ANSWER SCHEME
TEST 3
SK015
Chemistry 1
Semester 1
Session 2023/2024

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PAHANG MATRICULATION COLLEGE

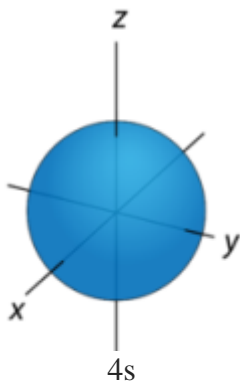**ANSWER SCHEME**
TEST 3
CHAPTER 1, 2, 4, 5, 6 & 7

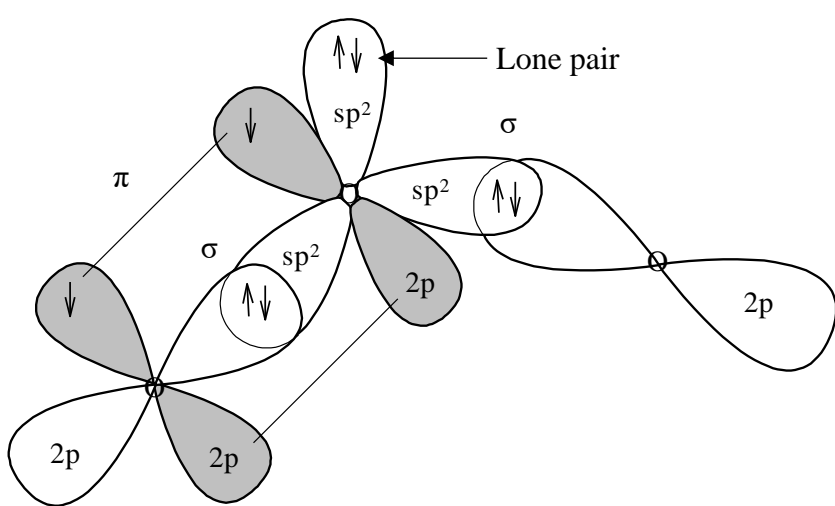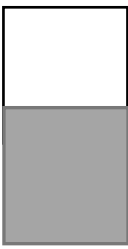| NO.	PART	SCHEME	MARKS	
1.	(a)	Average atomic mass of Mg $= \dfrac{\sum Q_i m_i}{\sum Q_i}$ @ $24.31 = \dfrac{(78.99 \times 23.985)+(X \times 24.986)+(11.01 \times 25.983)}{78.99 + X + 11.01}$ $X = 10.72\ \%$	1	M1
		Percentage abundance of ^{25}Mg = **10.72 %**	1	M2

(b)

$$\text{Mass C} = \frac{12.0\ \text{g C}}{44.0\ \text{g CO}_2} \times 1.503\ \text{g CO}_2 = \textbf{0.410 g}$$

$$\text{Mass H} = \frac{2.0\ \text{g H}}{18.0\ \text{g H}_2\text{O}} \times 0.414\ \text{g H}_2\text{O} = \textbf{0.046 g}$$

Mass O = mass of sample – (mass of C + mass of H)
  = 1.001 g – (0.410 + 0. 046) g
  = **0.545 g**

         &   1   M3

Element	C	H	O
Mass/g	0.410	0.046	0.545
Amount/mol	$\dfrac{0.410}{12.0} = \textbf{0.034}$	$\dfrac{0.046}{1.0} = \textbf{0.046}$	$\dfrac{0.545}{16.0} = \textbf{0.034}$
Simplest ratio	$\dfrac{0.034}{0.034} = \textbf{1}$	$\dfrac{0.046}{0.034} = \textbf{1.35}$	$\dfrac{0.034}{0.034} = \textbf{1}$
	$1 \times 3 = 3$	$1.35 \times 3 = 4$	$1 \times 3 = 3$

M4   1
M5   1

Empirical formula = **C$_3$H$_4$O$_3$**   1   M6

(c)

Assume; Mass $_{\text{solution}}$ = **100 g**

$$\%\,\text{w/w} = \frac{\text{mass of solute (g)}}{\text{mass of solution (g)}} \times 100\ \%$$

