

Relaxation-optimized transfer of spin order in Ising spin chains

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In this paper, we present relaxation optimized methods for the transfer of bilinear spin correlations along Ising spin chains. These relaxation optimized methods can be used as a building block for the transfer of polarization between distant spins on a spin chain, a problem that is ubiquitous in multidimensional nuclear magnetic resonance spectroscopy of proteins. Compared to standard techniques, significant reduction in relaxation losses is achieved by these optimized methods when transverse relaxation rates are much larger than the longitudinal relaxation rates and comparable to couplings between spins. We derive an upper bound on the efficiency of the transfer of the spin order along a chain of spins in the presence of relaxation and show that this bound can be approached by the relaxation optimized pulse sequences presented in the paper.

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I. INTRODUCTION

Relaxation (dissipation and decoherence) is a characteristic feature of open quantum systems. In practice, relaxation results in the loss of the signal and information and ultimately limits the range of applications. Recent work in optimal control of spin dynamics in the presence of relaxation has shown that these losses can be significantly reduced by exploiting the structure of relaxation [1–5]. This has resulted in significant improvement in sensitivity of many well established experiments in high resolution nuclear magnetic resonance (NMR) spectroscopy. In particular, by use of optimal control methods, analytical bounds have been achieved on the maximum polarization or coherence that can be transferred between coupled spins in the presence of very general decoherence mechanisms. In this paper, we look at the more general problem of the transfer of coherence or polarization between distant spins on an Ising spin chain in the presence of relaxation. This problem is ubiquitous in the multidimensional NMR spectroscopy of proteins, where polarization is transferred between distant spins located in the backbone and sidechains of the protein [6].

The system that we study in this paper is a linear chain of n weakly interacting spins one half placed in a static external magnetic field in the z direction (NMR experimental setup), with Ising type couplings of equal strength between nearest neighbors, see Fig. 1. The free evolution Hamiltonian of the system has the form

$$H_0 = \sum_{i=1}^n \omega_i I_{iz} + 2\pi J \sum_{i=1}^{n-1} I_{iz} I_{(i+1)z},$$

where ω_i is the Larmor frequency of spin i and J is the strength of the coupling between the spins. In a suitably chosen (multiple) rotating frame, which rotates with each spin at its resonance (Larmor) frequency, the free evolution Hamiltonian simplifies to

$$H_c = 2\pi J \sum_{i=1}^{n-1} I_{iz} I_{(i+1)z}. \quad (1)$$

Motivated by NMR spectroscopy of large molecules (like proteins) in a solution, we assume that the relaxation rates of the longitudinal operators with components only in the z direction, like I_{iz} , $2I_{iz} I_{(i+1)z}$ are negligible compared with relaxation rates for transverse operators like I_{ix} , $2I_{iz} I_{(i+1)y}$ [6]. The transverse relaxation is modeled by the Lindbladian with the general form [6]

$$L(\rho) = \sum_i \pi a_i [I_{iz}, [I_{iz}, \rho]] + \sum_{i,j} \pi b_{ij} [2I_{iz} I_{jz}, [2I_{iz} I_{jz}, \rho]].$$

In liquid state NMR spectroscopy, the two terms of the Lindblad operator model the relaxation mechanism caused by the chemical shift anisotropy and dipole-dipole interaction, respectively [6]. Here we neglect any interference effects between these two relaxation mechanisms [7]. Relaxation rates a_i , b_{ij} depend on various physical parameters, such as the gyromagnetic ratios of the spins, the internuclear distance, the correlation time of molecular tumbling, etc. We define the net transverse relaxation rate for spin i as [1] $k_a^i = a_i + \sum_j b_{ij}$. Without loss of generality in the subsequent analysis, we assume that k_a^i are equal and we denote this common transverse relaxation rate by k .

