

Course Number	AE8112
Course Title	Computational Fluid Dynamics and Heat Transfer
Semester/Year	Summer/Spring 2021
Instructor	Dr. Seth Dworkin

Problem Set 4

Submission Date	July 14, 2021
Programing Language Used	Fortran90

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Q1a | From the given problem, we can assume that the flow is incompressible (i.e. $\rho = \text{const.}$), and that the flow is viscous (since $\mu = 1.84 \times 10^{-5} \text{ kg/ms}$) So that the vector eqn for the conservation of momentum (c.o.mom) is,

$$\frac{\partial}{\partial t} (\rho \vec{u}_r) + \nabla (\rho \hat{u}_r \vec{u}_r) = -\nabla p + \nabla \cdot \vec{\tau}$$

where $\vec{\tau} \rightarrow$ represents the viscous stress tensor

$u_r \rightarrow$ represents the radial velocity

Since we assume $\rho = \text{const.}$, the continuity eqn will be

$$\nabla \cdot (\rho \vec{u}_r) = 0$$

This means we don't need pressure corrector to match the condition of our velocity in the above continuity eqn. So that the divergence in 1D, $\nabla \cdot \vec{\tau} = \frac{1}{r} \frac{\partial}{\partial r} (r \tau)$ for cylindrical coord.

and according to Newton's law of viscosity, ~~(10)~~

$$\tau = \tau_{rr}$$

where $\tau_{rr} = \mu \frac{\partial u_r}{\partial r}$ (for incompressible 1D flow)

Q1a) cont'd.

we also have the gradient

$$\nabla P = \frac{\partial P}{\partial r}$$

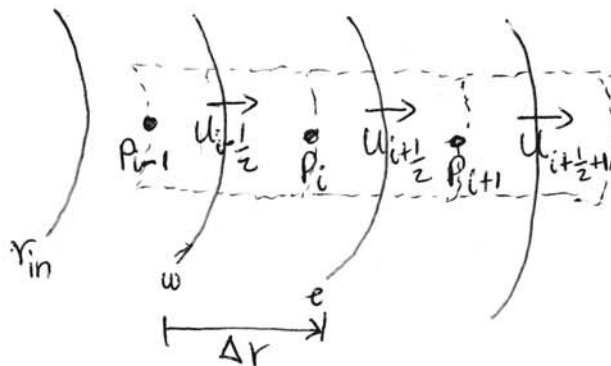
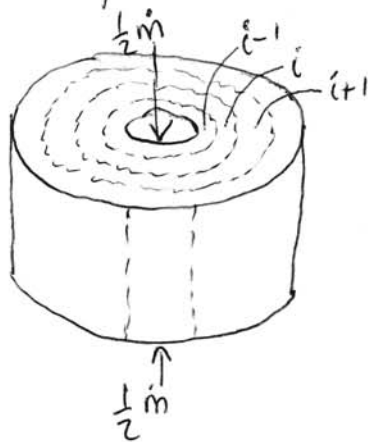
So that we have the Navier-Stokes eqn as
C.O.M.O.M.

$$\rho \frac{\partial u_r}{\partial t} + \rho u_r \frac{\partial u_r}{\partial r} = - \frac{\partial P}{\partial r} + \mu \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_r}{\partial r} \right) \quad (1.1)$$

and the continuity eqn will be

$$\rho \frac{1}{r} \frac{\partial (r u_r)}{\partial r} = 0 \quad (1.2)$$

if we consider the following staggered grid



So that integrating eqn (1.2) from the shifted grid $i-\frac{1}{2}$ to $i+\frac{1}{2}$

$$\int_{i-\frac{1}{2}}^{i+\frac{1}{2}} \frac{1}{r} \rho r u_r dA_r = \rho u_{i+\frac{1}{2}} A_{i+\frac{1}{2}} - \rho u_{i-\frac{1}{2}} A_{i-\frac{1}{2}} = 0$$

This give $u_{i+\frac{1}{2}} A_{i+\frac{1}{2}} = u_{i-\frac{1}{2}} A_{i-\frac{1}{2}}$

Q1a) cont'd.

