US012383415B2

(12) **United States Patent**
Hassler et al.

(10) **Patent No.: US 12,383,415 B2**
(45) **Date of Patent: Aug. 12, 2025**

(54) **INTRA-ARTICULAR JOINT REPLACEMENT AND METHOD**

(71) Applicant: **Tornier SAS**, Montbonnot-Saint-Martin (FR)

(72) Inventors: **Michel Hassler**, Saint Ismier (FR); **Gilles Walch**, Lyons (FR); **Pierric Deransart**, Saint Martin d'uriage (FR); **Lucile Ferrand**, Montbonnot (FR); **Pascal Boileau**, Nice (FR)

(73) Assignee: **TORNIER SAS**, Montbonnot-Saint-Martin (FR)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 170 days.

(21) Appl. No.: **18/458,322**

(22) Filed: **Aug. 30, 2023**

(65) **Prior Publication Data**

US 2023/0414379 A1 Dec. 28, 2023

Related U.S. Application Data

(60) Division of application No. 16/875,729, filed on May 15, 2020, now Pat. No. 11,771,568, which is a (Continued)

(51) **Int. Cl.**
A61F 2/40 (2006.01)
A61B 17/16 (2006.01)
(Continued)

(52) **U.S. Cl.**
CPC ***A61F 2/4684*** (2013.01); ***A61B 17/1615*** (2013.01); ***A61B 17/1684*** (2013.01);
(Continued)

(58) **Field of Classification Search**
CPC A61F 2/40–2002/4096; A61B 17/1666; A61B 17/1684
See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

2,666,430 A 1/1954 Altamirano
3,412,733 A * 11/1968 Ross A61B 17/1666 606/81
(Continued)

FOREIGN PATENT DOCUMENTS

CH 426096 A 12/1966
CH 507704 A 5/1971
(Continued)

OTHER PUBLICATIONS

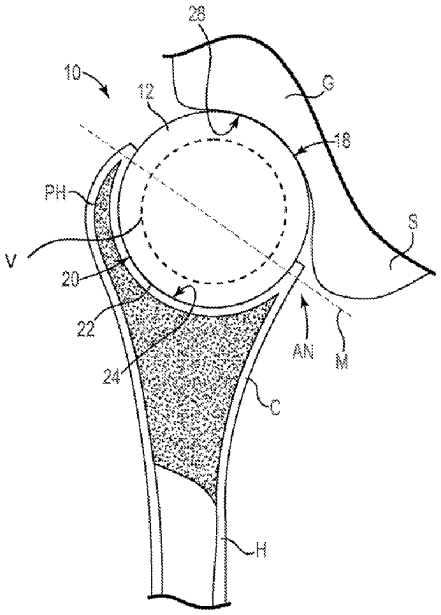
"Aequalis-Fracture Shoulder Prosthesis—Surgical Technique," Tornier, Inc., in 32 pages.
(Continued)

Primary Examiner — Zade Coley
(74) *Attorney, Agent, or Firm* — DUANE MORRIS LLP

(57) **ABSTRACT**

Methods of implanting a prosthesis to repair a joint include exposing a first bone of the joint; resecting an end portion of the first bone to form a resected end defining a resection plane; forming a concavity in the resected end portion of the first bone using a shaping tool, the concavity extending at least through a full hemispherical arc; selecting a diameter of the prosthesis to be implanted; and implanting a prosthesis having the selected diameter in the concavity.

10 Claims, 7 Drawing Sheets



Related U.S. Application Data

continuation of application No. 15/224,188, filed on Jul. 29, 2016, now Pat. No. 10,695,195, which is a division of application No. 12/768,154, filed on Apr. 27, 2010, now Pat. No. 9,408,652.

(51) **Int. Cl.**

A61B 17/88	(2006.01)
A61B 90/92	(2016.01)
A61F 2/46	(2006.01)
A61B 90/00	(2016.01)
A61F 2/30	(2006.01)

(52) **U.S. Cl.**

CPC ***A61B 17/885*** (2013.01); ***A61B 90/92*** (2016.02); ***A61F 2/4014*** (2013.01); *A61B 2090/062* (2016.02); *A61F 2002/30616* (2013.01)

(56) **References Cited**

U.S. PATENT DOCUMENTS

3,694,820	A		10/1972	Scales et al.
3,815,157	A		6/1974	Skorecki et al.
3,842,442	A		10/1974	Kolbel
3,864,758	A		2/1975	Yakich
3,869,730	A		3/1975	Skobel
3,916,451	A	*	11/1975	Buechel A61F 2/3854 403/56
3,938,193	A		2/1976	Sargunar
3,978,528	A		9/1976	Crep
3,979,778	A		9/1976	Stroot
3,992,726	A		11/1976	Freeman et al.
4,003,095	A		1/1977	Gristina
4,023,572	A	*	5/1977	Weigand A61B 17/1666 606/81
4,030,143	A	*	6/1977	Elloy A61F 2/40 623/19.12
4,040,131	A		8/1977	Gristina
4,054,955	A		10/1977	Seppo
4,126,924	A		11/1978	Akins et al.
4,131,116	A	*	12/1978	Hedrick A61B 17/1666 606/81
4,135,517	A		1/1979	Reale
4,179,758	A		12/1979	Gristina
4,206,517	A		6/1980	Pappas et al.
4,261,062	A		4/1981	Amstutz et al.
4,479,271	A		10/1984	Bolesky et al.
4,550,450	A		11/1985	Kinnett
4,662,891	A	*	5/1987	Noiles A61F 2/4609 623/22.25
4,693,723	A		9/1987	Gabard
4,822,370	A		4/1989	Schelhas
4,846,840	A		7/1989	Leclercq et al.
4,865,605	A		9/1989	Dines et al.
4,865,609	A		9/1989	Roche
4,892,549	A		1/1990	Figgie, III et al.
4,919,670	A		4/1990	Dale et al.
4,957,510	A		9/1990	Cremascoli
4,963,155	A		10/1990	Lazzeri et al.
4,964,865	A		10/1990	Burkhead et al.
5,030,233	A		7/1991	Ducheyne
5,032,132	A		7/1991	Matsen, III et al.
5,053,050	A		10/1991	Itay
5,080,673	A		1/1992	Burkhead et al.
5,080,685	A		1/1992	Bolesky et al.
5,127,920	A		7/1992	MacArthur
5,135,529	A		8/1992	Paxson et al.
5,163,961	A		11/1992	Harwin
5,181,928	A		1/1993	Bolesky et al.
5,192,329	A		3/1993	Christie et al.
5,201,882	A		4/1993	Paxson
5,206,925	A		4/1993	Nakazawa et al.
5,222,984	A		6/1993	Forte
5,261,914	A		11/1993	Warren
5,314,479	A		5/1994	Rockwood, Jr. et al.
5,314,487	A		5/1994	Schryver et al.
5,330,531	A		7/1994	Capanna
5,358,526	A		10/1994	Tornier
5,383,936	A		1/1995	Kubein-Meesenburg et al.
5,425,779	A		6/1995	Schlosser et al.
5,435,722	A	*	7/1995	Mandell A61C 1/052 433/165
5,443,515	A		8/1995	Cohen et al.
5,443,519	A		8/1995	Averill et al.
5,462,563	A		10/1995	Shearer et al.
5,507,817	A		4/1996	Craig et al.
5,507,818	A		4/1996	McLaughlin
5,507,819	A		4/1996	Wolf
5,507,824	A		4/1996	Lennox
5,534,033	A		7/1996	Simpson
5,549,682	A		8/1996	Roy
5,571,203	A		11/1996	Masini
5,580,352	A		12/1996	Sekel
5,702,447	A		12/1997	Walch et al.
5,702,457	A	*	12/1997	Walch A61F 2/4014 623/19.13
5,702,486	A		12/1997	Craig et al.
5,723,018	A	*	3/1998	Cyprien A61F 2/40 623/19.13
5,728,161	A		3/1998	Camino et al.
5,741,335	A		4/1998	Gerber et al.
5,755,719	A	*	5/1998	Frieze A61B 17/1666 606/81
5,755,807	A		5/1998	Anstaett et al.
5,779,709	A		7/1998	Harris, Jr. et al.
5,800,551	A		9/1998	Williamson et al.
5,800,557	A		9/1998	Elhami
5,879,355	A	*	3/1999	Ullmark A61F 2/4601 606/92
5,879,405	A		3/1999	Ries et al.
5,902,340	A		5/1999	White et al.
5,910,171	A		6/1999	Kummer et al.
5,928,285	A		7/1999	Bigliani et al.
5,941,706	A	*	8/1999	Ura A61C 3/02 433/165
5,944,758	A		8/1999	Mansat et al.
5,961,555	A		10/1999	Huebner
5,972,368	A		10/1999	McKay
5,984,927	A		11/1999	Wenstrom, Jr. et al.
6,015,437	A		1/2000	Stossel
6,027,503	A	*	2/2000	Khalili A61B 17/1666 606/81
6,033,439	A		3/2000	Camino et al.
6,045,302	A	*	4/2000	Orr B23B 51/0426 408/83
6,045,582	A		4/2000	Prybyla
6,045,583	A		4/2000	Gross et al.
6,090,145	A	*	7/2000	Hassler A61F 2/30721 623/23.14
6,096,084	A		8/2000	Townley
6,102,953	A		8/2000	Huebner
6,129,764	A		10/2000	Servidio
6,165,224	A		12/2000	Tornier
6,171,341	B1		1/2001	Boileau et al.
6,197,062	B1		3/2001	Fenlin
6,197,063	B1		3/2001	Dews
6,203,575	B1		3/2001	Farey
6,206,925	B1		3/2001	Tornier
6,221,076	B1	*	4/2001	Albrektsson A61B 17/1666 407/62
6,228,120	B1		5/2001	Leonard et al.
6,245,074	B1	*	6/2001	Allard A61B 17/1684 606/80
6,267,767	B1		7/2001	Strobel et al.
6,283,999	B1	*	9/2001	Rockwood, Jr. A61F 2/40 623/19.12
6,312,467	B1		11/2001	McGee
6,334,874	B1		1/2002	Tornier et al.
6,364,910	B1		4/2002	Shultz et al.
6,368,352	B1		4/2002	Camino et al.
6,368,353	B1		4/2002	Arcand