The time evolution (in the rotating frame) of the spin system density matrix ρ is given by the master equation

$$\dot{\rho} = -i[H, \rho] + L(\rho), \quad (2)$$

where $H = H_c + H_{rf}$ and H_{rf} is the control Hamiltonian. In the NMR context, the available controls are the components of

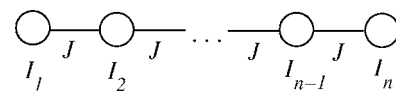


FIG. 1. The system that we study in this paper is a linear chain of n weakly interacting spins $\frac{1}{2}$ with Ising coupling between the next neighbors. The coupling constant is the same for all pairs of connected spins.

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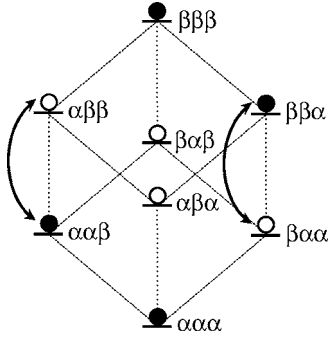


FIG. 2. Energy level diagram for the spin order transfer $2I_{1z}I_{2z} \rightarrow 2I_{2z}I_{3z}$. The relative vertical position of the states represents their relative energy. The dark circles represent population excess. State α corresponds to spin up and state β to spin down. The configuration depicted here corresponds to initial density matrix $2I_{1z}I_{2z}$. After the performance of the selective population inversions shown by the arrows, the configuration achieved corresponds to final density matrix $2I_{2z}I_{3z}$.

the transverse rf magnetic field. It is assumed that the resonance frequencies of the spins are well separated, so that each spin can be selectively excited (addressed) by an appropriate choice of the components of the rf field at its resonance frequency.

Consider now the problem of optimizing the polarization transfer

$$I_{1z} \rightarrow I_{nz} \quad (3)$$

along the linear spin chain shown in Fig. 1, in the presence of the relaxation mechanisms mentioned above. This problem can be stated as follows: Find the optimal transverse rf magnetic field in the control Hamiltonian H_{rf} such that starting from $\rho(0)=I_{1z}$ and evolving under Eq. (2) the target expectation value $\langle I_{nz} \rangle = \text{tr}\{\rho(t)I_{nz}\}$ is maximized.

To fix ideas, we analyze the case when $n=3$

$$I_{1z} \rightarrow I_{3z}. \quad (4)$$

This transfer is achieved conventionally using INEPT (insensitive nuclei enhanced by polarization transfer)-like pulse sequences [8–10]. Under the conventional transfer method, the initial state of the system I_{1z} evolves through the following stages:

$$I_{1z} \rightarrow 2I_{1z}I_{2z} \rightarrow 2I_{2z}I_{3z} \rightarrow I_{3z}. \quad (5)$$

In the first stage of the transfer, $I_{1z} \rightarrow 2I_{1z}I_{2z}$, spin 3 is decoupled from the chain using standard decoupling methods [11] and the initial polarization I_{1z} on spin 1 is rotated by the rf field (an appropriate $\pi/2$ pulse) to coherence I_{1x} , which then evolves under coupling Hamiltonian $2I_{1z}I_{2z}$ to $2I_{1y}I_{2z}$. When the expectation value $\langle 2I_{1y}I_{2z} \rangle$ is maximized, another $\pi/2$ pulse is used to rotate $2I_{1y}I_{2z}$ to $2I_{1z}I_{2z}$. This is the INEPT pulse sequence. The next stage $2I_{1z}I_{2z} \rightarrow 2I_{2z}I_{3z}$ is the so-called spin order transfer. Figure 2 shows the population inversions corresponding to this transfer. By a suitable $\pi/2$ rotation of spin 2, the density operator $2I_{1z}I_{2z}$ is transformed to $2I_{1z}I_{2x}$, which then evolves to $2I_{2x}I_{3z}$. When the expectation value $\langle 2I_{2x}I_{3z} \rangle$ is maximized, another $\pi/2$ pulse is used

to rotate $2I_{2x}I_{3z}$ to the spin order $2I_{2z}I_{3z}$. This is the concatenated INEPT (CINEPT) pulse sequence. The final stage transfer $2I_{2z}I_{3z} \rightarrow I_{3z}$ is similar to that in the first stage and is accomplished by the INEPT pulse sequence. The efficiency of these transfers is limited by the decay of transverse operators, due to the phenomenon of relaxation.