Similarly let's integrate the c.o.mom. of eqn (1.1) with the grid from $i-\frac{1}{2}$ to $i+\frac{1}{2}$ on the LHS and from i to $i+1$ on the RHS. And considering simple explicit scheme for the time discretization, as,

$$\int_V \int_n^{n+1} \rho \frac{\partial u}{\partial t} \Delta t \Delta V + \int_n^{n+1} \int_{i-\frac{1}{2}}^{i+\frac{1}{2}} \rho u r \frac{\partial u}{\partial r} \Delta V = - \int_n^{n+1} \int_i^{i+1} \frac{\partial p}{\partial r} \Delta V + \int_n^{n+1} \int_i^{i+1} u \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u}{\partial r} \right) \Delta V$$

This yields,

$$\begin{aligned} & \left(\rho u_{i+\frac{1}{2}}^{n+1} - \rho u_{i+\frac{1}{2}}^n \right) \Delta V + \left(\rho u_{i+\frac{1}{2}}^2 A_{i+\frac{1}{2}} - \rho u_{i-\frac{1}{2}}^2 A_{i-\frac{1}{2}} \right) \Big|_n \Delta t = \\ & - \left(p_{i+1} - p_i \right) \Big|_{n+1} A_{i+\frac{1}{2}} \Delta t + \frac{u r}{\Delta r} \left(u_{i+\frac{1}{2}+1} - u_{i+\frac{1}{2}} \right) \Big|_t A_{i+1} \Delta t \\ & - \frac{u r}{\Delta r} \left(u_{i+\frac{1}{2}} - u_{i-\frac{1}{2}} \right) \Big|_t A_i \Delta t \end{aligned}$$

simplifying gives, and re-arranging gives.

$$\begin{aligned} p_i^{n+1} = & \frac{\rho}{\Delta t A_{i+\frac{1}{2}}} \left(u_{i+\frac{1}{2}}^{n+1} - u_{i+\frac{1}{2}}^n \right) V_{i+\frac{1}{2}} + \frac{\rho}{A_{i+\frac{1}{2}}} \left(u_{i+\frac{1}{2}}^2 A_{i+\frac{1}{2}} - u_{i-\frac{1}{2}}^2 A_{i-\frac{1}{2}} \right) \\ & - \frac{u A_{i+1}}{\Delta r A_{i+\frac{1}{2}}} \left(u_{i+\frac{1}{2}+1}^n - u_{i+\frac{1}{2}}^n \right) + \frac{u A_i}{\Delta r A_{i+\frac{1}{2}}} \left(u_{i+\frac{1}{2}}^n - u_{i-\frac{1}{2}}^n \right) + p_{i+1}^{n+1} \end{aligned}$$

Q1a) cont'd.

From our above discretization we can put,

$$\text{the shifted c.v., } V_{i+\frac{1}{2}} = A_{i+\frac{1}{2}} \Delta r$$

with shifted cylindrical area/face ~~in the~~ \perp ar to the flow direction, $A_{i+\frac{1}{2}} = 2\pi r_{i+\frac{1}{2}} h$

where the height, $h = 0.5 \text{ m}$

So that
$$V_{i+\frac{1}{2}} = 2\pi r_{i+\frac{1}{2}} h \Delta r$$

Substituting these into our continuity part, we have,

$$\boxed{u_{i+\frac{1}{2}} = \frac{u_{i-\frac{1}{2}} r_{i-\frac{1}{2}}}{r_{i+\frac{1}{2}}}} \quad (1.3)$$

and for the c.o.mom. part, we have,

$$\boxed{P_i^{n+1} = \frac{\rho \Delta r}{\Delta t} (u_{i+\frac{1}{2}}^{n+1} - u_{i+\frac{1}{2}}^n) + \frac{\rho}{r_{i+\frac{1}{2}}} (u_{i+\frac{1}{2}}^2 r_{i+\frac{1}{2}} - u_{i-\frac{1}{2}}^2 r_{i-\frac{1}{2}}) - \frac{\mu r_{i+1}}{r_{i+\frac{1}{2}} \Delta r} (u_{i+\frac{1}{2}+1}^n - u_{i+\frac{1}{2}}^n) + \frac{\mu r_i}{r_{i+\frac{1}{2}} \Delta r} (u_{i+\frac{1}{2}}^n - u_{i-\frac{1}{2}}^n) + P_{i+1}^{n+1}} \quad (1.4)$$

