

Notes on Direct, Inverse & Differential Kinematics

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1 Introduction

2 Coordinate Transformation in 2D

The motion of manipulators and robots is often very complex and mathematically demanding. A single coordinate frame usually isn't sufficient and it's often convenient to use multiple coordinate frames (fixed or moving) to make things easier.

Terminology

Fixed and World coordinate frames are used interchangeably and mean the same thing.

Mobile and Moving coordinate frames are used interchangeably and mean the same thing.

2.1 What is a Coordinate Frame ?

If p is a vector in R^n and $X = \{x^1, x^2, \dots, x^n\}$ be a complete orthonormal set of R^n , then coordinates of p with respect to X are denoted as $[p]^x$.

$$p = \sum [p]_k^x \hat{x}^k$$
$$[p]_k^x = p \cdot \hat{x}^k$$

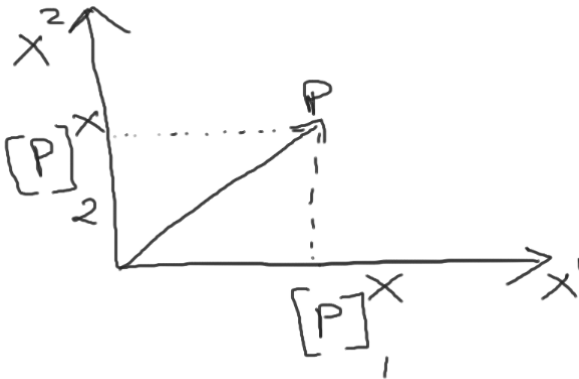


Figure 1: $p = [p]_1^x \hat{x}^1 + [p]_2^x \hat{x}^2$

2.2 Translation

Assume a fixed frame ($O_0 - X_0 - Y_0$) and a mobile frame ($O_1 - X_1 - Y_1$). Let C be a point in space. The relation between both the frames and C can be derived using simple math.

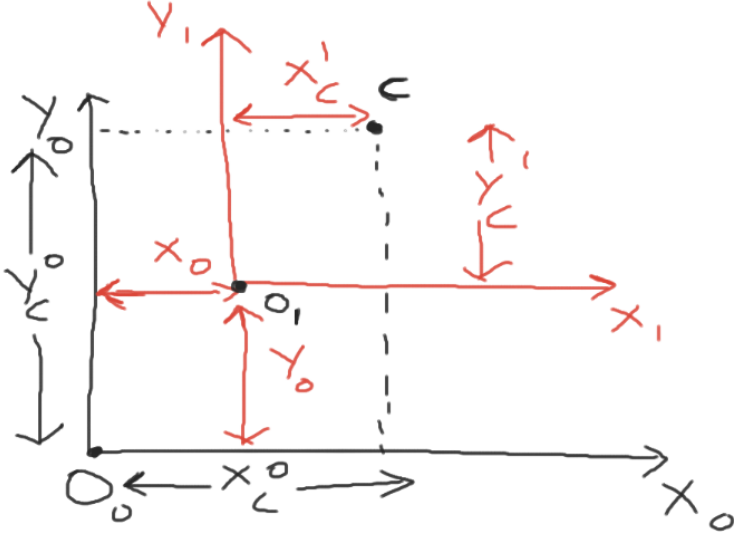


Figure 2: In red is the mobile frame and in black is the fixed frame

The following inferences can be made from the above figure:

Position of C wrt frame $(O_0 - X_0 - Y_0)$ can be represented as

$$C^0 = \begin{bmatrix} X_C^0 \\ Y_C^0 \end{bmatrix}$$

Position of C wrt frame $(O_1 - X_1 - Y_1)$ can be represented as

$$C^1 = \begin{bmatrix} X_C^1 \\ Y_C^1 \end{bmatrix}$$

Position of O_1 wrt frame $(O_0 - X_0 - Y_0)$ can be represented as

$$O_1^0 = \begin{bmatrix} X_0 \\ Y_0 \end{bmatrix}$$

Position of O_0 wrt frame $(O_1 - X_1 - Y_1)$ can be represented as

$$O_0^1 = \begin{bmatrix} -X_0 \\ -Y_0 \end{bmatrix}$$

2.3 Rotation

Assume a fixed frame $(O_0 - X_0 - Y_0)$ and a mobile frame $(O_1 - X_1 - Y_1)$. Let C be a point in space. The relation between both the frames and C can be derived using simple math.

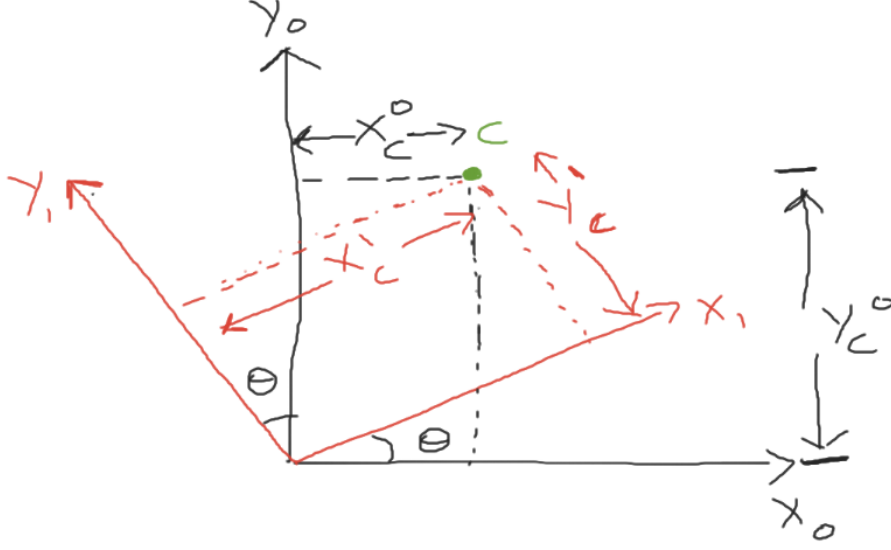


Figure 3: In red is the mobile frame and in black is the fixed frame

The following equations can be written down based on the above figure

$$\hat{X}_1 = (X_1 \cos \theta) \hat{X}_0 + (X_1 \sin \theta) \hat{Y}_0$$

$$\hat{Y}_1 = -(Y_1 \sin \theta) \hat{X}_0 + (Y_1 \cos \theta) \hat{Y}_0$$

Upon rearranging the terms,

$$\begin{bmatrix} \hat{X}_1 \\ \hat{Y}_1 \end{bmatrix} = \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} \hat{X}_0 \\ \hat{Y}_0 \end{bmatrix}$$

The above trigonometric matrix is called the rotation matrix, denoted by R . The relation between the coordinates of point C in the fixed and mobile frame can therefore be expressed as:

$$C^1 = R_0^1 C^0$$

2.4 Combined Translation and Rotation

Assume a fixed frame ($O_0 - X_0 - Y_0$) and a mobile frame ($O_2 - X_2 - Y_2$). Let us assume an intermediate mobile frame given by ($O_1 - X_1 - Y_1$).

Let C be a point of interest, The frame O_2 can be generated by translation from frame O_0 to give frame O_1 and then rotation by θ to give frame O_2 .