$$47.5\ \% = \frac{\text{mass of solute}}{100\ \text{g}} \times 100\ \%$$

$\therefore$ Mass $_{\text{solute (HBr)}}$ = **47.5 g**

       &   1   M7

@

Assume **47.5 g HBr in 100 g solution**

		$$n_{\text{solute (HBr)}} = \frac{\text{Mass}_{\text{solute (HBr)}}}{\text{Molar mass}_{\text{solute (HBr)}}}$$ $$n_{\text{solute (HBr)}} = \frac{47.5 \text{ g}}{(79.9 + 1.0) \text{ g mol}^{-1}}$$ $$= \textbf{0.587 mol}$$	1	**M8**
		$$\text{Mass}_{\text{solution}} = \rho_{\text{solution}} \times V_{\text{solution}}$$ $$100 \text{ g} = 1.30 \text{ g cm}^{-3} \times V_{\text{solution}}$$ $$V_{\text{solution}} = \textbf{76.923 cm}^3$$	1	**M9**
		$$\text{Molarity} = \frac{n_{\text{solute (HBr)}}}{V_{\text{solution}} (\text{dm}^3)}$$ $$= \frac{0.587 \text{ mol}}{0.0769 \text{ dm}^3}$$ $$= \textbf{7.63 M}$$	1	**M10**
(d)		$$MnO_4^-(aq) + SO_3^{2-}(aq) \rightarrow MnO_2(aq) + SO_4^{2-}(aq)$$		
		Oxidation: $SO_3^{2-} \rightarrow SO_4^{2-}$ Reduction: $MnO_4^- \rightarrow MnO_2$ &	1	**M11**
		$(SO_3^{2-} + H_2O \rightarrow SO_4^{2-} + 2H^+ + 2e) \times 3$ $(MnO_4^- + 4H^+ + 3e \rightarrow MnO_2 + 2H_2O) \times 2$ &	1	**M12**
		$3SO_3^{2-}(aq) + 2MnO_4^-(aq) + 2H^+(aq) \rightarrow 3SO_4^{2-}(aq) + 2MnO_2(aq) + H_2O(l)$	1	**M13**
(e) (i)		n_{NH_3} available $= 0.62$ mol n_{CO_2} available $= 0.56$ mol From equation; 2 mol $NH_3 \equiv$ 1 mol CO_2 0.62 mol $NH_3 \equiv$ **0.31 mol CO_2 (required)**	1	**M14**
		Since mole CO_2 available (0.56 mol) is **more than** mole CO_2 required (0.31 mol), CO_2 present in excess.	1	**M15**
		$\therefore$ **NH₃ is the limiting reactant.** @ 1 mol $CO_2 \equiv$ 2 mol NH_3 0.56 mol $CO_2 \equiv$ **1.12 mol NH_3 (required)** Since mole NH_3 available (0.62 mol) is **less than** mole NH_3 required (1.12 mol), NH_3 present in limits. $\therefore$ **NH₃ is the limiting reactant.**	1	**M16**

	(e) (ii)	2 mol $NH_3 \equiv$ 1 mol $(NH_2)_2CO$ 0.62 mol $NH_3 \equiv$ **0.31 mol $(NH_2)_2CO$ (required)**	1	**M17**
		Mass of $(NH_2)_2CO$ = 0.31 mol x (2[14.0 + 2(1.0)] + 12.0 + 16.0) g mol^{-1} = **18.60 g**	1 1	**M18** **M19**
	(e) (iii)	2 mol $NH_3 \equiv$ 1 mol CO_2 0.62 mol $NH_3 \equiv$ **0.31 mol CO_2 (required)**	1	**M20**
		n_{CO2} remained = n_{CO2} available – n_{CO2} required = 0.56 mol – 0.31 mol = **0.25 mol**	1	**M21**
		Mass$_{CO2}$ remained after the reaction = 0.25 mol x [12.0 + 2(16.0)] g mol^{-1} = **11.00 g**	1	**M22**
		TOTAL	**22**	
		MAX	**21**	
2.	**(a) (i)**	$\frac{1}{\lambda} = R_H \left(\frac{1}{n_1{}^2} - \frac{1}{n_2{}^2} \right)$, $n_1 < n_2$ @ $= (1.097 \times 10^7 \text{ m}^{-1}) \left(\frac{1}{1^2} - \frac{1}{3^2} \right)$ $\lambda = 1.02555 \times 10^{-7} \times 10^9$ nm = **102.55 nm**	1 1	**M1** **M2**
	(a) (ii)	$E_n = -R_H \left(\frac{1}{n^2} \right)$ @ $= -2.18 \times 10^{-18} \left(\frac{1}{2^2} \right)$ $= \mathbf{-5.45 \times 10^{-19} \text{ J}}$	1 1	**M3** **M4**
	(b) (i)	(n, l, m, s) : (3, 0, 0, -1/2) @ (3, 0, 0, +1/2)	1	**M5**
	(b) (ii)	4s and 3d orbital 4s	1	**M6**