(56) **References Cited**

U.S. PATENT DOCUMENTS

6,383,227 B1 5/2002 Baroud et al.
6,398,812 B1 6/2002 Masini
6,406,495 B1 6/2002 Schoch
6,406,496 B1 6/2002 Rüter
6,436,144 B1 8/2002 Ahrens
6,436,146 B1 * 8/2002 Hassler A61F 2/4261 623/18.11
6,436,147 B1 8/2002 Zweymüller
6,454,811 B1 9/2002 Sherwood et al.
6,458,136 B1 10/2002 Allard et al.
6,475,221 B1 * 11/2002 White A61B 17/1666 404/54
6,475,243 B1 11/2002 Sheldon et al.
6,494,913 B1 12/2002 Huebner
6,506,214 B1 1/2003 Gross
6,508,840 B1 1/2003 Rockwood, Jr. et al.
6,511,511 B1 1/2003 Slivka et al.
6,514,287 B2 2/2003 Ondrla et al.
6,520,994 B2 2/2003 Nogarin
6,530,957 B1 3/2003 Jack
6,541,022 B1 4/2003 Murphy et al.
6,558,425 B2 5/2003 Rockwood, Jr.
6,569,202 B2 5/2003 Whiteside
6,589,281 B2 7/2003 Hyde, Jr.
6,605,117 B2 8/2003 Kuberasampath et al.
6,620,197 B2 9/2003 Maroney et al.
6,626,946 B1 9/2003 Walch et al.
6,673,114 B2 1/2004 Hartdegen et al.
6,673,115 B2 1/2004 Resch et al.
6,679,916 B1 1/2004 Frankle et al.
6,692,563 B2 2/2004 Zimmermann
6,730,252 B1 5/2004 Teoh et al.
6,736,851 B2 5/2004 Maroney et al.
6,746,487 B2 6/2004 Scifert et al.
6,749,637 B1 6/2004 Bähler
6,755,866 B2 6/2004 Southworth
6,761,740 B2 7/2004 Tornier
6,767,928 B1 7/2004 Murphy et al.
6,780,190 B2 8/2004 Maroney
6,783,549 B1 * 8/2004 Stone A61B 17/1684 623/18.11
6,790,234 B1 * 9/2004 Frankle A61F 2/40 623/19.12
6,797,006 B2 9/2004 Hodorek
6,863,690 B2 3/2005 Ball et al.
6,875,234 B2 4/2005 Lipman et al.
6,887,277 B2 5/2005 Rauscher et al.
6,890,358 B2 5/2005 Ball et al.
6,902,584 B2 6/2005 Kwan et al.
6,942,699 B2 9/2005 Stone et al.
6,953,478 B2 10/2005 Bouttens et al.
6,969,406 B2 11/2005 Tornier
7,011,686 B2 * 3/2006 Ball A61F 2/4014 623/19.14
7,033,395 B2 4/2006 Cauthen
7,051,417 B2 5/2006 Michelson
7,066,959 B2 6/2006 Errico et al.
7,108,719 B2 9/2006 Horber
7,166,132 B2 1/2007 Callaway et al.
7,169,184 B2 1/2007 Dalla Pria
7,175,663 B1 2/2007 Stone
7,195,645 B2 3/2007 DiSilvestro et al.
7,238,207 B2 7/2007 Blatter et al.
7,238,208 B2 7/2007 Camino et al.
7,250,550 B2 7/2007 Overby et al.
7,297,163 B2 11/2007 Huebner
7,309,360 B2 12/2007 Tornier et al.
7,329,284 B2 2/2008 Maroney et al.
7,338,498 B2 3/2008 Long et al.
7,338,528 B2 3/2008 Stone et al.
7,462,197 B2 * 12/2008 Tornier A61F 2/4081 623/19.12
7,520,898 B2 * 4/2009 Re A61B 17/1714 623/13.14
7,604,637 B2 * 10/2009 Johnson A61F 2/30724 606/81
8,062,376 B2 * 11/2011 Shultz A61F 2/40 623/19.12
8,366,713 B2 * 2/2013 Long A61B 17/1675 606/80
8,414,586 B2 * 4/2013 Cawthan A61B 17/1666 606/81
8,864,834 B2 10/2014 Boileau et al.
8,974,536 B2 3/2015 Walch et al.
9,089,435 B2 7/2015 Walch et al.
9,408,652 B2 8/2016 Hassler et al.
10,251,755 B2 4/2019 Boileau et al.
10,413,416 B2 9/2019 Boileau et al.
10,695,195 B2 6/2020 Hassler et al.
2001/0032021 A1 10/2001 McKinnon
2001/0047210 A1 11/2001 Wolf
2001/0049561 A1 12/2001 Dews et al.
2002/0032484 A1 3/2002 Hyde, Jr.
2002/0099381 A1 7/2002 Maroney
2002/0138148 A1 9/2002 Hyde, Jr.
2002/0143402 A1 10/2002 Steinberg
2002/0151982 A1 10/2002 Masini
2002/0177901 A1 11/2002 Howie
2003/0009171 A1 1/2003 Tornier
2003/0065397 A1 * 4/2003 Hanssen A61F 2/34 623/23.23
2003/0097183 A1 5/2003 Rauscher et al.
2003/0114933 A1 6/2003 Bouttens et al.
2003/0125809 A1 7/2003 Iannotti et al.
2003/0149485 A1 8/2003 Tornier
2003/0158605 A1 8/2003 Tornier
2003/0181916 A1 * 9/2003 Wolford A61B 17/1666 606/81
2004/0002765 A1 * 1/2004 Maroney A61F 2/4014 623/19.12
2004/0006392 A1 1/2004 Grusin et al.
2004/0030394 A1 * 2/2004 Horber A61F 2/4014 623/19.12
2004/0034431 A1 2/2004 Maroney et al.
2004/0064189 A1 * 4/2004 Maroney A61F 2/30734 623/19.13
2004/0064190 A1 4/2004 Ball et al.
2004/0068320 A1 4/2004 Robie et al.
2004/0133276 A1 7/2004 Lang et al.
2004/0138754 A1 7/2004 Lang et al.
2004/0148033 A1 7/2004 Schroeder
2004/0193168 A1 * 9/2004 Long A61B 17/1684 606/80
2004/0193276 A1 9/2004 Maroney et al.
2004/0193277 A1 9/2004 Long et al.
2004/0193278 A1 9/2004 Maroney et al.
2004/0210317 A1 10/2004 Maroney et al.
2004/0220673 A1 11/2004 Pria
2004/0220674 A1 11/2004 Pria
2004/0225367 A1 11/2004 Glien et al.
2004/0230197 A1 11/2004 Tornier et al.
2004/0249383 A1 * 12/2004 White A61B 17/1666 606/80
2004/0267370 A1 12/2004 Ondrla
2005/0008672 A1 1/2005 Winterbottom et al.
2005/0010304 A1 1/2005 Jamali
2005/0015154 A1 1/2005 Lindsey et al.
2005/0033443 A1 2/2005 Blatter et al.
2005/0043805 A1 2/2005 Chudik
2005/0049709 A1 3/2005 Tornier
2005/0060039 A1 3/2005 Cyprien
2005/0065612 A1 3/2005 Winslow
2005/0085919 A1 4/2005 Durand-Allen et al.
2005/0085921 A1 4/2005 Gupta et al.
2005/0090902 A1 4/2005 Masini
2005/0107882 A1 5/2005 Stone et al.
2005/0113837 A1 * 5/2005 Salyer A61B 17/1666 606/80
2005/0113931 A1 5/2005 Horber
2005/0119531 A1 6/2005 Sharratt
2005/0143818 A1 6/2005 Yuan et al.
2005/0143829 A1 6/2005 Ondrla et al.

(56) **References Cited**

U.S. PATENT DOCUMENTS

2005/0159751	A1*	7/2005	Berthusen	A61B 17/1666 606/80
2005/0165490	A1	7/2005	Tornier	
2005/0177241	A1	8/2005	Angibaud et al.	
2005/0186247	A1	8/2005	Hunter et al.	
2005/0197708	A1	9/2005	Stone et al.	
2005/0209700	A1	9/2005	Rockwood, Jr. et al.	
2005/0216092	A1	9/2005	Marik et al.	
2005/0240267	A1	10/2005	Randall et al.	
2005/0245934	A1	11/2005	Tuke et al.	
2005/0251263	A1	11/2005	Forrer et al.	
2005/0256584	A1	11/2005	Farrar	
2005/0267590	A1	12/2005	Lee	
2005/0278030	A1	12/2005	Tornier et al.	
2005/0278031	A1	12/2005	Tornier et al.	
2005/0278032	A1	12/2005	Tornier et al.	
2005/0278033	A1	12/2005	Tornier et al.	
2005/0288681	A1	12/2005	Klotz et al.	
2005/0288791	A1	12/2005	Tornier et al.	
2006/0004462	A1	1/2006	Gupta	
2006/0009852	A1	1/2006	Winslow et al.	
2006/0020344	A1	1/2006	Shultz et al.	
2006/0025796	A1	2/2006	Merced-O	
2006/0030946	A1	2/2006	Ball et al.	
2006/0111787	A1*	5/2006	Bailie	A61F 2/4081 623/908
2006/0122705	A1*	6/2006	Morgan	A61F 2/4081 623/19.11
2006/0195110	A1*	8/2006	White	A61B 17/1684 606/81
2006/0235539	A1*	10/2006	Blunn	A61B 17/1666 623/23.11
2006/0241775	A1	10/2006	Buss	
2007/0078516	A1	4/2007	Emami	
2007/0142916	A1	6/2007	Olson, Jr. et al.	
2007/0156250	A1	7/2007	Seitz, Jr. et al.	
2007/0173945	A1	7/2007	Wiley et al.	
2007/0179562	A1	8/2007	Nycz	
2007/0198087	A1	8/2007	Coleman et al.	
2007/0225817	A1	9/2007	Reubelt et al.	
2007/0225818	A1	9/2007	Reubelt et al.	
2007/0225821	A1	9/2007	Reubelt et al.	
2007/0244564	A1	10/2007	Ferrand et al.	
2007/0250174	A1	10/2007	Tornier et al.	
2007/0276509	A1	11/2007	Ratcliffe et al.	
2008/0183297	A1*	7/2008	Boileau	A61B 17/1637 623/16.11
2009/0125113	A1	5/2009	Guederian et al.	
2009/0270993	A1*	10/2009	Maisonneuve	A61B 17/1778 623/19.14
2009/0287309	A1*	11/2009	Walch	A61B 17/1739 623/18.11
2009/0292364	A1*	11/2009	Linares	A61B 17/686 623/19.13
2009/0306782	A1*	12/2009	Schwyzer	A61F 2/4003 623/19.12
2010/0280517	A1*	11/2010	Cawthan	A61B 17/1666 606/81
2010/0280518	A1*	11/2010	Gary	A61B 17/1666 606/84
2011/0098822	A1	4/2011	Walch et al.	
2011/0166661	A1	7/2011	Boileau et al.	
2011/0213372	A1*	9/2011	Keefer	A61B 17/1735 606/85
2011/0264153	A1	10/2011	Hassler et al.	
2014/0058523	A1	2/2014	Walch et al.	
2015/0297354	A1	10/2015	Walch et al.	
2019/0358045	A1	11/2019	Boileau et al.	