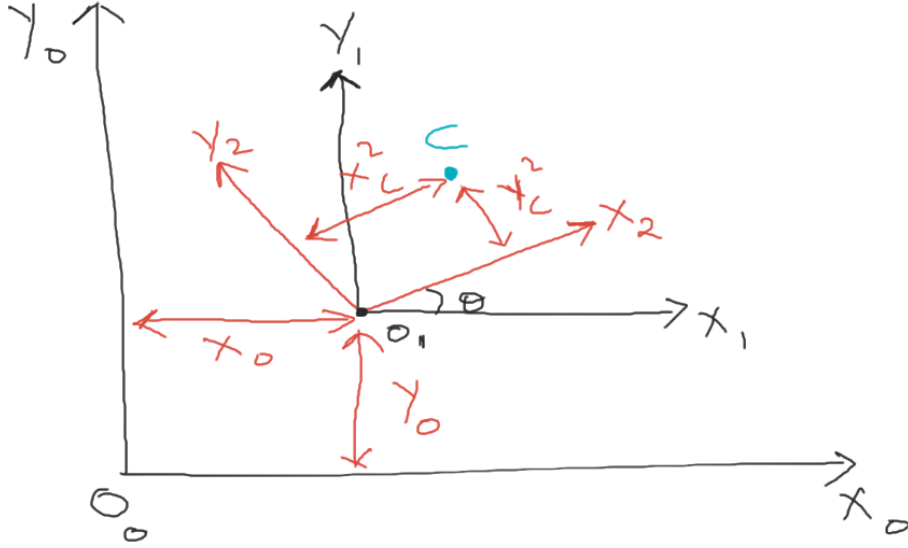


Figure 4: In red is the mobile frame and in black is the fixed frame

The coordinates of point C between the mobile and fixed frame can be related using the following:

$$C^0 = O_1^0 + R_1^0 C^1$$

2.5 2D - RR Manipulator

Consider the following manipulator diagram for a 2 DoF planar robotic arm

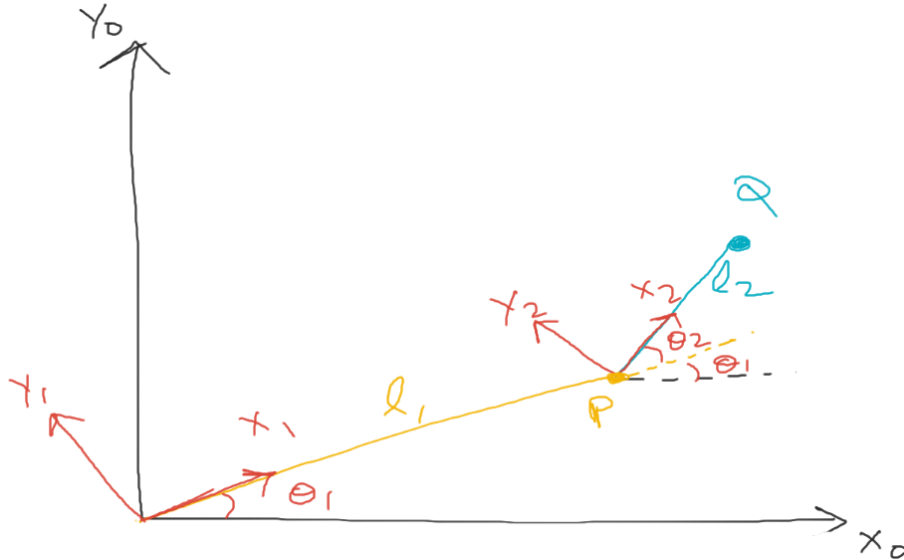


Figure 5: In red is the mobile frame and in black is the fixed frame

$$P^1 = \begin{bmatrix} l_1 \\ 0 \end{bmatrix}; Q^2 = \begin{bmatrix} l_2 \\ 0 \end{bmatrix};$$

$$R_1^0 = \begin{bmatrix} \cos \theta_1 & -\sin \theta_1 \\ \sin \theta_1 & \cos \theta_1 \end{bmatrix}; R_2^1 = \begin{bmatrix} \cos \theta_2 & -\sin \theta_2 \\ \sin \theta_2 & \cos \theta_2 \end{bmatrix};$$

$$P^0 = R_1^0 P^1$$

$$Q^1 = R_2^1 Q^2 + P^1$$

$$Q^0 = R_1^0 Q^1 = R_1^0 (R_2^1 Q^2 + P^1)$$

$$P^0 = \begin{bmatrix} X_p^0 \\ Y_p^0 \end{bmatrix} = \begin{bmatrix} l_1 \cos \theta_1 \\ l_1 \sin \theta_1 \end{bmatrix} \quad (1)$$

$$Q^0 = \begin{bmatrix} X_Q^0 \\ Y_Q^0 \end{bmatrix} = \begin{bmatrix} l_1 \cos \theta_1 + l_2 \cos (\theta_1 + \theta_2) \\ l_1 \sin \theta_1 + l_2 \sin (\theta_1 + \theta_2) \end{bmatrix} \quad (2)$$

2.5.1 Forward Kinematics

The equations for the RR manipulator can be used to draw the arm in MATLAB, the code for the same is given below.

```

1  clc
2  %clear all
3  close all
4  %% Manipulator Parameters
5  l1= 0.5; l2=0.3;
6  theta1 = 0.3; theta2 = 0.4;
7  %% World Frame
8  x_0=0; y_0=0;
9  %% Link 1
10 x_p0= l1*cos(theta1);
11 y_p0= l1*sin(theta1);
12 %% Link 2
13 x_q0 = l1*cos(theta1) + l2*cos(theta1+theta2);
14 y_q0 = l1*sin(theta1) + l2*sin(theta1+theta2);
15 %% Draw Lines
16 line([x_0,x_p0],[y_0,y_p0],'Linewidth',5,'Color',[204,204,1]/255);
17 line([x_q0,x_p0],[y_q0,y_p0],'Linewidth',5,'Color','cyan');
18 axis('equal');
19 xlabel('x');
20 ylabel('y');
21 title('RR-Manipulator')
```

Listing 1: RR-Manipulator Static Animation

Upon executing the code you should be able see something similar in your figure window

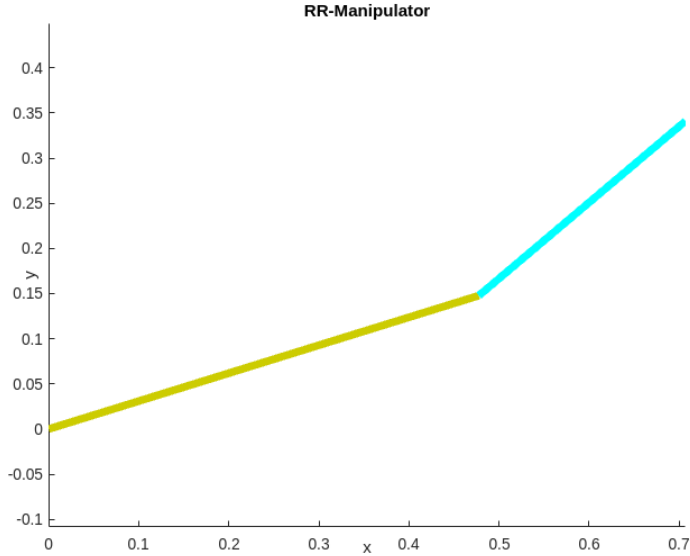


Figure 6: 2 DoF planar robotic manipulator

2.5.2 Inverse Kinematics

We can also solve for θ_1 and θ_2 given the end-effector position. This is most useful in everyday life implementation as we often know one way or another to which position our arm should move. This approach is called inverse kinematics.