$3d_{xy}$ @ $3d_{yz}$ @ $3d_{xz}$ @

$3d_{x2-y2}$ @ $3d_{z2}$

		* **Any 3d** orbital with **correct label**	**1**	**M7**
	(b) (iii)	Hund's Rule	**1**	**M8**
	(c)	Actual electronic configuration of copper is $1s^22s^22p^63s^23p^64s^13d^{10}$. It is because **fully-filled 3d orbital is more stable than partially-filled 3d orbital.**	**1** **1**	**M9** **M10**
		TOTAL	**10**	
3.	**(a) (i)**	$$\overset{-1\quad\ 0\quad\ 0}{:\!\overset{..}{\underset{..}{S}}\!-\!C\!\equiv\!N\!:}\qquad\qquad\overset{0\quad\ 0\quad\ -1}{\overset{..}{\underset{..}{S}}\!=\!C\!=\!\overset{..}{\underset{..}{N}}}$$ **I** **II**	**1** (I & II correct)	**M1**
	(a) (ii)	**Structure II** is the most plausible structure because the negative **formal charge is on the more electronegative nitrogen atom.**	**1** **1**	**M2** **M3**
	(b)	Valence electrons: $$\begin{array}{r} O : 3 \times 6 = \mathbf{18} \\ -\ \underline{4} \\ 14 \\ \underline{-12} \\ 2 \\ -\ \underline{2} \\ 0 \end{array}$$	**1**	**M4**
		@	**1**	**M5**
		Formal charge O in O_3 : FC $O_1 = 6 - [2 + 1/2(6)] = +1$ FC $O_2 = 6 - [4 + 1/2(4)] = 0$ } @ FC $O_3 = 6 - [6 + 1/2(2)] = -1$ $$\overset{(0)\ (+1)\ (-1)}{{}_2\!:\!\overset{..}{\underset{..}{O}}\!=\!\overset{xx}{\underset{1}{O}}\!-\!\overset{..}{\underset{..}{O}}\!:_3}$$ written in structure	**1**	**M6**

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Hybridisation process in O_3 :

Central atom
Ground state of O_1^+ : | $\uparrow\downarrow$ | $\uparrow$ | $\uparrow$ | $\uparrow$ |

         2s   2p

                                           &

Excited state of O_1^+ : | $\uparrow\downarrow$ | $\uparrow$ | $\uparrow$ | $\uparrow$ |

         2s   2p

| | 1 | M7 |

Hybrid state of O_1^+ : | $\uparrow\downarrow$ | $\uparrow$ | $\uparrow$ | | $\uparrow$ |

             sp^2 2p unhybridized

| | 1 | M8 |

Terminal atom

Ground state of O_2 : | $\uparrow\downarrow$ | $\uparrow\downarrow$ | $\uparrow$ | $\uparrow$ |

         2s   2p

                                           &

Ground state of O_3^- : | $\uparrow\downarrow$ | $\uparrow\downarrow$ | $\uparrow\downarrow$ | $\uparrow$ |

         2s   2p

| | 1 | M9 |

* Correct **shape and label of sp^2 hybrid orbital of O (Central atom)**   1   M10
* Show **e**, label **O, 2σ, 1π, 3 sp^2 orbital** and **2p.**   1   M11
* Molecular shape: **V-shape @ Bent**   1   M12

Explanation:

* **sp^2 hybrid orbital of O** overlap end to end with **2p orbital of O** to form **2σ bond** and occupied **one lone pair.**   1   M13
* **2p orbital of O overlap side by side with 2p orbital of O to form 1π.**   1   M14

| | (c) | NCl_3 has **higher** boiling point than **BCl_3** because **NCl_3 is a polar molecule** while **BCl_3 is a non-polar molecule**. | 1 | M15 |
| | | **Dipole-dipole forces** between NCl_3 molecules is **stronger than London forces @ dispersion forces** between BCl_3 molecule. | 1 | M16 |

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	(d)	Copper, **Cu is a metal** while carbon, **C is a non-metal.**	1	**M17**

	Conduction band	Conduction band
	Valence band	Valence band
	Metal, Cu	**Non-metal, C**
	@	

		There is **no band gap between valence band and conduction band** in Cu. Whereas a **large gap between valence band and conduction band** in C.	1	**M18**
		Thus, **electrons** can move **freely from valence band to conduction band of Cu to carry electricity** while **C does not.**	1	**M19**
		TOTAL	19	
		MAX	17	
4.	**(a)**	By using Boyle's Law: $P_1V_1 = P_2V_2$ $(1.2 \text{ atm}) (120 \text{ mL}) = P_2 (180 \text{ mL})$ @	1	**M1**
		$P_2 = \textbf{0.8 atm}$	1	**M2**
	(b)	By using ideal gas equation: $P_{CO_2} V = n_{CO_2} RT$ $P_{CO_2} = \dfrac{mRT}{VMr}$ $= \dfrac{(5.50 \text{ g})(0.08206 \text{ Latmmol}^{-1}\text{K}^{-1})(297.15 \text{ K})}{(10.0 \text{ L})(44.0 \text{ gmol}^{-1})}$ @ $= \textbf{0.305 atm}$ By using Dalton's Law: $P_T = P_{air} + P_{CO_2}$ $= 0.928 \text{ atm} + 0.305 \text{ atm}$	1	**M3**
		$P_T = \textbf{1.23 atm}$ 760 torr ≡ 1 atm 705 torr ≡ 0.928 atm	1	**M4**
	(c) (i)	**CH₃CH₂OH , CH₃OH , CH₃CHO** ⟶ Increasing vapour pressure	1	**M5**
	(c) (ii)	The **weaker the intermolecular forces** of the liquid molecules**, the higher the vapour pressure @ vice versa.**	1	**M6**
	(d) (i)	Phase diagram of water, **H₂O** has **negative slope** while phase diagram of carbon dioxide, **CO₂** has **positive slope.**	1	**M7**