FOREIGN PATENT DOCUMENTS

DE	1950937	U	12/1966
DE	19630298	A1	1/1998
EP	0257359	B1	11/1991
EP	0299889	B1	3/1992
EP	0524857	A1	1/1993
EP	0617934	A1	10/1994
EP	0549480	B1	8/1997
EP	0599429	B1	10/1997
EP	0797964	A1	10/1997
EP	0679375	B1	9/1998
EP	0864306	A2	9/1998
EP	0712617	B1	9/1999
EP	0715836	B1	10/2001
EP	0664108	B1	8/2002
EP	0809986	B1	10/2002
EP	0927548	B1	5/2003
EP	0807426	B1	10/2003
EP	1062923	B1	1/2004
EP	1380274	A1	1/2004
EP	0903128	B1	5/2004
EP	1195149	B1	7/2005
EP	1064890	B1	9/2005
EP	1477120	B1	2/2007
EP	0903127	B1	6/2007
EP	1570816	B1	2/2008
EP	1652482	B1	3/2008
EP	1607069	B1	12/2009
EP	1402853	B1	5/2010
EP	1402854	B1	7/2010
EP	1323395	B1	8/2016
EP	1952771	B1	10/2016
EP	1952788	B1	2/2018
EP	3335676	A1	6/2018
FR	2248820	B1	6/1976
FR	2216981	B1	5/1979
FR	2574283	B1	9/1989
FR	2545352	B1	1/1990
FR	2699400	B1	2/1995
FR	2704747	B1	7/1995
FR	2726994	B1	4/1997
FR	2737107	B1	9/1997
FR	2652498	B1	12/1997
FR	2664809	B1	12/1997
FR	2721200	B1	9/1999
FR	2835425	B1	4/2004
FR	2836039	B1	10/2004
SU	749392	A1	7/1980
WO	1991007932	A1	6/1991
WO	1993009733	A1	5/1993
WO	1996017553	A1	6/1996
WO	1998046172	A1	10/1998
WO	1999049792	A1	10/1999
WO	1999065413	A1	12/1999
WO	2000015154	A1	3/2000
WO	2000041653	A1	7/2000
WO	2000062718	A1	10/2000
WO	2001047442	A1	7/2001
WO	2002039931	A1	5/2002
WO	2002039933	A1	5/2002
WO	2002049516	A1	6/2002
WO	2002067821	A2	9/2002
WO	2003005933	A2	1/2003
WO	2003092513	A1	11/2003
WO	2003094806	A1	11/2003
WO	2006039483	A2	4/2006
WO	2007109291	A2	9/2007
WO	2007109319	A2	9/2007
WO	2007109340	A2	9/2007
WO	2008015724	A2	2/2008

OTHER PUBLICATIONS

"Aequalis-Fracture Suture Technique in 5 Steps," Tornier, Inc., in 2 pages.

"Aequalis-Glenoid Keeled and Pegged—Surgical Technique," Tornier, Inc., in 12 pages.

"Aequalis Press-Fit Shoulder Prosthesis—Surgical Technique," Tornier, Inc., in 27 pages.

"Aequalis Resurfacing Head", retrieved from http://www/tornier-us.com/upper/shoulder/shorec004/index.php?pop+1 on Apr. 14, 2010.

(56) **References Cited**

OTHER PUBLICATIONS

"Aequalis-Reversed™ Shoulder Prosthesis, Surgical Technique," Tornier, Inc., in 24 pages.
"Anatomic Glenoid, Surgical Technique," Smith & Nephew, Inc., Feb. 2000 in 6 pages.
"Anatomical Shoulder™—Cemented Shoulder Prosthesis Product Information and Surgical Technique," Sulzer Medica, 2000, in 30 paqes.
"Anatomical Shoulder™ System—The new removable head option," Zimmer Inc., 2004 in 6 paqes.
"Anatomical Shoulder™ System Surgical Technique—Removable head option for improved surgical results," Zimmer, Inc., 2004, in 33 paqes.
Apoil, A., "A Condyle for the Rotator Cuff Muscles: The Total Shoulder Prosthesis," Aesculap—ICP S.A., Feb. 1994, in 4 paqes.
Bigliani/Flatow®—The Complete Shoulder Solution, Designed by Shoulder Surgeons for Shoulder Surgery, Zimmer, Inc., 2001 in 6 paqes.
"Bigliani/Flatow®—The Complete Shoulder Solution, Total Shoulder Arthroplasty Surgical Technique," Zimmer, Inc., 2003, in 30 paqes.
Bigliani/Flatow®—The Complete Shoulder Solution, 4-Part Fracture of the Humerus Surgical Technique, Zimmer, Inc., 2001.
"Bio-Modular®/ Bi-Polar Shoulder Arthroplasty," Biomet, Inc., 1997, in 2 pages.
"Bio-Modular® Choice—Shoulder System—Surgical Technique," Biomet Orthopedics, Inc., 2004, in 16 paqes.
"Bio-Modular Total Shoulder Surgical Technique," Biomet Orthopedics, Inc., 2001.
Boileau, P., et al. "Adaptability and modularity of shoulder prosthese," Maitrise Orthopedique, https://www.maitriseorthop.com/corpusmaitri/orthopaedic/prothese_epaule_orthop/boileau_u s.shtml, downloaded Jan. 3, 2006.
Boileau, P., et al. "Arthroscopic Repair of Full-Thickness Tears of the Supraspinatus: Does the Tendon Really Heal?" The Journal of Bone and Joint Surgery, Inc., Jun. 2005, 87A(6): 1229-1240.
Buechel, F.F., "Buechel-Pappas™ Modular Salvage Shoulder System, Surgical Procedure," Endotec, Inc., Aug. 2001, in 8 pages.
Buechel, F.F., "Buechel-Pappas™ Resurfacing Shoulder System, Surgical Procedure" Endotec, Inc., Aug. 2000, in 8 paqes.
Buechel, F.F., "Buechel-Pappas™ Total Shoulder System, Surgical Procedure," Endotec, Inc., Aug. 2000, in 16 pages.
Cofield, R.H., "Cofield2 Total Shoulder System, Surgical Technique," Smith & Nephew, 1997, in 32 pages.
"Copeland™ Humeral Resurfacing Head," Biomet Orthopedics, Inc., 2001, in 12 pages.
"Delta CTA™ Reverse Shoulder Prosthesis—Surgical Technique," DePuy International Ltd., revised Aug. 2004, in 28 pages.
"Design Rationale," Latitude® Total Elbow, pp. 3-38.
Fenlin, Jr., J.M., "Total Glenohumeral Joint Replacement," Symposium on Surgery of the Shoulder, Orthopedic Clinics of North America, Apr. 1975, 6(2): 565-583.
"Global C.A.P. TM Surgical Technique, Resurfacing Humeral Head Implant," DePuy International, Ltd., revised Oct. 2004, in 23 pages.
Hertel, R., "Technical considerations for implantation of Epoca glenoid components (Leseprobe)," Epoca Newsletter, May 14, 2001, in 1 page.
Klein, T.J., et al., "Mechanically Favorable Bone Remodeling in Rotator Cuff Arthropathy Patients with Good Function," Minneapolis Sports Medicine Center and University of Minnesota, in 2 paqes.
Mansat, M., "Neer 3™, Surgical Technique for Fractures," Smith & Nephew, Sep. 2000, in 19 pages.
Nicholson, G.P., "Chapter 7: Arthroplasty and Rotator Cuff Deficiency," Shoulder Arthroplasty, 2005, DD. 149-166.
"Offset Head: Bio-Modular® Total Shoulder," Biomet, Inc. 2000 in 2 pages.
"The Foundation® Total Shoulder System," Encore Surgical, in 2 pages.
"The Townley Modular Shoulder—Design by Reason," Biopro, Inc., in 2 pages.
"Tornier Surgical Technique Addendum, Tornier Aequalis® Reversed Hemi-Adaptor Technique," Tornier, Inc., Aug. 8, 2005.
"Tornier Surgical Technique Addendum, Aequalis® Reversed Shoulder Polyethylene Insert," Tornier, Inc., Oct. 8, 2005, in 1 page.
"Zimmer® Shoulder Retractors," Zimmer, Inc., 2000, in 2 pages.
On-Final Office Action issued in connection with U.S. Appl. No. 14/754,506, Jul. 19, 2022, 9 pages.
Final Office Action issued in connection with U.S. Appl. No. 14/574,506, Mar. 18, 2022, 15 pages.
Non-Final Office Action issued in connection with U.S. Appl. No. 14/754,506, Sep. 23, 2021, 11 pages.

