# Monopole Antennas

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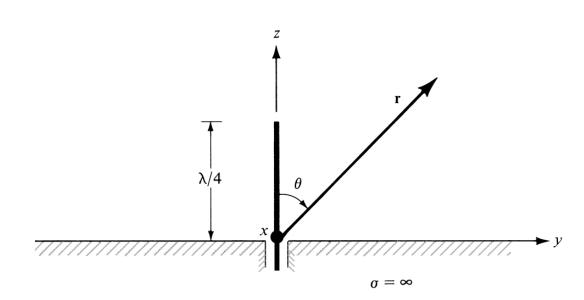
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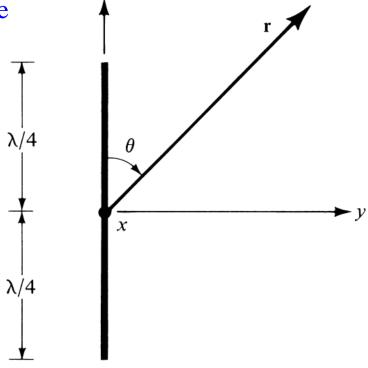
#### Monopole Antenna on Infinite Ground Plane

#### Quarter-wavelength monopole Antenna on Infinite Ground Plane

Note:  $\lambda/4$  length is only valid when ground plane size is infinite



 $\lambda$ 4 monopole on infinite electric conductor



Equivalent  $\lambda 2$  dipole

#### Monopole Antenna on Infinite Ground Plane

#### Far fields - Electric and Magnetic fields

Far-fields E and H for the  $\lambda/4$  monopole above the ground plane are same as that of dipole antenna

$$E_{\theta} \simeq j\eta \frac{I_0 e^{-jkr}}{2\pi r} \left[ \frac{\cos\left(\frac{\pi}{2}\cos\theta\right)}{\sin\theta} \right], H_{\phi} \simeq j \frac{I_0 e^{-jkr}}{2\pi r} \left[ \frac{\cos\left(\frac{\pi}{2}\cos\theta\right)}{\sin\theta} \right]$$

Input Impedance

$$Z_{in}(monopole) = \frac{Z_{in}(dipole)}{2} = \frac{73 + j42.5}{2} = 36.5 + j21.25$$

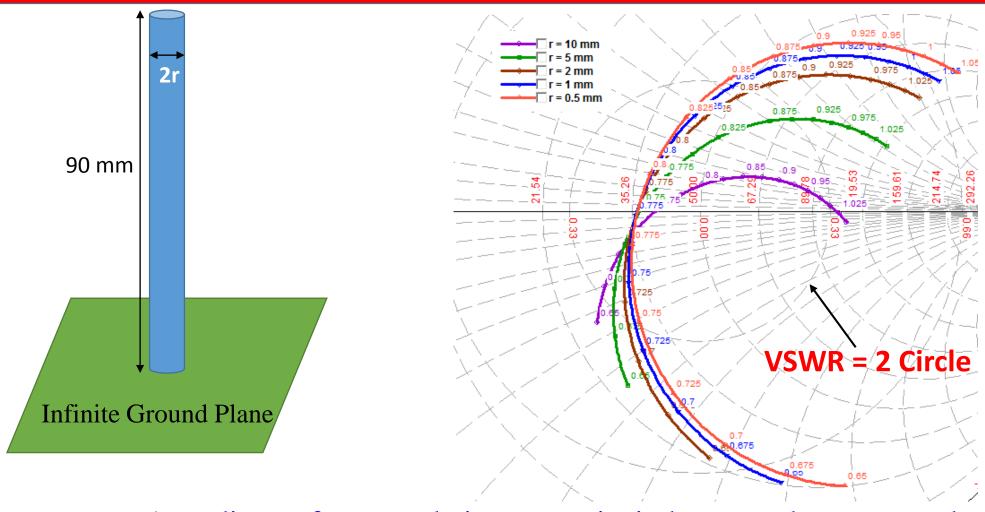
Directivity

$$D(monopole) = 2 * D(dipole) = 2 * 1.643 = 3.286$$

Height h for Real Input Impedance

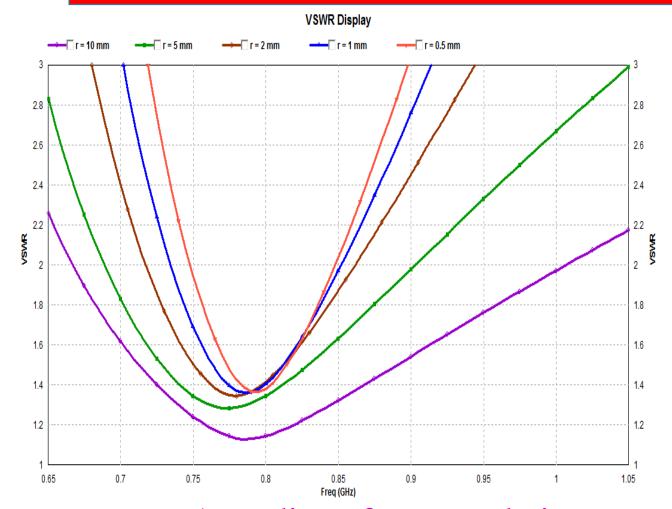
 $h + r \simeq 0.24\lambda$ , where r is the radius of wire and  $r < \lambda/20$ 

# Effect of Varying Radius of Monopole on Infinite Ground Plane on Impedance Plot



As radius r of monopole increases, its inductance decreases and hence impedance plot shifts down.