In our recent work on relaxation optimized control of coupled spin dynamics [1], we showed that the efficiency of the first and the last step (the two INEPT stages) in Eq. (5) can be significantly improved by controlling precisely the way in which magnetization is transferred from longitudinal operators to transverse operators. In other words, instead of using $\pi/2$ (hard) pulses to rotate longitudinal to transverse operators (and the inverse), we can exploit the fact that longitudinal operators are long lived by making these rotations gradually, saving this way, magnetization. This transfer strategy is called relaxation optimized pulse element (ROPE).

In this paper we derive relaxation optimized pulse sequences for the intermediate transfer (the CINEPT stage),

$$2I_{1z}I_{2z} \rightarrow 2I_{2z}I_{3z}. \quad (6)$$

This relaxation optimized transfer of spin order can then be used as a building block for the polarization transfer (3) through the scheme

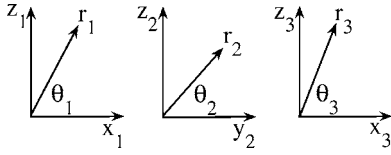
$$I_{1z} \rightarrow 2I_{1z}I_{2z} \rightarrow 2I_{2z}I_{3z} \rightarrow \cdots \rightarrow 2I_{(n-1)z}I_{nz} \rightarrow I_{nz}. \quad (7)$$

II. THE OPTIMAL CONTROL PROBLEM AND AN UPPER BOUND FOR THE EFFICIENCY

In this section, we formulate the problem of transfer in Eq. (6) as a problem of optimal control and derive an upper bound on the transfer efficiency. To simplify the notation, we introduce the following symbols for the expectation values of operators that play a part in the transfer. Let $z_1 = \langle 2I_{1z}I_{2z} \rangle$, $x_1 = \langle 2I_{1z}I_{2x} \rangle$, $y_2 = \langle \sqrt{2}(2I_{1z}I_{2y}I_{3z} + I_{2y}/2) \rangle$, $x_3 = -\langle 2I_{2x}I_{3z} \rangle$, and $z_3 = \langle 2I_{2z}I_{3z} \rangle$. As a control variable we use the transverse rf magnetic field, pointing say, in the y direction (in the rotating frame), so $H_{rf} = \omega_y(t)I_{2y}$. Note that $\omega_y(t)$ is the component of the field in the rotating frame, so it is actually the envelope of the rf field. The carrier frequency of the rf field is the resonance frequency of spin 2. Using Eq. (2), we find that the evolution of the system, in time units of $1/(\pi J\sqrt{2})$, is given by

$$\begin{bmatrix} \dot{z}_1 \\ \dot{x}_1 \\ \dot{y}_2 \\ \dot{x}_3 \\ \dot{z}_3 \end{bmatrix} = \begin{bmatrix} 0 & -\Omega_y & 0 & 0 & 0 \\ \Omega_y & -\xi & -1 & 0 & 0 \\ 0 & 1 & -\xi & -1 & 0 \\ 0 & 0 & 1 & -\xi & -\Omega_y \\ 0 & 0 & 0 & \Omega_y & 0 \end{bmatrix} \begin{bmatrix} z_1 \\ x_1 \\ y_2 \\ x_3 \\ z_3 \end{bmatrix}, \quad (8)$$

where $\Omega_y(t) = \omega_y(t)/(\pi J\sqrt{2})$ and $\xi = k/(J\sqrt{2})$. The initial condition is $(z_1, x_1, y_2, x_3, z_3) = (1, 0, 0, 0, 0)$.

FIG. 3. Auxiliary variables r_i .