* cited by examiner

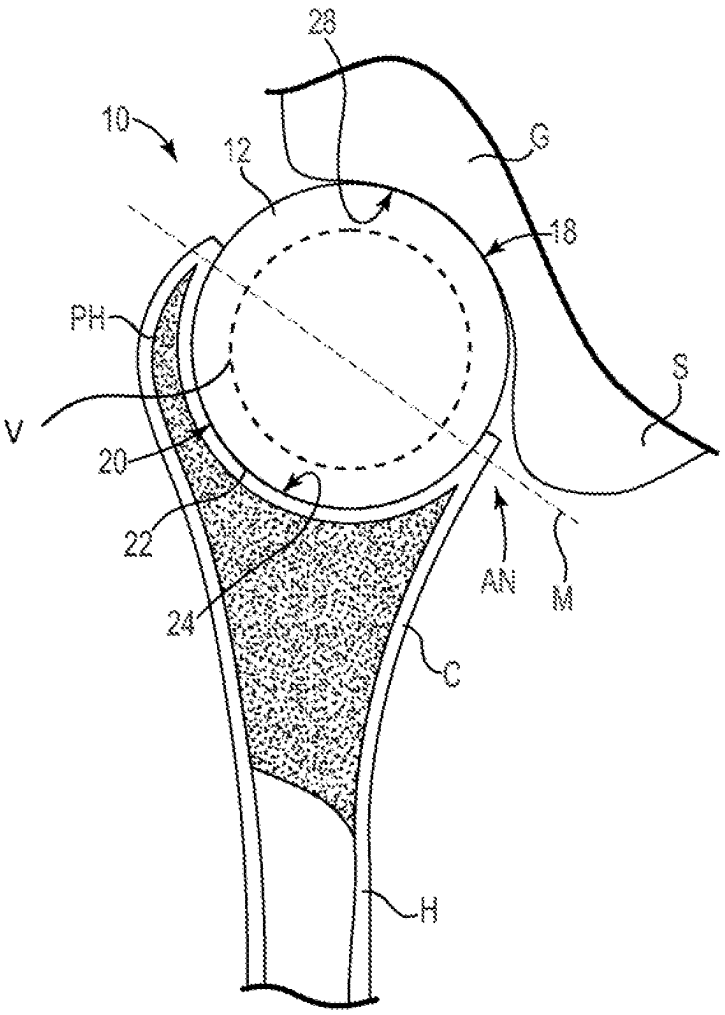


Fig. 1

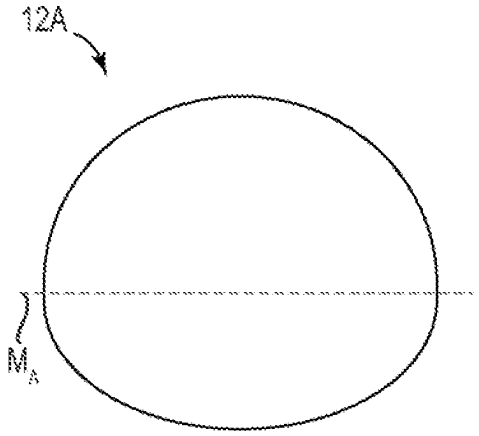


Fig. 2

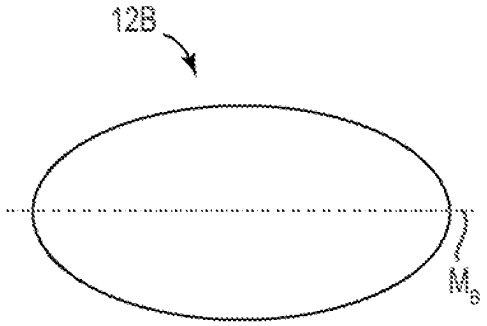


Fig. 3

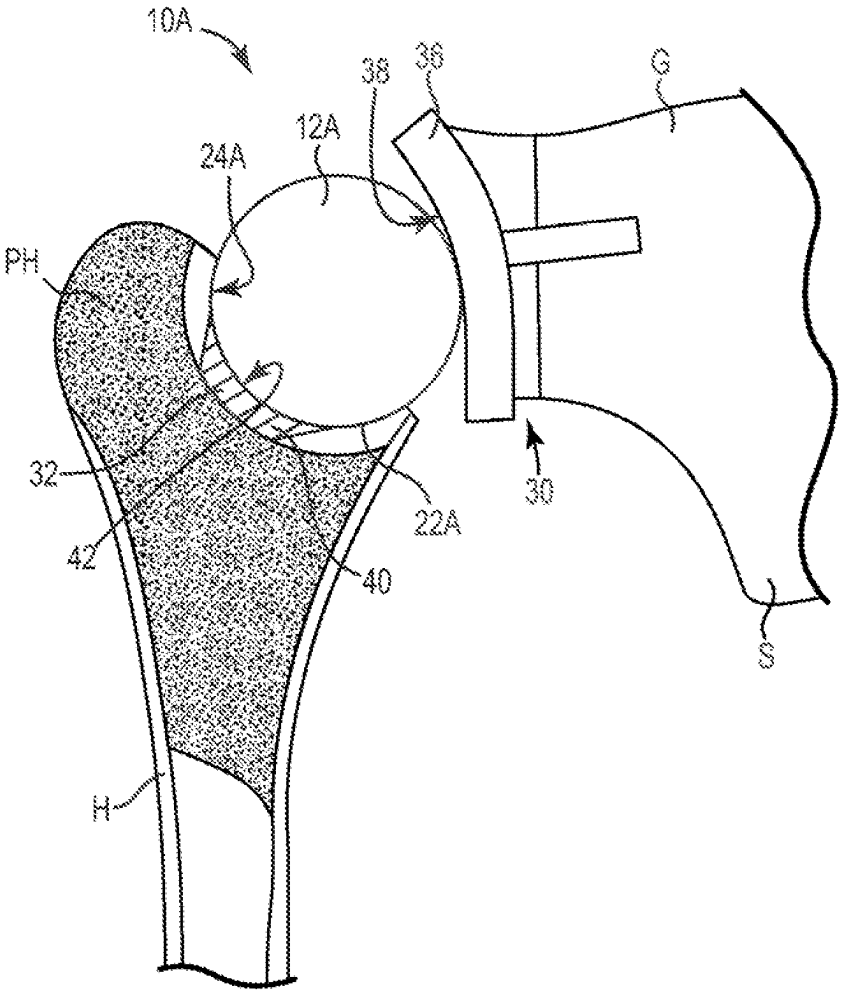


Fig. 4

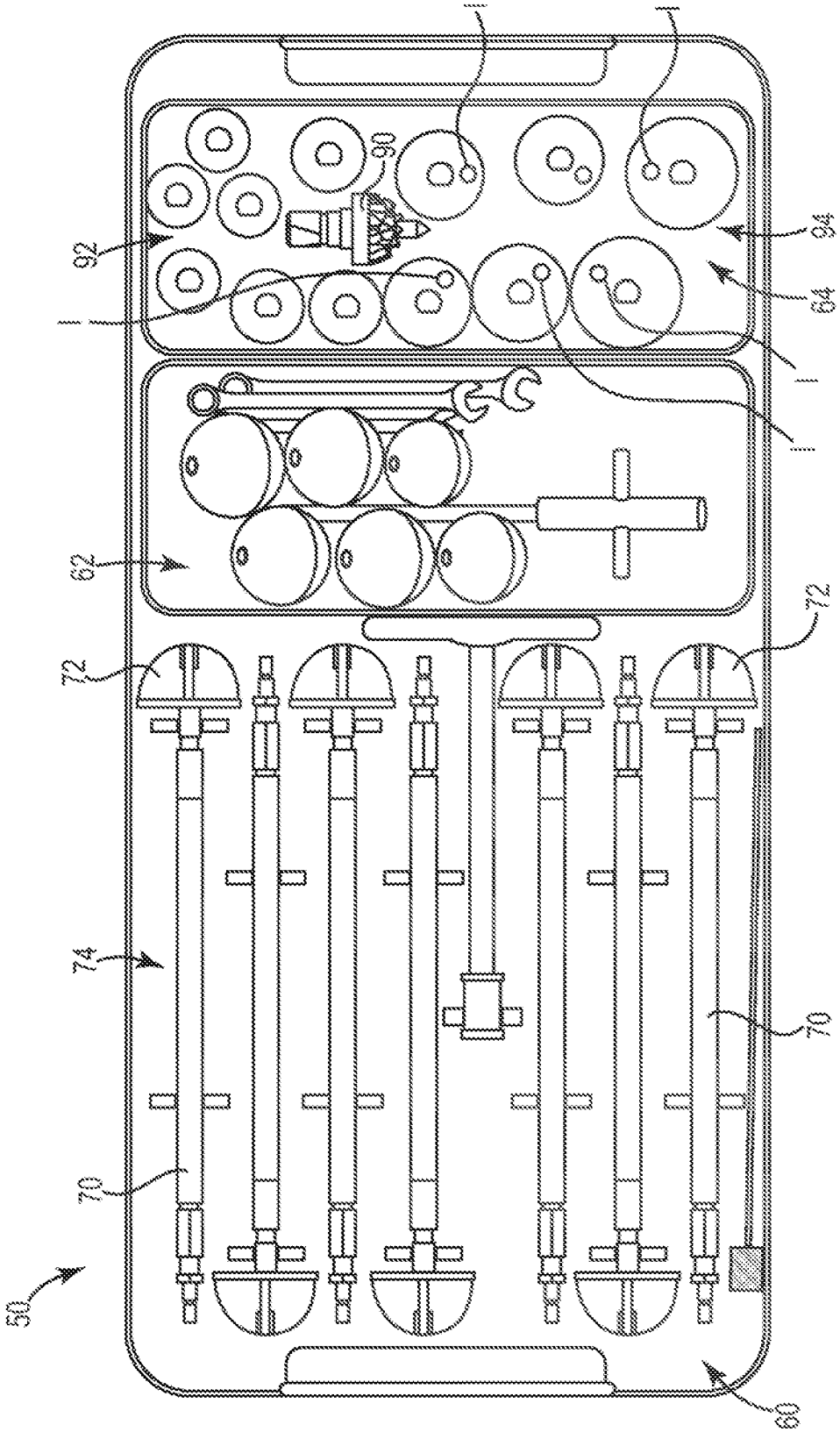


Fig. 5

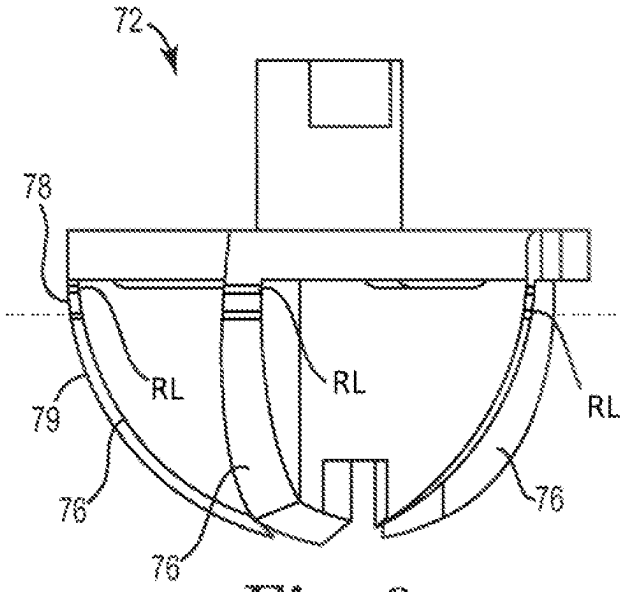


Fig. 6

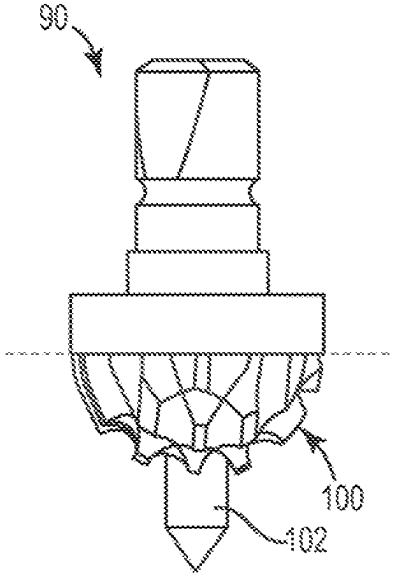


Fig. 8

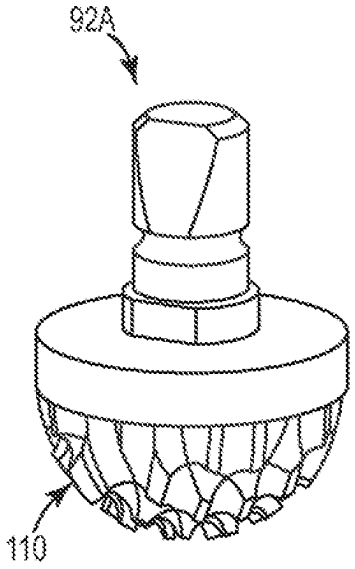


Fig. 9

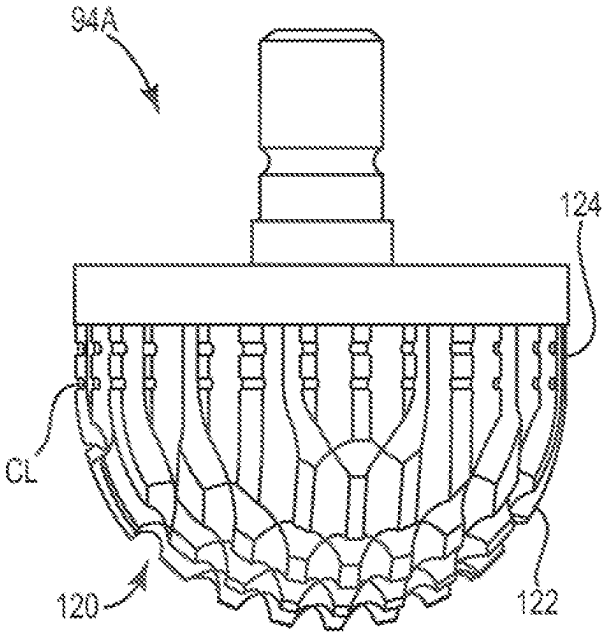


Fig. 10

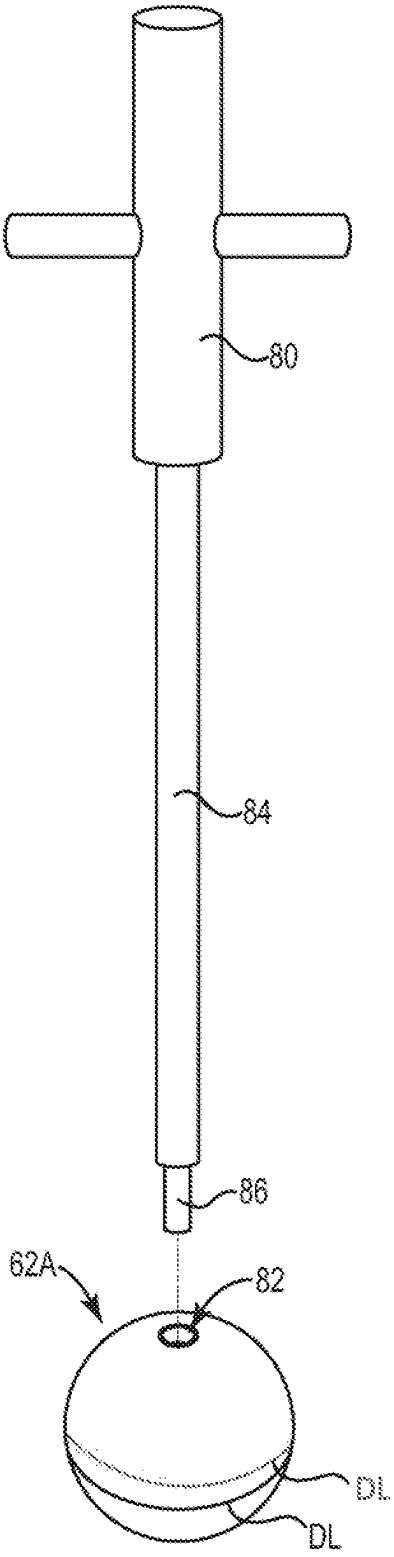


Fig. 7

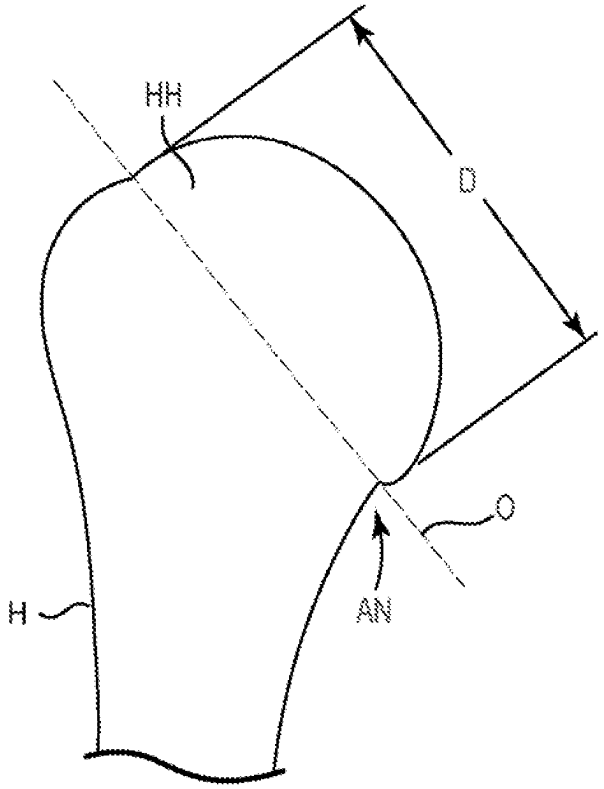


Fig. 11

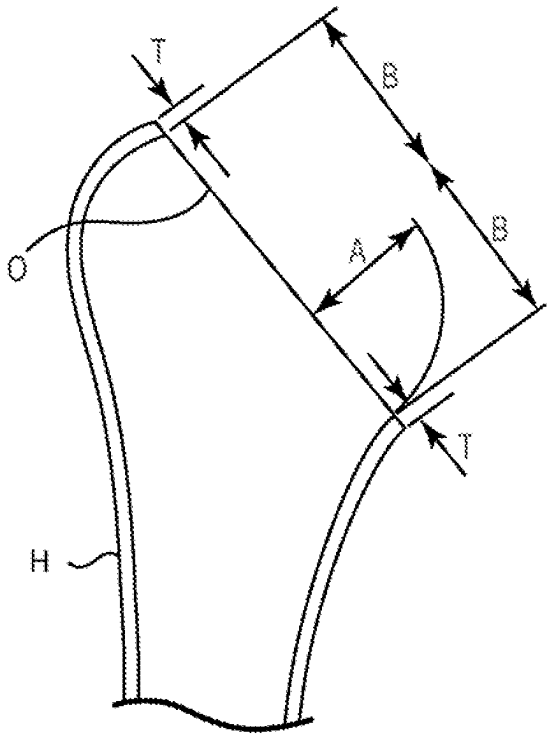


Fig. 12

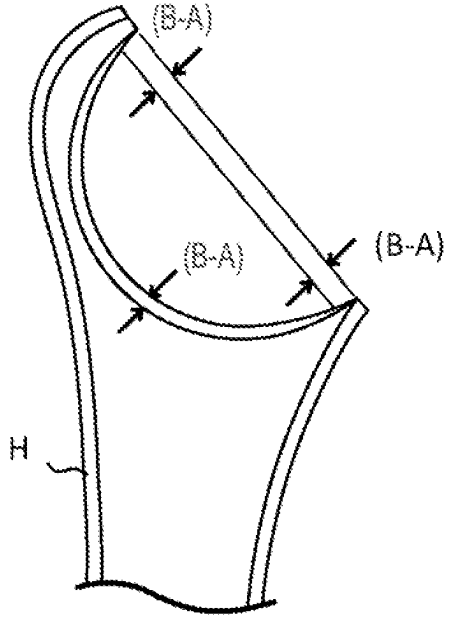


Fig. 13

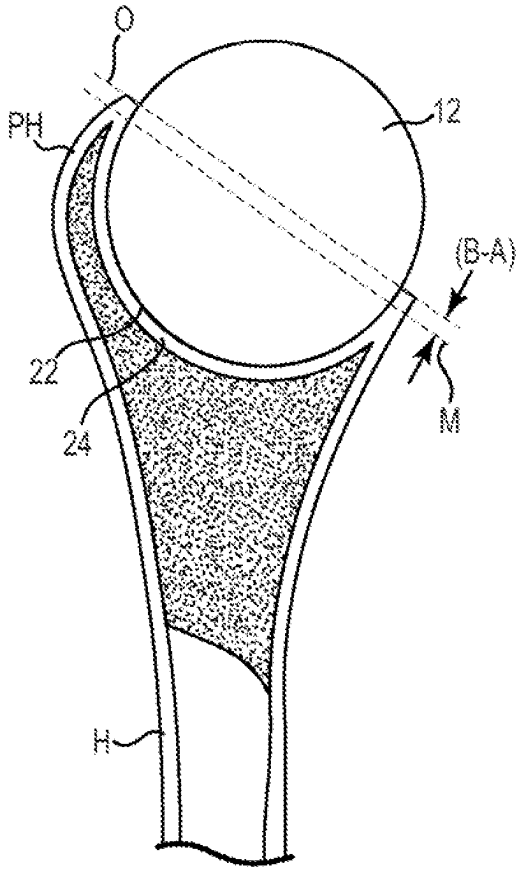


Fig. 14

INTRA-ARTICULAR JOINT REPLACEMENT AND METHOD

CROSS REFERENCE TO RELATED APPLICATIONS

This application is a divisional of a co-pending U.S. patent Application Ser. No. 16/875,729, filed on May 15, 2020, which is a continuation of U.S. patent application Ser. No. 15/224,188, filed on Jul. 29, 2016 (U.S. Pat. No. 10,695,195), which is a divisional of U.S. patent application Ser. No. 12/768,154, filed on Apr. 27, 2010 (U.S. Pat. No. 9,408,652), which are all hereby incorporated by reference in their entirety.

BACKGROUND

One type of method used to replace damaged joints (e.g., shoulder joints) is interpositional arthroplasty. The method of interpositional arthroplasty uses tissue from the patient or an artificial replacement to repair a damaged or malformed joint. An interpositional implant is positioned at the joint to act as an engagement surface between two adjacent bone structures to allow articular movement.

SUMMARY

Some embodiments relate to a method of implanting a prosthesis to repair a joint. The method includes displacing a first bone from the joint formed by an intersection between the first bone and a second bone. An end portion of the first bone is resected to define a resected end. A concavity is formed into the resected end using a shaping tool. The bone is compacted to form a support layer lining the concavity. The prosthesis is implanted in the concavity against the support layer without attaching the prosthesis to the support layer, the prosthesis including a first surface and a second surface opposite the first surface, each of the first and second surfaces being substantially convex in shape. The joint is reformed with the prosthesis such that the prosthesis remains unattached to the support layer and the first and second bones articulate about the prosthesis.