Below given program is a simple example on how we can use matlab to solve the obtained system of non-linear equations for a given value of end-effector positions x_{ref}, y_{ref} , using *fsolve*. Other numerical methods for solving system of non-linear equations that can be implemented from scratch will be discussed in later sections.

```

1 clc
2 close all
3 l1 = 0.5; l2 = 0.5;
4 x_ref = 0.5; y_ref = 0;
5 param = [l1 l2 x_ref y_ref];
6 x0 = [0.1 0.1];
7 [x,fval,exitflag] = fsolve(@Lec2_InvFun,x0,optimoptions('fsolve','Display',
    'iter'),param)
8 theta1 = x(1);
9 theta2 = x(2);
10 %% World Frame
11 x_0=0; y_0=0;
12 %% Link 1
13 x_p0= l1*cos(theta1);
14 y_p0= l1*sin(theta1);
15 %% Link 2
16 x_q0 = l1*cos(theta1) + l2*cos(theta1+theta2);
17 y_q0 = l1*sin(theta1) + l2*sin(theta1+theta2);
18 %% Draw Lines
19 line([x_0,x_p0],[y_0,y_p0],'Linewidth',5,'Color',[204,204,1]/255);

```



```

20 line([x_q0,x_p0],[y_q0,y_p0'],'Linewidth',5,'Color','cyan');
21 axis('equal');
22 xlabel('x');
23 ylabel('y');
24 title('RR-Manipulator')

```

Listing 2: RR-Manipulator Static Inverse Kinematics

As you might have noticed the above program depends on an external function called `Lec2_InvFun`. The code for the function is given below.

```

1 function F = Lec2_InvFun(x,param)
2 l1=param(1); l2=param(2);
3 x_ref=param(3); y_ref=param(4);
4 theta1=x(1); theta2=x(2);
5 x_q0 = l1*cos(theta1) + l2*cos(theta1+theta2);
6 y_q0 = l1*sin(theta1) + l2*sin(theta1+theta2);
7 F = [x_q0 - x_ref; y_q0 - y_ref];
8 end

```

Listing 3: Additional Function for Manipulator

Upon executing the code you should be able to see something similar in your figure window

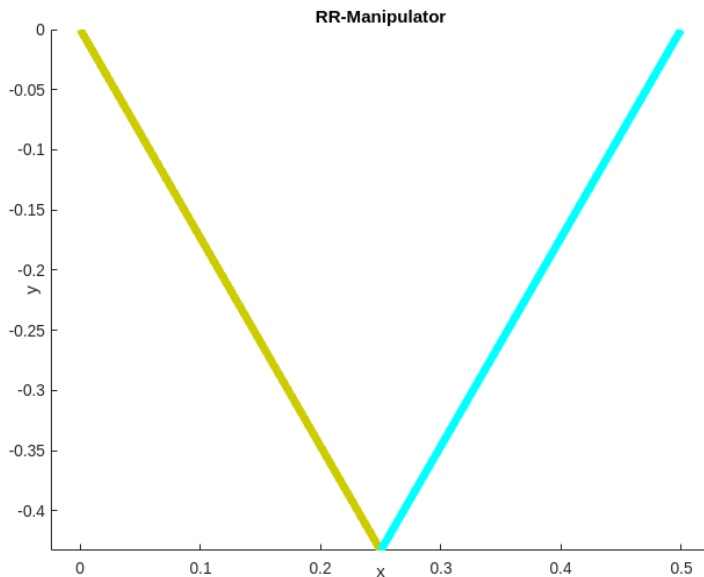


Figure 7: Manipulator Pose for $(x_{ref}, y_{ref}) = (0.5, 0)$

2.5.3 Tracing Trajectories

If we can write the mathematical equation for a curve the x,y points on the curve can be passed into the inverse kinematics block for the manipulator which allows the robotic arm to trace the shape of the curve. The below given program does the same, it also shows the animation of the manipulator.

Note, that the below given program uses `Lec2_InvFun` for running.

```

1  clc
2  close all
3  %% Parameter Setting
4  l1 = 1; l2 = 1;
5  %% Trajectory Generator
6  phi = linspace(0,2*pi,51);
7  x_ref = 1+0.5*cos(phi); y_ref = 0.5+0.5*sin(phi);
8  theta1 = 0.5; theta2 = 0.5;
9  theta1_f = zeros(length(phi),1);
10 theta2_f = zeros(length(phi),1);
11 for i=1:length(phi)
12 theta = [theta1,theta2];
13 options = optimoptions('fsolve','Display','Off','MaxIter',100,'MaxFunEval',
    ,300);
14 param = [l1 l2 x_ref(i) y_ref(i)];
15 [x,fval,exitflag] = fsolve(@Lec2_InvFun,theta,options,param);
16 theta1 = x(1); theta2 = x(2);
17 theta1_f(i,1) = x(1);
18 theta2_f(i,1) = x(2);
19 end
20 %% World Frame
21 x_0=0; y_0=0;
22 %% Animation
23 for i=1:length(phi)
24 % Link 1
25 x_p0= l1*cos(theta1_f(i));
26 y_p0= l1*sin(theta1_f(i));
27 % Link 2
28 x_q0 = l1*cos(theta1_f(i)) + l2*cos(theta1_f(i) + theta2_f(i));
29 y_q0 = l1*sin(theta1_f(i)) + l2*sin(theta1_f(i) + theta2_f(i));
30 % Tracer
31 plot(x_q0,y_q0,'ko','MarkerSize',5,'MarkerEdgeColor','k','MarkerFaceColor',
    , 'k');
32 hold on;
33 h1 = line([x_0,x_p0],[y_0,y_p0],'Linewidth',5,'Color',[204,204,1]/255);
34 h2 = line([x_q0,x_p0],[y_q0,y_p0],'Linewidth',5,'Color','cyan');
35 grid on;
36 axis('equal');
37 xlabel('x');
38 ylabel('y');
39 title('RR-Manipulator')
40 xlim([-2 2]);
41 ylim([-2 2]);
42 pause(0.3);
43 if i < length(phi)
44 delete(h1);
45 delete(h2);
46 end
47 end

```

Listing 4: Trajectory Trace

Upon executing the code you should be able see something similar in your figure window