The efficiency of the conventional method (CINEPT) for transfer $z_1 \rightarrow z_3$ can be easily found. At $t=0$, z_1 is transferred to x_1 by application of a $(\pi/2)_y$ pulse on spin 2. Couplings evolve x_1 to y_2 which further evolves to x_3 . As a function of time, $x_3(t) = e^{-\xi t} \sin^2(t/\sqrt{2})$. This is maximized for $t_m = \sqrt{2} \cot^{-1}(\xi/\sqrt{2})$. At $t=t_m$ a second $(\pi/2)_y$ pulse is applied on spin 2, rotating the maximum value from x_3 to z_3 . This value is the efficiency η_{CI} of the conventional method

$$\eta_{CI} = \exp[-\xi\sqrt{2} \cot^{-1}(\xi/\sqrt{2})] \sin^2[\cot^{-1}(\xi/\sqrt{2})]. \quad (9)$$

A better efficiency can be achieved if we store magnetization in the decoherence free longitudinal operators z_i while the system is evolving. This is done by rotating z_i to x_i gradually, instead of using $\pi/2$ hard pulses. This is the physical concept behind the relaxation optimized transfer strategy. For the specific transfer examined in this paper, we first find an upper bound for the maximum efficiency and in the next section we calculate numerically the magnetic field $\Omega_y(t)$ that approaches this bound.

In order to derive the upper bound, we use an augmented system instead of the original one (8). The augmentation is done in two steps. First, we suppose that we can rotate z_1 to x_1 and x_3 to z_3 independently using two different controls, say $\Omega_1(t)$ and $\Omega_3(t)$, instead of the common control $\Omega_y(t)$. Next, we provide y_2 with a relaxation free partner z_2 and with a control $\Omega_2(t)$ which can rotate y_2 to z_2 . The augmented system is

$$\begin{bmatrix} \dot{z}_1 \\ \dot{z}_2 \\ \dot{z}_3 \\ \dot{x}_1 \\ \dot{y}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 & -\Omega_1 & 0 & 0 \\ 0 & 0 & 0 & 0 & -\Omega_2 & 0 \\ 0 & 0 & 0 & 0 & 0 & -\Omega_3 \\ \Omega_1 & 0 & 0 & -\xi & -1 & 0 \\ 0 & \Omega_2 & 0 & 1 & -\xi & -1 \\ 0 & 0 & \Omega_3 & 0 & 1 & -\xi \end{bmatrix} \begin{bmatrix} z_1 \\ z_2 \\ z_3 \\ x_1 \\ y_2 \\ x_3 \end{bmatrix}. \quad (10)$$

Observe that system (10) reduces to system (8) for $\Omega_1 = -\Omega_3 = \Omega_y$ and $\Omega_2 = 0$. Thus, if we know the maximum achievable value of z_3 starting from $(1, 0, 0, 0, 0, 0)$ and evolving under system (10), then this is an upper bound for the maximum achievable value of z_3 with evolution described by the original system (8).

Let $r_1 = \sqrt{x_1^2 + z_1^2}$, $r_2 = \sqrt{y_2^2 + z_2^2}$ and $r_3 = \sqrt{x_3^2 + z_3^2}$. Using $\Omega_i(t)$ we can control the angles θ_i , shown in Fig. 3, independently. If we assume that the control can be done arbitrarily fast as compared to the evolution of couplings or relaxation rates then we can think of θ_i as control variables. The equations for the evolution of r_i are

$$\begin{bmatrix} \dot{r}_1 \\ \dot{r}_2 \\ \dot{r}_3 \end{bmatrix} = \begin{bmatrix} -\xi u_1^2 & -u_1 u_2 & 0 \\ u_1 u_2 & -\xi u_2^2 & -u_2 u_3 \\ 0 & u_2 u_3 & -\xi u_3^2 \end{bmatrix} \begin{bmatrix} r_1 \\ r_2 \\ r_3 \end{bmatrix}, \quad (11)$$

where the new control parameters are $u_i(t) = \cos[\theta_i(t)]$. The goal is to find the largest achievable value of r_3 starting from $(r_1, r_2, r_3) = (1, 0, 0)$ by appropriate choice of $u_i(t)$. This problem can be solved analytically. The optimal solution is characterized by maintaining vanishingly small values of dr_2/dt , i.e., $(u_1 r_1 - u_3 r_3)/u_2 r_2 = \xi$ and by $u_3 r_3/u_1 r_1 = \kappa$, where

$$\kappa = \frac{(\sqrt{\xi^2 + 2} - \xi)^2}{2}. \quad (12)$$

The maximum achievable value of r_3 is also κ . We will prove it in the following.