# Effect of Varying Radius of Monopole on Infinite Ground Plane on VSWR Plot



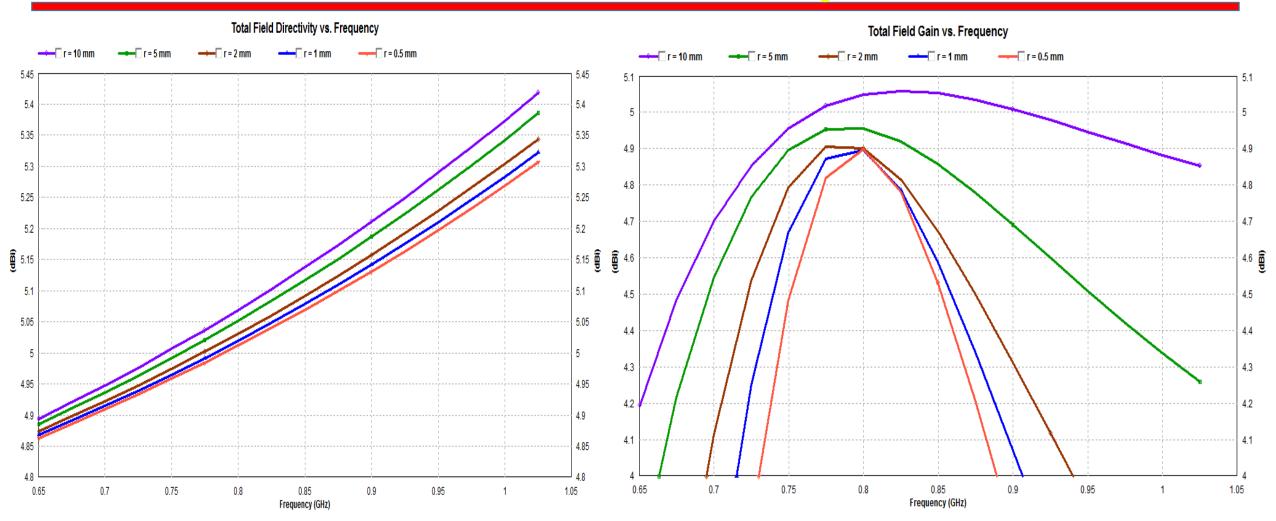
# Resonance frequency calculation using $h + r = 0.24\lambda$

$$f = 0.24 c / (h + r)$$

Radius (in mm)	Theoretical frequency (in MHz)	Bandwidth for VSWR < 2 (in MHz)	%BW
0.5	795.6	748 to 847	12.4%
1	791.2	734 to 852	14.9%
2	782.6	717 to 861	18.3%
5	757.9	689 to 903	26.9%
10	720.0	667 to 1007	42.1%

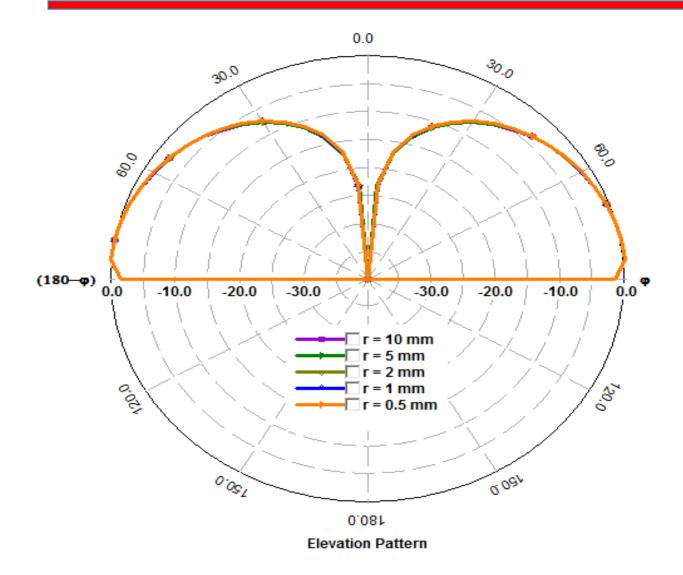
As radius of monopole increases, resonance frequency decreases slightly but BW increases significantly.

