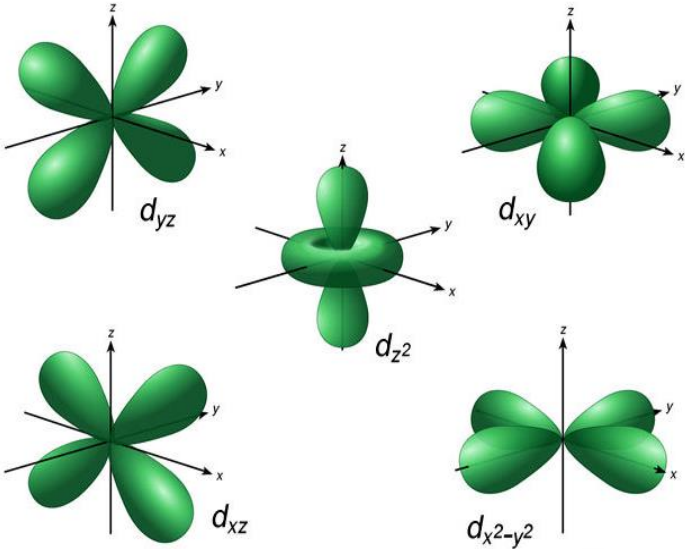


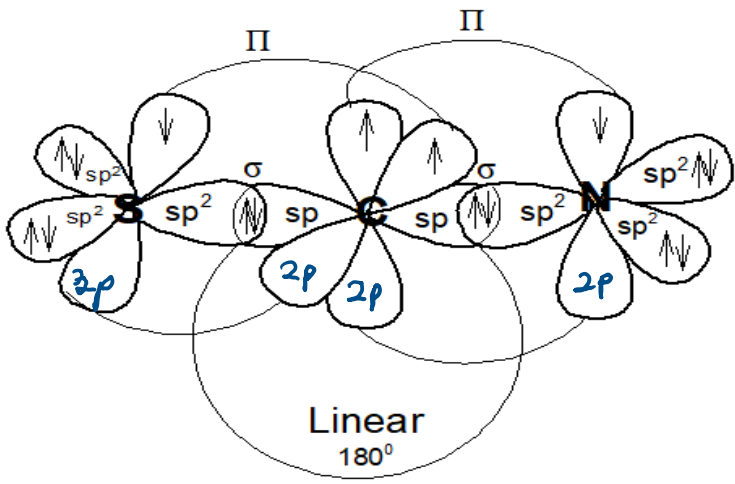
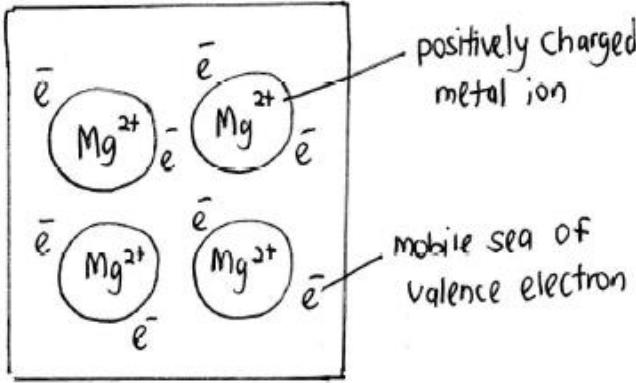
[illegible]

	(c)(i)	$\text{density} = \frac{\text{mass of solution}}{\text{volume of solution}}$ $\text{mass of solution} = \text{density} \times \text{volume of solution}$ $\text{mass of solution} = 1.329 \text{ gml}^{-1} \times 1000 \text{ ml}$ $\text{mass of solution} = 1329 \text{ g} \dots\dots\dots$ $\% \text{ w/w} = \frac{\text{mass of solute}}{\text{mass of solution}} \times 100$ <p style="text-align: right;">@</p> $\% \text{ w/w} = \frac{571.6 \text{ g}}{1329 \text{ g}} \times 100 \dots\dots\dots$ $= 43.01 \% \dots\dots\dots$	1	M10
	(c)(ii)	$\text{mol } H_2SO_4 = \frac{571.6 \text{ g}}{98.1 \text{ g mol}^{-1}}$ $\text{mol } H_2SO_4 = 5.8267 \text{ mol} \dots\dots\dots$ <p>Mass of solvent = mass of solution - mass of solute  = 1329 - 571.6  = 757.4 g @  = 0.7574 kg .....</p> $\text{Molality} = \frac{\text{mol of solute}}{\text{mass of solvent (kg)}}$ <p style="text-align: right;">@</p> $\text{Molality} = \frac{5.827 \text{ mol}}{0.7574 \text{ (kg)}}$ $= 7.693 \text{ m @ mol kg}^{-1} \dots\dots\dots$	1	M12
			1	M13
			1	M14
			1	M15
	(d)(i)	$\% \text{ yield} = \frac{\text{actual yield}}{\text{theoretical yield}} \times 100$ <p style="text-align: right;">@</p> $78.1 = \frac{120 \text{ g}}{\text{theoretical yield}} \times 100$ $\text{theoretical yield} = 153.65 \text{ g} \dots\dots\dots$ $\text{mol } P_4S_3 = \frac{153.65 \text{ g}}{220.3 \text{ g mol}^{-1}} = 0.6975 \text{ mol} \dots\dots\dots$	1	M16
			1	M17
			1	M18