Using variables $p_i = r_i^2$, $m_i = u_i r_i / \sqrt{\sum_j (u_j r_j)^2}$, and $d\tau/dt = \sum_i^3 (u_i r_i)^2$, Eq. (11) can be rewritten as

$$\frac{d}{d\tau} \begin{bmatrix} p_1(\tau) \\ p_2(\tau) \\ p_3(\tau) \end{bmatrix} = \text{diag}[A m(\tau) m^T(\tau)], \quad (13)$$

where

$$A = 2 \begin{bmatrix} -\xi & -1 & 0 \\ 1 & -\xi & -1 \\ 0 & 1 & -\xi \end{bmatrix}, \quad (14)$$

$m^T = (m_1, m_2, m_3)$ and $\text{diag}(X)$ represents the vector containing diagonal entries of the square matrix X . The goal is to find the controls $m_i(\tau)$ [$\sum_i m_i^2(\tau) = 1$] and the largest achievable value of p_3 starting from $(p_1, p_2, p_3) = (1, 0, 0)$. Equation (13) implies that

$$\begin{bmatrix} p_1(T) \\ p_2(T) \\ p_3(T) \end{bmatrix} = \begin{bmatrix} p_1(0) \\ p_2(0) \\ p_3(0) \end{bmatrix} + \text{diag} \left(A \int_0^T m(\tau) m^T(\tau) d\tau \right).$$

Let $M = \int_0^T m(\tau) m^T(\tau) d\tau$. Note that M is a symmetric, positive semidefinite matrix. By definition $p_i(\tau) \geq 0$ for all τ . At final time T , we must have $p_1(T) = 0$ and $p_2(T) = 0$, as any nonzero value of $p_1(T)$ or $p_2(T)$ can be partly transferred to p_3 and the final value of $p_3(T)$ further increased. Since $[p_1(0), p_2(0), p_3(0)] = (1, 0, 0)$, it implies that M should be such that $(AM)_{11} = -1$, $(AM)_{22} = 0$ and $(AM)_{33}$ is maximized over all positive semidefinite M satisfying the above constraints. This problem is a special case of a semidefinite programming problem [12]. If the symmetric part of matrix A is negative definite, as in our case (14), then it can be shown that the optimal solution M to the above stated semidefinite programming problem is a rank one matrix [13], i.e., $M = mm^T$ for some constant m and therefore the ratio $u_i r_i / u_j r_j$ in (11) is constant throughout. The condition $(AM)_{22} = 0$ implies $(u_1 r_1 - u_3 r_3)/\xi = u_2 r_2$. Substituting for $u_2 r_2$ in (11), we obtain

$$\begin{bmatrix} \dot{r}_1 \\ \dot{r}_3 \end{bmatrix} = \begin{bmatrix} -(\xi + 1/\xi)u_1^2 & u_1 u_3 / \xi \\ u_1 u_3 / \xi & -(\xi + 1/\xi)u_3^2 \end{bmatrix} \begin{bmatrix} r_1 \\ r_3 \end{bmatrix}. \quad (15)$$