>> Now applying the initial & Boundary conditions, we should start by first solving eqn (1.3),

Q 1a) cont'd.!

by assuming at ^{the first} ~~ghost~~ point $i=1$, the eqn becomes

$$u_{i+\frac{1}{2}} = \frac{u_{in} r_{in}}{r_{i+\frac{1}{2}}}$$

And we are given the Volumetric flow rate,

$$\dot{m}_{in} = u_{in} A_{in} = u_{in} 2\pi r_{in} h = 10^{-5} (e^{2t} - 1)$$

so that

$$u_{in} r_{in} = \frac{\dot{m}}{2\pi h}$$

$$u_{in} = \frac{\dot{m}}{2\pi h r_{in}}$$

This gives us,

$$u_{i+\frac{1}{2}} = \frac{\dot{m}}{2\pi h r_{i+\frac{1}{2}}}$$

Since this is a function of time, we can say that at an initial time, $t=0$, the radial velocity, $u_r^{n=0} = 0$ (i.e. no flow). So that we can increase the time by $t=t+\Delta t$ and calculate u_r^{n+1} , where $\Delta t = 0.01$ sec.

Hence with the calculated velocity vector, we can use eqn (1.4) to calculate the pressure, by starting from the last grid point ($i=n$), since we are given $P_{out} = 101325 \text{ N/m}^2$.

Q1a] cont'd:

And if we assume that P_{out} is independent of time, so that at the last grid point we have,

$$P_n^{n+1} = \frac{\rho \Delta r}{\Delta t} (U_{n+\frac{1}{2}}^{n+1} - U_{n+\frac{1}{2}}^n) + \frac{\rho}{r_{n+\frac{1}{2}}} (U_{n+\frac{1}{2}}^2 r_{n+\frac{1}{2}} - U_{n-\frac{1}{2}}^2 r_{n-\frac{1}{2}}) - \frac{\mu r_{n+1}}{\Delta r r_{n+\frac{1}{2}}} (U_{n+\frac{1}{2}}^n - U_{n+\frac{1}{2}}^n) + \frac{\mu r_n}{\Delta r r_{n+\frac{1}{2}}} (U_{n+\frac{1}{2}}^n - U_{n-\frac{1}{2}}^n) + P_{out}$$

Similarly at the first grid point we will have the velocity terms as,

$$P_1^{n+1} = \frac{\rho \Delta r}{\Delta t} (U_{1+\frac{1}{2}}^{n+1} - U_{1+\frac{1}{2}}^n) + \frac{\rho}{r_{1+\frac{1}{2}}} (U_{1+\frac{1}{2}}^2 r_{1+\frac{1}{2}} - U_{in}^2 r_{in}) - \frac{\mu r_{1+1}}{\Delta r r_{1+\frac{1}{2}}} (U_{1+\frac{1}{2}+1}^n - U_{1+\frac{1}{2}}^n) + \frac{\mu r_1}{\Delta r r_{1+\frac{1}{2}}} (U_{1+\frac{1}{2}}^n - U_{in}^n) + P_{1+1}^{n+1}$$

>> Checking the consistency of units of eqn (1.4), we have

$$\frac{kg}{ms^2} = \frac{kg \cancel{mm}}{m^3 \cancel{s} \cancel{s}} + \frac{kg \cancel{mm}}{m^3 \cancel{s} \cancel{s}} + \frac{kg \cancel{m^2} \cancel{m}}{m^3 \cancel{ms^2}} - \frac{kg \cancel{m^2} \cancel{m}}{m^3 \cancel{ms^2}} - \frac{kg \cancel{mm}}{m \cancel{s} \cancel{ms}} + \frac{kg \cancel{mm}}{m \cancel{s} \cancel{ms}} + \frac{kg \cancel{mm}}{m \cancel{s} \cancel{ms}} - \frac{kg \cancel{mm}}{m \cancel{s} \cancel{ms}} + \frac{kg}{ms^2}$$