# Effect of varying Radius of Monopole on infinite Ground Plane on Directivity and Gain



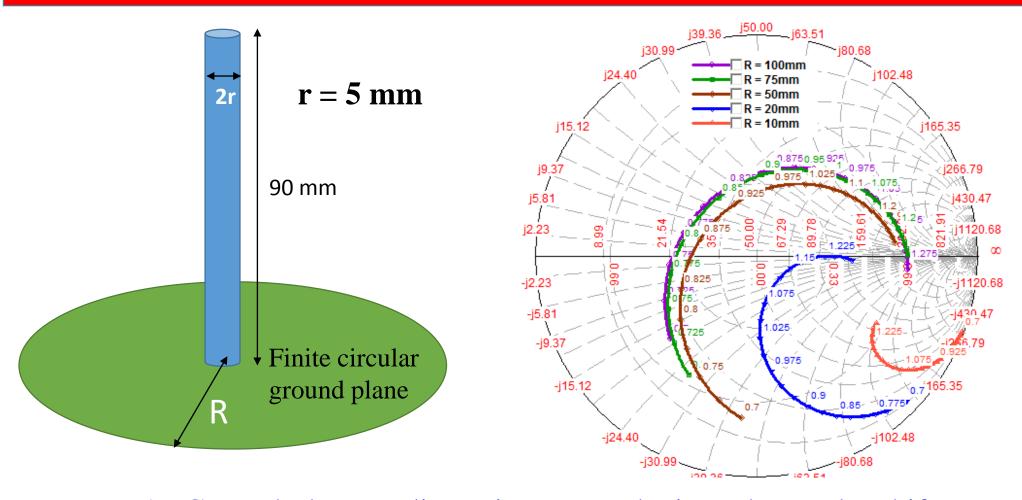
As radius of monopole increases, the directivity increases marginally by 0.05 dB at center frequency but gain BW increases significantly

# Effect of Varying Radius of Monopole on Infinite Ground Plane on Radiation Pattern



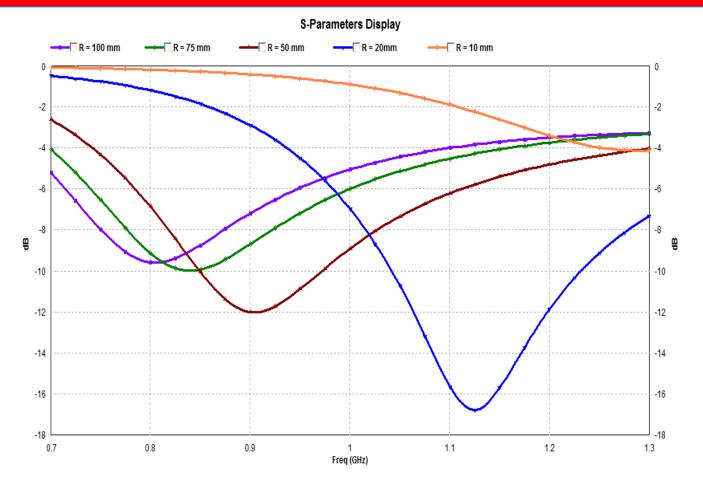
With change in the radius of monopole, there is no significant change in the radiation pattern.

# Effect of Varying Finite Ground Plane Size on Input Impedance of Monopole



As Ground Plane Radius R increases, the impedance plot shifts towards inductive region. Hollow cylindrical monopole can be taken.

# Effect of Varying Size of Finite Ground Plane on $S_{11}$ Plot (h = 90 mm, r = 5mm)

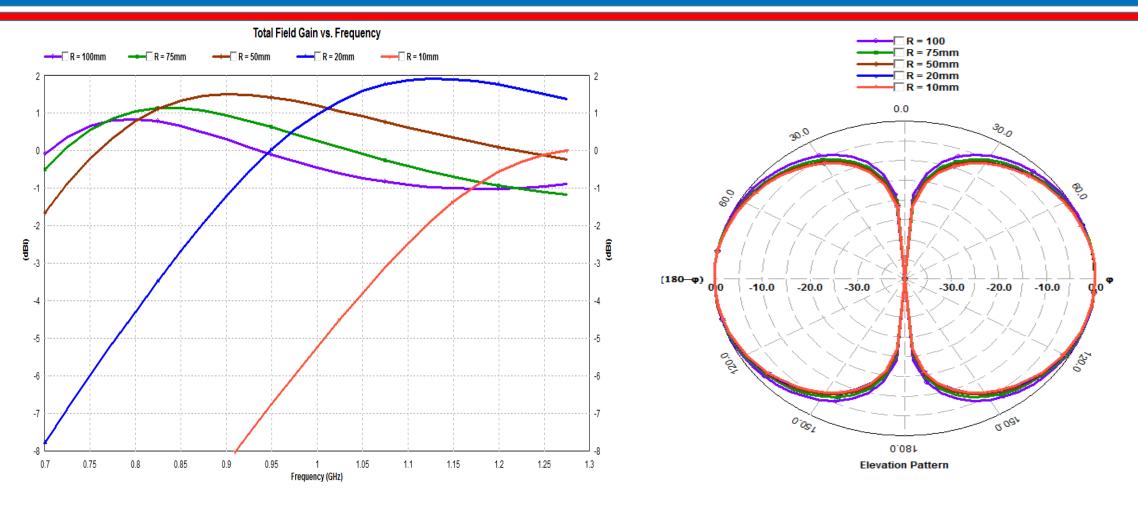


Radius (R) of Ground Plane (in mm)	Simulated Center frequency f <sub>o</sub> (in MHz)	At f <sub>o</sub> Simulated Input Impedance (in Ω)
10	1280	95-j99
20	1120	84.6-j1
50	905	33.5+j13
75	840	29+j15
100	800	28+j14
Infinite	775	41+j7.6

As Ground Plane Radius R increases, the resonance frequency decreases.