Some embodiments relate to a bone recess forming tool. The tool includes a forming head having a forming surface defining a convex hemispherical portion and an upswept portion extending beyond the convex hemispherical portion, the forming surface being adapted to form a recess into a bone.

Still other embodiments relate to a surgical kit of parts for implanting joint prostheses available in a plurality of graduating diameters. The kit includes a plurality of test prostheses each graduating in diameter such that each one of the test prostheses has a diameter corresponding to one of the available graduating diameters of the joint prosthesis. The kit also includes a plurality of reamers each graduating in diameter such that each one of the reamers has a diameter corresponding to one of the available graduating diameters of the joint prosthesis. The kit also includes a plurality of compactors each graduating in diameter such that each one of the compactors has a diameter corresponding to one of the available graduating diameters of the joint prosthesis. Each one of the test prostheses, reamers, and compactors having the same diameter forms an operational tool set for implanting a joint prosthesis of the same diameter, and further wherein each of the test prostheses, reamers, and compactors include colored indicia indicating to which operational tool set a particular test prosthetic, reamer, and compactor belongs.

While multiple embodiments are disclosed, still other embodiments of the present invention will become apparent to those skilled in the art from the following detailed description, which shows and describes illustrative embodiments of the invention. Accordingly, the drawings and detailed description are to be regarded as illustrative in nature and not restrictive.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. **1** shows a joint system, according to some embodiments.