$$\text{so that } \frac{kg}{ms^2} = \frac{kg}{ms^2} \text{ true}$$

\therefore our discretized formulation is consistent in its units.
These formulation in boxes are used in our program, using fortran90.

```
!*****Begin Header*****
```

```
!This program was written by Godswill Ezeorah, Student Number: 501012886 on July 07, 2021.
```

```
!This program solves a Navier-Stokes equation using finite volume method
```

```
!and was written as a solution to AE8112 PS4 q1b
```

```
!*****End Header*****
```

```
program Navier_Stokes
```

```
  implicit none
```

```
  DOUBLE PRECISION, DIMENSION(:), ALLOCATABLE :: ri, P, U, Uo
```

```
  DOUBLE PRECISION, PARAMETER :: h=0.5, rin=0.01, rout=0.11, Pout=0, Patm=101325
```

```
  DOUBLE PRECISION, PARAMETER :: rho=1.2, mu=1.84D-5, Pi=4*atan(1.0)
```

```
  DOUBLE PRECISION :: mdot, t, dt, dr, r, rp, rn, aa, ab, ac, ad, u1, uo1
```

```
  DOUBLE PRECISION :: rnh, rph
```

```
  INTEGER :: n, i
```

```
  open(1, file = 'PS4_Q2b_withMu.txt', status = 'unknown')
```

```
  !Variable initialization and definition
```

```
  t=0.01
```

```
  n=100 !Number of control volumes
```

```
  ALLOCATE(ri(n), P(n), U(n), Uo(n))
```

```
  dr = (rout-rin)/n
```

```
  dt = 0.01 !time step
```

```
  Uo = 0
```

```
do while (t <= 1)
```

```
  t = t+dt
```

```
  r=rin
```

```
  mdot = (10D-5)*(exp(2*t)-1)
```

```
do i = 1, n !This loop solves velocity using our continuity formulation
```

```
  rp = r+dr
```

```
  if (i==1) then !for first grid point
```

```
    U(i)=mdot/(2*pi*h*rp)
```

```
  else !for all other grid points
```

```
    U(i)=U(i-1)*r/rp
```

```
  end if
```

```
  ri(i)=r
```

```
  r=r+dr
```

```
end do
```

```
  r=rout
```

```
do i = n, 1, -1 !This loop solves pressure backward using our momentum formulation
```

```
  rn = r-dr
```

```
  rnh = r-dr/2
```

```
  rph = r+dr/2
```

```
  aa = (rho*dr)*(U(i)-Uo(i))/dt
```

```
  ab = rho*(r*Uo(i)**2-rn*Uo(i-1)**2)/r
```

```
  ac = mu*rph*(Uo(i+1)-Uo(i))/(dr*r)
```



```

ad = mu*rn*h*(Uo(i)-Uo(i-1))/(dr*r)
if ( i == n ) then      !for last grid point
    ac = mu*(Uo(i)-Uo(i))/dr
    P(i) = aa+ab-ac+ad+Pout
elseif ( i >= 2 ) then !for all other grid points
    P(i) = aa+ab-ac+ad+P(i+1)
else                    !for first grid point
    u1=(10D-5)*(exp(2*t)-1)/(2*pi*h*rin)
    uo1=(10D-5)*(exp(2*(t-dt))-1)/(2*pi*h*rin)
    aa = (rho*dr)*(U(i)-Uo(i))/dt
    ab = rho*(r*Uo(i)**2-rin*Uo1**2)/r
    ac = mu*rph*(Uo(i+1)-Uo(i))/(dr*r)
    ad = mu*r*(Uo(i)-Uo1)/(dr*r)
    P(i) = aa+ab-ac+ad+P(i+1)
end if
r=r-dr
end do
Uo = U
end do

!Printing results
do i = 1, n
    write(1,*) ri(i), P(i)+Patm
end do
print *, 'Velo. Diff',U(1)-U(n)
print *, 'press. Diff',P(1)-P(n)
write(*,2) 'Radius =', ri
write(*,1) '(Pressure - Patm) =', P
write(*,2) 'Velocity =', U
1 format(a20,100E10.3)
2 format(a11,100f7.3)
close (1)
end program Navier_Stokes

```


Q 2a | I wish to test the grid independence of my previous solution. I will continually double my grid, starting from 8 points, until ~~my~~ a tolerance is reached. This tolerance is set to

$$Tol = 1e^{-4}$$

And the condition for this tolerance to be met is based of L_2 error of Pressure at the first grid point (P_1).