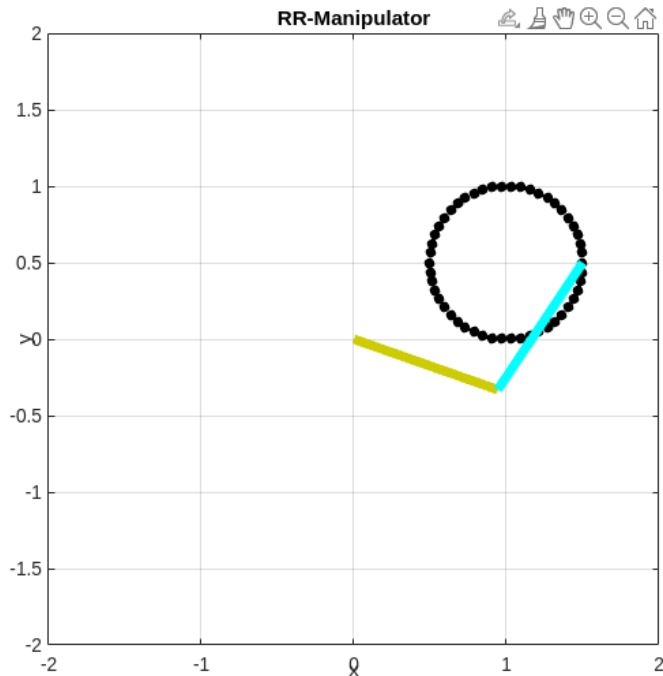


Figure 8: Manipulator motion for a given circular trajectory

2.6 Differential Drive

Consider a fixed frame $(O_0 - X_0 - Y_0)$ and a mobile frame $(O_1 - X_1 - Y_1)$, the mobile frame is attached to a two wheel differential drive robot, such that the X_1 axis is pointing forwards and the Y_1 is perpendicular to the orientation of the wheels.

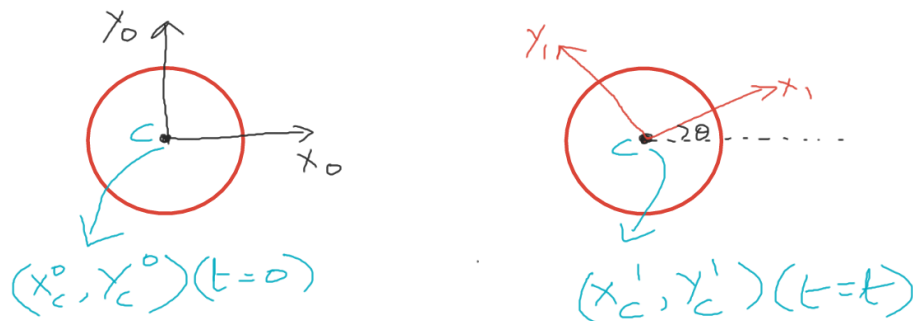


Figure 9: Manipulator motion for a given circular trajectory

Let r be the radius of the wheels and $2b$ be the distance between the wheels, and θ be the angle the mobile frame makes with the horizontal of the fixed frame.

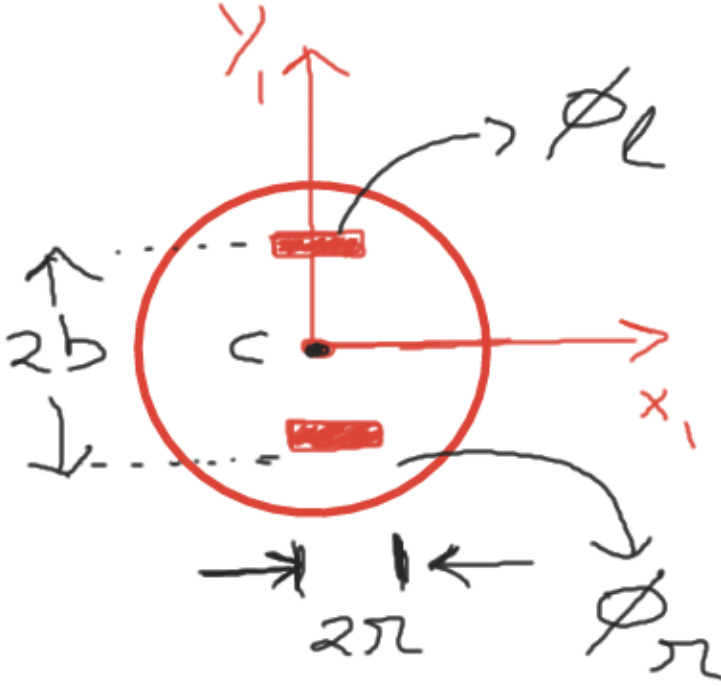


Figure 10: Manipulator motion for a given circular trajectory

2.6.1 Forward Kinematics

The forward kinematics of the differential drive car involves finding $(X_C^0(t), Y_C^0(t))$ given b, r , initial position $(X_C^0(t=0), Y_C^0(t=0))$ and the driving history of the robot $(\phi_r(t), \phi_l(t))$.

The distance traveled by the wheel if it rotates by an angle ϕ is given by $r\phi$. The rate of change of distance travelled by the wheel is therefore given by $r\dot{\phi}$. Assuming the right wheel is denoted by the subscript r, similar assumptions and derivations can be made for the left wheel.

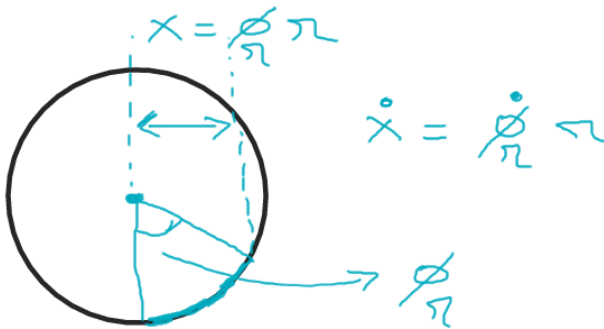


Figure 11: Cross-sectional view of the right wheel

Case 1: $\dot{\phi}_l = 0, \dot{\phi}_r \neq 0$

The distance moved by the right wheel is given by, $X_{wr} = r\phi_r$. The velocity of the right

A diagram showing a particle (black dot) moving in a magnetic field. A red circle is drawn around the particle. A red arrow points from the particle towards the top right. A black arrow points from the particle towards the bottom right. The particle is labeled $p_L = 0$. The magnetic field is labeled w_R . The particle's position is labeled C . The particle's velocity is labeled $\dot{x}_L = 0.5\pi\dot{\phi}_R$. The magnetic field vector is labeled $\vec{x}_{wR} = \pi\dot{\phi}_R$.

From geometry, the speed of the center C in the direction of X_1 can be written as,

Case 2: $\dot{\phi}_l \neq 0, \dot{\phi}_r = 0$

$$\dot{X}_{wl}^1 = r\dot{\phi}_l$$

From case 1 & 2, the velocity of the point C in the directions of X_1 and Y_1 can be written down as,

$$\dot{Y}_C^1 = 0 \quad (4)$$

$$\dot{C}^0 = R_1^0 \dot{C}^1$$

$$\begin{bmatrix} \dot{X}_C^0 \\ \dot{Y}_C^0 \end{bmatrix} = \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} \dot{X}_C^1 \\ \dot{Y}_C^1 \end{bmatrix}$$

$$\begin{bmatrix} \dot{X}_C^0 \\ \dot{Y}_C^0 \end{bmatrix} = \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} 0.5r(\dot{\phi}_r + \dot{\phi}_l) \\ 0 \end{bmatrix}$$

$$X_C^0(t) = 0.5r(\dot{\phi}_r + \dot{\phi}_l) \cos \theta$$

For finding the expression for rate of change of θ ,

$$X_{wr} = r\phi_r$$

from geometry,

$$X_{wr} = 2b\theta$$

therefore gives,

$$\dot{\theta} = \frac{r\dot{\phi}_r}{2b}$$

Similar arguments can be made for the other case, only exception being the angle θ is negative. Therefore from case 1 and 2 the following can be derived.