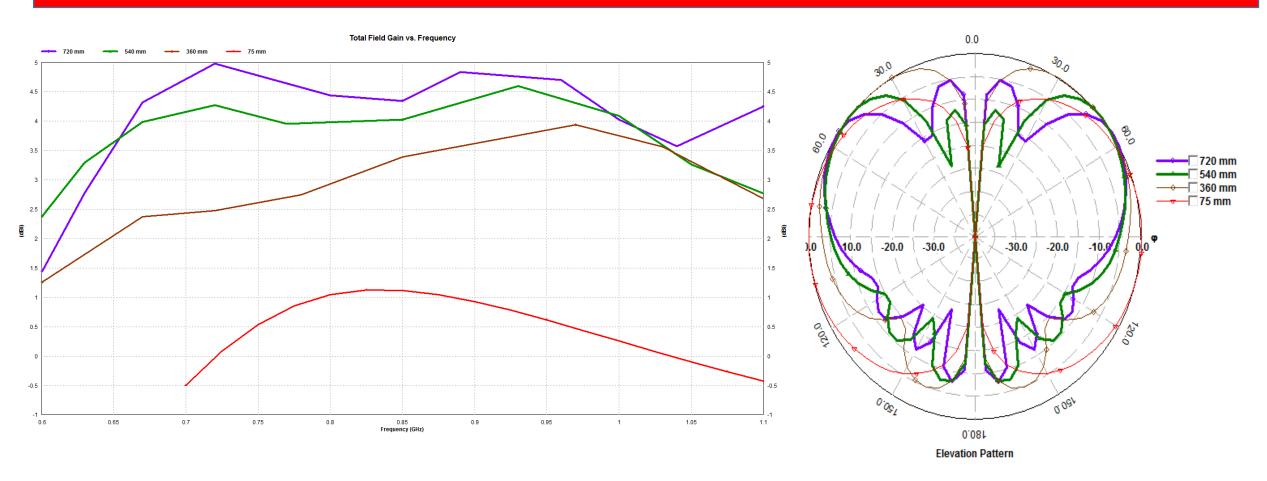
Applications – Cellular and cordless telephones, walkie-talkies, CB radios, etc.

# Effect of Varying Size of Small Ground Plane on Gain and Radiation Pattern (h = 90 mm, r = 5 mm)



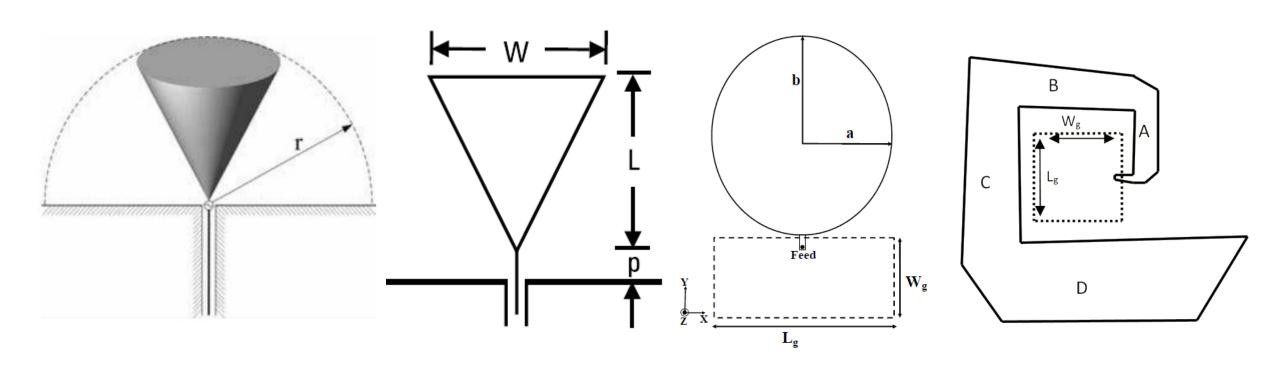
As Ground Plane Radius R increases, the gain maxima shifts towards lower resonance frequency. Gain and radiation pattern of a monopole antenna on small ground plane ( $< \lambda$ ) are similar to that of dipole antenna.

# Effect of Varying Size of Large Ground Plane on Gain and Radiation Pattern



Gain of monopole antenna on large ground plane (>  $\lambda$ ) is greater than that of dipole antenna and it approaches to gain of around 5 dB, which is for infinite ground plane.