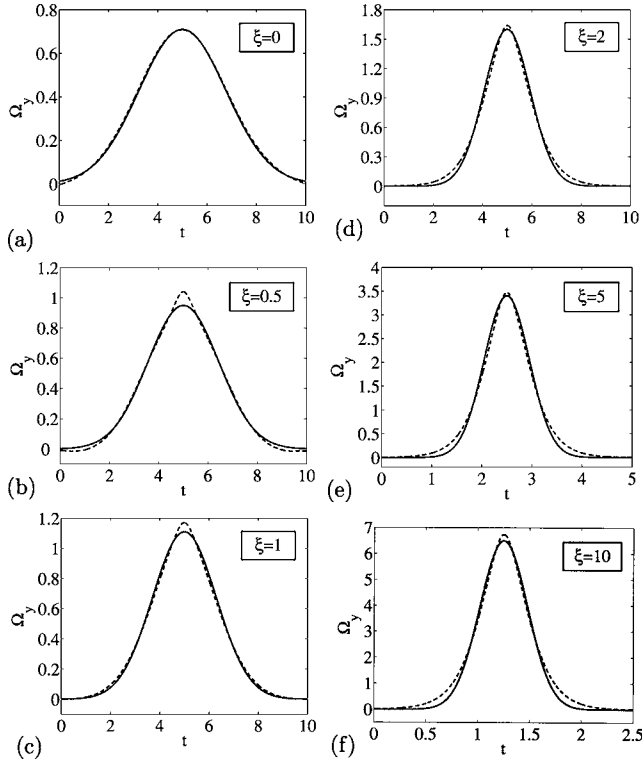


FIG. 4. Optimal pulse (dashed line) calculated using a numerical optimization method based on a steepest descent algorithm, for various values of the normalized relaxation parameter $\xi = k/(J\sqrt{2})$. Time t is measured in units $1/(\pi J\sqrt{2})$ and rf field Ω_y in units $\pi J\sqrt{2}$. The Gaussian pulse (solid line) approximates very well the optimal pulse shape and gives a similar efficiency. This suggests that instead of using the initial numerical optimization method, we can use Gaussian pulses of the form (16), optimized with respect to A and σ for each value of ξ .

We now simply need to maximize the gain in r_3 to loss in r_1 , i.e., the ratio $\dot{r}_3/(-\dot{r}_1)$. This yields $u_3 r_3 / u_1 r_1 = \kappa$, with κ given in (12). The corresponding maximum efficiency for transfer $r_1 \rightarrow r_3$ is also κ . This is the maximum efficiency for transfer $z_1 \rightarrow z_3$ under the augmented system (10), and thus an upper bound for the efficiency of the same transfer under the original system (8).

III. NUMERICAL CALCULATION OF THE OPTIMAL rf FIELD AND DISCUSSION

Having established an analytical upper bound (12) for the efficiency, we now try to find numerically a rf field $\Omega_y(t)$ that approaches this bound, for each value of the parameter ξ . We emphasize that in this section the original system (8) is employed.

At first, we use a numerical optimization method based on a steepest descent algorithm. For the application of the method we use a finite time window T . For values of normalized relaxation ξ in $(0-1)$, a time interval $T=10$ (normalized time units) is enough. For larger values of ξ we can use even shorter T . The optimal rf field $\Omega_y(t)$ that we find with this method, for various ξ , is shown in Fig. 4. Note that as ξ

TABLE I. For various values of $\xi \in [0, 1]$, the optimal values of A, σ and the corresponding efficiency are shown. We present also for comparison the efficiency achieved by the steepest descent method.

ξ	A	σ	Gaussian pulse	Steepest descent
1.00	1.11	1.30	0.2510	0.2512
0.95	1.09	1.32	0.2661	0.2662
0.90	1.07	1.34	0.2824	0.2825
0.85	1.05	1.36	0.3000	0.3001
0.80	1.03	1.38	0.3190	0.3191
0.75	1.02	1.39	0.3396	0.3397
0.70	1.00	1.41	0.3619	0.3620
0.65	0.98	1.43	0.3861	0.3863
0.60	0.97	1.44	0.4124	0.4126
0.55	0.96	1.44	0.4410	0.4413
0.50	0.95	1.44	0.4721	0.4726
0.45	0.94	1.45	0.5060	0.5067
0.40	0.93	1.46	0.5428	0.5439
0.35	0.92	1.46	0.5830	0.5846
0.30	0.91	1.46	0.6270	0.6292
0.25	0.90	1.47	0.6750	0.6780
0.20	0.89	1.48	0.7277	0.7315
0.15	0.88	1.48	0.7855	0.7900
0.10	0.85	1.52	0.8494	0.8536
0.05	0.79	1.60	0.9203	0.9232
0.00	0.73	1.71	0.9999	1.0000