$$\dot{\theta} = \frac{r}{2b}(\dot{\phi}_r - \dot{\phi}_l)$$

Therefore to summarize,

$$\begin{aligned} \dot{X}_C^0 &= v \cos \theta \\ \dot{Y}_C^0 &= v \sin \theta \\ \dot{\theta} &= \omega \\ v &= 0.5r(\dot{\phi}_r + \dot{\phi}_l) \\ w &= \frac{r}{2b}(\dot{\phi}_r - \dot{\phi}_l) \end{aligned}$$

To find X_C^0, Y_C^0, θ , we will be using Euler's integration.

$$\begin{aligned} \dot{X}_C^0 &= \frac{X_C(t_{i+1}) - X_C(t_i)}{t_{i+1} - t_i} = v(t_i) \cos \theta(t_i) \\ \dot{Y}_C^0 &= \frac{Y_C(t_{i+1}) - Y_C(t_i)}{t_{i+1} - t_i} = v(t_i) \sin \theta(t_i) \\ \dot{\theta} &= \frac{\theta(t_{i+1}) - \theta(t_i)}{t_{i+1} - t_i} = \omega(t_i) \end{aligned}$$

Upon rearranging the terms,

$$\begin{aligned} X_C^0(t_{i+1}) &= X_C^0(t_i) + hv(t_i) \cos \theta(t_i) \\ Y_C^0(t_{i+1}) &= Y_C^0(t_i) + hv(t_i) \sin \theta(t_i) \\ \theta(t_{i+1}) &= \theta(t_i) + h\omega(t_i) \end{aligned}$$

```

1 clc
2 close all
3
4 parms.R = 0.1; %Radius of the chassis for animation
5 %% Initialize States
6 fps = 10;
7 parms.delay = 0.2;
8 z0 = [0 0 -pi/2]; %initial position of the car
9 h = 0.1; %step size

```

```

10 %% Motion
11 t1 = 0:h:1;
12 speed1 = ones(1,length(t1));
13 omega1 = zeros(1,length(t1));
14 t2 = 1+h:h:2;
15 speed2 = zeros(1,length(t2));
16 omega2 = pi/2*ones(1,length(t2));
17 t3 = 2+h:h:3;
18 speed3 = ones(1,length(t3));
19 omega3 = zeros(1,length(t3));
20 t4 = 3+h:h:4;
21 t5 = 4+h:h:5;
22 t6 = 5+h:h:6;
23 t7 = 6+h:h:7;
24 t = [t1 t2 t3 t4 t5 t6 t7];
25 speed = [speed1 speed2 speed3 speed2 speed3 speed2 speed3];
26 omega = [omega1 omega2 omega3 omega2 omega3 omega2 omega3];
27 %% Euler Integration
28 z = z0; %Initial parameters
29 for i=1:length(t)-1
30     u = [speed(i) omega(i)];
31     zz = Lec3_Euler(h,z0,u);
32     z0 = zz;
33     z = [z;z0];
34 end
35 % t_interp = linspace(0,t(end),fps*t(end));
36 % [m,n] = size(z);
37 % for i=1:n
38 %     z_interp(:,i) = interp1(t,z(:,i),t_interp);
39 % end
40 %% Animation
41 figure(1)
42 Lec3_Animate(t,z,parms);

```

Listing 5: Main program for differential drive

```

1 function Lec3_Animate(t,z,parms)
2 R = parms.R;
3 phi = linspace(0,2*pi);
4 x_circle = R*cos(phi);
5 y_circle = R*sin(phi);
6 % if (parms.writeMovie)
7 %     mov = VideoWriter(parms.nameMovie);
8 %     open(mov);
9 %end
10 n = length(t);
11 for i=1:n
12     theta = z(i,3);
13     x_robot = z(i,1) + x_circle;
14     y_robot = z(i,2) + y_circle;
15     x_dir = z(i,1) + [0 R*cos(theta)];
16     y_dir = z(i,2) + [0 R*sin(theta)];
17     plot(z(1:i,1),z(1:i,2),'r','Linewidth',2); hold on;
18     light_blue = [176,224,230]/255;

```

```

19 h1= patch(x_robot,y_robot,light_blue);
20 h2 = line(x_dir,y_dir,'Color','black','Linewidth',2);
21 axis('equal');
22 %span = max([-min(min(z(:,1:2))) max(max(z(:,1:2)))]);
23 %span = max([span 2]);
24 %axis([-span span -span span]);
25 axis([-2 2 -2 2]);
26 grid on;
27 pause(parms.delay)
28 delete(h1);
29 delete(h2);
30 % if (parms.writeMovie)
31 %     axis off %does not show axis
32 %     set(gcf,'Color',[1,1,1]) %set background to white
33 %     writeVideo(mov,getframe);
34 % end
35 end
36 % if (parms.writeMovie)
37 %     close(mov);
38 end

```

Listing 6: Function for animation

```

1 function F = Lec3_Euler(h,z0,u)
2 v = u(1);
3 omega = u(2);
4 x_t0 = z0(1);
5 y_t0 = z0(2);
6 theta_t0 = z0(3);
7 xdot_c = v*cos(theta_t0);
8 ydot_c = v*sin(theta_t0);
9 thetadot = omega;
10 x_t1 = x_t0 + xdot_c*h;
11 y_t1 = y_t0 + ydot_c*h;
12 theta_t1 = theta_t0 + thetadot*h;
13 F = [x_t1, y_t1, theta_t1];
14 end

```

Listing 7: Euler Integration function for differential drive

Upon successful execution of the above program you should be able to see a figure similar to this

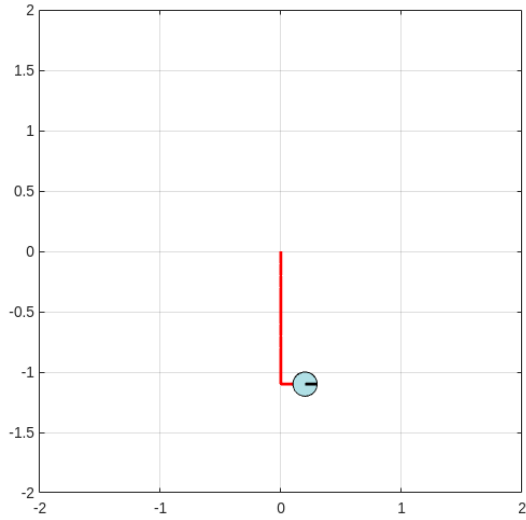


Figure 13: Simulation of Diff. Drive

2.6.2 Inverse Kinematics

Inverse Kinematics is defined as finding the values of v, ω given (X_P^0, Y_P^0) as a function of time, where P is a point fixed on the robot as shown in the figure.