#### Broadband Monopole Antenna Configurations



Conical Monopole Antenna

Triangular Monopole Antenna Printed Elliptical
Monopole
Antenna

Bent Monopole Antenna

#### Conical Monopole Antenna



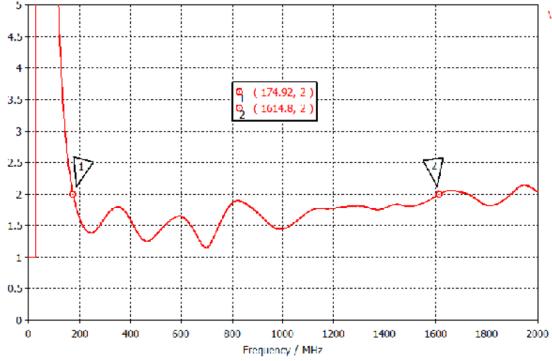
Slant length =  $\lambda/4$  at lowest frequency of operation.

$$Z_{in} = 60 \ln \left[ \cot \left( \frac{\alpha}{4} \right) \right]$$

where  $\alpha$  is cone angle.

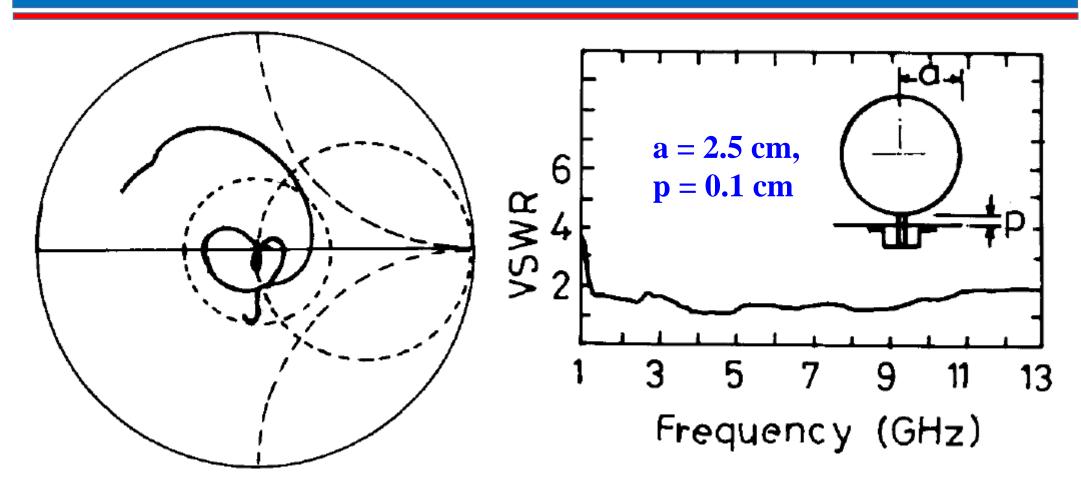
For 
$$\alpha = 90^{\circ}$$
,  $Z_{in} = 52.9 \Omega$ 

Physical Specifications			
Height of cone	300 mm		
Maximum radius of cone	300 mm		
Minimum radius of cone	5 mm		
Distance from ground	2 mm		
Cone angle	90°		



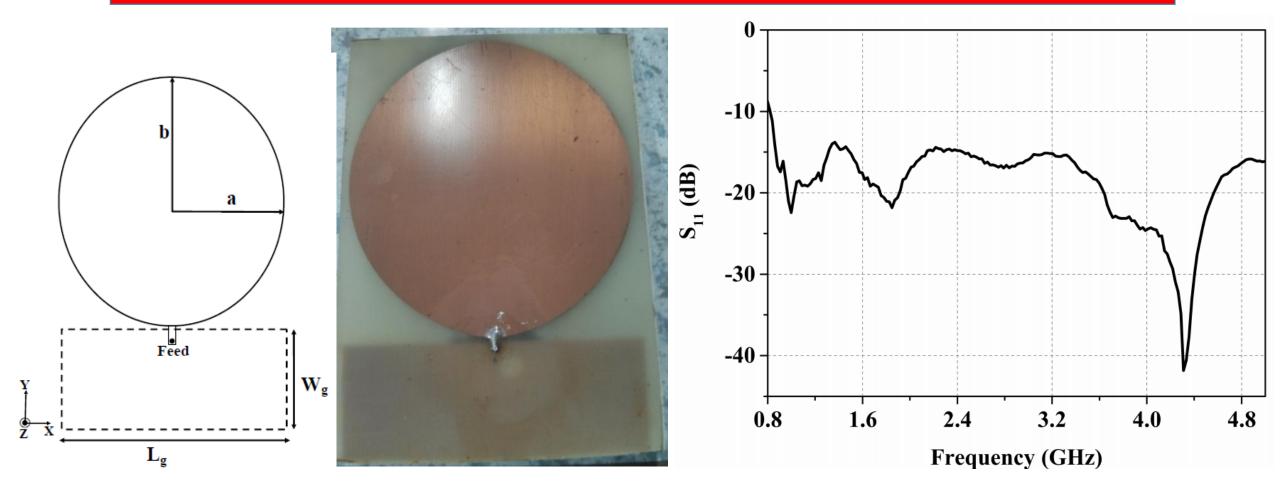
Bandwidth for VSWR  $\leq$  2 is from 175 to 1615 MHz.