increases, the optimal pulse becomes shorter in time and acquires a larger peak value. The reason for this is that for larger ξ the transfer $z_1 \rightarrow z_3$ should be done faster, in order to reduce the time spent in the transverse plane and hence the relaxation losses. Now observe that the optimal pulse shape can be very well approximated by a Gaussian profile of the form

$$\Omega_y(t) = A \exp \left[- \left(\frac{t - T/2}{\sqrt{2}\sigma} \right)^2 \right], \quad (16)$$

with A, σ appropriately chosen. As a result, the efficiency that we find using the appropriate Gaussian pulse is very close to what we find using the original pulse. This suggests that instead of using the initial numerical optimization method, we can use Gaussian pulses of the form (16), optimized with respect to A and σ for each value of ξ . The optimal A, σ are found by numerical simulations. For each ξ we simulate the equations of system (8) with $\Omega_y(t)$ given by Eq. (16), for many values of A and σ . We choose those values that give the maximum $z_3(T)$. In Table I, we show the optimal A, σ for various values $\xi \in [0, 1]$. We also show the corresponding efficiency, as well as the efficiency achieved by the initial numerical optimization method. Observe how close these two groups of values lie. The choice of the Gaussian shape is indeed successful.

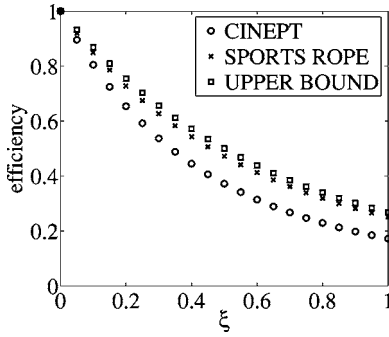


FIG. 5. Efficiency for the conventional method (CINEPT), Eq. (9), and for our method (SPORTS ROPE), for the values of the normalized relaxation parameter $\xi = k/(J\sqrt{2})$ shown in Table I. The upper bound (12) for the efficiency is also shown.

Figure 5 shows the efficiency of the conventional method (CINEPT), i.e., η_{CI} from Eq. (9), the efficiency of our method (SPORTS ROPE, spin order transfer with relaxation optimized pulse element), and the upper bound κ from Eq. (12), for the values of the relaxation parameter ξ shown in Table I. Note that for large ξ (large relaxation rates), SPORTS ROPE gives a significant improvement over CINEPT. Also note that it approaches fairly well the upper bound.

Using the Gaussian pulse shape we can get a quantitative impression of the robustness of SPORTS ROPE. In Fig. 6 we give a gray-scale topographic plot of the efficiency [$z_3(T)$ with $T=10$] as a function of A and σ for $\xi=1$. The maximum value can be found from Table I and is 0.2510. The white region corresponds to values ≥ 0.24 , while the black region to values $< \eta_{CI}(\xi=1)=0.1727$. The intermediate gray regions correspond to values between these two limits. Obviously, SPORTS ROPE is quite robust.

In Fig. 7(a), we plot the time evolution of the various transfer functions (expectation values of operators) that participate in the transfer $z_1 \rightarrow z_3$, when the optimal Gaussian pulse for $\xi=1$, shown in Fig. 4(c), is applied to system (8). Observe the gradual building of the intermediate variables

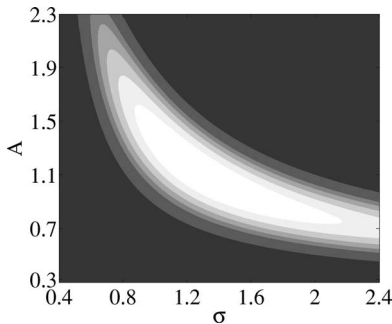


FIG. 6. Gray-scale topographic plot of the efficiency as a function of the amplitude A (units $\pi J\sqrt{2}$) and the standard deviation σ [units $1/(\pi J\sqrt{2})$] of the Gaussian pulse for $\xi=1$. The maximum value can be found from Table I and is 0.2510. The white region corresponds to values ≥ 0.24 , while the black region to values $< \eta_{CI}(\xi=1)=0.1727$. The intermediate gray regions correspond to the intervals $[0.23, 0.24)$, $[0.22, 0.23)$, $[0.21, 0.22)$, $[0.20, 0.21)$, and $[0.1727, 0.20)$ (from white to black).