That is

$$\frac{\sqrt{\sum_{N=8}^{N+N} P_1(N)}}{J} < Tol$$

Where J , is the number of consider/summed ~~grid points~~.

P_1 at each consider grid point set, before the tolerance is met.

>> The below code is ran ~~at~~ $t=1$ sec, and at this time the table below is extracted, and used to plot the error as a function of grid points.

From the plot below, I observe that the solution doesn't change that much after 2048 grid points.

∴ Therefore the optimal ^{number of} grid points for this problem is 2048.

```

!*****Begin Header*****
!This program was written by Godswill Ezeorah, Student Number: 501012886 on July 07, 2021.
!This program solves a Navier-Stokes equation using finite volume method
!and was written as a solution to AE8112 PS4 q2
!*****End Header*****

program Navier_Stokes
  implicit none
  DOUBLE PRECISION, DIMENSION(:), ALLOCATABLE :: ri, P, U, Uo, Po
  DOUBLE PRECISION, PARAMETER :: h=0.5, rin=0.01, rout=0.11, Pout=0
  DOUBLE PRECISION, PARAMETER :: rho=1.2, mu=1.84D-5, Pi=4*atan(1.0)
  DOUBLE PRECISION :: mdot, t, dt, dr, r, rp, rn, aa, ab, ac, ad, u1, uo1
  DOUBLE PRECISION :: rph, rnh, L2, Tol
  INTEGER :: n, i, j
  open(1, file = 'PS4_Q2a.txt', status = 'unknown')
  !Variable initialization and definition
  n=8
  L2=1
  Tol=1D-4
  j=1
  !The below loop increases the number of gridpoint until tolerance is met.
  do while (L2>Tol)
    t=0.01
    ALLOCATE(ri(n), P(n), U(n), Uo(n), Po(j))
    dr = (rout-rin)/n
    dt = 0.01 !time step
    Uo = 0
