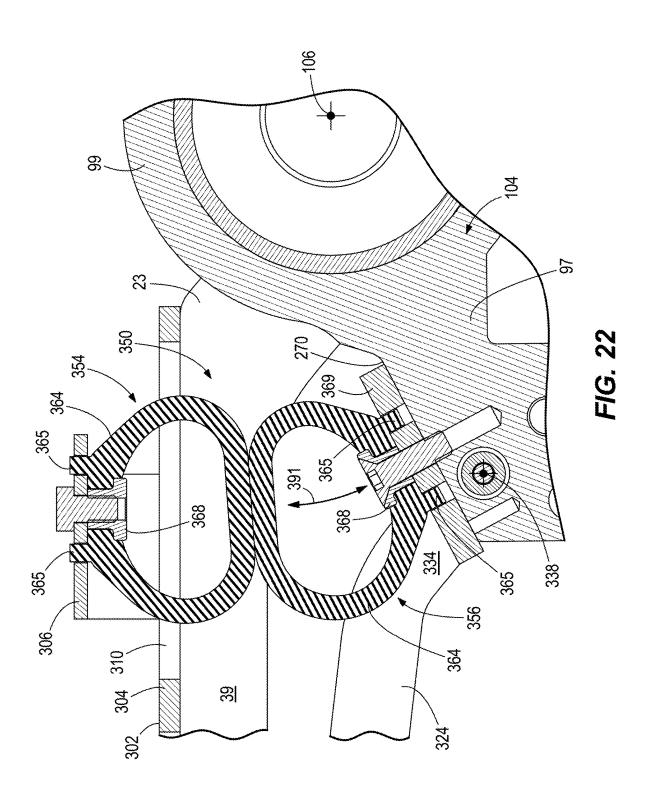


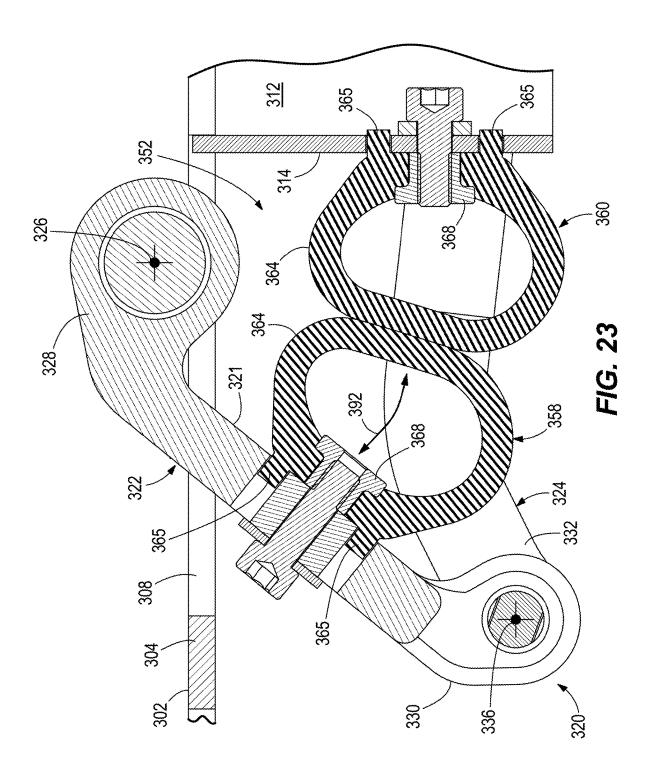


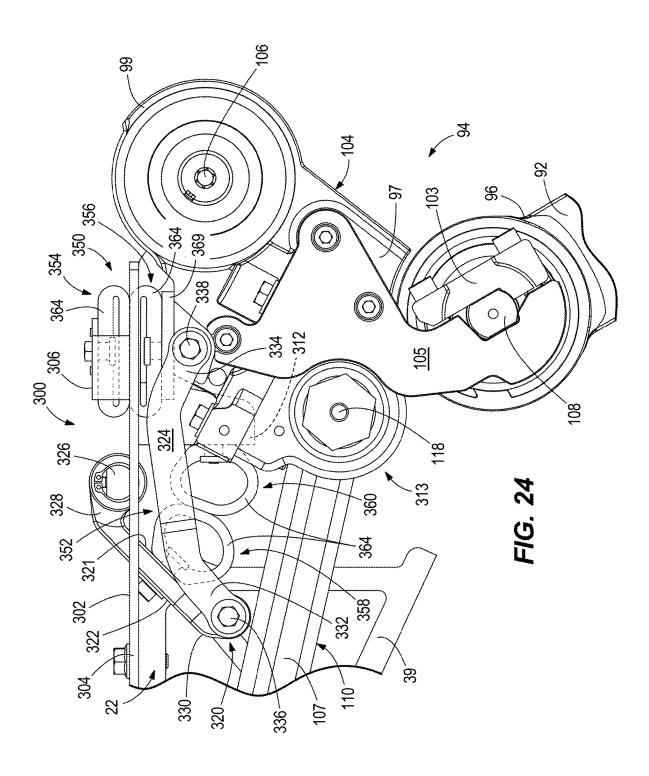


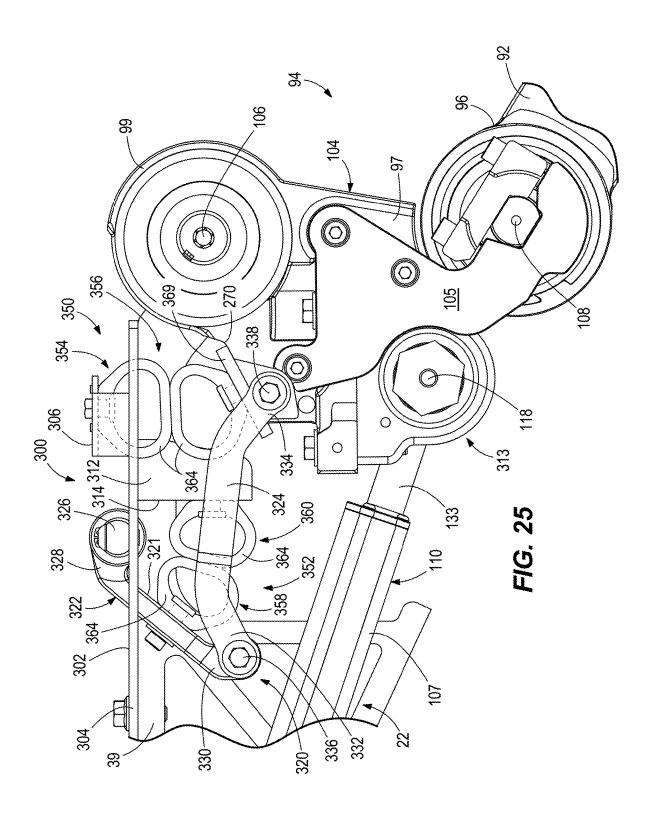


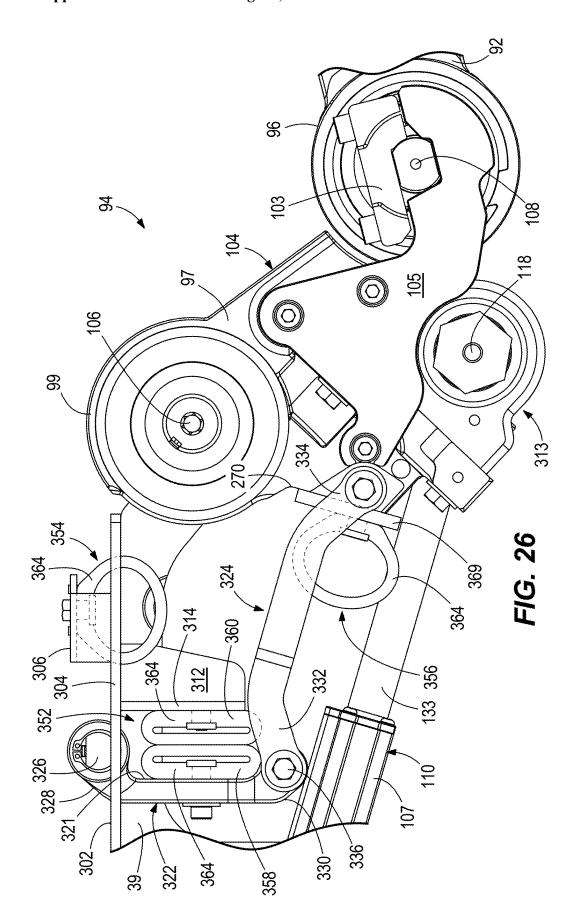


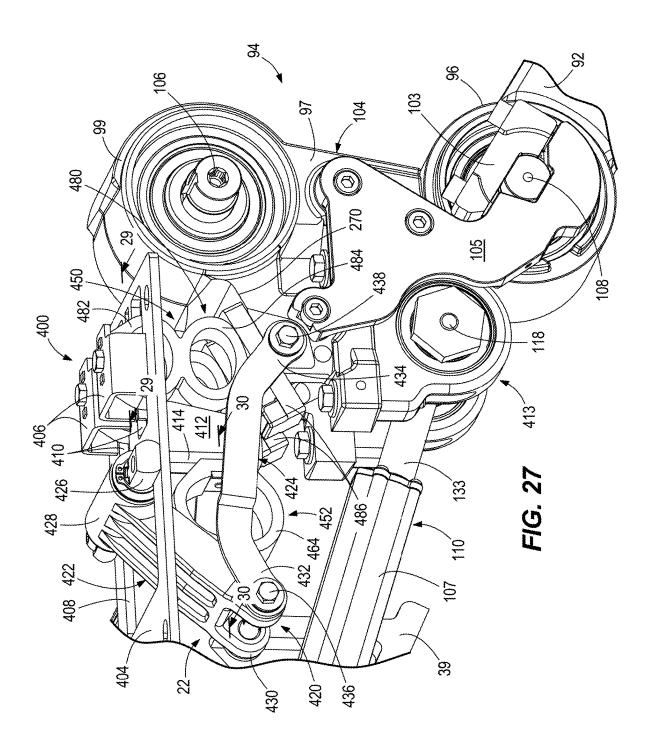


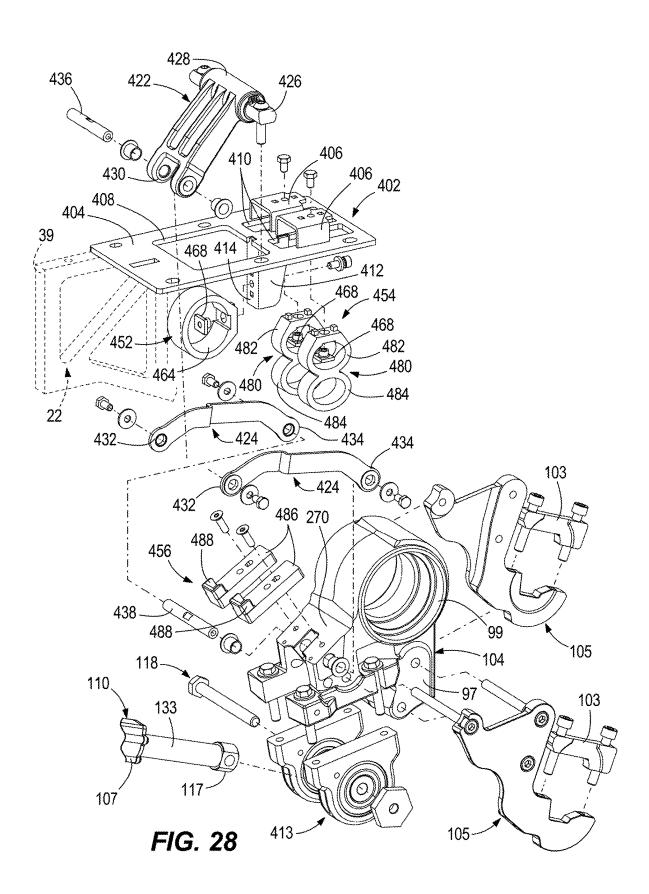


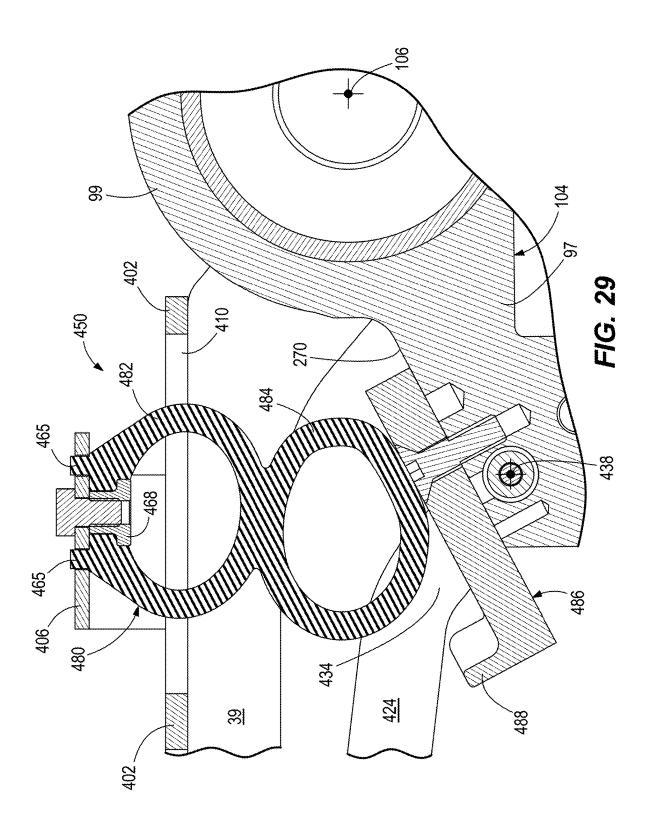


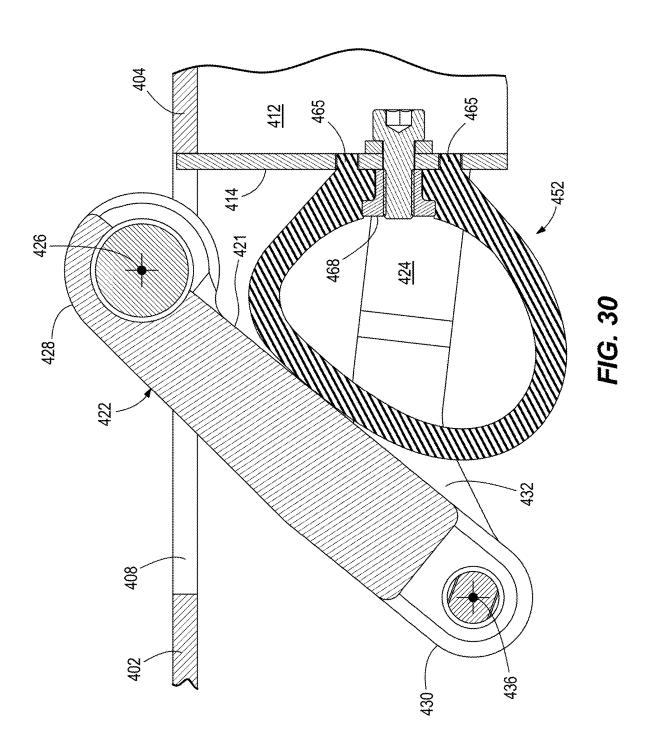


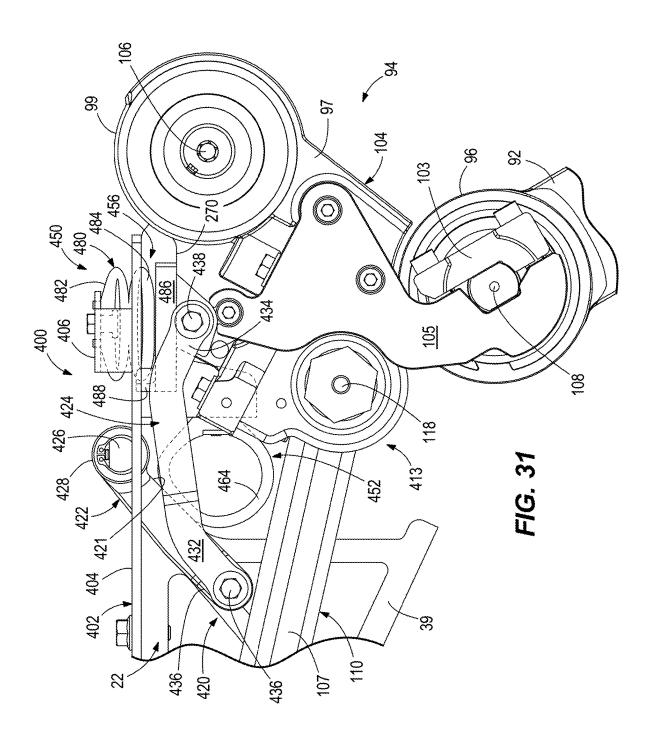


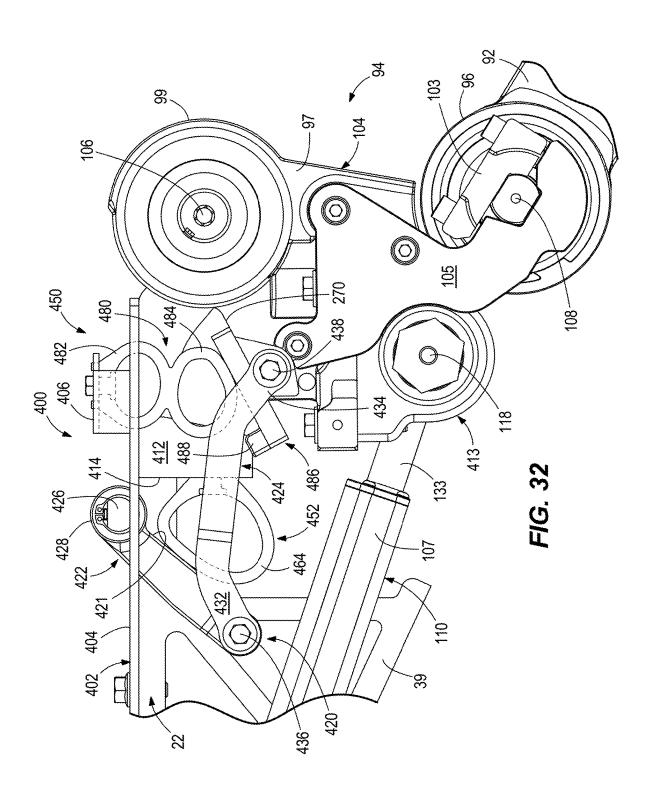


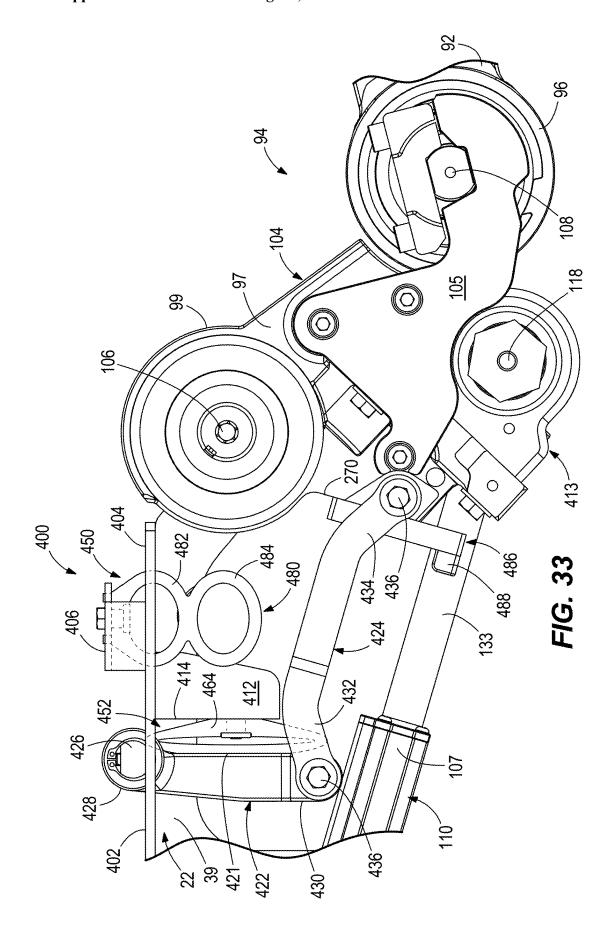