		$8 \text{ mol } P_4S_3 \equiv 3 \text{ mol } S_8$ $0.6975 \text{ mol } P_4S_3 \equiv 0.6975 \text{ mol } P_4S_3 \times \frac{3 \text{ mol } S_8}{8 \text{ mol } P_4S_3}$ $= \mathbf{0.2616 \text{ mol } S_8}$ ..... $\text{mass } S_8 = 0.2616 \text{ mol} \times 256.8 \text{ g mol}^{-1}$ $= \mathbf{67.18 \text{ g}}$ ... ..	<b>1</b>          <b>1</b>	<b>M19</b>          <b>M20</b>
	(d)(ii)	$3 \text{ mol } S_8 \equiv 8 \text{ mol } P_4$ $\mathbf{0.2616 \text{ mol } S_8} \equiv \mathbf{0.2616 \text{ mol } S_8} \times \frac{8 \text{ mol } P_4}{3 \text{ mol } S_8}$ $= \mathbf{0.6976 \text{ mol } P_4}$ ..... $\text{mol of } P_4 \text{ left} = \mathbf{1.2 \text{ mol} - 0.6976 \text{ mol}}$ $= \mathbf{0.5024 \text{ mol } P_4}$ .....	<b>1</b>          <b>1</b>	<b>M21</b>          <b>M22</b>
		<b>TOTAL</b>	<b>22</b>	
		<b>MAX</b>	<b>21</b>	

NO	PART	SCHEME	MARKS	
2	(a)(i)	$\Delta E = R_H \left( \frac{1}{n_i^2} - \frac{1}{n_f^2} \right) @ = 2.18 \times 10^{-18} \left( \frac{1}{6^2} - \frac{1}{2^2} \right)$ $= -4.844 \times 10^{-19} \text{ J (unit insist) } \dots\dots\dots$	1	M1
	(a)(ii)	Visible region	1	M3
	(b)(i)	<b>3d orbitals (any two answer)</b> 	1	M4
			2 (shape and label)	M5 M6
	(b)(ii)	$1s^2 2s^2 2p^6 3s^2 3p^6 4s^2 3d^2$	1	M7
	(c)	Expected electronic configuration: $1s^2 2s^2 2p^6 3s^2 3p^6 4s^2 3d^4$  Actual electronic configuration: $1s^2 2s^2 2p^6 3s^2 3p^6 4s^1 3d^5$  Half-filled $3d^5$ orbital is more stable than partially orbital $3d^4$	1	M8
			1	M9
			1	M10
		TOTAL	10	

NO	PART	SCHEME	MARKS	
3	(a)(i)	$\left[ \begin{array}{c} \ddot{\text{S}}=\text{C}=\ddot{\text{N}} \\ \vdots \quad \vdots \end{array} \right]^- \quad \left[ \text{:S}\equiv\text{C}-\ddot{\text{N}}\text{:} \right]^- \quad \left[ \text{:}\ddot{\text{S}}-\text{C}\equiv\text{N}\text{:} \right]^-$ <p>Structure I                      Structure II                      Structure III</p>	1 1 1	M1 M2 M3
	(a)(ii)	$\begin{array}{ccc} \begin{array}{c} (0) \quad (0) \quad (-1) \\ \left[ \begin{array}{c} \ddot{\text{S}}=\text{C}=\ddot{\text{N}} \\ \vdots \quad \vdots \end{array} \right]^- \\ \text{Structure I} \end{array} & \begin{array}{c} (+1) \quad (0) \quad (-2) \\ \left[ \text{:S}\equiv\text{C}-\ddot{\text{N}}\text{:} \right]^- \\ \text{Structure II} \end{array} & \begin{array}{c} (-1) \quad (0) \quad (0) \\ \left[ \text{:}\ddot{\text{S}}-\text{C}\equiv\text{N}\text{:} \right]^- \\ \text{Structure III} \end{array} \end{array}$ <p>correct all formal charge ...</p> <p><b>Structure I</b></p> <p>Structure I have <b>lower formal charge</b> and the <b>negative charge (-1)</b> is at the <b>most electronegative atom, Nitrogen</b></p>	1  1  1	M4  M5  M6
	(a)(iii)	Molecular Geometry – <b>Linear</b> Bond Angle - <b>180°</b>	1 1	M7 M8
	(a)(iv)	<p><b>Type of hybrid of S: sp</b></p> <p>OR</p>	1  1  1	M9  M10  M11  M12