		@ Freezing/melting curve **of H_2O slope to the left** while freezing/melting curve **of CO_2 slope to the right**.		
	(d) (ii)	It is because **ice is less dense** (occupy larger volume) **than water.** @ It is because **solid H_2O is less dense** (occupy larger volume) **than liquid H_2O.**	1	M8
	(d) (iii)	The **kinetic energy** of the water vapour **decreases**.	1	M9
		TOTAL	**9**	
5.	**(a)**	$$Q_c = \frac{[SO_3]^2}{[SO_2]^2 \, [O_2]}$$ $$= \frac{(10)^2}{(0.010)^2 \, (0.010)}$$ @	1	M1
		$= 1.0 \times 10^8$	1	M2
		$Q_c > K_c$	1	M3
		The **mixture is not at equilibrium** because:	1	M4
		- the ratio of **initial concentration of product is too large**.	1	M5
		- **product must be converted into reactant**.	1	M6
		The reaction is proceeded from **right to left**.	1	M7
	(b)	This reaction is exothermic. Decreasing temperature causes the **equilibrium position shift to right** to re-establish the equilibrium. Therefore, **the amount of SO_2 and O_2 decrease** and **the amount of SO_3 increase** until the equilibrium is reached.	1 1	M8 M9
		TOTAL	**9**	
6.	**(a) (i)**	$pH = -\log [H^+]$ $1.85 = -\log [H^+]$ **$[H^+] = x = 0.0141$ M**	1	M1

Concentration (M)	HNO$_2$(aq) $\rightleftharpoons$	NO$_2^-$(aq) +	H$^+$(aq)
Initial	0.235	0	0
Change	- x	+ x	+ x
Equilibrium	0.235-x	x	x

1 (Eq + phase) — M2

1 — M3

$$K_a = \frac{[NO_2^-] \, [H^+]}{[HNO_2]}$$
$$= \frac{(0.0141)^2}{(0.235-0.0141)}$$
    @

1 — M4

$= 9.00 \times 10^{-4}$

1 — M5

	(a) (ii)							1	M6

Concentration (M)	$HNO_2(aq)$ + $OH^-(aq)$	$\rightarrow$	$NO_2^-(aq)$ +	$H_2O(\iota)$
Initial	0.235	$\frac{(0.01\ mol)}{(1\ L)} = 0.01$	0.240	-
Change	-0.01	-0.01	+0.01	-
Equilibrium	0.225	0	0.250	-

$$pH = pK_a + \log\left[\frac{NO_2^-}{HNO_2}\right]$$

$$= -\log(9.00 \times 10^{-4}) + \log\frac{(0.250)}{(0.225)}$$

$\}$ @

$$= \mathbf{3.09}$$

(a)(ii) marks: M6 = 1, M7 = 1, M8 = 1, M9 = 1

(b)

pH vs Volume of KOH (mL); Equivalence point (pH > 7) at 25 mL; pH axis showing 2 and 7.

Axis 1 (pH & Vol KOH) — M10

1 (Shape + Eq. point) — M11

(c)

Concentration (M)	$Ag_2SO_4(s)$ $\rightleftharpoons$	$2Ag^+(aq)$ +	$SO_4^{2-}(aq)$
Initial	-	0	0
Change	-	+2s	+s
Equilibrium	-	2s	s

1 — M12

$[Ag^+] = 2s = 1.5 \times 10^{-2}$ M

$\therefore s = \mathbf{7.5 \times 10^{-3}\ M}$

1 — M13

$K_{sp} = [Ag^+]^2\,[SO_4^{2-}]$

$= (2s)^2\,(s)$ $\}$ @

1 — M14

$= 4s^3$

$= 4\,(7.5 \times 10^{-3})^3$

$= \mathbf{1.69 \times 10^{-6}}$

1 — M15

		TOTAL	15	
		MAX	14	

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