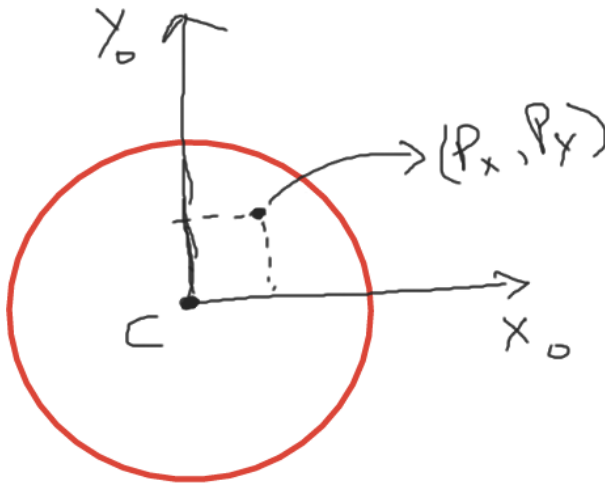


Figure 14: Simulation of Diff. Drive

From previous sections, we have the following relations

$$\begin{aligned}
P^0 &= R_1^0 P^1 \\
C^0 &= R_1^0 C^1 \\
P^0 - C^0 &= R_1^0 (P^1 - C^1) \\
\begin{bmatrix} X_P^0 - X_C^0 \\ X_P^0 - Y_C^0 \end{bmatrix} &= \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} X_P^1 - X_C^1 \\ Y_P^1 - Y_C^1 \end{bmatrix} \\
\begin{bmatrix} X_P^0 - X_C^0 \\ X_P^0 - Y_C^0 \end{bmatrix} &= \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} P_X \\ P_Y \end{bmatrix} \\
\begin{bmatrix} X_P^0 \\ Y_P^0 \end{bmatrix} &= \begin{bmatrix} X_C^0 \\ Y_C^0 \end{bmatrix} + \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} P_X \\ P_Y \end{bmatrix} \\
\begin{bmatrix} X_C^0 \\ Y_C^0 \end{bmatrix} &= \begin{bmatrix} X_P^0 \\ Y_P^0 \end{bmatrix} + \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} P_X \\ P_Y \end{bmatrix}
\end{aligned}$$

Differentiating the above equations with time,

$$\begin{aligned}
\begin{bmatrix} \dot{X}_P^0 \\ \dot{Y}_P^0 \end{bmatrix} &= \begin{bmatrix} \dot{X}_C^0 \\ \dot{Y}_C^0 \end{bmatrix} + \begin{bmatrix} \dot{\theta} \sin \theta & -\dot{\theta} \cos \theta \\ \dot{\theta} \cos \theta & -\dot{\theta} \sin \theta \end{bmatrix} \begin{bmatrix} P_X \\ P_Y \end{bmatrix} \\
\begin{bmatrix} \dot{X}_P^0 \\ \dot{Y}_P^0 \end{bmatrix} &= \begin{bmatrix} v \cos \theta \\ v \sin \theta \end{bmatrix} + \begin{bmatrix} \omega \sin \theta & -\omega \cos \theta \\ \omega \cos \theta & -\omega \sin \theta \end{bmatrix} \begin{bmatrix} P_X \\ P_Y \end{bmatrix} \\
\begin{bmatrix} \dot{X}_P^0 \\ \dot{Y}_P^0 \end{bmatrix} &= \begin{bmatrix} \cos \theta & (-P_X \sin \theta - P_Y \cos \theta) \\ \sin \theta & (P_X \cos \theta - P_Y \sin \theta) \end{bmatrix} \begin{bmatrix} v \\ \omega \end{bmatrix}
\end{aligned}$$

We will be using a proportional controller for driving the error towards zero.

$$\begin{aligned}
\dot{X}_P^0 &= K_{P_x} (X_{ref} - X_P^0) \\
\dot{Y}_P^0 &= K_{P_y} (Y_{ref} - Y_P^0)
\end{aligned}$$

Where K_{P_x}, K_{P_y} are user chosen gains and X_{ref}, Y_{ref} are the desired reference points. Substituting these values in the above derived equations.

$$\begin{aligned}
\begin{bmatrix} K_{P_x} (X_{ref} - X_P^0) \\ K_{P_y} (Y_{ref} - Y_P^0) \end{bmatrix} &= \begin{bmatrix} \cos \theta & (-P_X \sin \theta - P_Y \cos \theta) \\ \sin \theta & (P_X \cos \theta - P_Y \sin \theta) \end{bmatrix} \begin{bmatrix} v \\ \omega \end{bmatrix} \\
\begin{bmatrix} v \\ \omega \end{bmatrix} &= \begin{bmatrix} \cos \theta - \left(\frac{P_X}{P_Y}\right) \sin \theta & \sin \theta + \left(\frac{P_X}{P_Y}\right) \cos \theta \\ -\left(\frac{1}{P_X}\right) \sin \theta & -\left(\frac{1}{P_X}\right) \cos \theta \end{bmatrix} \begin{bmatrix} K_{P_x} (X_{ref} - X_P^0) \\ K_{P_y} (Y_{ref} - Y_P^0) \end{bmatrix}
\end{aligned}$$

Also from forward kinematics we know the following,

$$\begin{aligned}
\dot{X}_C^0 &= v \cos \theta \\
\dot{Y}_C^0 &= v \sin \theta \\
\dot{\theta} &= \omega
\end{aligned}$$

All of the above derived equations can be used to create a trajectory following differential drive robot the code attached below follows a mathematical trajectory called "astroid" the code also has an PD controller implemented to keep the error close to zero.

```

1  clc
2  close all
3  %% Parameters
4  parms.R = 0.1;
5  parms.px = 0.05;
6  parms.py = 0;
7  parms.Kp = 100;
8  parms.Kd = 0.5;
9  parms.delay = 0.001;
10 t0 = 0;
11 tend = 10;
12 fps = 10;
13 t=t0:0.01:tend;
14 h = 0.01;
15 %% Trajectory
16 x_center = 0;
17 y_center = 0;
18 a = 1;
19 x_ref = x_center+a*cos(2*pi*t/tend).^3;
20 y_ref = y_center+a*sin(2*pi*t/tend).^3;
21 %% Initilization
22 theta0 = pi/2;
23 [x0 y0] = Lec4_ptP_to_ptC(x_ref(1),y_ref(1),theta0,parms);
24 z0 = [x0 y0 theta0];
25 z = z0;
26 e = [0 0];
27 v = 0;
28 omega = 0;
29 for i=1:length(t)-1
30 x_c = z(end,1);
31 y_c = z(end,2);
32 theta = z(end,3);
33 [x_p, y_p] = Lec4_ptC_to_ptP(x_c,y_c,theta,parms);
34 error = [x_ref(i+1)-x_p y_ref(i+1)-y_p];
35 e = [e; error];
36 err_p_dot = [parms.Kp*error(1)+parms.Kd*((e(end,1)-e(end-1,1))/h); parms.Kp*error(2)+parms.Kd*((e(end,2)-e(end-1,2))/h)];
37 c = cos(theta); s=sin(theta);
38 px = parms.px; py = parms.py;
39 A = [c-(py/px)*s s+(py/px)*c; ...
40 -(1/px)*s (1/px)*c];
41 u = A*err_p_dot; %u = [v omega]
42 v = [v; u(1)];
43 omega = [omega; u(2)];
44 %zz = ode4(@Lec4_RHS,[t(i) t(i+1)],z0,u);
45 zz = Lec3_Euler(h,z0,u);
46 z0 = zz(end,:);
47 z = [z; z0];
48 end
49 t_interp = linspace(t0,tend,fps*tend);