				
	(b)	<p>The <b>open hexagonal structure</b> of the ice accounts for the fact that <b>ice is less dense than water due to larger volume of ice.</b></p> <p><b>OR</b></p> <p>When ice melts, some of the <b>hydrogen bonds are broken.</b> This allows the water molecules to be <b>more compactly arranged, resulting in decrease in volume.</b></p> <p>When volume decreases, density increases. Therefore, water has a higher density than ice.</p>	<p><b>1</b></p> <p><b>1</b></p> <p><b>1</b></p> <p><b>1</b></p>	<p><b>M13</b></p> <p><b>M14</b></p>
	(c)(i)		<p><b>1</b> (Drawing)</p> <p><b>1</b> (Label)</p>	<p><b>M15</b></p> <p><b>M16</b></p>
	(c)(ii)	<p><b>Aluminium has 3 valence electrons, sodium has one.</b> The higher the number of valence electrons, the stronger the metallic bonds.</p> <p>@</p> <p><b>The size of aluminium is smaller than sodium.</b> The smaller the atom, the stronger the metallic bonds.</p>	<p><b>1</b></p>	<p><b>M17</b></p>
		<b>TOTAL</b>	<b>17</b>	

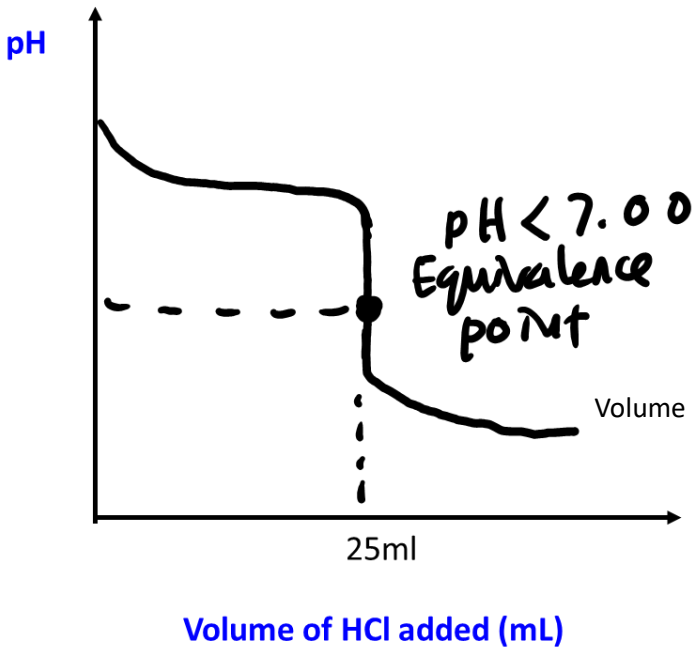
NO	PART	SCHEME	MARKS	
4	(a) (i)	$P_T = P_{O_2} + P_{H_2O} @ P_{O_2} = (770 - 35.5)mmHg$ .....	1	M1
		$= 734.5 mmHg$ .....	1	M2
		$734.5mmHg \times \frac{1 atm}{760 mmHg}$		
		$= 0.966 atm$		
	(a) (ii)	$n_{O_2} = \frac{P_{O_2}V}{RT} @ = \frac{0.966 atm \times 0.25 L}{0.08206 \times 299.15 K}$	1	M3
		$= 9.84 \times 10^{-3} mol$ .....	1	M4
		$2KClO_3 (s) \rightarrow 2KCl (s) + 3O_2 (g)$	1	
		3 mol $O_2 \equiv$ 2 mol $KClO_3$	1	
		$9.84 \times 10^{-3} mole \equiv 6.56 \times 10^{-3} mol KClO_3$ .....	1	M5
		Mass = $6.56 \times 10^{-3} mol KClO_3 \times (122.6 g mol^{-1})$ $= 0.804g$ .....	1	M6
	(b)	Propanone has <b>higher</b> vapour pressure than propanol	1	M7
		<b>Intermolecular forces of propanone are weaker than propanol</b> , so easier to vapourised to form vapour	1	M8
		Propanol – <b>Hydrogen bond</b>	1	M9
		Propanone – <b>van der Waals forces (Dipole- dipole forces)</b>	1	M10
		TOTAL	10	
		MAX	9	