### Broadband Circular Monopole Antenna



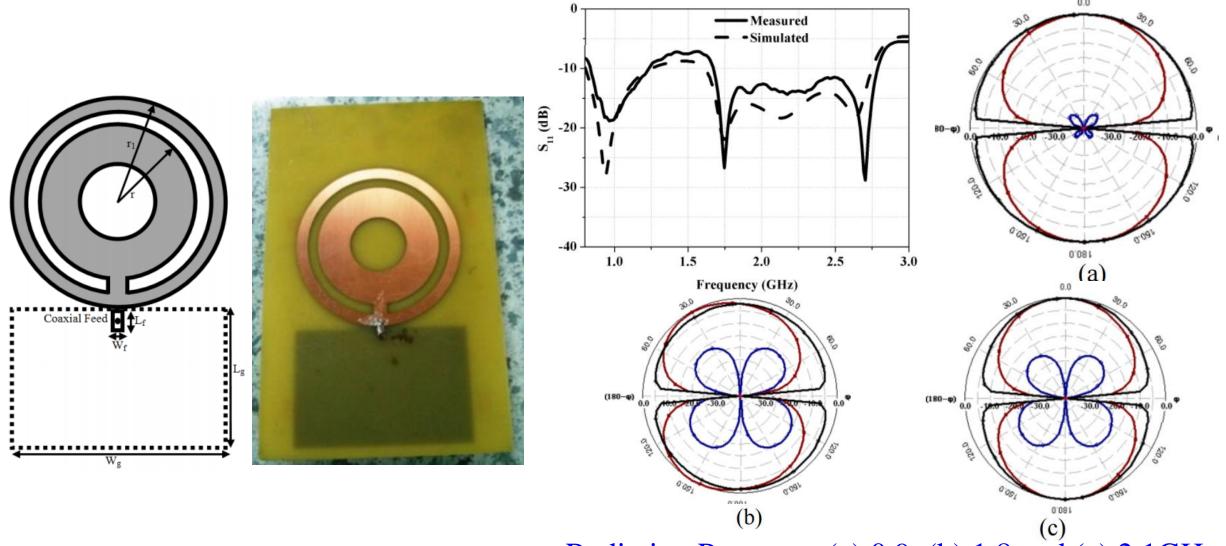
Bandwidth for VSWR  $\leq$  2 is from 1.17 GHz to 12 GHz, which corresponds to BW ratio of 1:10.2 but radiation pattern varies over the bandwidth.

### Printed Broadband Elliptical Monopole Antenna



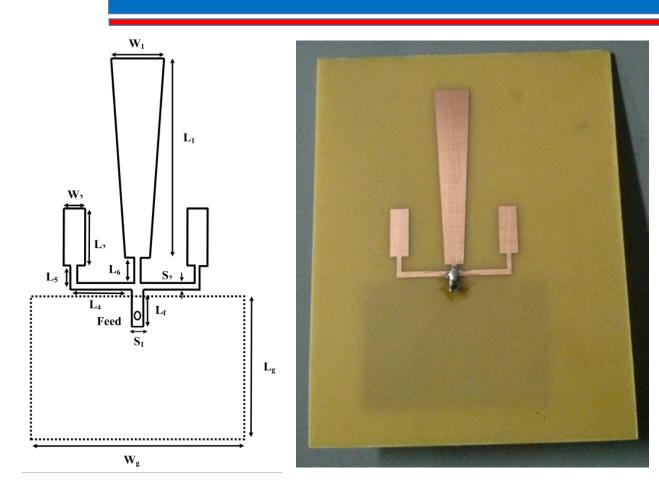
Bandwidth for  $|S_{11}| < -10$  dB is very large but radiation pattern varies over the bandwidth.