FIG. **2** shows an interpositional implant, according to some embodiments.

FIG. **3** shows another interpositional implant, according to some embodiments.

FIG. **4** shows another joint system, according to some embodiments.

FIG. **5** shows a surgical kit, according to some embodiments.

FIG. **6** shows a reamer of the surgical kit of FIG. **5**, according to some embodiments.

FIG. **7** shows a test implant and handle of the surgical kit of FIG. **5**, according to some embodiments.

FIG. **8** shows a starter compactor of the kit of FIG. **5**, according to some embodiments.

FIG. **9** shows an initial compactor of the kit of FIG. **5**, according to some embodiments.

FIG. **10** shows a final compactor of the kit of FIG. **5**, according to some embodiments.

FIGS. **11-14** are illustrative of a method of implanting and forming the joint system of FIG. **1**, according to some embodiments.

While the invention is amenable to various modifications, permutations, and alternative forms, specific embodiments have been shown by way of example in the drawings and are described in detail below. The intention, however, is not to limit the invention to the particular embodiments described. On the contrary, the invention is intended to cover all modifications, equivalents, and alternatives falling within the scope of the invention as defined by the appended claims.

DETAILED DESCRIPTION

FIG. **1** is a schematic view of a joint system **10** (e.g., a glenohumeral joint system) including an interpositional implant **12**, a first boney structure, or bone (e.g., a humerus H) and a second boney structure, or bone (e.g., a glenoid G), where the first and second boney structures articulate about the interpositional implant **12**. As shown in FIG. **1**, in some embodiments, the interpositional implant **12** is interposed between the two boney structures—the humerus H and the glenoid G—to help repair joint function. Although the implant **12** is primarily discussed as being implanted in a human patient's shoulder, the implant **12** may also be modified and implanted in other locations. For example, the implant **12** is optionally modified to be implanted between a variety of boney structures in a hip, ankle, hand, foot, or other joint, for example, whether human or other animal.

Generally, the interpositional implant **12**, also described as an interpositional prosthesis, is formed as a single piece, or monolithic unit, and includes at least two convex surfaces, although implants formed of separate, connected parts

are contemplated. As shown, the implant **12** includes a convex first surface **18** and a convex second surface **20** opposed to the first surface **18**, though the interpositional implant **12** is optionally non-spherical and the surfaces **18**, **20** optionally have different radii of curvature from one other. As shown, the first surface **18** is in direct contact with the glenoid G, and in particular the glenoid cavity, and the second surface **20** is in direct contact with a portion of the humerus H.

The implant **12** generally defines a midline M between the first and second convex surfaces **18**, **20**. For example, while FIG. **1** shows a generally spherical, or spheroid shape for the interpositional implant **12**, while FIG. **2** shows an interpositional implant **12**A having an upper, spheroid portion above a midline M_A and a lower, spherical portion below the midline M_A having a different radius of curvature. FIG. **3** shows an interpositional implant **12**B having a more symmetrical spheroid shape (e.g., a prolate spheroid shape) above and below a midline M_B. In still other embodiments, the convexities of the first and/or second surfaces **18**, **20** are complex, including multiple radii, including the shapes described in U.S. Patent Application Publication 2007/0225818, filed Mar. 21, 2007, and titled "Non-Spherical Articulating Surfaces in Shoulder and Hip Replacement," the entire contents of which are incorporated herein by reference for all purposes. Moreover, although some shapes for the implant **12** have been described, a variety of shapes are contemplated, such as an egg-shaped implant, for example.

In some embodiments, the interpositional implant **12** defines the midline M in an antero-posterior plane and a height perpendicular to the midline M, for example in a supero-inferior plane). In the case of a sphere, the diameter of the sphere corresponds to both the width of the implant **12** along the midline M and the maximum effective height of the sphere perpendicular to the midline M. The implant **12** is formed of an outer layer of pyrocarbon, or pyrolytic carbon, over a graphite substrate or is formed substantially entirely of pyrocarbon, for example. Some examples of pyrolytic carbon implants and associated use for joint repair are described in U.S. Pat. No. 6,436,146, filed Jan. 18, 2000, and titled "Implant for Treating Ailments of a Joint or Bone," the entire contents of which is incorporated herein by reference for all purposes. In some embodiments, the interpositional implant **12** is characterized by a Young's Modulus of from about 10 GPa to about 35 GPa, for example, or from about 21 to about 28 GPa, for example, which is relatively low compared to the much higher Young's modulus of titanium implants. The interpositional implant **12** is optionally hollow or otherwise defines an internal void V as indicated in FIG. **1** by a broken circle. Although a single, substantially spherical void, or internal hollow portion, is indicated the void V optionally takes a variety of shapes and forms, including multiple voids (e.g., a plurality of larger voids or a plurality of smaller voids similar to a sponge structure) or other forms. By including one or more voids, the weight of the implant **12** is optionally reduced and/or other properties of the implant **12** are adjusted as desired.

As shown in FIG. **1**, the humeral head of the humerus H is removed, or resected, proximate the anatomical neck AN, where the humerus H defines a proximal humerus PH. The humerus defines a recess **22** that is substantially concave in shape, extending at least through a full hemispherical arc, although other shapes are also contemplated. The recess **22**, also described as a concavity or a pocket, has an articulation surface **24**, or reinforcement bed, that lines the recess **22** which, as described in greater detail below, is optionally formed via compacting and/or reaming methodology. The articulation surface **24** forms a reinforced bed, or liner, for contacting the interpositional implant **12**. As described in greater detail, the recess **22** is formed into epiphyseal/metaphyseal bone of the humerus H and optionally extends into the diaphysis in some embodiments, though typically preferential to limit the recess **22** to the metaphyseal bone. Where the recess **22** extends into the diaphysis, or where the metaphyseal bone is thin or has degenerated, a plug or plugs (e.g., made of bone from the humeral head (not shown) or other bone material) are optionally used to reinforce any holes or weak spots in the articulation surface **24** produced during formation. In some embodiments, and as described in greater detail below, the articulation surface **24** is formed of cortical or cortical-like bone C that forms over time following surgical insertion of the interpositional implant **12**. Generally, the depth of the recess **22** is measured or otherwise evaluated from the bottom of the recess **22** to a plane of the resected end of the humerus H, although other reference planes are employed as appropriate.

Generally, the interpositional implant **12** is not cemented, adhered, or otherwise fixed to the articulation surface **24**, leaving the interpositional implant **12** free to rotate in the recess **22**. In some embodiments, however, there is some frictional engagement between the recess and the interpositional implant **12**—for example, in association with press fitting the interpositional implant **12** into the recess **22** and/or following growth of the humerus H.

The glenoid G defines an articulation surface **28** and, in some embodiments, the articulation surface **28** corresponds to the natural glenoid cavity where no or very little surface modification is made to the glenoid cavity during implantation. Use of the implant **12** with an unmodified glenoid cavity can be particularly beneficial for partial replacement of a shoulder joint in cases where the rotator cuff is still functional. In other embodiments, the articulation surface **28** is formed into the scapula S at the glenoid cavity (e.g., using the reaming and/or compacting methodology similar to that used with the humerus H (described in greater detail below) or a glenoid component is attached to the glenoid G for interacting with the implant **12** as shown in FIG. **4**.

As shown in FIG. **1**, and as discussed in greater detail below, the interpositional implant **12** optionally interacts directly with an articulation surface **28** of the glenoid G, e.g., without any intermediate components between the interpositional implant **12** and the glenoid cavity. In some embodiments, and as shown in FIG. **1**, the interpositional implant **12** also interacts directly with the articulation surface **24**, which is formed in the humerus H according to some methods of preparing the humerus H for receiving the interpositional implant **12**.

In other embodiments, and as shown in FIG. **4**, a joint system **10**A further includes one or both of a glenoid component **30** (e.g., implanted in a scapula S of the glenoid G) and/or a humeral component **32**, such as those described in U.S. Patent Application Publication 2009/0287309 ("the '309 Publication"), filed Dec. 17, 2008, and titled "Intra-Articular Joint Replacement," the entire contents of which is incorporated herein by reference for all purposes.

The glenoid component **30** includes an articular member **36** with a generally concave articular surface **38** that engages interpositional implant **12**A, where the interpositional implant **12**A is optionally substantially similar to the implant **12** and is laterally remote from the resected surface of the glenoid G in the sense that, if the articular member **36** were

omitted, the interpositional implant **12**A would be directly juxtaposed with the glenoid G (e.g., as is shown in the system **10** of FIG. **1**).

The humeral component **32** optionally supplements, or reinforces, a recess **22**A in the humerus H, where the recess **22**A defines articulation surface **24**A substantially similar to articulation surface **24**. The humeral component **32** optionally includes an articular member **40** with a generally concave surface **42** formed from a resected portion of the humerus H and installed in the recess **22**A according to similar methodology to that described in the '309 Publication, for example. Where both the glenoid and humeral components **30**, **32** are present, the interpositional implant **12**A is positioned between the articular member **36** of the glenoid component **30** and the articular member **40** of the humeral component **16**A—the radius of the interpositional implant **12**A being typically equal to or less than the radii of the concave articular surfaces **38**, **42**.

FIG. **5** illustrates a surgical kit **50**, or kit of parts, used in association with some surgical methods for implanting the interpositional implant **12**. The kit **50** includes a plurality of reamers **60**, a plurality of test implants **62**, and a plurality of compactors **64**. The kit **50** also optionally includes wrenches, pilot hole tips/bits, cleaning tips/bits, and other components as desired. In some embodiments, the kit **50** is prepackaged as a sterile unit and/or is adapted to be sterilized prior to use (e.g., via autoclave).

In some embodiments, the plurality of reamers **60** are described as forming or shaping tools and are provided in graduating sizes. The plurality of reamers **60** are generally indicated for use in preparing the recess **22** in the resected end of the humerus H. Each of the plurality of reamers includes a shaft **70** and a cutting head **72**. In some embodiments, one of the plurality of reamers **60** is a starter reamer **74** having a smaller cutting head diameter than the other reamers **60**. The starter reamer **74** is optionally utilized early in the formation process of the recess **22** in order to form initial cuts into the resected head of the humerus H, for example. In some embodiments, the starter reamer **74** is cannulated and includes an optional pilot tip (not shown), such as a sharp thin projection inserted into the cannulated reamer and projecting from the reamer tip to guide the reaming process. The reamers **60** are optionally adapted to have reaming diameters graduating in size from about 34 mm to about 46 mm (e.g., in 2 mm increments), although a variety of dimensions are contemplated.

Each shaft **70** is optionally color coded and/or otherwise marked with indicia (e.g., lettering) which, as described in greater detail, indicates whether a particular reamer **60** belongs to a corresponding operational tool set, where the tool sets are generally grouped by size (e.g., corresponding to an expected size for the implant **12** to be placed in the resected head of the humerus H). The cutting head **72** of one of the plurality of reamers **60** is shown in FIG. **6**, according to some embodiments. Each of the reamers **60** is optionally substantially similar other than differing generally in reaming diameter, and as such the cutting heads of the plurality of reamers **60** are described collectively with reference to the head **72** shown in FIG. **6**.