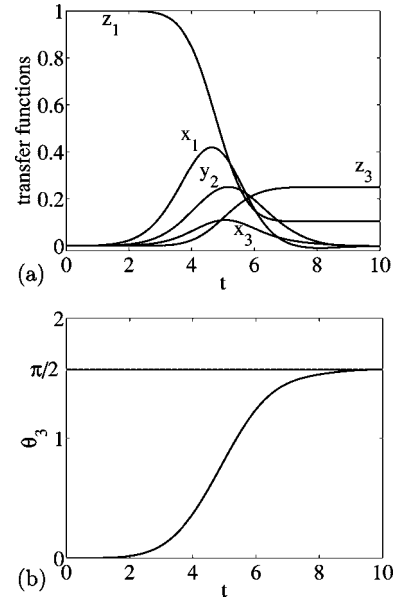


FIG. 7. (a) Time evolution of the various transfer functions (expectation values of operators) participating in the transfer $z_1 \rightarrow z_3$, when the optimal Gaussian pulse for $\xi=1$, shown in Fig. 4(c), is applied to system (8). Time is measured in units $1/(\pi J\sqrt{2})$. (b) The angle $\theta_3 = \tan^{-1}(z_3/x_3)$ of the vector \mathbf{r}_3 with the x axis, expressed in radians, as a function of time. Observe that initially \mathbf{r}_3 is parallel to the x axis ($\theta_3=0$), but under the action of the Gaussian pulse is rotated gradually to the z axis ($\theta_3=\pi/2$).

x_1 , y_2 , and x_3 . Note that $dr_2/dt = \dot{y}_2 \neq 0$. There is no contradiction with the optimality condition $dr_2/dt=0$ derived in Sec. II during the calculation of the upper bound, since this condition refers to the augmented system (10) and not the original one (8) used here. In Fig. 7(b) we plot the angle $\theta_3 = \tan^{-1}(z_3/x_3)$ of the vector \mathbf{r}_3 with the x axis, as a function of time. Observe that initially \mathbf{r}_3 is parallel to the x axis ($\theta_3=0$), but under the action of the Gaussian pulse is rotated gradually to z axis ($\theta_3=\pi/2$). This gradual rotation of \mathbf{r}_3 (as well as of \mathbf{r}_1) is a characteristic feature of the SPORTS ROPE transfer scheme.

We remark that for the general transfer $I_{1z} \rightarrow I_{nz}$, more than one intermediate steps $2I_{(i-1)z}I_{iz} \rightarrow 2I_{iz}I_{(i+1)z}$ are necessary. Since the equations that describe the i th transfer are the same as (8), we just need to apply the same Gaussian pulse but centered, in the frequency domain, at the resonance frequency of spin i . In this sequence of Gaussian pulses we should add at the beginning and at the end the optimal pulses for the first and the final step, respectively, see Eq. (7). These pulses can be calculated using the theory presented in [1]. Finally, note that the same scheme can be used for the coherence transfer $I_{1\alpha} \rightarrow I_{n\beta}$, where α, β can be x or y . We just need to add the initial and final $\pi/2$ pulses that accomplish the rotations $I_{1\alpha} \rightarrow I_{1z}$, $I_{nz} \rightarrow I_{n\beta}$.

IV. CONCLUSION

In this paper, we derived an upper bound on the efficiency of spin order transfer along an Ising spin chain, in the presence of relaxation, and calculated numerically relaxation op-

timized pulse sequences approaching this bound. Using these methods, a significant reduction in relaxation losses is achieved, compared to standard techniques, when transverse relaxation rates are much larger than the longitudinal relaxation rates and comparable to couplings between spins. These relaxation optimized methods can be used as a building block for the transfer of polarization or coherence between distant spins on a spin chain. This problem is ubiquitous in multidimensional NMR spectroscopy of proteins. The methods presented can also be used to answer interesting

questions in the context of quantum information, for example, what is the maximum entanglement that can be generated in the presence of relaxation.

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