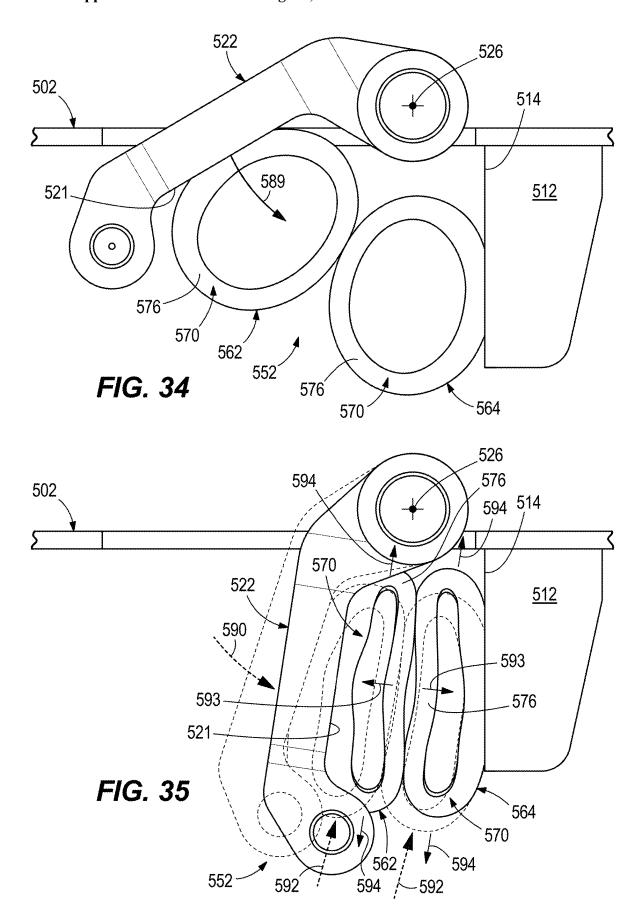












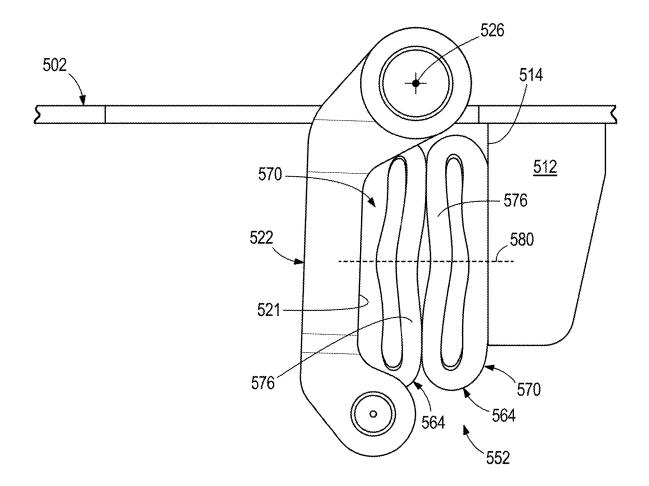
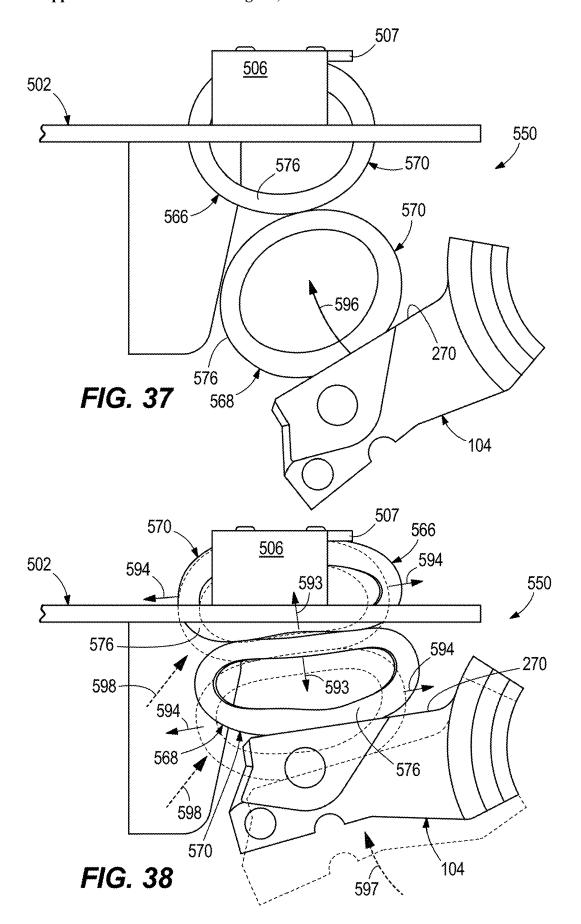
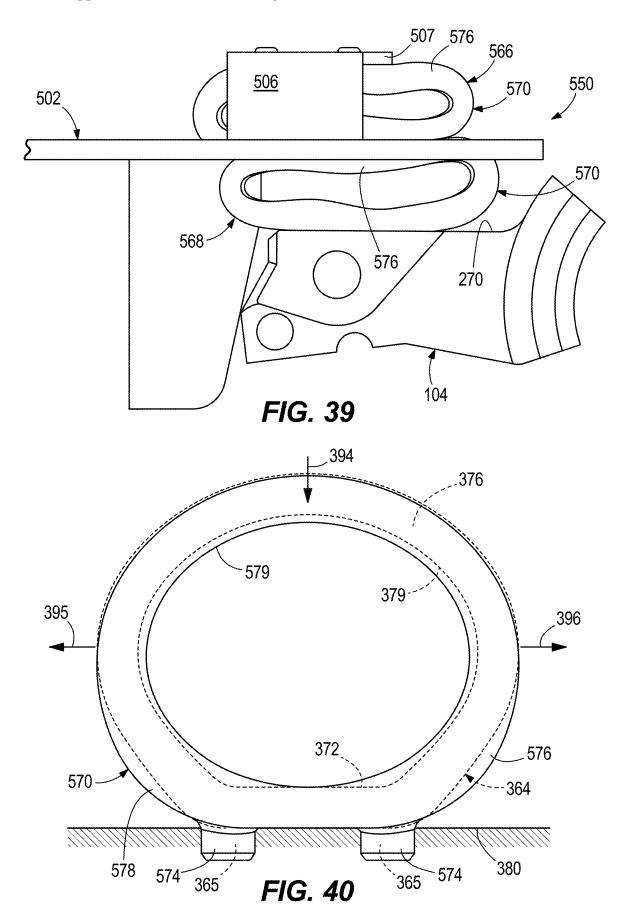


FIG. 36





## EXERCISE MACHINES HAVING DAMPENER FOR REDUCING ACTUATOR BACKLASH

# CROSS REFERENCE TO RELATED APPLICATION

[0001] This application claims the benefit of U.S. Provisional Patent Application No. 63/553,865, filed Feb. 15, 2024, which application is incorporated herein by reference in its entirety.