As shown in FIG. **6**, the head **72** is generally dome-shaped and includes a plurality of arcuate blades **76**, the profiles of which define a cutting or forming surface. In particular, the head **72** has a substantially convex outer profile such that the head **72** is adapted to cut, or carve a generally concave recess into bone, e.g., into the resected head of the humerus H. The convex outer profile of the cutting head **72** extends at least through a full hemispherical arc that defines a reaming diameter of the cutting head **72**. In some embodiments, the head **72** is adapted to cut at least a full hemisphere and optionally includes an extended cutting portion **78** sweeping upward beyond a hemispherical cutting portion **79** of the cutting head **72**. By extending the diameter of cut to a full hemisphere or more, the head **72** is adapted to form fully hemispherical recesses and recesses deeper than the diameter of cut of the cutting head **72**. In some embodiments, the extended cutting portion **78** includes one or more demarcation lines RL for indicating one or more selected reaming depths (two are shown in FIG. **6**, though more or less are employed as appropriate). In some embodiments, a first one of the demarcation lines RL is located approximately at a height corresponding to the transition from the hemispherical cutting portion **79** to the extended cutting portion **78** and a second one of the demarcation lines RL is located a pre-determined height above the first demarcation line RL, although a variety of heights are contemplated. As shown, the demarcation lines RL are optionally grooves formed into the blades **76** that are adapted or otherwise configured to be viewed by a surgeon during reaming.

FIG. **7** shows a first test implant **62**A of the plurality of test implants **62** along with an associated handle **80** for manipulating the test implants **62**. In some embodiments, each of the test implants **62** is substantially similar other than differing generally in size and color, and as such the test implants **62** are described collectively with reference to the first test implant **62**A shown in FIG. **7**. Though the test implants **62** are shown as being substantially similar, it should be understood that test implants of differing shape, material, or other characteristic(s) are also contemplated.

As shown, the first test implant **62**A is substantially spherical, or spheroid, and has one or more test depth lines DL. In some embodiments, a first one of the test depth lines DL is located approximately at a height corresponding to an equator of the first test implant **62**A and a second one of the test depth lines DL is located a pre-determined height above the first test depth line DL, although a variety of heights are contemplated. Although two test depth lines DL are shown in FIG. **7**, a greater or fewer number are contemplated as appropriate. As referenced above, the first test implant **62**A is optionally color coded and is made of a material that is suitable for being temporarily implanted to check whether the implant **12** will perform as desired. The first test implant **62**A also includes a receptacle **82** for securing the first test implant **62**A to the handle **80**. For example, the receptacle **82** optionally includes female threads for mating with the handle **80**. In some embodiments, the test implants **62** having diameters graduating in size similar to the size selections available for the implant **12**, for example from about 36 mm to about 46 mm (e.g., in 2 mm increments), although a variety of dimensions are contemplated.

As shown, the handle **80** includes an elongate shaft **84** terminating with a tip **86** suitable for connecting to the test implants **62**. For example, the tip **86** is optionally provided with male threads for securing the tip **86** to receptacles in the test implants **62**, such as the receptacle **82** in the first test implant **62**A.

In some embodiments, the plurality of compactors **64** are described as forming or shaping tools and are provided in graduating sizes. Though generally used to form a compacted, more structurally sound surface, the compactors **64** are also optionally used to break up and remove pieces of bone as appropriate. In some embodiments, the plurality of compactors **64** include a starter compactor **90** (FIG. **8**) with an optional pilot tip, a plurality of initial compactors **92** (such as the one shown in FIG. **9**), and a plurality of final

compactors **94** (such as the one shown in FIG. **10**). As described further, and according to some methods, the starter compactor **90** is optionally used to begin the compacting process, one or more of the initial compactor **92** are used to continue the compacting process, and one of the final compactors **94** is used to finalize the recess **22** into a suitable depth and form for receiving the implant **12**.

The starter compactor **90** shown in FIG. **8** has a convex compacting surface **100**, also described as a forming surface, that extends through a hemispherical arc and is adapted to break up and compact bone (e.g., cancellous or spongy bone) as it forms a substantially concave cavity. As shown, the convex compacting surface **100** is generally equal to a full hemisphere in shape as designated by the broken line in FIG. **8**, although the compacting surface **100** is optionally extended beyond a full hemispherical shape. For example, in some embodiments the compacting surface **100** is continued to sweep beyond a hemispherical shape. As shown, the starter compactor **90** optionally includes a pilot tip **102** to help ensure an accurate starting point for forming the recess **22**. In some embodiments, the starter compactor **90** is adapted to have a forming/compacting diameter of about 20 mm, although a variety of dimensions are contemplated.

The initial compactors **92** graduate in size and, through an iterative process, can be used to progressively form a larger and larger compacted recess into the resected end of the humerus H. The initial compactors **92** are optionally substantially similar other than differing generally in size, and as such the initial compactors **92** are described collectively with reference to a first initial compactor **92**A shown in FIG. **9**. In some embodiments, the initial compactors **92** are adapted to have forming/compacting diameters graduating in size from about 22 mm to about 34 mm (e.g., in 2 mm increments), although a variety of dimensions are contemplated.

The first initial compactor **92**A has a compacting surface **110** adapted to break up and compact bone (e.g., cancellous or spongy bone) as it forms a substantially concave cavity with the compacting surface **110**. Similarly to the starter compactor **90**, the convex compacting surface **110** is equal to a full hemisphere in shape, although other configurations are contemplated. For example, in some embodiments the compacting surface **100** is continued and sweeps beyond the fully hemispherical shape.

The final compactors **94** also graduate in size and are each optionally color coded to a corresponding one of the reamers **60** and test implants **62** forming one of the operational sets. For example, as shown in FIG. **5**, each of the final compactors **94** includes indicia I, such as a colored dot, for indicating to which operational set the compactor **94** belongs. The final compactors **94** are optionally substantially similar other than differing generally in size, and as such the final compactors **94** are described collectively with reference to a first final compactor **94**A shown in FIG. **10**. In some embodiments, the final compactors **92** are adapted to have forming/compacting diameters graduating in size from about 36 mm to about 46 mm (e.g., in 2 mm increments), although a variety of dimensions are contemplated.

The first final compactor **94**A has a compacting surface **120** adapted to break up and compact bone (e.g., cancellous or spongy bone) as it forms a substantially concave cavity with the compacting surface **120**. As shown in FIG. **10**, the compacting surface **120** defines a hemispherical portion **122** and an upswept portion **124**, where the compacting surface is extended, sweeping upward along a substantially straight line beyond the hemispherical portion **122** through the upswept portion **124**. In at least this manner, the compacting surface **120** is adapted to form/compact the recess **22** to a full hemisphere and to a depth greater than the forming/compacting diameter while helping ensure that substantially all, or at least a greater portion of, the articulation surface **24** is compacted and thereby reinforced for receiving the implant **12**.

In some embodiments, the first final compactor **94**A defines one or more visible demarcation lines CL (e.g., a groove or line in the compacting surface **120**) at one or more predetermined heights from the bottom of the compacting surface **120** for delineating a desired forming/compacting depth at which to cease a compacting process. Although two demarcation lines CL are shown in FIG. **10**, embodiments with greater or fewer demarcation lines are contemplated as appropriate. In some embodiments, the demarcation lines CL are provided in regular increments (e.g., 2 mm) for indicating a plurality of formation/compaction depths. In some embodiments, a first one of the demarcation lines CL is located approximately at a height corresponding to the transition from the hemispherical portion **122** to the upswept cutting portion **124** and a second one of the demarcation lines CL is located a pre-determined height above the first demarcation line CL, although a variety of heights are contemplated. Moreover, in some embodiments the demarcation lines RL, the test depth lines DL, and/or the demarcation lines CL are provided at corresponding heights to one another, such that a single operational set (described in further detail below) has a uniform set of depth markings on the tool used in a surgical joint repair/replacement procedure to form the recess **22** to a demarcated depth using the markings on the compactors **60** and reamers **64** and test the performance of the recess **22** to that depth using the markings on the test implant **62**.

As referenced above, in some embodiments the reamers **60**, test implants **62**, and final compactors **94** graduate in size and are color coded and/or include indicia (e.g., writing) to group reamers **60**, test implants **62**, and compactors **64** into operational sets. For example, a single operational set is optionally designated by a single color, where the single operational set includes one of the reamers **60**, one of the test implants **62**, and one of the compactors **64**. Table 1 that follows is provided as an illustrative example and shows diametrical reaming/forming/test dimensions corresponding to a plurality of graduating, color coded operational sets, according to some embodiments, although other dimensions, color coding, and/or other indicia are contemplated.

TABLE 1

Operational Sets				
Operational Set	Diameter	Compactor Coding	Reamer Coding	Test Implant Coding
1	36 mm	Red	Red	Red
2	38 mm	Yellow	Yellow	Yellow
3	40 mm	Green	Green	Green
4	42 mm	Blue	Blue	Blue
5	44 mm	Grey	Grey	Grey
6	46 mm	White	White	White

In view of the foregoing, a surgeon or other user provided with the surgical kit **50** is able to quickly and reliably select an operational tool set for a particular implant size.

Some methods for implanting the interpositional implant **12** to form the joint system **10** are described below with reference to FIGS. **1-10** (previously discussed) and FIGS. **11-14** which are illustrative of a method of selecting an appropriate depth of implantation.

In some embodiments, a preoperative assessment of the existing (e.g., degenerated) joint system in the patient is performed. The preoperative assessment optionally includes using frontal and axillary radiographs, as well as CT scanning to evaluate orientation of the glenoid G, quality of bone stock in the humerus H and glenoid G, and any muscle degeneration of the rotator cuff, for example. Based upon the preoperative assessment, the surgeon makes an initial determination of the optimal size and/or shape of the implant **12**. In some embodiments, the implant **12** is available in a variety of diameters, where the surgeon or other user initially selects from a plurality of sizes (e.g., such as 36 mm, 38 mm, 40 mm, 42 mm, 44 mm, and 46 mm diameter spheres, although a variety of dimensions are contemplated). From the foregoing, in some embodiments, each of the sizes has a corresponding operational set to be used during implantation, such as those shown in Table 1.

Exposure of the humerus H and glenoid G is optionally accomplished via any of a variety of techniques. In some embodiments, the surgical incision is made using a deltopectoral approach to the humerus H and glenoid G. The incision is made from a tip of the coracoid process and follows the deltopectoral groove. The upper part of the pectoralis major is optionally released to improve external rotation, the clavipectoral fascia is incised at an outer edge of the coracobiceps, and the acromioclavicular ligament is partially severed to facilitate exposure of the sub-scapular and circumflex vessels. The circumflex vessels are then ligated to achieve hemostasis during the entire surgical procedure. The axillary nerve is identified and protected. After the superior arthrotomy, the subscapularis is incised with the capsule to about an inch and a half of the bicipital groove at the neck anatomy. By raising the arm in adduction and external rotation and retropulsion, the humeral head is then dislocated forward. The anterior capsule is released from front to back, allowing the exposure of osteophytes. Ultimately, the humeral head is freed and displaced from the glenoid G and exposed for processing.