NO	PART	SCHEME	MARKS																	
5	(a)	<div><math display="block">[\text{NO}_2]_i = \frac{0.5 \text{ mol}}{5\text{L}} = \mathbf{0.1 \text{ M}}</math><table><tr><td></td><td colspan="3"><math>2\text{NO}_2 (\text{g}) \rightleftharpoons 2\text{NO} (\text{g}) + \text{O}_2 (\text{g})</math></td></tr><tr><td>Initial (M)</td><td>0.1</td><td>0</td><td>0</td></tr><tr><td>Change (M)</td><td><math>-2x</math></td><td><math>+2x</math></td><td><math>+x</math></td></tr><tr><td>Equilibrium (M)</td><td><math>0.1-2x</math></td><td><math>2x</math></td><td><math>x</math></td></tr></table><p>At equilibrium; <math>[\text{NO}_2] = \frac{0.2 \text{ mol}}{5\text{L}} = 0.04 \text{ M}</math> <math>0.1 - 2x = 0.04</math>  <math>x = \mathbf{0.03 \text{ M}}</math> .....</p><p><math>K_c = \frac{[\text{NO}]^2 [\text{O}_2]}{[\text{NO}_2]^2} @</math> .....</p><p><math>= \frac{(2 \times 0.03)^2 (0.03)}{(0.1-2(0.03))^2}</math>  <math>= \mathbf{0.0675}</math> .....</p></div>		$2\text{NO}_2 (\text{g}) \rightleftharpoons 2\text{NO} (\text{g}) + \text{O}_2 (\text{g})$			Initial (M)	0.1	0	0	Change (M)	$-2x$	$+2x$	$+x$	Equilibrium (M)	$0.1-2x$	$2x$	$x$	<div>1</div> <div>1</div> <div>1</div>	<div>M1</div> <div>M2</div> <div>M3</div> <div>M4</div>
	$2\text{NO}_2 (\text{g}) \rightleftharpoons 2\text{NO} (\text{g}) + \text{O}_2 (\text{g})$																			
Initial (M)	0.1	0	0																	
Change (M)	$-2x$	$+2x$	$+x$																	
Equilibrium (M)	$0.1-2x$	$2x$	$x$																	
	(b)	<div><math>\alpha = \frac{[\text{ }]\text{change}}{[\text{ }]\text{initial}} @</math> .....</div> <div><math>= \frac{2(0.03)}{0.1}</math></div> <div><math>= \mathbf{0.6}</math> .....</div>	<div>1</div> <div>1</div>	<div>M5</div> <div>M6</div>																
	(c)	<div><b>Increase temperature</b></div> <div>The <b>forward reaction is endothermic</b>. By increase the temperature of the system, the equilibrium position will shift to the right to increase the yield of NO</div> <div><b>Reduce pressure</b></div> <div>By decrease pressure of the system, the equilibrium position will shift to the right to increase the pressure by increase the number of moles of gases and the yield of NO</div> <div><b>OR</b></div>	<div>1</div> <div>1</div> <div>1</div> <div>1</div>	<div>M7</div> <div>M8</div> <div>M9</div> <div>M10</div>																



		<p><b>Remove NO or O<sub>2</sub></b></p> <p>Because concentration NO or O<sub>2</sub> decrease, the equilibrium position will shift to favour the production of NO</p> <p><b>OR</b></p> <p><b>Addition of NO<sub>2</sub></b></p> <p>Because concentration NO<sub>2</sub> increase, the system will consume the added NO<sub>2</sub>, the equilibrium position will shift to favour the production of NO</p> <p><i>(Choose only two)</i></p>		
		<b>TOTAL</b>	<b>10</b>	
		<b>MAX</b>	<b>9</b>	