    do while (t <= 1)
      t = t+dt
      r=rin
      mdot = (10D-5)*(exp(2*t)-1)
      do i = 1, n !This loop solves velocity using our continuity formulation
        rp = r+dr
        if (i==1) then !for first grid point
          U(i)=mdot/(2*pi*h*rp)
        else !for all other grid points
          U(i)=U(i-1)*r/rp
        end if
        ri(i)=r
        r=r+dr
      end do
      r=rout
      do i = n, 1, -1 !This loop solves pressure backward using our momentum formulation
        rn = r-dr
        rnh = r-dr/2
        rph = r+dr/2

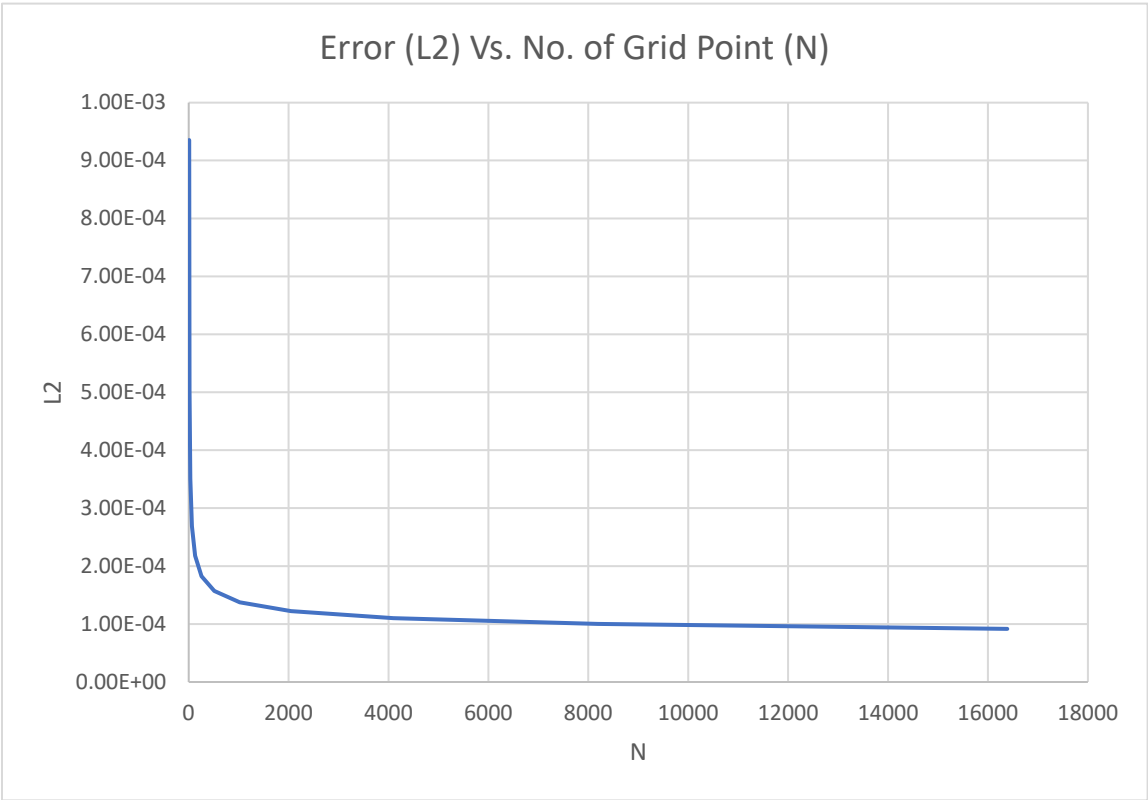
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```

aa = (rho*dr)*(U(i)-Uo(i))/dt
ab = rho*(r*Uo(i)**2-rn*Uo(i-1)**2)/r
ac = mu*rph*(Uo(i+1)-Uo(i))/(dr*r)
ad = mu*rnh*(Uo(i)-Uo(i-1))/(dr*r)
if ( i == n ) then !for last grid point
    ac = mu*(Uo(i)-Uo(i))/dr
    P(i) = aa+ab-ac+ad+Pout
elseif ( i >= 2 ) then !for all other grid points
    P(i) = aa+ab-ac+ad+P(i+1)
else !for first grid point
    u1=(10D-5)*(exp(2*t)-1)/(2*pi*h*rin)
    uo1=(10D-5)*(exp(2*(t-dt))-1)/(2*pi*h*rin)
    aa = (rho*dr)*(U(i)-Uo(i))/dt
    ab = rho*(r*Uo(i)**2-rin*Uo1**2)/r
    ac = mu*rph*(Uo(i+1)-Uo(i))/(dr*r)
    ad = mu*r*(Uo(i)-Uo1)/(dr*r)
    P(i) = aa+ab-ac+ad+P(i+1)
end if
r=r-dr
end do
Uo = U
end do
Po(j)=P(1)
L2=norm2(Po)/j
print *, 'No. of gridpoints.',n
print *, 'L2 Error',L2
write(1,*) n, L2
if ( L2>Tol ) then
    DEALLOCATE(ri, P, U, Uo, Po)
    n=n+n
    j=j+1
end if
end do
close (1)
end program Navier_Stokes