#### **FIELD**

[0002] The present disclosure relates to exercise equipment, for example personal exercise machines.

## BACKGROUND

[0003] U.S. Pat. Pub. No. 2023/0025399 is incorporated herein by reference and discloses an exercise machine for performing a striding exercise motion. The exercise machine has a frame, first and second pedal members, first and second foot pads on the first and second pedal members, respectively, wherein the first and second foot pads are configured to move in respective elliptical paths during the striding exercise motion, and first and second rocker arms. The first and second pedal members are pivotably coupled to the first and second rocker arms and move with the first and second rocker arms relative to the frame. An adjustment device pivotably couples the first and second rocker arms to the frame. The adjustment device is configured to actively adjust and set a position of the first and second rocker arms relative to the frame, respectively, which thereby changes an incline shape of the elliptical paths, respectively, during the striding exercise motion.

## **SUMMARY**

[0004] This Summary is provided to introduce a selection of concepts which are further described below in the Detailed Description. This Summary is not intended to identify key or essential features of the claimed subject matter, nor is it intended to be used as an aid in limiting the scope of the claimed subject matter.

[0005] In non-limiting examples disclosed herein, an exercise machine comprises a frame, a rocker arm operable to perform a striding exercise motion relative to the frame, and an actuator coupling the rocker arm to the frame. The actuator is configured to adjust a position of the rocker arm relative to the frame to adjust an incline of the striding exercise motion. A dampener is configured to apply a preload force on the actuator that dampens reversing loads from the rocker arm to thereby reduce backlash in the actuator.

[0006] In independent examples, the preload force may comprise a tension force. In independent examples, the preload force may comprise a compression force. The dampener may comprise a spring. The spring may comprise an elastomer. The spring may comprise a first spring member and a second spring member that is coupled to the first spring member.

[0007] In independent examples, the preload force may comprise at least one of a tension force and a compression force. The dampener may be configured to apply the at least one of the tension force and the compression force on the actuator. The actuator may be configured to extend and

retract, and the dampener may be configured to apply the compression force when the actuator is extended and to apply the tension force when the actuator is retracted. The dampener may configured to apply the preload force via at least one of the tension force and the compression force throughout movement of the exercise machine into and between a low-incline configuration and a high-incline configuration. The dampener may comprise a first spring configured to apply the tension force on the actuator and a second spring configured to apply the compression force on the actuator.

[0008] In independent examples, the actuator may comprise a linear actuator having a first end pivotably coupled to the frame and a second end pivotably coupled to the rocker arm. An incline link may pivotably couple the rocker arm to the frame, the second end of the linear actuator being pivotably coupled to the rocker arm via the incline link. The dampener may comprise a spring configured to bias the incline link relative to the frame to apply said preload force as a tension force on the actuator. The dampener may comprise a spring configured to bias the incline link relative to the frame to apply said preload force as a compression force on the actuator.

[0009] In independent examples, the dampener may comprise a first spring and a second spring, said first spring and said second spring being configured to abut each other to apply the preload force. In independent examples, one of the first spring and the second spring travels along a non-linear path relative to the other one of the first spring and the second spring, and at least one of the first spring and the second spring has a shape configured to generally maintain alignment between the first spring and the second spring as the first spring and the second spring arc compressed along the non-linear path.

[0010] In non-limiting examples disclosed herein, an exercise machine comprises a frame, a rocker arm operable to perform a striding exercise motion relative to the frame, and an incline link pivotably coupling the rocker arm to the frame. A linear actuator has a first end pivotably coupled to the frame and a second end pivotably coupled to the incline link, and the linear actuator is extendible and retractable to adjust a position of the rocker arm relative to the frame. A dampener is configured to apply at least one of a tension force and a compression force on the linear actuator that dampens reversing loads from the rocker arm to thereby reduce backlash in the linear actuator.

[0011] In independent examples, the dampener may be configured to apply both the tension force and the compression force on the linear actuator. The linear actuator may be configured to extend and retract, and said dampener configured to apply the compression force when the linear actuator is extended and to apply the tension force when the linear actuator is retracted. The dampener may comprise a first spring configured to apply the tension force on the linear actuator and a second spring configured to apply the compression force on the linear actuator. The dampener may comprise a spring that is compressed between the incline link and the frame upon retraction of the linear actuator, which applies the tension force on the linear actuator.

[0012] In independent examples, a pivot linkage may be coupled to the frame and to the incline link, and the dampener may comprise a spring that is compressed between the pivot linkage and the frame upon extension of the linear actuator, which applies the compression force on

the linear actuator. The pivot linkage may comprise a spring arm and a connecting link that are pivotably coupled together.

[0013] In independent examples, the dampener may comprise a spring that is compressed between the incline link and the frame upon retraction of the linear actuator, which applies the tension force on the linear actuator, and a pivot linkage may be coupled to the frame and to the incline link. The dampener may comprise a spring that is compressed between the pivot linkage and the frame upon extension of the linear actuator, which applies the compression force on the linear actuator.

[0014] In independent examples, the dampener may comprise a low-incline dampener configured to dampen the reversing loads when the exercise machine is in a low-incline configuration and a high-incline dampener configured to dampen the reversing loads when the exercise machine is in a high-incline configuration. The low-incline dampener may be configured to apply the tension force and said high-incline dampener being configured to apply the compression force.

## BRIEF DESCRIPTION OF THE DRAWINGS

[0015] The present disclosure is described with reference to the following Figures. The same numbers are used throughout the Figures to reference like features and like components. Unless otherwise specifically noted, articles illustrated in the drawings are not necessarily drawn to scale. [0016] FIG. 1 is a side perspective view of a first non-limiting example of an exercise machine having certain features removed such as support column, base member and stabilizer covers.

[0017] FIG. 2 is a rear view thereof having a front stabilizer covers removed.

[0018] FIG. 3 is a side view thereof having front and rear covers and stabilizer covers removed.

[0019] FIG. 4 is an opposite side view thereof having front and rear covers and stabilizer covers removed.

[0020] FIG. 5 is a top view thereof having base member and stabilizer covers removed.

[0021] FIG. 6 is an exploded view of portions of the front of the machine.

[0022] FIG. 7 is another exploded view of the portions illustrated in FIG. 6.

[0023] FIG. 8 is a schematic view showing a low-incline elliptical path of travel of foot pads on the machine.

[0024] FIG. 9 is a schematic view showing a medium-incline elliptical path of travel of foot pads on the machine. [0025] FIG. 10 is a schematic view showing a high-incline elliptical path of travel of foot pads on the machine.

[0026] FIG. 11 is a perspective view of an embodiment of the bridge of an exercise machine according to the present disclosure.

[0027] FIG. 12 is a perspective view of an adjustment device located in the bridge of FIG. 11, the adjustment device including a dampener.

[0028] FIG. 13 is a view of section 13-13, taken in FIG.

[0029] FIG. 14 is an exploded perspective view of the dampener and portions of the adjustment device of FIG. 12. [0030] FIG. 15 is a view of section 15-15, taken in FIG. 13.

[0031] FIG. 16 is a view of section 16-16, taken in FIG. 12.

[0032] FIG. 17 is a side elevation view of the bridge of FIG. 12 in which the exercise machine is in a low-incline configuration, wherein a bridge arm members are removed to expose the dampener and portions of the adjustment device.

[0033] FIG. 18 is the side elevation view of the bridge of FIG. 17, wherein the exercise machine is in a medium-incline configuration.

[0034] FIG. 19 is the side elevation view of the bridge of FIG. 18, wherein the exercise machine is in a high-incline configuration.

[0035] FIG. 20 is a perspective view of the bridge of an exercise machine having another embodiment of a dampener.

[0036] FIG. 21 is an exploded perspective view of the dampener and portions of an adjustment device of FIG. 20. [0037] FIG. 22 is a view of section 22-22, taken in FIG. 20.

[0038] FIG. 23 is a view of section 23-23, taken in FIG. 20.

[0039] FIG. 24 is a side elevation view of the bridge of FIG. 20 in which the exercise machine is in a low-incline configuration, wherein a bridge arm members are removed to expose the dampener and portions of an adjustment device.

[0040] FIG. 25 is the side elevation view of the bridge of FIG. 24, wherein the exercise machine is in a medium-incline configuration.

[0041] FIG. 26 is the side elevation view of the bridge of FIG. 25, wherein the exercise machine is in a high-incline configuration.

[0042] FIG. 27 is a perspective view of the bridge of an exercise machine with another embodiment of a dampener. [0043] FIG. 28 is an exploded perspective view of the dampener and portions of an adjustment device of FIG. 27 [0044] FIG. 29 is a view of section 29-29, taken in FIG. 27.

[0045] FIG. 30 is a view of section 30-30, taken in FIG. 27.

[0046] FIG. 31 is a side elevation view of the bridge of FIG. 27 in which the exercise machine is in a low-incline configuration, wherein a bridge arm members are removed to expose the dampener and portions of an adjustment device.

[0047] FIG. 32 is the side elevation view of the bridge of FIG. 31, wherein the exercise machine is in a medium-incline configuration.

[0048] FIG. 33 is the side elevation view of the bridge of FIG. 32, wherein the exercise machine is in a high-incline configuration.

[0049] FIG. 34 is a partial side elevation view of an embodiment of a high-incline dampener having spring members in which the exercise machine is in a low-incline configuration.

[0050] FIG. 35 is the partial side elevation view of FIG. 34 in which the exercise machine is in a medium-incline configuration.

[0051] FIG. 36 is the partial side elevation view of FIG. 35 in which the exercise machine is in a high-incline configuration

[0052] FIG. 37 is a partial side elevation view of an embodiment of a low-incline dampener having spring members in which the exercise machine is in a high-incline configuration.

[0053] FIG. 38 is the partial side elevation view of FIG. 37 in which the exercise machine is in a medium-incline configuration.

[0054] FIG. 39 is the partial side elevation view of FIG. 38 in which the exercise machine is in a low-incline configuration.

[0055] FIG. 40 is a side schematic view comparing embodiments of a spring member for a dampener.

#### DETAILED DESCRIPTION OF THE DRAWINGS

[0056] FIGS. 1-5 illustrate a personal exercise machine 20 for performing a striding exercise motion. The machine 20 extends from front to back in a longitudinal direction L, from top to bottom in a vertical direction V, and from side to opposite side in a lateral or horizontal direction H. The machine 20 is generally symmetrical in the horizontal direction H, so that the components on one side of the machine 20 are the same as or are mirror images of the components on the opposite side of the machine 20. As such, the descriptions provided below regarding components on one side of the machine 20 equally apply to the components on the opposite side of the machine 20.

[0057] The machine 20 has a frame 22 including a longitudinally extending base member 24. Horizontally extending stabilizer members 26 extend from the front and rear of the base member 24 and prevent the machine 20 from tipping over in the horizontal direction H. Each stabilizer member  $26\ \mathrm{has}\ \mathrm{feet}\ 28\ \mathrm{for}\ \mathrm{supporting}\ \mathrm{the}\ \mathrm{frame}\ 22\ \mathrm{above}\ \mathrm{the}\ \mathrm{ground}.$ The frame 22 has a forward support column 30 which extends vertically upwardly from the front of the base member 24. An angular gusset 32 braces and supports the forward support column 30 relative to the base member 24. A bridge 34 is mounted on top of the forward support column 30. The bridge 34 has a horizontally extending body 36 with opposing first and second arms 38 extending rearwardly therefrom. As such, the bridge 34 generally has a U-shape and defines an "activity zone" between the arms 38 for the user's body and/or arms during performance of the striding exercise motion. A generally trapezoidal-shaped stationary handlebar 42 is rigidly mounted on the body 36 between the arms 38 and is for manually grasping by a user operating the machine 20.