```

```

50 [m,n] = size(z);
51 for i=1:n
52 z_interp(:,i) = interp1(t,z(:,i),t_interp);
53 end
54 figure(1)
55 Lec3_Animate(t_interp,z_interp,parms);
56 figure(2)
57 subplot(2,1,1)
58 plot(t,v,'m'); hold on
59 plot(t,omega,'c');
60 ylabel('Velocity');
61 legend('v','\omega','Location','Best');
62 subplot(2,1,2)
63 plot(t,e(:,1),'r'); hold on
64 plot(t,e(:,2),'b');
65 legend('error x','error y','Location','Best');
66 ylabel('error');
67 xlabel('time');

```

Listing 8: Main Program

```

1 function [x_p,y_p] = Lec4_ptC_to_ptP(x_c,y_c,theta,parms)
2 c = cos(theta); s = sin(theta);
3 p = [parms.px; parms.py];
4 Xp = [c -s; s c]*p + [x_c; y_c];
5 x_p = Xp(1); y_p = Xp(2);
6 end

```

Listing 9: Supporting Function

```

1 function [x_c,y_c] = Lec4_ptP_to_ptC(x_p,y_p,theta,parms)
2 c = cos(theta); s = sin(theta);
3 p = [parms.px; parms.py];
4 Xc = -[c -s; s c]*p + [x_p; y_p];
5 x_c = Xc(1); y_c = Xc(2);
6 end

```

Listing 10: Supporting Function

```

1 function Y = ode4(odefun,tspan,y0,varargin)
2 %ODE4 Solve differential equations with a non-adaptive method of order 4.
3 % Y = ODE4(ODEFUN,TSPAN,Y0) with TSPAN = [T1, T2, T3, ... TN] integrates
4 % the system of differential equations y' = f(t,y) by stepping from T0
  to
5 % T1 to TN. Function ODEFUN(T,Y) must return f(t,y) in a column vector.
6 % The vector Y0 is the initial conditions at T0. Each row in the
  solution
7 % array Y corresponds to a time specified in TSPAN.
8 %
9 % Y = ODE4(ODEFUN,TSPAN,Y0,P1,P2...) passes the additional parameters
10 % P1,P2... to the derivative function as ODEFUN(T,Y,P1,P2...).
11 %
12 % This is a non-adaptive solver. The step sequence is determined by
  TSPAN
13 % but the derivative function ODEFUN is evaluated multiple times per
  step.

```

```

14 % The solver implements the classical Runge-Kutta method of order 4.
15 %
16 % Example
17 %     tspan = 0:0.1:20;
18 %     y = ode4(@vdp1,tspan,[2 0]);
19 %     plot(tspan,y(:,1));
20 %     solves the system y' = vdp1(t,y) with a constant step size of 0.1,
21 %     and plots the first component of the solution.
22 %
23 if ~isnumeric(tspan)
24 error('TSPAN should be a vector of integration steps.');
```

```

25 end
26 if ~isnumeric(y0)
27 error('Y0 should be a vector of initial conditions.');
```

```

28 end
29 h = diff(tspan);
30 if any(sign(h(1))*h <= 0)
31 error('Entries of TSPAN are not in order.')
```

```

32 end
33 try
34 f0 = feval(odefun,tspan(1),y0,varargin{:});
35 catch
36 msg = ['Unable to evaluate the ODEFUN at t0,y0. ',lasterr];
37 error(msg);
38 end
39 y0 = y0(:); % Make a column vector.
40 if ~isequal(size(y0),size(f0))
41 error('Inconsistent sizes of Y0 and f(t0,y0).');
```

```

42 end
43 neq = length(y0);
44 N = length(tspan);
45 Y = zeros(neq,N);
46 F = zeros(neq,4);
47 Y(:,1) = y0;
48 for i = 2:N
49 ti = tspan(i-1);
50 hi = h(i-1);
51 yi = Y(:,i-1);
52 F(:,1) = feval(odefun,ti,yi,varargin{:});
53 F(:,2) = feval(odefun,ti+0.5*hi,yi+0.5*hi*F(:,1),varargin{:});
54 F(:,3) = feval(odefun,ti+0.5*hi,yi+0.5*hi*F(:,2),varargin{:});
55 F(:,4) = feval(odefun,tspan(i),yi+hi*F(:,3),varargin{:});
56 Y(:,i) = yi + (hi/6)*(F(:,1) + 2*F(:,2) + 2*F(:,3) + F(:,4));
57 end
58 Y = Y.';

```

Listing 11: Optional Function -ode4

```

1 function zdot = Lec4_RHS(t,z,u)
2 v = u(1); omega = u(2);
3 theta = z(3);
4 x_c_dot = v*cos(theta);
5 y_c_dot = v*sin(theta);
6 theta_dot = omega;

```

```
7 zdot = [x_c_dot y_c_dot theta_dot]';
```

Listing 12: Optional Function - rhs

Upon successful execution of the above program, you will end up with the following two figures.

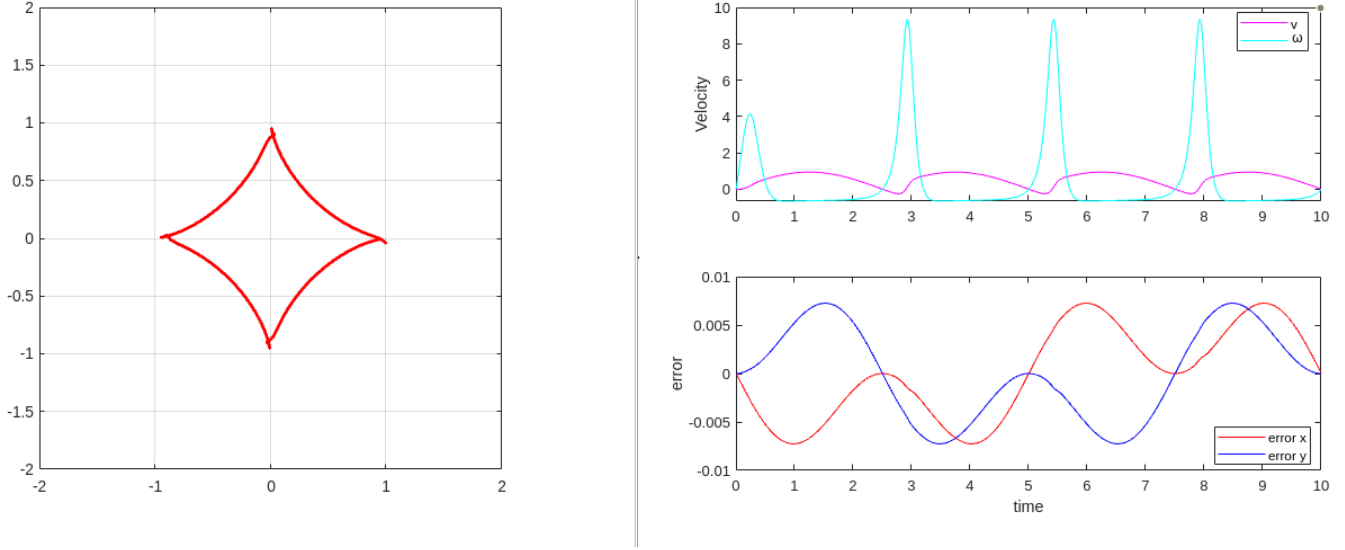


Figure 15: Simulation of Diff. Drive

2.7 Projectile Motion

2-D projectile motion will be analyzed in this section, Euler Lagrange Equations will be introduced and used for finding out the equations of motion of the projectile.