As indicated in FIG. **11**, once dislocated, the humeral head HH is resected (e.g., at the anatomical neck AN) to form a resected end defining a resection plane O (FIG. **12**). Transverse dimensions of the anatomical neck AN or the resected humeral head are then measured using calipers or other measuring tool in at least two planes to assess the size of implant use. In some embodiments, the two planes are generally perpendicular to one another, such as the anteroposterior and superoinferior planes. In some embodiments, where the measurements along the planes are different from one another, the smallest of the measurements is selected as the humeral head size. In some embodiments, the implant size is either initially selected or is confirmed to be about 2 mm to about 4 mm below the humeral head size.

In order to determine a depth at which the implant **12** is to be installed (or alternatively, to what depth the recess **22** should be formed), the smallest of the resected end measurements is selected as the initial resected end diameter D.

As shown in FIG. **12**, based upon empirical or other data, the resected end diameter D is correlated to a predicted projection height A, also described as a desired projection height A, of the implant **12** above the resection plane O that will help ensure proper tensioning of the glenohumeral joint once the implant is received by the glenoid G and the joint has healed. For example, empirical data may be obtained relating to natural projection heights (i.e., in healthy joints) of the humeral head relative to humeral head diameter at the anatomical neck. A thickness of the cortical bone at the resection plane O is either estimated via empirical data or is directly measured using any of a variety of techniques (e.g., using a micrometer, radiographs, and others). In some embodiments, the implant diameter (and, therefore implant radius B) is selected by subtracting the thickness T of the cortical bone from the end diameter D (D−(2×T)=implant diameter). As shown in FIGS. **12** and **13**, generally, the radius B of the implant **12** is greater than the predicted projection height A, such that B minus A equals the depth the midline M of the implant **12** is preferably pushed down with respect to the resection plane O in order to help ensure the surface of the implant **12** projecting from the recess **22** is well-positioned for proper tensioning of the joint as shown in FIG. **14**. In terms of implant height, the depth the midline M is depressed with respect to the resection plane O is one-half the implant height minus the predicted projection height A.

In some embodiments, after a diameter of the implant **12** is selected and the depth of the recess **22** is determined, the recess **22** is formed according to a reaming and compacting process. With the implant diameter known, the surgeon selects the corresponding operational set (one of the reamers **60**, one of the test implants **62**, and one of the compactors **64**) for forming the recess **22**.

The reaming and compacting processes are generally used iteratively to form the recess **22** with an adequate depth. As previously referenced, the reamers **60** are well suited to forming a fully hemispherical and/or deeper shape for the recess **22** (in comparison to traditional reamers that terminate the cutting surface prior to a full hemisphere).

Similarly, the compactors **64** are also well suited to forming fully hemispherical recesses and/or deeper recesses. In some embodiments, the visible demarcation on each of the final compactors **94** (e.g., visible demarcation CL) corresponds to the desired depth to which the recess is to be formed and compacted relative to the resection plane O, which, in some embodiments is greater than the radius B of the implant **12** by an amount corresponding to the implant radius B minus the predicted projection height A. Using the visible demarcations, such as demarcation CL, a surgeon performing the compacting process is readily able to visualize when the desired recess depth has been achieved.

The compacting process is particularly useful to reinforce the articulation surface **24**. For example, compacting helps artificially densify the spongious metaphyseal bone, building a stronger lining or floor to receive the implant **12**. It has been surprisingly found that by using a relatively low Young's modulus for the implant **12** (e.g., low relative to titanium, for example), further bone densification of the articulation surface **24** is encouraged over time during operational loading, but without overly stressing the articulation surface **24**. Eventually, the bone density at the surface **24** may approach that of the cortical bone of the humerus, as generally indicated in FIG. **14** by the continuous, white region on the exterior surface and recess **22** of the humerus H.

In some embodiments, compaction begins with the starter compactor **90** (e.g., being of 20 mm diameter). The starter compactor **90** helps initially center the recess **22** in the middle of the resection plane O and ensures that the recess **22** remains centered during ensuing compacting/reaming with larger diameter tools.

Compaction of the metaphyseal bone continues by gradually increasing the diameter of compaction with the initial compactors **92** until one of the final compactors **94** corresponding to the operational set that has been selected is used to form the recess **22** to its final, predetermined size. The starter compactor **90** and initial compactors **92** are generally

only inserted to the depth of their respective compacting surfaces (e.g., only up to a single radial depth of cut) to help ensure that the recess **22** is not initially formed too deep. Thus, in some embodiments, each of the starter and initial compactors **90**, **92** is inserted to the end of the cutting surface, which marks the height corresponding to a hemisphere. In some embodiments, this also helps avoid risk of humeral fracture during the initial compacting phases.

Once the recess **22** is sufficiently formed, the final compactor **94** of the selected operational set is used to form the recess **22** to the predetermined depth by compacting the articulation surface **24** with the final compactor **94** until the demarcation line is generally parallel with the resection plane O. If, during the process, it appears that the final compactor **94** will contact the external cortical bone, or if the final compactor **94** actually begins to contact the cortical bone, the surgeon optionally switches to a smaller diameter for the implant **12**.

Additionally, where the quality of the metaphyseal bone is poor, the surgeon optionally strengthens the articulation surface **24** during compaction by packing pieces of bone grafts taken from the humeral head into the recess **22**. Depending on the quality of the bone in the humerus H, the compacting and reaming process can lead to an opening on the medullary canal at the bottom of the newly-created articulation surface **24**. In some embodiments, the surgeon blocks or plugs such an opening with a plug material (e.g., a cement or bone slurry) or using a plug built using the resected head (e.g., similar to the articular member **36** of the joint system **10**A shown in FIG. **4**).

Alternatively, if the cancellous bone is dense and inhibits satisfactory preparation of the recess **22**, the reamers **60** are used to mill/ream the recess **22**, where reaming stops once the reamer **60** has been inserted to the full hemispherical depth of the cutting surface of the reamer **60**. Where reaming is needed, the recess **22** is prepared by starting with a smaller reamer diameter (e.g., 34 mm) and gradually increasing the reamer diameter up to the selected diameter of the implant **12**. As previously mentioned, reaming and compaction are optionally used interchangeably by the surgeon until a satisfactory depth for the recess **22** is achieved and the articulation surface **24** is in an acceptable state.

Once the recess **22** has been formed as desired, the test implant **62** of the selected operational set is selected. For example, using the color coding previously mentioned, the test implant **62** of the same color as the final reamer **60** and final compactor **64** is used. The test implant **62** is assembled onto the handle **80**. The test implant **62** is then introduced in the recess **22**. The test depth lines DL of the test implant **62** help the surgeon visualize whether the test implant **62** has been sufficiently inserted into the recess **22** and, in turn, whether the recess **22** is formed to a sufficient depth. The test implant **62** is then placed into contact with the glenoid G to allow articulation about the test implant **62**. Stability and mobility testing is performed by physically manipulating the humerus. During testing the handle **80** is optionally removed to facilitate freedom of movement and later resecured to the test implant **62** for removal thereof from the recess **22**. During the stability and mobility testing, the surgeon verifies there is no gleno-humeral impingement or impingement between the humerus and the acromion.

The test implant **62** is removed after testing with the aid of the handle **80**. If the surgeon perceives too much tension in the muscles or articulation of the joint appears particularly tight, a smaller test implant **62** is and/or a smaller size of the implant **12** is selected or the surgeon optionally attempts to depress the test implant **62** further into the recess **22** and/or depress the implant **12** further into the recess upon implantation thereof. If the surgeon perceives insufficient tension in the muscles and/or in the case of gleno-humeral impingement, a larger size for the test implant **62** and/or implant **12** can be selected instead, with additional compacting/reaming steps as appropriate.

Once the testing is completed to the surgeon's satisfaction, the implant **12** of the selected size (typically of the same diameter as the test implant **62**) is then selected and introduced into the recess **22**. In some embodiments, where the implant **12** is formed of pyrocarbon, for example, it is important that the surface of the implant **12** not be maned or otherwise damaged. For example, the implant **12** should not be impacted into place in the recess **22**. The implant **12** is not cemented or otherwise fixed in the recess **22** according to some embodiments. The joint is reformed with the implant **12** in place, for example, according to the general methodology that follows.

The scapula S is repaired tendon-by-tendon as necessary and the aid of bone sutures secured to the humerus are used as needed. Where fixed to the humerus, the tendon is optionally displaced medially to promote recoupration and external rotation. Wound closure proceeds step-by-step in a traditional manner and the arm can be immoblized with a sling, for example. Generally, the same post operatives are recommended to that of a total prosthesis joint replacement (e.g., non-strenuous exercise and work resumed the first day after surgery with a sufficient waiting period before increased stretching/movement of the joint).

Various modifications, permutations, and additions can be made to the exemplary embodiments and aspects of the embodiments discussed without departing from the scope of the present invention. For example, while the embodiments describe concave articular surface above refer to particular features, the scope of this invention also includes embodiments having different combinations of features and embodiments that do not include all of the features. Accordingly, the scope of the present invention is intended to embrace all such alternatives, modifications, permutations, and variations as fall within the scope of the claims, together with all equivalents thereof.

What is claimed is:

1. A method of repairing a joint, the method comprising:
exposing a first bone of the joint;
resecting an end portion of the first bone to form a resected end defining a resection plane;
forming a concavity in the resected end portion of the first bone using a shaping tool, the concavity extending at least through a full hemispherical arc;
selecting a diameter of the prosthesis to be implanted; and
implanting a prosthesis having the selected diameter in the concavity.

2. The method of claim **1**, wherein forming the concavity comprises compacting the resected end portion of the first bone with a plurality of compactors having gradually increasing diameters.

3. The method of claim **1**, wherein forming the cavity comprises shaping the resected end portion of the first bone until a demarcation line on the shaping tool is parallel with the resection plane.

4. The method of claim **3**, wherein the demarcation line is at a position on the shaping tool that corresponds to a diameter of the prosthesis minus a predicted projection height of the prosthesis above the resected end that promotes adequate tensioning of the joint.

5. The method of claim 1, wherein forming the concavity comprises reaming the resected end portion of the first bone with a plurality of reamers having gradually increasing diameters.

6. The method of claim 1, wherein forming the concavity comprises iteratively compacting and reaming the resected end portion of the first bone.

7. The method of claim 1, further comprising selecting a test prosthesis based on a final shaping tool used to form the concavity.

8. The method of claim 7, further comprising selecting the test prosthesis having a same color as the final shaping tool.

9. The method of claim 7, further comprising introducing the test prosthesis into the concavity.

10. The method of claim 9, further comprising confirming the concavity is formed to a sufficient depth using depth lines on the test prosthesis.

* * * * *