[0058] A user console 44 is mounted to and extends generally upwardly from the bridge 34. The console 44 includes a display screen 46 oriented towards the user operating the machine 20. As conventional, the console 44 can include a processor and memory and be configured for controlling various devices associated with the machine 20, including for control of resistance and/or incline as for example will be further described herein below. The display screen 46 optionally can be a touch screen wherein the user operating the machine 20 can manually touch the screen to input commands to the console 44 for controlling the machine 20. Optionally, input buttons 48 are located on the stationary handlebar 42 and are for manually inputting commands to the console 44. Optionally, input buttons can be located elsewhere such as on the upper ends of hand grips 127, described herein below. Input commands entered via the display screen 46 and/or input buttons 48 can for example include an increase or decrease in resistance of the machine 20 and/or increase or decrease in incline of the machine 20, and/or the like. Optionally biomechanical sensors 45 can be provided on the stationary handlebar 42 and/or on hand grips 127 for sensing heart rate of the user when the user manually grasps the stationary handlebar 42 and/or the hand grips 127.

[0059] At the rear of the machine 20, the frame 22 further includes a rear support column 50 which extends angularly upwardly and rearwardly from the rear of the base member 24. A resistance mechanism 52 is mounted to the rear support column 50, including for example via a rear frame plate (not illustrated in FIG. 4) mounted to the rear support column 50 and/or the base member 24. The type and configuration of the resistance mechanism 52 is conventional and can vary from what is illustrated and described. In the illustrated example the resistance mechanism 52 is a hybrid generator-brake configured to provide a resistance to a striding motion performed on the machine 20, as will be further described herein below, and also configured to generate power based upon the striding motion, for example for powering the console 44. A suitable resistance mechanism is the "FB Six Series" sold by Chi Hua. The resistance mechanism 52 is connected to a pulley wheel 56 by a belt 58 and is configured so that rotation of the pulley wheel 56 rotates the resistance mechanism 52. The pulley wheel 56 is connected to the rear support column 50 by a center shaft 60 (see FIG. 8). The pulley wheel 56 and center shaft 60 are fixed relative to each other such that these components rotate together.

[0060] At the rear of the machine 20, radially opposed crank arms 62 have radially inner ends keyed to (fixed to) the center shaft 60 so that the crank arms 62 remain radially opposed to each other (i.e., 180 degrees apart) and so that rotation of the crank arms 62 and center shaft 60 causes rotation of the pulley wheel 56 about a pulley wheel pivot axis 64 defined by the center shaft 60. Rotation of the pulley wheel 56 is resisted by the resistance mechanism 52 via an electro magnet 66, as is conventional and well known in the art.

[0061] The machine 20 further has first and second pedal members 68 centrally located on opposite sides of the frame 22. The pedal members 68 are elongated in the longitudinal direction L, each having a central portion 70, a front portion 72 which extends generally forwardly and upwardly from the central portion 70, and a rear portion 74 which extends generally rearwardly and upwardly from the central portion 70 to a tail portion 76 which extends rearwardly from the rear portion 74 and generally but not necessarily parallel to the central portion 70.

[0062] At the rear of the machine 20, first and second elongated stride links 78 are freely rotatably (pivotably) coupled to the radially outer ends of the opposed crank arms 62, by for example bearings, at a stride link-crank arm pivot axis 80. Each stride link 78 has a first end which is pivotably coupled to a respective tail portion 76 of a pedal member 68 at a stride link-pedal member pivot axis 82. Each stride link 78 has an opposite, second end which is pivotably coupled to a distal or rear end of an elongated idler link 84 at a stride link-idler link pivot axis 86. The opposite, proximal or front end of the idler link 84 is pivotably coupled to the base member 24 at an idler link-base member pivot axis 88. As illustrated in the figures, the stride link-crank arm pivot axis 80 is located along the stride link 78 between the stride link-pedal member pivot axis 82 and stride link-idler link pivot axis 86 and in particular is closer to the stride linkpedal member pivot axis 82 than the stride link-idler link

pivot axis 86. In other examples, the pivot axis 80 is at the center of the stride link 78 or closer to the pivot axis 86.

[0063] First and second foot pads 90 are supported on the central portions 70 of the first and second pedal members 68. The foot pads 90 are for supporting the user's feet during performance of the elliptical striding motion and travel along an elliptical path which is incline adjustable, as will be further described herein below.

[0064] The machine 20 further has first and second rocker arms 92 which are pivotably coupled to the frame 22 by an adjustment device 94, which will be further described herein below. The type and configuration of the adjustment device 94 can vary. The rocker arms 92 have an upper end portion 96, a lower end portion 98, and an elbow portion 100 located between the upper end portion 96 and the lower end portion 98 so that the upper end portion 96 and lower end portion 98 extend at an angle relative to each other. The lower end portions 98 are pivotably coupled to the front portion 72 of the pedal members 68 at a rocker arm-pedal member pivot axis 102 so that the pedal members 68 are pivotably movable relative to the rocker arms 92 and also so that pivoting of the rocker arms 92 relative to the frame 22 causes commensurate pivoting and/or translating of the pedal members 68 relative to the frame 22, i.e., so that these components pivot and/or translate together relative to the frame 22.

[0065] Referring to FIGS. 3, 4, 6 and 7, the adjustment device 94 is located in the bridge 34 and extends into the noted arms 38 on both sides of the activity zone. The adjustment device 94 is specially configured to facilitate selective adjustment and setting of a position of the rocker arms 92 relative to the frame 22, respectively, specifically the position of pivot axis 108, which thereby changes an incline shape of elliptical paths of travel of the foot pads 90, respectively, during the striding exercise motion, as will be further described herein below. The adjustment device 94 can be controlled by the noted controller based upon a stored exercise program or based upon an input by the operator to the console 44. For example this can be controlled via touch screen, input buttons 48 on the stationary handlebar 42 and/or input buttons on the upper ends of hand grips 127. As will be evident from the illustrated examples and the following description, the type and configuration of the adjustment device 94 can vary.

[0066] In the first example illustrated in FIGS. 1-10, the adjustment device 94 includes first and second incline links 104 which pivotably couple the upper end portion 96 of the rocker arms 92 to the frame 22. More specifically, the incline links 104 have an upper portion which is pivotably coupled to the frame 22 at an incline link-frame pivot axis 106. The incline links 104 further have a lower portion which is pivotably coupled to the upper end portion 96 of the rocker arm 92 at an incline link-rocker arm pivot axis 108 which is located generally below the incline link-frame pivot axis 106. Conventional bearings support the noted couplings so that the incline links 104 are pivotable relative to the noted axes 106. 108.

[0067] The adjustment device 94 is configured to pivot the first and second incline links 104 relative to the frame 22 (i.e., about the incline link-frame pivot axis 106) to thereby adjust and set the position of the rocker arms 92 relative to the frame 22, in particular to adjust and set the position of the incline link-rocker arm pivot axis 108 relative to the frame 22 (i.e., about the incline link-frame pivot axis 106). In the illustrated example, the adjustment device 94 includes

first and second linear actuators 110. Note that the type of linear actuator 110 can vary from what is illustrated and described. In the illustrated example, the linear actuator 110 includes an electro-mechanical linear actuator, which has an electric gearmotor 120, a leadscrew assembly 121 and, a leadnut and tube assembly 125 (see FIGS. 6, 7, and 13). As illustrated in FIG. 13, the linear actuator 110 has a body 107 (i.e., the housing 119) with a forward end 115 pivotably coupled to the bridge 34 of the frame 22 by a trunnion assembly 113, particularly at an actuator-bridge pivot axis 114. The linear actuator 110 has an opposite, rear end 117 at a distal end of a tube 133 of the leadnut and tube assembly 125 that is pivotably coupled to the incline link 104 at an actuator-incline link pivot axis 118 (sec FIGS. 6 and 13). A conventional bearing, which is best seen in exploded view in FIG. 7, supports the coupling at the actuator-incline link pivot axis 118. The actuator-incline link pivot axis 118 is offset relative to the incline link-frame pivot axis 106 and the incline link-rocker arm pivot axis 108. In the illustrated non-limiting example, the incline link 104 is a generally triangular plate member wherein the incline link-frame pivot axis 106, incline link-rocker arm pivot axis 108 and actuator-incline link pivot axis 118 are located at the respective three apexes of the triangular shape.

[0068] The gearmotor 120, leadscrew assembly 121, and leadnut and tube assembly 125 are configured to lengthen or shorten the linear actuator 110 upon an input command from the noted controller, which can be based upon an operator input to the console 44 or based upon a program in the noted controller, as described herein above. Operation of the gearmotor 120 in a first direction rotates the leadscrew 123 of the leadscrew assembly 121 in the first direction which causes the leadnut and tube assembly 125 to travel outwardly along the leadscrew 123 and outwardly relative to the housing 119 of linear actuator 110, thus lengthening the linear actuator 110. Operation of the gearmotor 120 in an opposite, second direction oppositely rotates the leadscrew 123 in the second direction which cause the leadnut and tube assembly 125 to retract inwardly relative to the housing 119, thus shortening the linear actuator 110. Thus, the linear actuator 110 is configured to extend and retract the leadnut and tube assembly 125 relative to the actuator body 107 (i.e., the housing 119), for example along the axis 109 and in the direction of arrows 111 in FIG. 13. Due to the relative locations of the incline link-frame pivot axis 106, incline link-rocker arm pivot axis 108, actuator-bridge pivot axis 114, and actuator-incline link pivot axis 118, extension of the linear actuator 110 pivots the incline link 104 rearwardly along an arc relative to the bridge 34, which moves the incline link-rocker arm pivot axis 108 rearwardly relative to the frame 22, along an arc relative to the incline link-frame pivot axis 106. As illustrated and described herein below, this increases or raises the incline of the elliptical path of the foot pads 90 during the striding motion. Conversely, shortening the linear actuator 110 pivots the incline link 104 forwardly along the arc relative to the bridge 34 and along an arc relative to the incline link-frame pivot axis 106. This moves the incline link-rocker arm pivot axis 108 forwardly along the arc relative to the frame 22. As illustrated and described herein below, this reduces or lowers the incline of the elliptical path of the foot pads 90 during the striding

[0069] It is important to note that the adjustment device 94 does not need to include two actuators, as shown in the first

example. In other examples, a single adjustment device connected to both of the incline links 104 is employed, via for example an electric motor, worm gears, pulleys, and/or any other conventional mechanism for causing the abovenoted adjustment of the relative position of the axes.

[0070] Referring to FIGS. 1-5, the machine 20 has movable handle members 122 which are pivotably coupled to opposite sides of the bridge 34 at a handle member-bridge pivot axis 124. Each handle member 122 has an upper end with a hand grip 127 for manually grasping by the user performing the striding exercise motion. Each handle member 122 has a lower end which is pivotably coupled to a coupler link 126 at a handle member-coupler link pivot axis 128. Thus, the handle member 122 and respective coupler link 126 pivot together about the handle member-bridge pivot axis 124 and the coupler link 126 is pivotable relative to the handle member 122 about the handle member-coupler link pivot axis 128. Each coupler link 126 has a forward end portion 130 coupled to the handle member 122 at the handle member-coupler link pivot axis 128 and a rearward end portion 132 pivotably coupled to the central portion 70 of the pedal member 68 at a coupler link-pedal member pivot axis 134. Thus, the coupler link 126 is pivotable relative to the pedal member 68 about the coupler link-pedal member pivot axis 134. An elbow portion 136 is located between the forward and rearward end portions 130, 132 so that the forward end portion 130 extends angularly upwardly relative to the rearward end portion 132. As such, the user standing on the foot pads 90 and manually grasping the hand grips 127 can alternately push and pull on the hand grips 127 to thereby apply pushing and pulling forces on the pedal members 68 via the coupler links 126, which assists the striding exercise motion, as will be further described herein below.