2.7.1 Forward Kinematics

Let the position of the projectile wrt to the fixed frame be denoted as (X, Y) . The launch angle is denoted by θ and the drag force is given by $\vec{F}_d = -Cv^2\hat{v}$.

$$\vec{F}_d = -Cv^2\hat{v} = -Cv^2 \frac{\vec{v}}{|\vec{v}|} = -C|v|\hat{v}$$

$$F_x = -C\dot{x}\sqrt{\dot{x}^2 + \dot{y}^2}$$

$$F_y = -C\dot{y}\sqrt{\dot{x}^2 + \dot{y}^2}$$

From Euler-Lagrange Formulaism,

$$L = T - V$$

$$T = 0.5mv^2 = 0.5m(\dot{x}^2 + \dot{y}^2)$$

$$V = mgy$$

$$L = 0.5m(\dot{x}^2 + \dot{y}^2) - mgy$$

Given that,

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_j} \right) - \frac{\partial L}{\partial q_j} = Q_j$$

In the direction of x,

$$\frac{d}{dt} \left(\frac{\partial(0.5m(\dot{x}^2 + \dot{y}^2) - mgy)}{\partial \dot{x}} \right) - \frac{\partial(0.5m(\dot{x}^2 + \dot{y}^2) - mgy)}{\partial x} = -C\dot{x}\sqrt{\dot{x}^2 + \dot{y}^2}$$

$$\ddot{x} = -\frac{C}{m}\dot{x}\sqrt{\dot{x}^2 + \dot{y}^2}$$

In the direction of y,

$$\frac{d}{dt} \left(\frac{\partial(0.5m(\dot{x}^2 + \dot{y}^2) - mgy)}{\partial \dot{y}} \right) - \frac{\partial(0.5m(\dot{x}^2 + \dot{y}^2) - mgy)}{\partial y} = -C\dot{y}\sqrt{\dot{x}^2 + \dot{y}^2}$$

$$\ddot{y} = -g - \frac{C}{m}\dot{y}\sqrt{\dot{x}^2 + \dot{y}^2}$$

Integrating \ddot{x} and \ddot{y} wrt time should give us \dot{x}, \dot{y}, x, y .

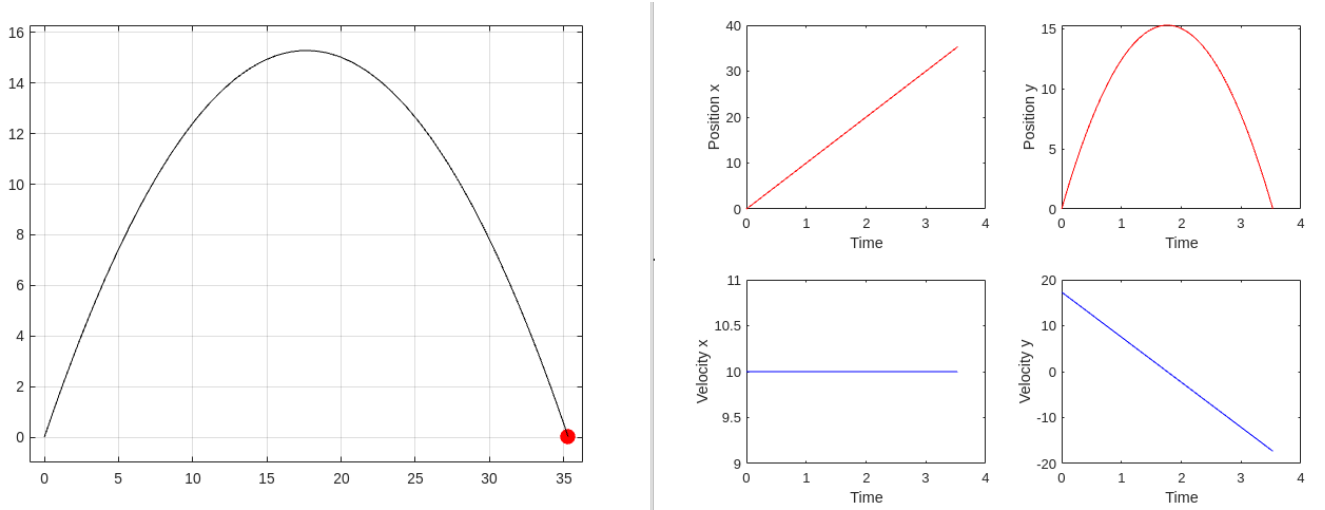


Figure 16: Simulation of Diff. Drive

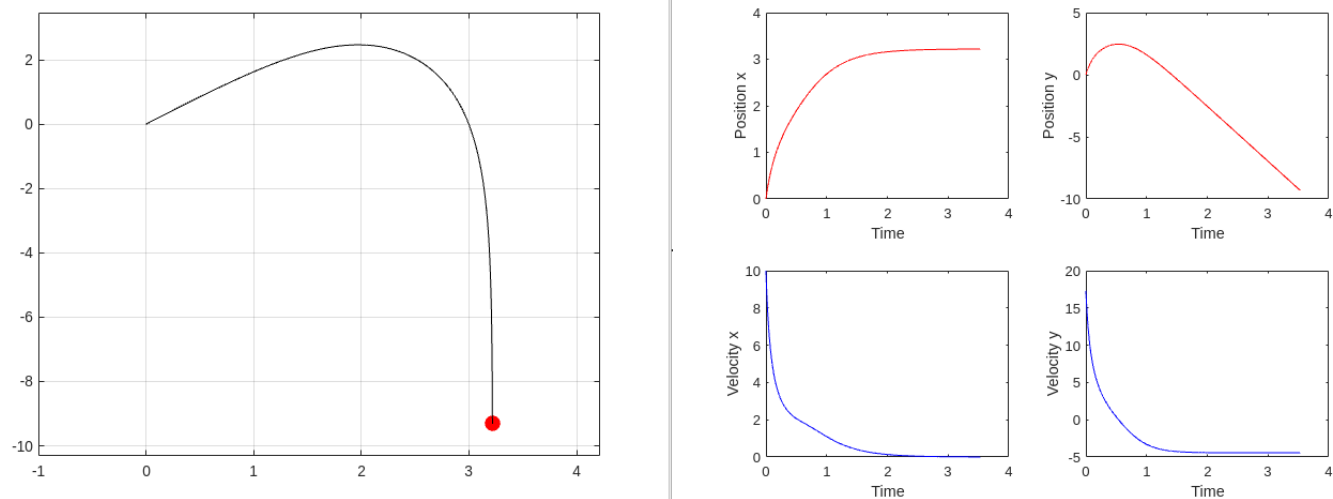


Figure 17: Simulation of Diff. Drive

2.7.2 Inverse Kinematics