```


No. of Grid Point (N)	Error (L2)
8	9.35E-04
16	5.05E-04
32	3.51E-04
64	2.69E-04
128	2.18E-04
256	1.83E-04
512	1.57E-04
1024	1.38E-04
2048	1.22E-04
4096	1.10E-04
8192	1.00E-04
16384	9.18E-05



Q 2 b | cont'd.!

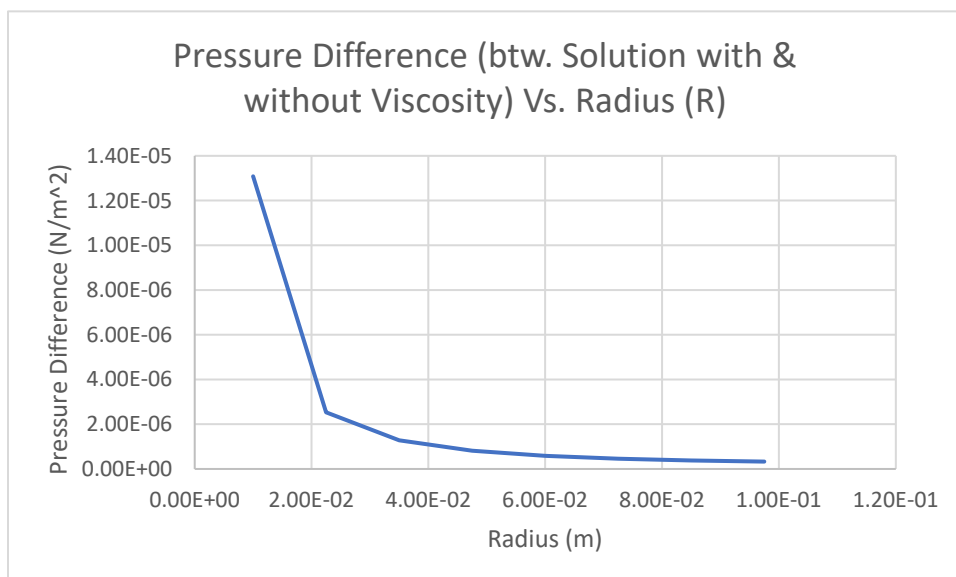
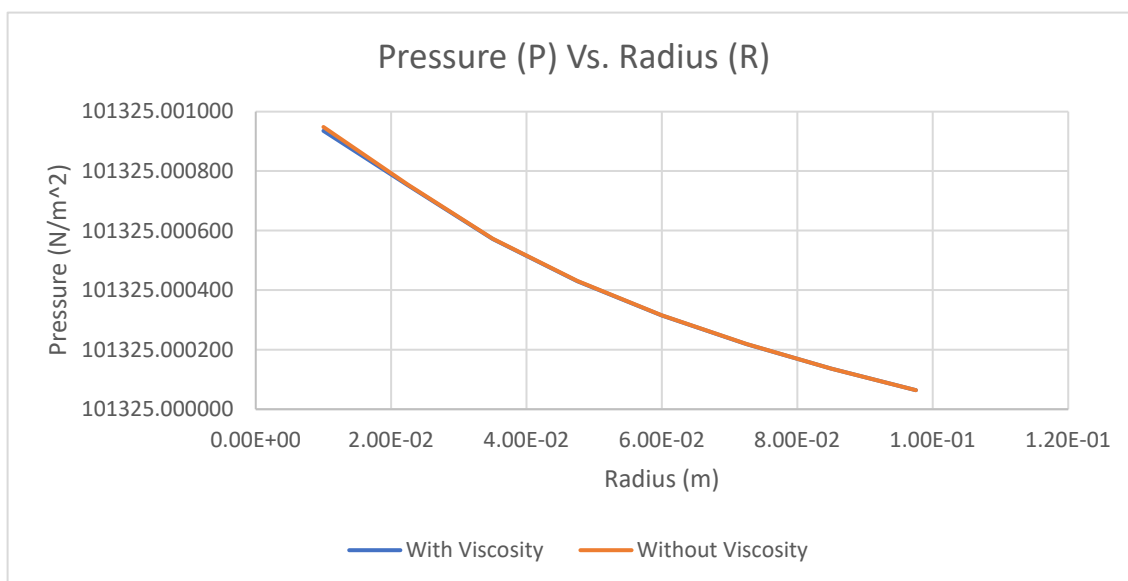
In addition, I also considered the effect of neglecting the Viscous term, to our solution.

From table below, we can see that the pressure solution without viscosity is ~~very~~ has a very very small increase from the solution with viscosity, ~~these~~

This is true as can be observed from the Navier-Stokes eqn (c.o.mom.). But the increase is very negligible, especially ~~to~~ towards the outer radius, as observed from the pressure difference (between with & without viscosity) plot below, as a function of radius for 8 gridpoint.

∴ Therefore from the observation of the solution plots between → with & without viscosity, we can say that viscosity has negligible effect on our solution.

With Viscosity		Without Viscosity	
Radius(m)	Pressure (N/m ²)	Radius (m)	Pressure (N/m ²)
1.00E-02	101325.000935	1.00E-02	101325.000948
2.25E-02	101325.000752	2.25E-02	101325.000754
3.50E-02	101325.000572	3.50E-02	101325.000573
4.75E-02	101325.000430	4.75E-02	101325.000431
6.00E-02	101325.000315	6.00E-02	101325.000316
7.25E-02	101325.000219	7.25E-02	101325.000219
8.50E-02	101325.000136	8.50E-02	101325.000137
9.75E-02	101325.000064	9.75E-02	101325.000064