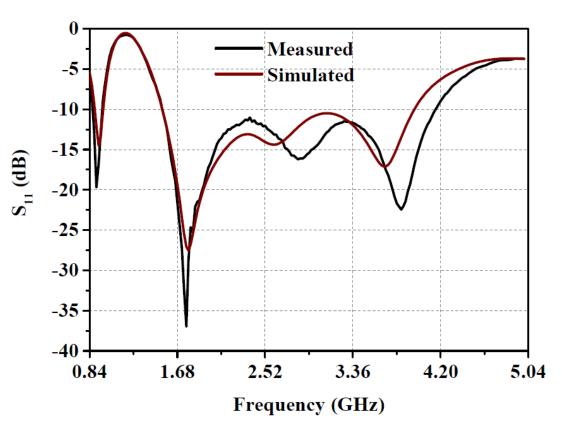
# Dual Band Dual Ring Monopole Antenna



Radiation Pattern at (a) 0.9, (b) 1.8 and (c) 2.1GHz

# Dual Band Trident Monopole Antenna

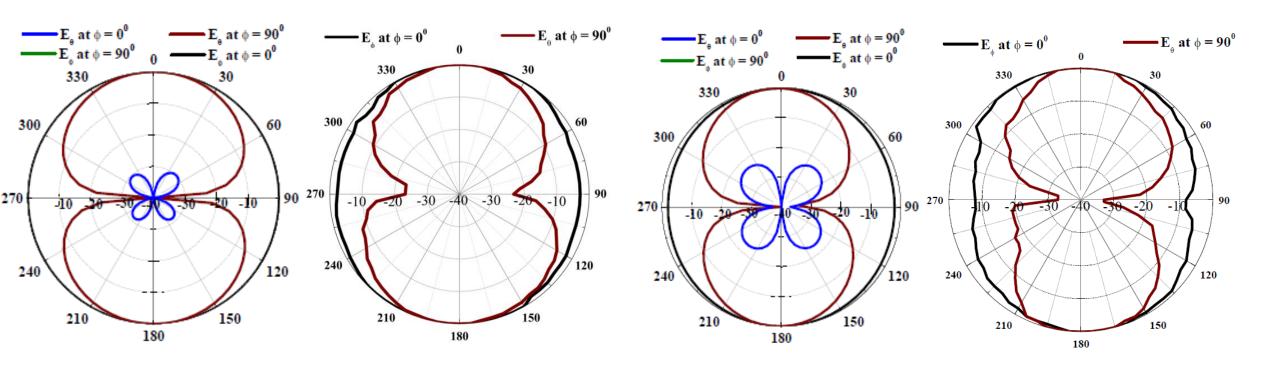




Central monopole is designed to resonate at GSM 900 band. Two monopoles placed on each side of central monopole resonate at GSM1800 band.