[0071] FIGS. 8-10 are schematic views of the machine 20 showing the paths of travel A1-A3 of the foot pads 90 and the paths of travel B1-B3 of the stride link-pedal member pivot axis 82 during low-incline (FIG. 8), medium-incline (FIG. 9), and high-incline (FIG. 10). In each figure, the rocker arms 92 have a different position of swing range, which is determined by position of the adjustment device 94. FIG. 8 illustrates low-incline, where the linear actuators 110 are retracted and thus the incline links 104 are pivoted about the incline link-frame pivot axis 106 towards the bridge 34 (i.e., clockwise about the incline link-frame pivot axis 106 in the side view illustrated in FIG. 8). This moves the incline link-rocker arm pivot axis 108 along an arc towards the bridge 34 and via connection of the rocker arms 92 and pedal members 68, positions the foot pads 90 so as to follow the low-incline elliptical path of travel A1. FIG. 9 illustrates medium-incline, wherein the linear actuators 110 are moderately extended and thus the incline links 104 are pivoted about the incline link-frame pivot axis 106 away from the bridge 34 (i.e., counter-clockwise about the incline linkframe pivot axis 106 from the side view illustrated in FIG. 9). This moves the incline link-rocker arm pivot axis 108 along an arc away from the bridge 34 and via connection of the rocker arms 92 and pedal members 68, positions the foot pads 90 to follow the medium-incline elliptical path of travel A2. FIG. 10 illustrates a high-incline situation, wherein the linear actuators 110 are further extended and thus the incline links 104 are pivoted about the incline link-frame pivot axis 106 away from the bridge 34 (i.e., further counter-clockwise about the incline link-frame pivot axis 106 from the side view illustrated in FIG. 10). This moves the incline linkrocker arm pivot axis 108 along the arc further away from the bridge 34 and via connection of the rocker arms 92 and pedal members 68, positions the foot pads 90 to follow the high-incline elliptical path of travel A3. It is important to understand that the three positions illustrated in FIGS. 8-10 are exemplary and other positions are possible via operation of the adjustment device 94, which can be automatically controlled by programming of the console 44 and/or by inputs to the console 44 and/or input buttons 48 and/or other input buttons such as on the upper ends of hand grips 127. [0072] By comparison of FIGS. 8-10, it can be seen that the machine 20 is advantageously configured to maintain a substantially compact and constant length (in the length direction L) of the paths of travel A1-A3 throughout the adjustments made by the adjustment device 94. The configurations of the various components advantageously take up a relatively small footprint. The ends of the rocker arms 92 advantageously do not swing beyond the front of the frame 22, thus maintaining a small footprint. The paths of travel B1-B3 are also substantially constant, due to the stride link configuration illustrated and described herein above. The rear linkage including the stride links 78 advantageously does not swing beyond the rear portion of the frame 22, thus maintaining a small footprint. The configuration of the movable handle members 122 and the coupler link 126 is advantageous in that the overall path of movement (i.e., swing range of the handle members 122 about the handle member-bridge pivot axis 124) is substantially constant

[0073] Advantageously, the foot pads 90 are located on the pedal members 68 at a distance rearward of the rocker arm-pedal member pivot axis 102 to create a more natural, vertical height of the paths of travel A1-A3. This feature in combination with the path of travel B1-B3 yields a more natural, and smooth path of travel A1-A3 in all incline settings. Also, the path of travel (arc) along which the incline link travels, as described herein above, is tilted upward towards the rear portion of travel, towards high-incline. This tailors/blends some additional vertical height to the overall ellipse height as it adjusts to a high-incline setting.

despite changes in incline via the adjustment device 94.

[0074] During research and development, the present inventor determined that performance of an exercise motion on an exercise machine, for example the machine 20 of FIGS. 1-10, may apply a reversing load on the actuator 110 as the user moves the foot pads 90 along their travel paths A1-A3 (FIGS. 8-10). When the direction of travel of the foot pads 90 switches from a forward direction to a reverse direction, a load applied on the actuator 110 by the rocker arm 92 also reverses, thereby switching between applying a compressive load and a tensile load onto the actuator 110. Reversing the load on the actuator 110 may cause actuator backlash as relative movement occurs between components of the actuator 110 and between the actuator 110 and the mounting locations/hardware for the actuator 110 due to the clearances that must be present between the various components. For example, referring to FIG. 13, reversing loads may cause relative motion between at least one of the actuator 110 and the actuator-bridge pivot axis 114; the actuator 110 and the actuator-incline link pivot axis 118; the leadscrew 123 and bearing supports and/or gears in a gearset 129 connecting the leadscrew 123 to the gearmotor 120; the leadscrew 123 and the leadnut 131 of the leadnut and tube assembly 125; the incline link 104 and the actuator; the

incline link 104 and the rocker arm; and any other connected components which have a clearance between each other.

[0075] The present inventor determined that the actuator backlash may create an undesirable noise and/or an undesirable jerk or jolt that may be felt by a user. Additionally or alternatively, when the actuator backlash occurring on one side of an exercise machine differs from the actuator backlash occurring on the other side of the machine, a user may feel an unbalanced, undesirable backlash feeling between the two sides of the machine. For these reasons, the present inventor determined that reversing loads on known exercise machines may cause actuator backlash that can result in an undesirable feeling and/or noise for a user. The present inventor thus have realized a need in the art to provide dampening to reduce the actuator backlash and/or reduce the effects of the actuator backlash on an exercise machine. The present disclosure is a result of these efforts.

[0076] FIGS. 11 and 12 illustrate an embodiment of a bridge 34 for an exercise machine, for example the machine 20 of FIGS. 1-10, that includes a dampener 200 configured to apply a preload force on the actuator 110 that dampens reversing loads from the rocker arm 92 to thereby reduce backlash in the actuator 110. The bridge 34 of FIGS. 11 and 12 is mounted on top of the forward support column 30 of the frame 22 and has a horizontally extending body 36 with opposing first and second arms 38 extending rearwardly from the body 36. In the illustrated embodiments, each arm 38 includes a dampener 200 configured to dampen actuator backlash on the corresponding side of the machine 20. Each arm 38 includes two rearwardly extending bridge arm members 39 that are spaced laterally apart from each other such that the adjustment devices 94 and the dampeners 200 are supported on the corresponding arm 38 between the opposing bridge arm members 39.

[0077] As previously mentioned, the machine 20 is generally symmetrical in the horizontal direction H, so that the components on one side of the machine 20 are the same as or are mirror images of the components on the opposite side of the machine 20. As such, the descriptions provided below regarding a dampener 200 on one side of the bridge 34 equally apply to the components on the opposite side of the bridge 34.

[0078] With continued reference to FIGS. 11 and 12, the incline link 104 of the adjustment device 94 is pivotably coupled on the frame 22 by the incline link-frame pivot axis 106, which extends through a hub portion 99 of the body 97 of the incline link 104. Opposing lateral ends of the incline link-frame pivot axis 106 are supported on support portions 23 of the bridge arm members 39, and respective clamp members 103 couple the incline link-frame pivot axis 106 to the support portions 23. The second end 117 (FIG. 13) of the linear actuator 110 is pivotably coupled to the body 97 of the incline link 104 by an actuator-incline link pivot axis 118, which is coupled to the incline link 104 by a trunnion assembly 213. The upper end portion 96 of the rocker arm 92 is pivotably coupled to the incline link 104 by incline link-rocker arm pivot axis 108. The incline link-rocker arm pivot axis 108 is supported on the incline link 104 by bracket plates 105 coupled to opposing lateral surfaces of the incline link body 97, and clamp members 103 clamp opposing ends of the incline link-rocker arm pivot axis 108 to the bracket plates 105. Thus, the second end 117 of the actuator 110 is coupled to the rocker arm 92 via the incline link 104, and the incline link 104 pivotably couples the rocker arm 92 to the frame 22.

[0079] Referring to FIGS. 12, 14, and 18, the illustrated dampener 200 is configured as a dual preload dampener system that includes two dampener sub-assemblies 250, 252 that are each configured to apply a preload force on the actuator 110 that dampens reversing loads from the rocker arm 92. A low-incline dampener 250 (see also FIG. 15) is configured to dampen the reversing loads when the machine 20 is in a low-incline configuration (FIG. 8), and a highincline dampener 252 (see also FIG. 16) is configured to dampen the reversing loads when the machine 20 is in a high-incline configuration (FIG. 10). The dampener 200 includes a mounting plate 202 that is configured to support the dampener 200 on the arm 38 between the two bridge arm members 39 and a pivot linkage 220 that extends between, and operatively couples, the mounting plate 202 to the incline link 104. The mounting plate 202 has a generally planar body 204 that is coupled to an upper surface of the bridge arm members 39, for example with mechanical fasteners. Upper mounting brackets 206 extend upwards from the planar body 204 and are positioned over openings 210 formed through the planar body 204. As discussed in greater detail below, the upper mounting brackets 206 are configured to support at least a portion of the low-incline dampener 250, which extend through a corresponding one of the openings 210.

[0080] With continued reference to FIGS. 12, 14, and 18, the pivot linkage 220 (FIG. 18) is coupled to the frame 22 (via the mounting plate 202) and the incline link 104. The pivot linkage 220 includes a spring arm 222 and connecting links 224 that are pivotably coupled together by a pivot linkage pivot axis 236. The spring arm 222 has a body that extends between a first end 228 and an opposite second end 230. The first end 228 of the spring arm 222 is pivotably coupled to an upper surface of the mounting plate 202 by a spring arm-plate axis 226, about which the spring arm 222 can pivot relative to the mounting plate 202. The body of the spring arm 222 extends through an opening 208 formed through the planar body 204 of the mounting plate 202.

[0081] The connecting links 224 are pivotably coupled to opposing lateral sides of the second end 230 of the spring arm 222 by the pivot linkage pivot axis 236 such that the spring arm 222 and the connecting links 224 may pivot relative to each other about a pivot linkage pivot axis 236. The connecting links 224 each extend from the first end 232 to a second end 234 that is pivotably coupled to a corresponding lateral side of the incline link 104 such that the connecting links 224 may pivot relative to the incline link 104 about a connecting link-incline link pivot axis 238. In some embodiments, bushings 237 may support at least one of the spring arm-plate axis 226, the pivot linkage pivot axis 236, and the connecting link-incline link pivot axis 238 in the corresponding component(s). Some embodiments, however, may omit at least one of the bushings 237.

[0082] As previously mentioned, the dampener 200 is configured as dual preload dampeners with a low-incline dampener 250 and a high-incline dampener 252 that each apply a preload force on the actuator 110 (e.g., via the incline link 104 and/or pivot linkage 220) to dampen the reversing loads and reduce backlash in the actuator 110. In the illustrated embodiments, the low-incline dampener 250 includes at least one spring 262, 264 configured to apply a

tension preload force on the actuator 110 and the high-incline dampener 252 includes at least one spring 262, 264 configured to apply a compression preload force on the actuator 110.

[0083] Referring to FIGS. 14, 15, and 18, the low-incline dampener 250 includes two first dampener assemblies 254 and two second dampener assemblies 256 to apply the tension preload force on the actuator 110. In the illustrated embodiment, (FIGS. 15 and 18), each one of the second dampener assemblies 256 corresponds to (e.g., abuts, interfaces, aligns with, etc.) one of the first dampener assemblies 254. Each one of the first dampener assemblies 254 includes the spring 262 that is configured as a (flat metal) leaf spring 262 supported on a lower surface of one of the upper mounting brackets 206 on the mounting plate 202. Referring to FIG. 15, the leaf springs 262 of the first dampener assemblies 254 have a mounting side 274 that is clamped between a clamp member 266 and the corresponding upper mounting bracket 206 and an abutting side 276 which abuts a portion of the corresponding second dampener assembly 256. The leaf springs 262 include a bend to join the mounting and abutting sides 274, 276. The leaf springs 262 may be compressed by pressing the abutting side 276 towards the mounting side 274, thereby bending or deflecting the spring 262. Thus the abutting side 276 is biased apart from the mounting side 274 due to the resiliently deformable nature of the leaf spring 262. In some examples, the bend of the leaf spring 262 is configured based on an orientation of the corresponding elastomer spring 264 to reduce bending (e.g., deformation in the longitudinal direction L of FIG. 11) of the elastomer spring 264. That is, an angle (e.g., uncompressed angle) between the mounting and abutting sides 274, 276 of the leaf spring 262 enables contact between the elastomer spring 264 to compress (deform) substantially linearly while reducing horizontal or longitudinal deformation of the elastomer spring 264. Furthermore, the bend of the leaf spring 262 is configured such that the mounting and abutting sides 274, 276 are substantially aligned (e.g., parallel) when the first and second dampener assemblies 254, 256 are in fully compressed states (FIGS. 17 and 19), which further reduces horizontal bending of the corresponding elastomer spring 264. In the illustrated embodiments, the leaf springs 262 are formed from a rigidly or elastically deformable metal material. Some embodiments, however, may include at least one leaf spring formed from a different

[0084] With continued reference to FIGS. 14, 15, and 18, the second dampener assemblies 256 of the low-incline dampener 250 each include a first spring 262 (i.e., a first spring member) and a second spring 264 (i.e., a second spring member) that is coupled to the first spring 262. In the illustrated embodiments, the first springs 262 of the second dampener assemblies 256 are configured as leaf springs 262 and the second springs 264 are configured as elastomeric springs 264. Each elastomeric spring 264 is formed from a resiliently deformable material that has an annular body that deforms when compressed between two objects/surfaces. The resiliently deformable nature of the elastomeric springs 264 biases the body back into its annular form, thereby biasing the objects/surfaces apart from each other.

[0085] Referring to FIG. 15, the mounting side 274 of the leaf springs 262 are coupled to the mounting surface 270 of the incline link 104, for example with mechanical fasteners. The elastomeric springs 264 are each coupled to the abut-

ment side 276 of the corresponding leaf spring 262. In the illustrated embodiments, the elastomeric springs 264 are clamped onto the leaf springs 262 between a clamp member 268 and the abutment side 276, for example with a mechanical fastener. As the linear actuator 110 is retracted, for example when the machine 20 is moved into the low-incline configuration (FIGS. 8 and 17), the elastomeric springs 264 of the second dampener assemblies 256 are configured to abut the abutting sides 276 of the leaf springs 262 of the first dampener assemblies 254. Thus, as discussed in greater detail below, the spring 262 of the first dampener assembly 254 and the springs 262, 264 of the second dampener assembly 256 of the low-incline dampener 250 are configured to be compressed between the mounting plate 202 and the incline link 104 when the actuator 110 is retracted, thereby applying a tensile preload force onto the actuator 110.