NO	PART	SCHEME	MARKS																					
6	(a)(i)	<table border="1"> <tr> <td></td><td colspan="4"><math>\text{NH}_3(\text{aq}) + \text{H}_2\text{O}(\text{l}) \rightleftharpoons \text{NH}_4^+(\text{aq}) + \text{OH}^-(\text{aq})</math></td></tr> <tr> <td>[ ]<sub>Initial</sub>(M)</td><td>0.1</td><td>-</td><td>0</td><td>0</td></tr> <tr> <td>[ ]<sub>Change</sub>(M)</td><td>-x</td><td>-</td><td>+x</td><td>+x</td></tr> <tr> <td>[ ]<sub>Equilibrium</sub>(M)</td><td>0.1-x</td><td>-</td><td>x</td><td>x</td></tr> </table> $K_b = \frac{[\text{NH}_4^+][\text{OH}^-]}{[\text{NH}_3]} @$ $1.8 \times 10^{-5} = \frac{x^2}{0.1 - x} @$ <p><i>Assume Kb is very small, x is very small, then 0.10-x = 0.1</i></p> <p><i>Hence</i></p> $[\text{OH}^-] = x = 1.3416 \times 10^{-3} \text{ M}$ $\text{pOH} = -\log[\text{OH}^-]$ $\text{pOH} = -\log[1.3416 \times 10^{-3}]$ $\text{pOH} = 2.87$ $\text{pH} = 14 - \text{pOH}$ $\text{pH} = 14 - 2.87$ $\text{pH} = 11.13$		$\text{NH}_3(\text{aq}) + \text{H}_2\text{O}(\text{l}) \rightleftharpoons \text{NH}_4^+(\text{aq}) + \text{OH}^-(\text{aq})$				[ ] <sub>Initial</sub> (M)	0.1	-	0	0	[ ] <sub>Change</sub> (M)	-x	-	+x	+x	[ ] <sub>Equilibrium</sub> (M)	0.1-x	-	x	x	<p><b>1</b></p> <p><b>1</b></p> <p><b>1</b></p> <p><b>1</b></p>	<p><b>M1</b></p> <p><b>M2</b></p> <p><b>M3</b></p> <p><b>M4</b></p>
	$\text{NH}_3(\text{aq}) + \text{H}_2\text{O}(\text{l}) \rightleftharpoons \text{NH}_4^+(\text{aq}) + \text{OH}^-(\text{aq})$																							
[ ] <sub>Initial</sub> (M)	0.1	-	0	0																				
[ ] <sub>Change</sub> (M)	-x	-	+x	+x																				
[ ] <sub>Equilibrium</sub> (M)	0.1-x	-	x	x																				

	a(ii)	<p>When addition 25 ml HCl, equivalence point was achieves, produce salt <math>\text{NH}_4\text{Cl}</math> and water.</p> <p><math>\text{NH}_4^+</math> is strong conjugate acid from weak base, it will hydrolysis with water.</p> $\text{NH}_4^+ (\text{aq}) + \text{H}_2\text{O} (\text{l}) \rightleftharpoons \text{NH}_3 (\text{aq}) + \text{H}_3\text{O}^+ (\text{aq})$ <p>The production of <math>\text{H}_3\text{O}^+</math> ions, causes pH of the solution is less than 7.</p> <p><math>\text{NH}_4\text{Cl}</math> is a acidic salt.</p>	1	M5
	(a)(iii)		<p>1 (Shape)</p> <p>1 (eq. point &lt;7)</p> <p>1 (label &amp; axes)</p>	<p>M8</p> <p>M9</p> <p>M10</p>
(b)		$\text{Ba}(\text{NO}_3)_2(\text{aq}) \rightarrow \text{Ba}^{2+}(\text{aq}) + 2\text{NO}_3^-(\text{aq})$ <p><math>[\text{Ba}^{2+}]_{\text{new}}</math></p> $M_1V_1 = M_2V_2$ $0.025 \text{ M} \times 20 \text{ ml} = M_2 \times 50 \text{ ml}$ <p><math>M_2 = 0.01 \text{ M}</math></p> $\text{NaF}(\text{aq}) \rightarrow \text{Na}^+(\text{aq}) + \text{F}^-(\text{aq})$ <p><math>[\text{F}^-]_{\text{new}}</math></p> $M_1V_1 = M_2V_2$ $0.03 \text{ M} \times 30 \text{ ml} = M_2 \times 50 \text{ ml}$ <p><math>M_2 = 0.018 \text{ M}</math></p>	1	M11
			1	M12

		$BaF_2(s) \rightleftharpoons Ba^{2+}(aq) + 2F^{-}(aq)$	<b>1</b>	<b>M13</b>
		$Q_{sp} = [Ba^{2+}][F^{-}]^2 @$	<b>1</b>	<b>M14</b>
		$= (0.01)(0.018)^2$		
		$= 3.24 \times 10^{-6}$	<b>1</b>	<b>M15</b>
		$Q_{sp} > K_{sp}$		
		The solution is supersaturated in which the concentration of ions are too large. Thus, <b>precipitate. BaF<sub>2</sub> will form</b> until $Q_{sp} = K_{sp}$	<b>1</b>	<b>M16</b>
		<b>TOTAL</b>	<b>16</b>	
		<b>MAX</b>	<b>14</b>	