Bandwidth = 870-980MHz 1.5 to 4.2GHz

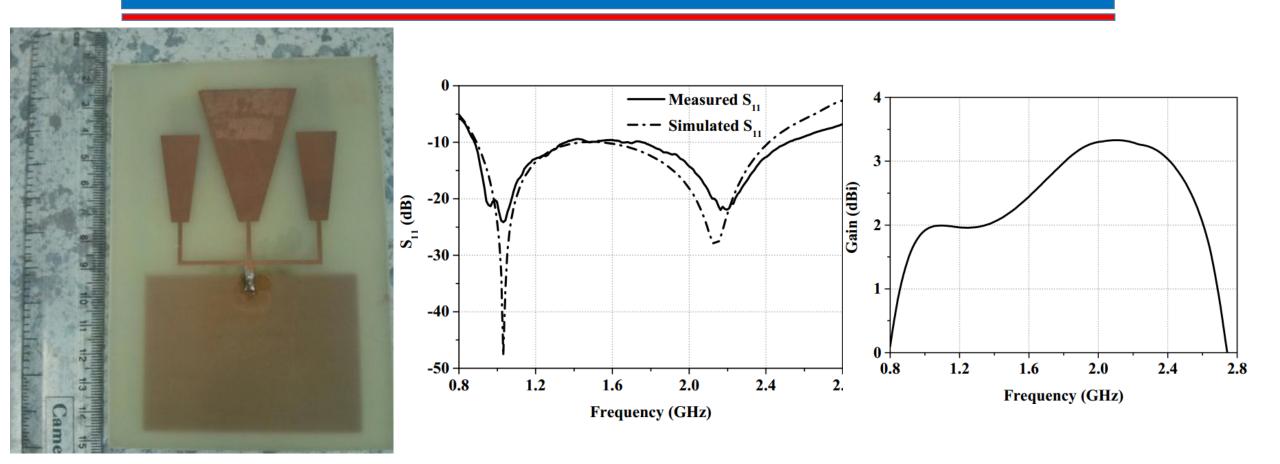
# Dual Band Trident Monopole Antenna



Simulated and Measured Radiation Patterns at 920MHz HPBW in E-plane = 80°

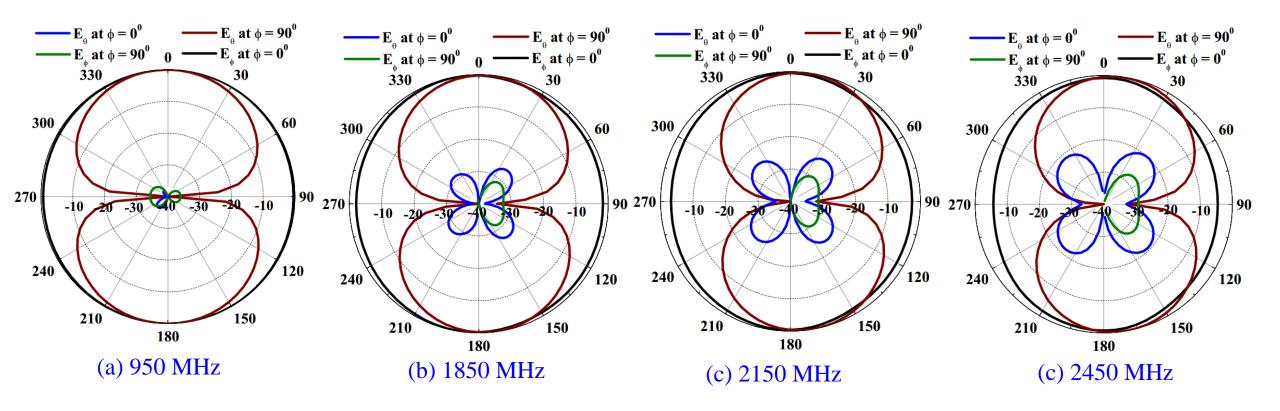
Simulated and Measured Radiation Patterns at 2150MHz HPBW in E-plane = 55°

# Broadband Trident Monopole Antenna



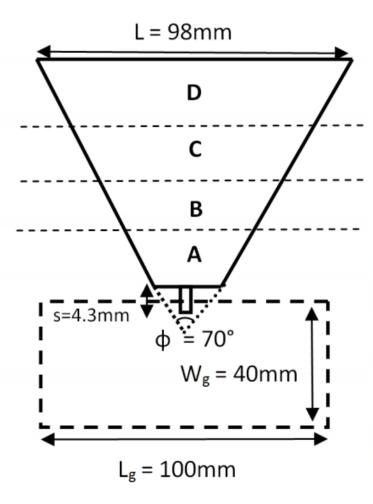
Bandwidth of the trident monopole antenna is increased by flaring all three monopoles

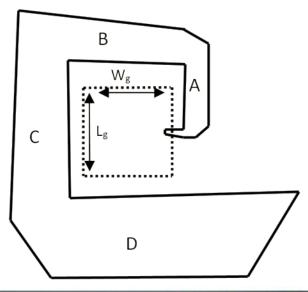
# Broadband Trident Monopole Antenna Pattern

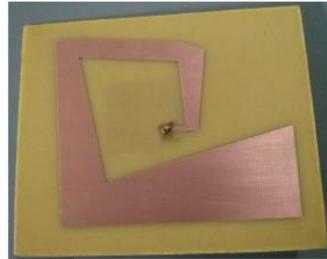


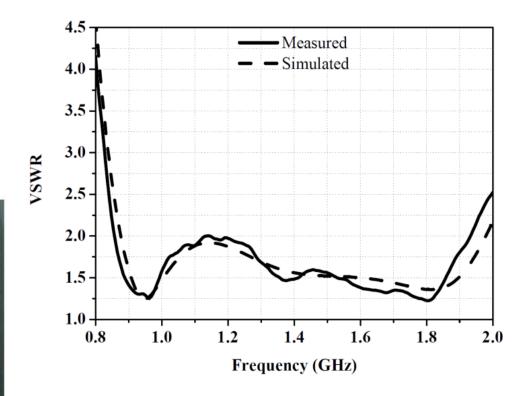
Radiation pattern of the broadband trident monopole antenna at (a) 950 MHz, (b) 1850 MHz, (c) 2.15 GHz, and (d) 2.45 GHz

# Broadband Dual Polarized Bent Triangular Antenna

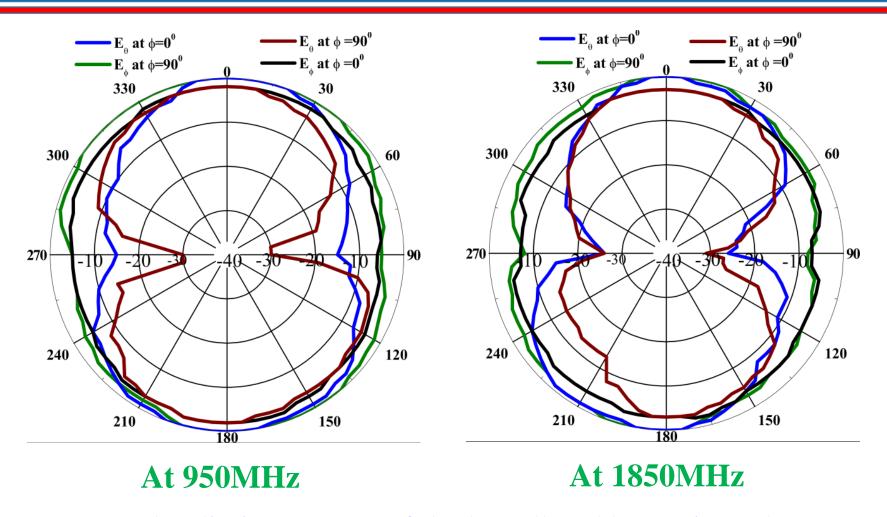








### Bent Triangular Antenna Radiation Pattern



Measured radiation pattern of the broadband bent triangular antenna. Both H and V polarizations are present.