[0086] Referring to FIGS. 14, 16, and 18, the high-incline dampener 252 includes a first dampener assembly 258 and a second dampener assembly 260 (FIGS. 16 and 18) that each include at least one spring 262, 264, and which are configured to apply a compression preload force on the actuator 110. The first dampener assembly 258 of the high-incline dampener 252 includes a spring 262 configured as a leaf spring 262, and the second dampener assembly 260 includes an elastomeric spring 264. Referring to FIG. 16, the leaf spring 262 of the first dampener assembly 258 has a mounting side 274 that is clamped between a clamp member 266 and a rear surface 221 of the spring arm 222, for example using mechanical fasteners, thereby coupling the leaf spring 262 to the spring arm 222. The elastomeric spring **264** of the second dampener assembly **260** is coupled to a lower mounting bracket 212 of the mounting plate 202. More specifically, the elastomeric spring 264 is clamped between a forward-facing mounting surface 214 of the lower mounting bracket 212 and a clamp member 268, thereby coupling the elastomeric spring 264 to the lower mounting bracket 212 of the mounting plate 202.

[0087] As the linear actuator 110 is extended, for example when the machine 20 is moved into the high-incline configuration (FIGS. 10 and 19), the leaf spring 262 of the first dampener assembly 258 is moved into abutment with the elastomeric spring 264 of second dampener assembly 260 as the spring arm 222 pivots rearwardly about the spring arm-plate axis 226. Thus, as discussed in greater detail below, the springs 262, 264 of the first and second dampener assemblies 258, 260 of the high-incline dampener 252 are configured to be compressed between the lower mounting bracket 212 of the mounting plate 202 and spring arm 222 when the actuator 110 is extended, thereby applying a compressive preload force onto the actuator 110. As the first and second dampener assemblies 258, 260 are compressed between the lower mounting bracket 212 of the mounting plate 202 and the spring arm 222, the leaf spring 262 and the elastomeric spring 264 of the first and second dampener assemblies 258, 260 are simultaneously compressed, thereby gradually increasing the compressive preload force onto the actuator 110.

[0088] As previously mentioned, the illustrated dampener 200 is configured to apply at least one preload force on the actuator 110 to reduce the actuator backlash feel and noise experience by a user when operating the machine 20 in any

incline configuration (low-incline (FIG. 17), high-incline (FIG. 19), and any intermediate, i.e., medium, incline (FIG. 18).

[0089] When the actuator 110 of the adjustment device 94 moves to a retracted position and forwardly rotates the incline link 104 such that the machine 20 is in a low-incline configuration, the dampener 200 applies a tensile preload force on the linear actuator 110. For example, referring to FIG. 17, the springs of the low-incline dampener 250 are compressed between the incline link 104 and the frame 22. In particular, the elastomer spring 264 of the second lowincline dampener assembly 256 is compressed between the abutment sides 276 of the leaf springs 262 of the first and second low-incline dampener assemblies 254, 256. Furthermore, the leaf spring 262 of the first low-incline dampener assembly 254 are compressed between the upper mounting brackets 206 of the mounting plate 202 on the frame 22 and the elastomer springs 264, and the leaf spring 262 of the second low-incline dampener assembly 256 are compressed between the elastomer springs 264 and the mounting surface 270 of the incline link 104.

[0090] With continued reference to FIG. 17, the compressed springs 262, 264 of the low-incline dampener 250 bias the incline link 104 to pivot about the incline link-frame pivot axis 106 to move away from the mounting plate 202. This creates a tensile force that is exerted on the actuator 110 by the springs 262, 264 of the low-incline dampener 250. This tensile preload force acts to pull the second end 117 of the actuator 110 away from the first end 115 thereof (FIG. 13). By biasing the ends 115, 117 of the actuator 110 apart from each other to hold the actuator 110 in tension, the reversing loads from the cyclical movement of the rocker arm 92 are dampened by the low-incline dampener 250, thereby reducing actuator backlash in the low-incline configuration.

[0091] As the actuator 110 extends to increase the incline level of the machine 20, the incline link 104 moves away from the springs 262, 264 of the low-incline dampener 250, and said springs 262, 264 therefore become less compressed (e.g., when in a medium-incline configuration as illustrated in FIG. 18) until they are at a "free" state in which the springs 262, 264 are not compressed (FIG. 19). At the same time, the springs 262, 264 of the high-incline dampener 252 are increasingly compressed. For example, when then machine 20 is in a medium-incline configuration, as illustrated in FIG. 18, the leaf spring 262 and the elastomeric spring 264 of the high-incline dampener 252 are simultaneously compressed,

[0092] When the actuator 110 of the adjustment device 94 moves to an extended position and rearwardly rotates the incline link 104 such that the machine 20 is in a high-incline configuration, the dampener 200 applies a compressive preload force on the linear actuator 110. For example, referring to FIGS. 16 and 19, the springs 262, 264 of the high-incline dampener 252 are compressed between the pivot linkage 220 and the frame 22. In particular, the elastomer spring 264 of the second high-incline dampener assembly 260 is compressed between the mounting surface 214 of the lower mounting bracket 212 and the abutment side 276 of the leaf spring 262 of the first high-incline dampener assembly 258. The leaf spring 262 of the first high-incline dampener assembly 258 is compressed between

the body of the spring arm 222 of the pivot linkage 220 and the elastomer spring 264 of the second high-incline dampener assembly 260.

[0093] With continued reference to FIG. 19, the compressed springs 262, 264 of the high-incline dampener 252 bias the spring arm 222 to pivot about the spring arm-plate axis 226 away from the lower mounting bracket 212. Pivoting movement of the spring arm 222 relative to the frame 22 transmits the preload force from the springs 262, 264 to the incline link 104 via the connecting links 224 such that the pivot linkage 220 biases the incline link 104 towards the front of the machine 20. This creates a compressive force that is exerted on the actuator 110 by the springs 262, 264 of the high-incline dampener 250 via the spring arm 222, the connecting links 224, and the incline link 104. This compressive preload force acts to push the second end 117 of the actuator 110 towards the first end 115 thereof (FIG. 13). By biasing the ends 115, 117 of the actuator 110 towards each other to hold the actuator 110 in compression, the reversing loads from the cyclical movement of the rocker arm 92 are dampened by the high-incline dampener 252, thereby reducing actuator backlash in the high-incline configuration.

[0094] As the actuator 110 retracts to decrease the incline level of the machine 20, the spring arm 222 moves away from the lower mounting bracket 212 of the mounting plate 202, and the springs 262, 264 of the high-incline dampener 252 becomes less compressed until the springs 262, 264 are closer to their "free" state (FIG. 17), or, in some embodiments, until said springs 262, 264 are in their "free" state. At the same time, the springs 262, 264 of the low-incline dampener 250 move into abutment with each other and are increasingly compressed as the machine 20 is returned to the low-incline configuration by the adjustment device 94.

[0095] Advantageously, the preload forces exerted on the actuator 110 by the low-incline dampener 250 and the high-incline dampener 252 dampen reversing external loads that occur when operating the machine 20, for example the loads from the user applied via the rocker arm 92. As a result of the applied preload forces, the low-incline dampener 250 and the high-incline dampener 252 enhance the stiffness of the adjustment device 94 and reduces noise levels during operation of the machine 20. The preload force(s) are internal to the machine 20 and do not require the direct or indirect application of an external force by a user, thereby enhancing the user experience without requiring input from the user.

[0096] Referring to FIG. 18, the low and high-incline dampeners 250, 252 of the dampener 200 are configured to have some overlap in the application of their respective preload forces. As the springs 262, 264 of the low-incline dampener 250 or the high-incline dampener 252 move toward disengagement and the compression of said springs 262, 264 is reduced, the preload force applied by the said springs 262, 264 is reduced. At the same time, as the springs 262, 264 of the other of the low-incline dampener 250 or the high-incline dampener 252 move towards engagement and/ or are increasingly compressed, the preload force applied by said springs 262, 264 is increased. When in a medium or intermediate incline configuration (FIG. 18), the springs 262, 264 of the low-incline dampener 250 are compressed between the frame 22 and the incline link 104 and the springs 262, 264 of the high-incline dampener 252 are compressed between the frame 22 and the pivot linkage 220. Thus, the dampener 200 simultaneously applies compressive

preload forces and a tensile preload forces on the liner actuator 110 in intermediate incline configurations.

[0097] Advantageously, the dual preload configuration of the dampener 200 consistently/constantly provides at least one preload force that act on the actuator 110 via the incline link 104 to dampen the reversing loads when the machine 20 is in a low-incline configuration, a high-incline configuration, or any intermediate incline configuration between the high and low-incline configurations (i.e., a medium-incline configuration). While the low-incline dampener 250 and the high-incline dampener 252 advantageously target the incline ranges of the machine 20 in which the user experiences the most actuator backlash feel and noise, the low and highincline dampeners 250, 252 also work in conjunction to reduce actuator backlash by dampening externally applied reversing loads when the machine 20 is in any intermediate incline configuration. Furthermore, because the dampener 200 includes the springs 262, 264, the preload force is variable through the range of incline settings of the machine 20. That is, the preload force of the dampener 200 is higher in magnitude when the machine 20 is at the high-incline and low-incline configurations. More specifically, the tension preload force of the low-incline dampener 250 is higher when the machine 20 is in the low-incline configuration (FIG. 17) relative to another incline configuration of the machine 20. Likewise, the compression preload forced of the high-incline configuration (FIG. 19) is higher relative to another incline configuration of the machine 20 (e.g., the medium-incline configuration of FIG. 18).

[0098] In the embodiments of FIGS. 11-19, the dampener 200 includes a low-incline dampener 250 and a high-incline dampener 252 that both include at least one leaf spring 262 and at least one elastomeric spring 264. The magnitude of the applied spring forces may be adjusted to a desired level by selecting at least one of the shape, size, material, and any other property of the leaf springs 262 and the elastomer springs 264. Advantageously, the use of two different types of springs 262, 264 allow for greater customization of the preload forces due to the variations in possible spring configurations available due to the difference in possible properties of the leaf spring 262 and the elastomer spring 264. Furthermore, use of at least one elastomer spring 264 may reduce or eliminate an undesirable noise that might occur due to the contact between two metal components. Some embodiments of a dampener, however, may be configured with a low-incline dampener and/or a high-incline dampener that have a different spring configuration than those of FIGS. 11-19.

[0099] For example, FIGS. 20-26 illustrate another embodiment of a dampener 300 that includes a low-incline dampener 350 and a high-incline dampener 352 that are respectively configured to exert a tensile preload force and a compressive preload force onto the liner actuator 110 to reduce actuator backlash caused by reversing loads from the rocker arm 92. Similar to the embodiments of FIGS. 11-19, an incline link 104 operatively links the rocker arm 92, the actuator 110, and the frame together. Additionally, the dampener 300 of FIGS. 20-26 includes a mounting plate 302 configured to support the dampener 300 on the arms 38 of the frame 22 and a pivot linkage 320 that couples the mounting plate 302 to the incline link 104.

[0100] In the embodiments of FIGS. 20-26, various components of the machine 20, for example components of the bridge 34, components of the adjustment device 94, certain

components of the dampener 300 (e.g., the mounting plate 302 and the pivot linkage 320), and other related support components are similar to or the same as those described with respect to the exercise machine and dampener 200 of FIGS. 10-19 and will not be described in detail again. However, as noted above, like reference numbers are used throughout FIGS. 20-26 to reference like features and like components discussed with respect to FIGS. 11-19.

[0101] Referring to FIGS. 20, 21, and 25, the illustrated dampener 300 is configured as a dual preload dampener system that includes two dampener sub-assemblies 350, 352 that are each configured to apply a preload force on the actuator 110 that dampens reversing loads from the rocker arm 92. A low-incline dampener 350 (see also FIG. 22) is configured to dampen the reversing loads when the machine 20 is in a low-incline configuration (FIG. 8), and a highincline dampener 352 (see also FIG. 23) is configured to dampen the reversing loads when the machine 20 is in a high-incline configuration (FIG. 10). The low-incline dampener 350 includes at least one spring 364 configured to apply a tension preload force on the actuator 110 and the highincline dampener 352 includes at least one spring 364 configured to apply a compression preload force on the actuator 110.

[0102] Referring to FIGS. 21, 22, and 25, the low-incline dampener 350 includes two first low-incline dampener subassemblies 354 and two second low-incline dampener subassemblies 356 (FIGS. 22 and 25). In the illustrated examples, each one of the second dampener assemblies 356 corresponds to (e.g., abuts, interfaces, aligns with, etc.) one of the first dampener assemblies 354. The first dampener assemblies 354 of the low-incline dampener 350 include springs 364 configured as annular elastomer springs 364 that are clamped onto a lower surface of one of the upper mounting brackets 306 with a clamping member 368 (configured as a nut in the illustrated embodiments), and which extend downward therefrom through a corresponding opening 310 through the body 304 of the mounting plate 302. The second dampener assemblies 356 of the low-incline dampener 350 each include a spring 364 configured as an elastomeric spring 364 and a mounting member 369. The mounting members 369 are positioned on the mounting surface 270 of the incline link 104 and are clamped between the elastomeric spring 364 and the mounting surface 270. Each of the elastomeric springs 364 is clamped onto a corresponding mounting member 369 by a clamping member 368 (configured as a spacer in the illustrated embodiments). As illustrated in FIG. 23, the elastomeric springs 364 include at least one locating protrusion 365 that engages openings on the respective one of the upper mounting bracket 306 and the mounting member 369. This may be useful, for example, to retain the elastomeric springs 364 in a desired position. In some embodiments, at least one of the mounting members 369 may be formed as an integral part of the incline link 104. Additionally or alternatively, a clamping member 368 of one of the first dampener assemblies 354 and/or a clamping member 368 of one of the second dampener assemblies 356 may be differently configured than those of the illustrated embodiments.

[0103] Referring to FIG. 24, as the linear actuator 110 is retracted, for example when the machine 20 is moved into the low-incline configuration (FIGS. 8 and 24), the elastomeric springs 364 of the first and second low-incline dampener assemblies 354, 356 are configured to move into

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figuration.

abutment with each other. When the machine 20 is in the low-incline configuration the elastomeric springs 364 of the low-incline dampener 350 are compressed between the mounting plate 302 on the frame 22 and the mounting surface  $\tilde{270}$  of the incline link 104. The compressed springs 364 of the low-incline dampener 350 bias the incline link 104 to pivot about the incline link-frame pivot axis 106 to move away from the mounting plate 302. This creates a tensile force that is exerted on the actuator 110 by the springs 364 of the low-incline dampener 350 via the incline link 104. This tensile preload force pulls the second end 117 of the actuator 110 away from the first end 115 thereof (FIG. 13). By biasing the ends 115, 117 of the actuator 110 apart from each other to hold the actuator 110 in tension, the reversing loads from the cyclical movement of the rocker arm 92 are dampened by the low-incline dampener 350,

thereby reducing actuator backlash in the low-incline con-

[0104] Referring to FIGS. 21, 23, and 25, the high-incline dampener 352 includes a first high-incline dampener subassembly 358 and a corresponding second high-incline dampener sub-assembly 360 (FIGS. 23 and 25), both of which include a spring 364 configured as an elastomeric spring 364 with a resiliently deformable annular body. Referring to FIGS. 23 and 25, the elastomeric spring 364 of the first dampener assembly 358 is clamped between a clamp member 368 and a rear surface 321 of the spring arm 322, thereby coupling said spring 364 to the spring arm 322 of the pivot linkage 320. The elastomeric spring 364 of the second dampener assembly 360 is clamped between a forward-facing mounting surface 314 of the lower mounting bracket 312 and a clamp member 368, thereby coupling the elastomeric spring 364 to the lower mounting bracket 312 of the mounting plate 302. As with the elastomeric springs 364 of the low-incline dampener 350, the elastomeric springs 364 of the high-incline dampener 352 include locating protrusions 365 which engage openings on the corresponding surface 314, 321 to which each spring 364 is attached.

[0105] Referring to FIG. 26, as the linear actuator 110 is extended, for example when the machine 20 is moved into the high-incline configuration (FIGS. 10 and 26), the elastomeric spring 364 of the first high-incline dampener assembly 358 is moved towards and pressed into the elastomeric spring 364 of second dampener assembly 360 as the spring arm 322 pivots about the spring arm-plate axis 326. When the actuator 110 of the adjustment device 94 has been extended to move the incline link 104 such that the machine 20 is in a high-incline configuration, springs 364 of the high-incline dampener 352 are compressed between the spring arm 322 and the lower mounting bracket 312. The compressed springs 364 of the high-incline dampener 352 bias the spring arm 322 to pivot about the spring arm-plate axis 326 away from the lower mounting bracket 312. Pivoting movement of the spring arm 322 relative to the frame 22 transmits the preload force from the springs 364 to the incline link 104 via the connecting links 324 such that the pivot linkage 320 biases the incline link 104 towards the front of the machine 20. This creates a compressive force that is exerted on the actuator 110 by the springs 364 of the high-incline dampener 352 via the spring arm 322, the connecting links 324, and the incline link 104. This compressive preload force pushes the second end 117 of the actuator 110 towards the first end 115 thereof (FIG. 13). By biasing the ends 115, 117 of the actuator 110 towards each other to hold the actuator 110 in compression, the reversing loads from the cyclical movement of the rocker arm 92 are dampened by the high-incline dampener 352, thereby reducing actuator backlash in the high-incline configuration.

[0106] Referring to FIG. 25, low and high-incline dampeners 350, 352 of the dampener 300 are configured to have some overlap in the application of their respective preload forces. As the springs 364 of one of the low-incline dampener 350 and the high-incline dampener 352 move toward disengagement and the compression of said springs 364 is reduced, the preload force applied by the said springs 364 is reduced. At the same time, as the springs 364 of the other one of the low-incline dampener 350 and the high-incline dampener 352 move towards engagement and/or are increasingly compressed, the preload force applied by said springs 364 is increased. When in a medium-incline configuration (FIG. 25), the springs 364 of the low-incline dampener 350 are compressed between the frame 22 and the incline link 104 and the springs 364 of the high-incline dampener 352 are compressed between the frame 22 and the pivot linkage 320. Thus, the dampener 300 simultaneously applies a compressive preload force and a tensile preload force on the liner actuator 110 in intermediate incline configurations.

[0107] As explained herein above, performance of a striding exercise motion causes the elastomeric springs 364 in the low-incline dampener 350 and the high-incline dampener 352 to be pressed together along a non-linear, arcshaped path based on the pivoting movement of the incline link 104 and spring arm 322, respectively. For example, referring to FIG. 22, pivoting movement of the incline link 104 about the incline link-frame pivot axis 106 causes the elastomeric spring 364 of the second low-incline dampener assembly 356 to move towards and away from the mounting plate 302 along an arc-shaped path exemplarily indicated by arrow 391. Similarly, referring to FIG. 23, pivoting movement of the spring arm 322 about the spring arm-plate axis 326 causes the elastomeric spring 364 of the first highincline dampener assembly 358 to move towards and away from the mounting plate 302 along an arc-shaped path exemplarily indicated by arrow 392.

[0108] During research and experimentation, the present inventor determined that the above-described non-linear compression of the elastomeric springs 364 may cause the elastomeric springs 364 to deform unevenly such that they do not remain centered relative to each other. Referring now to FIG. 40, the above-described elastomeric spring 364 is shown in dashed lines. The elastomeric spring 364 includes a resiliently deformable body 376 having a generally flat lower inner surface 372 that transitions into a curved radially inner surface 379. Relative to this embodiment, the present inventor determined that when the body 376 is not compressed in a consistent linear direction (i.e., non-linear compression) it tends to deform or move more in one horizontal direction 395 relative to the surface 380 to which it is attached than in the opposite horizontal direction 396 based on the angle at which the compressive force 394 is applied.

[0109] FIG. 40 also depicts an alternate embodiment of a deformable spring member 570 in solid lines. The deformable spring member 570 has a different shape than the spring 364 shown in dashed lines. Like the spring 364, the spring member 570 has an annular body 576 and at least one locating protrusion 574 configured to engage a corresponding opening to secure the spring member 570 to the corre-

spring members 570 remaining generally centered on a shared centerline 580 in the high-incline configuration.
Some embodiments, however, may be differently configured.

[0112] Referring to FIGS. 37-39, embodiments of a low-incline dampener 550 may be configured with first and second low-incline dampeners 566, 568 that each include at

sponding mounting surface/location 380. The body 576 has a generally oval shape and has a radially inner surface 579 that is generally elliptical. Through research and experimentation, the present inventor determined that the depicted shape of the deformable spring member 570 is such that it advantageously self-corrects against the above-described tendency of the elastomeric spring 364 to move horizontally relative to the surface 380 to which it is attached. For example, the thickness of a lower portion 578 of the spring member body 576 is greater than at other locations around the annular body 576, which provides increased resistance to lateral forces which might otherwise cause asymmetric bulging of the spring members 570. Additionally, when compared to the abrupt changes in curvature of the elastomeric spring 364 between the flat inner surface 372 and the curved inner surface 379, the smooth, generally continuous curvature around the entire radially inner surface 579 of the body 576 resists undesirable asymmetric bulging of the spring member 570.

[0112] Referring to FIGS. 37-39, embodiments of a lowincline dampener 550 may be configured with first and second low-incline dampeners 566, 568 that each include at least one spring member 570 with a shape that is configured to self-correct for non-linear compression of the spring members 570 resulting from the pivoting movement of the incline link 104 about the incline link-frame pivot axis 106 (FIG. 22). Embodiments of the spring member 570 may mounted on their respective mounting surfaces using a clamp member (e.g., any of the illustrated clamp members 268, 368, 468), a screw, bolt, and/or other mechanical fastener, an adhesive, and/or another fastening arrangement. When the machine 20 is moved from the high-incline configuration (FIG. 37) into the low-incline configuration (FIG. 39), the spring member 570 of the second low-incline dampener 568 is moved towards the upper mounting bracket 506 along the arc-shaped path indicated by arrow 596 and is pressed against the spring member 570 of the first lowincline dampener 566.

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[0110] FIGS. 34-36 illustrate an embodiment of a highincline dampener 552 that includes a first high-incline dampener 562 and a second high-incline dampener 564 that each have spring members 570 configured, as explained above, to self-correct for non-linear compression of the spring members 570 resulting from the pivoting movement of the spring arm 522 about the spring arm-plate axis 526. Embodiments of the spring member 570 may be mounted on their respective mounting surfaces using a clamp member (e.g., any of the illustrated clamp members 268, 368, 468), a screw, bolt, and/or other mechanical fastener, an adhesive, and/or another fastening arrangement. Similar to the abovedescribed embodiments, when the machine 20 is moved from the low-incline configuration (FIG. 34) into the highincline configuration (FIG. 36), the elastomeric spring member 570 of the first high-incline dampener 562 is moved towards the lower mounting bracket 512 along the arcshaped path indicated by arrow 589 and pressed against the spring member 570 of the second high-incline dampener

[0113] Referring to FIG. 38, continued pivoting movement of the incline link 104 causes the two spring members 570 to be non-linearly compressed, for example along the compression path indicated by arrow 597. As each spring member 570 is compressed and deformed, their bodies 576 are squashed in a normal direction (vertically) relative to their respective supporting surface 507, 270 (for example as indicated by arrows 593) and tend to be pushed or squeezed outward or expanded in a parallel direction (horizontally) relative to their respective supporting surface 507, 270 (for example as indicated by arrows 594). The collective result of the forces exerted on the spring members 570 is a tendency for their bodies 576 to asymmetrically bulge outward and away from the incline link-frame pivot axis 106. The shape of the spring member 570 advantageously self-corrects for the above-described non-linear compression of said spring members 570 along path 597 by causing the spring bodies 576 to deform such that the two spring members 570 remain relatively centered relative to each other, thereby countering the tendency of the spring members 570 to asymmetrically bulge outward. For example, the shape of the illustrated spring members 570 promotes deformation of said spring members 570 towards the pivot axis of the incline link 104, for example indicated by arrows 598. As illustrated in FIG. 39, this correction for non-linear compression of the spring members 570 results in the spring members 570 remaining generally centered relative to each other in the low-incline configuration.

[0111] Referring to FIG. 35, continued pivoting movement of the spring arm 522 causes the two spring members 570 to be non-linearly compressed, for example along the compression path indicated by arrow 590. As each spring member 570 is compressed and deformed, their bodies 576 are squashed in a normal direction (vertically) relative to their respective supporting surface 514, 521, (for example as indicated by arrows 593) and tend to be pushed or squeezed outward or expanded in a parallel direction (horizontally) relative to their respective supporting surface 514, 521 (for example as indicated by arrows 594). The collective result of the forces exerted on the spring members 570 is a tendency for their bodies 576 to bulge outward and away from the spring arm-plate axis 526. However, advantageously, the shape of the spring member 570 is configured to self-correct for the non-linear compression of said spring members 570 by causing the spring bodies 576 to deform such that the two spring members 570 remain relatively centered relative to each other. For example, the shape of the illustrated spring members 570 promotes deformation of said spring members 570 towards the pivot axis 526 of the spring arm 522, as exemplarily indicated by arrows 592. As illustrated in FIG. 36, this correction for non-linear compression of the spring members 570 counters the tendency of the spring members 570 to asymmetrically bulge outward and results in the

[0114] In the embodiments of FIGS. 11-19 and FIGS. 20-26, the illustrated dampener 200, 300 includes low-incline dampeners 250, 350 and high-incline dampeners 252, 352 that each include a plurality of springs 262, 264, 364 configured to exert compressive and/or tensile preload forces onto the actuator 110. Some embodiments of a dampener, however, may be configured with a low-incline dampener and/or a high-incline dampener that includes one spring.

[0115] For example, FIGS. 27-33 illustrate another embodiment of a dual preload dampener 400 that includes a low-incline dampener 450 and a high-incline dampener 452 with a single spring 480, 464 configured to exert a tensile

preload force and a compressive preload force, respectively, onto the liner actuator 110 to reduce actuator backlash cause by reversing loads from the rocker arm 92. Similarly to the dampeners 200, 300 of FIGS. 11-26, an incline link 104 operatively links the rocker arm 92, the actuator 110, and the frame together. Additionally, the dampener 400 of FIGS. 27-33 includes a mounting plate 402 configured to support the dampener 400 on the arms 38 of the frame 22 and a pivot linkage 420 that couples the mounting plate 402 to the incline link 104.

[0116] In the embodiments of FIGS. 27-33, various components of the machine 20, for example components of the bridge 34, components of the adjustment device 94, certain components of the dampener 400 (e.g., the mounting plate 402 and the pivot linkage 420), and other related support components are similar to or the same as those described with respect to the exercise machine and dampeners 200, 300 of FIGS. 11-26 and will not be described in detail again. However, as noted above, like reference numbers are used throughout FIGS. 27-33 to reference like features and like components discussed with respect to FIGS. 11-26.

[0117] Referring to FIGS. 28, 29, and 32, the low-incline dampener 450 includes a twin elastomer spring 480 clamped to a bottom surface of the upper mounting bracket 406 by a clamp member 468 and an abutment member 486 coupled to the mounting surface 270 of the incline link 104. The twin elastomer spring 480 is formed from a resiliently deformable material has a first annular body portion 482 and a second annular body portion 484 that are configured to deform when the twin elastomer spring 480 is compressed. The twin elastomer spring 480 has a generally figure eight shaped body with the first annular body portion 482 including locating protrusions 465 and being configured to be coupled to the upper mounting bracket 406. The second annular body portion 484 is formed on the first annular body portion 482 on a side opposite the locating protrusions. Advantageously, the first and second annular body portions 482, 484 allow the twin elastomer spring 480 to function and be compressed similarly to an arrangement with two springs. The abutment member has a body that is coupled to the mounting surface 270 of the incline link 104 and a stop member 488 that projects outward from the body portion in a direction opposite the mounting surface 270.

[0118] Referring to FIG. 31, as the linear actuator 110 is retracted, for example when the machine 20 is moved into the low-incline configuration (FIGS. 8 and 31), the twin elastomer spring 480 of the low-incline dampener 450 is configured to move into abutment with the abutment member 486 on the incline link 104. When the machine 20 is in the low-incline configuration the twin elastomer spring 480 is compressed between the mounting bracket 406 on the frame 22 and the abutment member 486. As the twin elastomer spring 480 is compressed, the first and second annular body portions 482, 484 are correspondingly compressed. Advantageously, the stop member 488 on the abutment member 486 may limit and/or reduce horizontal deformation (e.g., the deformation along a longitudinal axis L of FIGS. 11, 12) of the twin elastomer spring 480 relative to the mounting surface 270 and the abutment member 486. The compressed annular body portions 482, 484 of the lowincline dampener 450 bias the incline link 104 to pivot about the incline link-frame pivot axis 106 to move away from the mounting plate 402. This creates a tensile force that is exerted on the actuator 110 by the twin elastomer spring 480 of the low-incline dampener 450 via the incline link 104. This tensile preload force acts to pull the second end 117 of the actuator 110 away from the first end 115 thereof (FIG. 13). By biasing the ends 115, 117 of the actuator 110 apart from each other to hold the actuator 110 in tension, the reversing loads from the cyclical movement of the rocker arm 92 are dampened by the low-incline dampener 450, thereby reducing actuator backlash in the low-incline configuration.

[0119] Referring to FIGS. 28, 30, and 32, the high-incline dampener 452 includes a spring 464 configured as an elastomeric spring 464 with a resiliently deformable annular body. Referring to FIGS. 30 and 32, the elastomeric spring 464 is clamped between a forward-facing mounting surface 414 of the lower mounting bracket 412 and a clamp member 468, thereby coupling the elastomeric spring 464 to the lower mounting bracket 412 of the mounting plate 402. As with the twin elastomer spring 480 of the low-incline dampener 450, the elastomeric spring 464 of the high-incline dampener 452 includes locating protrusions 465 which engage openings on the mounting surface 414 of the lower mounting bracket 412.

[0120] Referring to FIG. 33, as the linear actuator 110 is extended, for example when the machine 20 is moved into the high-incline configuration (FIGS. 10 and 33), the rear surface 421 of the spring arm 422 is moved towards and pressed against the elastomeric spring 464 as the spring arm 422 pivots about the spring arm-plate axis 426. When the actuator 110 of the adjustment device 94 has been extended to move the incline link 104 such that the machine 20 is in a high-incline configuration, the spring 464 of the highincline dampener 452 is compressed between the spring arm 422 and the lower mounting bracket 412. The compressed spring 464 of the high-incline dampener 452 exerts a spring force that bias the spring arm 422 to pivot about the spring arm-plate axis 426 away from the lower mounting bracket 412. Pivoting movement of the spring arm 422 relative to the frame 22 transmits the preload force from the spring 464 to the incline link 104 via the connecting links 424 such that the pivot linkage 420 biases the incline link 104 towards the front of the machine 20. This creates a compressive force that is exerted on the actuator 110 by the springs 464 of the high-incline dampener 452 via the spring arm 422, the connecting links 424, and the incline link 104. This compressive preload force acts to push the second end 117 of the actuator 110 towards the first end 115 thereof (FIG. 13). By biasing the ends 115, 117 of the actuator 110 towards each other to hold the actuator 110 in compression, the reversing loads from the cyclical movement of the rocker arm 92 are dampened by the high-incline dampener 452, thereby reducing actuator backlash in the high-incline configuration.

[0121] Similarly to the dampeners 200, 300 of FIGS. 11-26, the low and high-incline dampeners 450, 452 of the dampener 400 of FIGS. 27-33 are configured to have some overlap in the application of their respective preload forces. As the springs 464, 480 of one of the low-incline dampener 450 and the high-incline dampener 452 move toward disengagement and the compression of said springs 464, 480 is reduced, the preload force applied by the said springs 464, 480 is reduced. Substantially simultaneously, as the springs 464, 480 of the other one of the low-incline dampener 450 and the high-incline dampener 452 move towards engagement and/or are increasingly compressed, the preload force applied by said springs 464, 480 is increased. When in a

medium-incline configuration (FIG. 32), the twin elastomer spring 480 of the low-incline dampener 450 is compressed between the frame 22 and the incline link 104 and the elastomer spring 464 of the high-incline dampener 452 is compressed between the frame 22 and the pivot linkage 420. Thus, the dampener 400 simultaneously applies compressive preload forces and a tensile preload forces on the liner actuator 110 in intermediate incline configurations.

[0122] Although specific advantages have been enumerated above, various examples may include some, none, or all of the enumerated advantages. Other technical advantages may become readily apparent to one of ordinary skill in the art after review of the following figures and description. Modifications, additions, or omissions may be made to the systems, apparatuses, and methods described herein without departing from the scope of the disclosure. For example, the components of the systems and apparatuses may be integrated or separated. Moreover, the operations of the systems and apparatuses disclosed herein may be performed by more, fewer, or other components and the methods described may include more, fewer, or other steps. Additionally, steps may be performed in any suitable order. As used in this document, "each" refers to each member of a set or each member of a subset of a set.

- 1. An exercise machine comprising:
- a frame,
- a rocker arm operable to perform a striding exercise motion relative to the frame,
- an actuator coupling the rocker arm to the frame, the actuator being configured to adjust a position of the rocker arm relative to the frame to adjust an incline of the striding exercise motion, and
- a dampener configured to apply a preload force on the actuator to dampen reversing loads from the rocker arm and reduce backlash in the actuator.
- 2. The exercise machine according to claim 1, wherein said preload force includes a tension force.
- **3**. The exercise machine according to claim **1**, wherein said preload force includes a compression force.
- **4**. The exercise machine according to claim **1**, wherein said dampener includes a spring.
- 5. The exercise machine according to claim 4, wherein said spring includes an elastomer.
- 6. The exercise machine according to claim 4, wherein said spring includes a first spring member and a second spring member coupled to the first spring member.
- 7. The exercise machine according to claim 1, wherein said preload force includes at least one of a tension force and a compression force, and said dampener is configured to apply the at least one of the tension force and the compression force on the actuator.
- **8**. The exercise machine according to claim **7**, wherein said actuator is configured to extend and retract, and said dampener is configured to apply the compression force when the actuator is extended and to apply the tension force when the actuator is retracted.
- 9. The exercise machine according to claim 7, wherein said dampener includes a first spring configured to apply the tension force on the actuator and a second spring configured to apply the compression force on the actuator.
- 10. The exercise machine according to claim 1, wherein said actuator includes a linear actuator having a first end pivotably coupled to the frame and a second end pivotably coupled to the rocker arm.

- 11. The exercise machine according to claim 10, further including an incline link pivotably coupling the rocker arm to the frame, the second end of the linear actuator being pivotably coupled to the rocker arm via the incline link.
- 12. The exercise machine according to claim 11, wherein said dampener including a spring configured to bias the incline link relative to the frame to apply said preload force as a tension force on the actuator.
- 13. The exercise machine according to claim 11, wherein said dampener including a spring configured to bias the incline link relative to the frame to apply said preload force as a compression force on the actuator.
- 14. The exercise machine according to claim 1, said dampener including a first spring and a second spring, said first spring and said second spring being configured to abut each other to apply the preload force.
- 15. The exercise machine according to claim 14, wherein one of the first spring and the second spring travels along a non-linear path relative to the other one of the first spring and the second spring, and wherein at least one of the first spring and the second spring has a shape configured to generally maintain alignment between the first spring and the second spring as the first spring and the second spring are compressed along the non-linear path.
- 16. The exercise machine according to claim 1, wherein said dampener is configured to apply said preload force throughout movement into and between a low-incline configuration and a high-incline configuration.
  - 17. An exercise machine comprising:
  - a frame,
  - a rocker arm operable to perform a striding exercise motion relative to the frame,
  - an incline link pivotably coupling the rocker arm to the frame,
  - a linear actuator having a first end pivotably coupled to the frame and a second end pivotably coupled to the incline link, the linear actuator being extendible and retractable to adjust a position of the rocker arm relative to the frame, and
  - a dampener configured to apply at least one of a tension force and a compression force on the linear actuator that dampens reversing loads from the rocker arm to thereby reduce backlash in the linear actuator.
- 18. The exercise machine according to claim 17, wherein said dampener is configured to apply both the tension force and the compression force on the linear actuator.
- 19. The exercise machine according to claim 17, wherein said linear actuator is configured to extend and retract, and said dampener is configured to apply the compression force when the linear actuator is extended and to apply the tension force when the linear actuator is retracted.
- 20. The exercise machine according to claim 17, wherein said dampener includes a first spring configured to apply the tension force on the linear actuator and a second spring configured to apply the compression force on the linear actuator.
- 21. The exercise machine according to claim 17, wherein the dampener includes a spring that is compressed between the incline link and the frame upon retraction of the linear actuator, which applies the tension force on the linear actuator.
- 22. The exercise machine according to claim 17, further comprising a pivot linkage coupled to the frame and to the incline link, wherein the dampener includes a spring, and

wherein the dampener is configured to compress the spring between the pivot linkage and the frame when the linear actuator is in an extended position to apply the compression force on the linear actuator.

- 23. The exercise machine according to claim 22, wherein the pivot linkage includes a spring arm and a connecting link that are pivotably coupled together.
- 24. The exercise machine according to claim 17, further comprising a pivot linkage coupled to the frame and the incline link, the dampener comprising a first spring and a second spring, the dampener configured to compress the first spring between the incline link and the frame when the linear actuator is in a retracted position to apply the tension force on the linear actuator, the dampener configured to compress the second spring between the pivot linkage and the frame when the linear actuator is in an extended position to apply the compression force on the linear actuator.
- 25. The exercise machine according to claim 17, wherein said dampener includes a low-incline dampener configured to dampen the reversing loads when the exercise machine is in a low-incline configuration and a high-incline dampener configured to dampen the reversing loads when the exercise machine is in a high-incline configuration.

- 26. The exercise machine according to claim 25, wherein said low-incline dampener is configured to apply the tension force and said high-incline dampener being configured to apply the compression force.
- 27. The exercise machine according to claim 25, wherein said dampener is configured to apply at least one of said tension force and said compression force throughout movement into and between a low-incline configuration and a high-incline configuration.
- 28. The exercise machine according to claim 17, wherein the dampener comprises a first spring supported on the frame and a second spring supported on a movable member, wherein the first spring and the second spring are compressed between the frame and the movable member to generate at least one of the tension force and the compression force; and

wherein the second spring travels along a non-linear path relative to the frame, and at least one of the first spring and the second spring has a shape configured to generally maintain alignment between the first spring and the second spring as the first spring and the second spring are compressed along the non-linear path.

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