Q2c Finally I also consider solving problem 1, using finite difference method, described below; we have our c.o.mom eqn as (from eqn (1.1)),

$$\rho \frac{\partial u_r}{\partial t} + \rho u_r \frac{\partial u_r}{\partial r} = - \frac{\partial p}{\partial r} + \mu \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_r}{\partial r} \right)$$

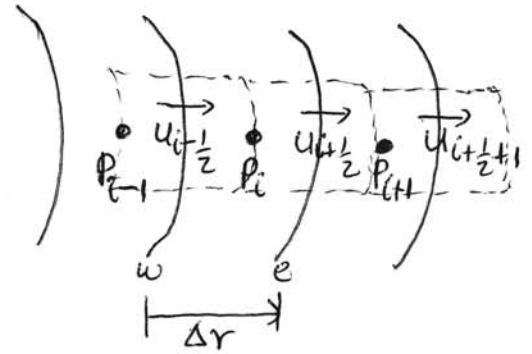
and the continuity eqn as, (from eqn (1.2)),

$$\rho \frac{1}{r} \left(\frac{\partial (r u_r)}{\partial r} \right) = 0$$

We know that from Taylor series expansion, we have the first and second order derivative for equispaced staggered grid (assuming from $u_{i+\frac{1}{2}}$ to $u_{i+\frac{1}{2}}$), we have

$$\frac{\partial u_r}{\partial r} = \frac{u_{i+\frac{1}{2}} - u_{i-\frac{1}{2}}}{2\Delta r}$$

and
$$\frac{\partial^2 u_r}{\partial r^2} = \frac{u_{i-\frac{1}{2}} - 2u_i + u_{i+\frac{1}{2}}}{\Delta r^2}$$



Applying the derivative product rule to the continuity, we have,

$$\rho \frac{1}{r} \frac{\partial r}{\partial r} u_r + \rho \frac{1}{r} r \frac{\partial u_r}{\partial r}$$

and applying the Taylor series derived eqn, we have,

Q2c | cont'd.

$$\frac{\rho u_i}{r_i} + \frac{\rho}{2\Delta r} \left(u_{i+\frac{1}{2}} - u_{i-\frac{1}{2}} \right) = 0$$

let $u_i = \frac{u_{i+\frac{1}{2}} + u_{i-\frac{1}{2}}}{2}$ assuming linear profile for our velocity, we get

$$\frac{\rho}{2r_i} u_{i+\frac{1}{2}} + \frac{\rho}{2r_i} u_{i-\frac{1}{2}} + \frac{\rho}{2\Delta r} u_{i+\frac{1}{2}} - \frac{\rho}{2\Delta r} u_{i-\frac{1}{2}} = 0$$

multiplying by $\frac{2}{\rho}$, we get (and re-arranging)

$$u_{i+\frac{1}{2}} = \frac{u_{i-\frac{1}{2}} \left(\frac{1}{\Delta r} - \frac{1}{r_i} \right)}{\left(\frac{1}{r_i} + \frac{1}{\Delta r} \right)}$$

Now apply the derivative product rule to our momentum eqn, we have

$$\rho \frac{\partial u_r}{\partial t} + \rho u_r \frac{\partial u_r}{\partial r} = - \frac{\partial P}{\partial r} + \frac{\mu}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_r}{\partial r} \right) + \frac{\mu}{r} r \frac{\partial^2 u_r}{\partial r^2}$$

we have

$$\rho \frac{\partial u_r}{\partial t} + \rho u_r \frac{\partial u_r}{\partial r} = - \frac{\partial P}{\partial r} + \frac{\mu}{r} \frac{\partial u_r}{\partial r} + \mu \frac{\partial^2 u_r}{\partial r^2}$$

now lets apply the standard forward diff,

$$\frac{\partial u_r}{\partial t} = \frac{u_i^{n+1} - u_i^n}{\Delta t}$$

and the Tylor series derived eqn, we have,

Q2c Cont'd.!

$$\frac{p}{\Delta t} (u_i^{n+1} - u_i^n) + \frac{p u_i}{2 \Delta r} (u_{i+\frac{1}{2}} - u_{i-\frac{1}{2}}) = - \left(\frac{p_{i+1} - p_i}{2 \Delta r} \right) + \frac{\mu}{2 r_i \Delta r} (u_{i+\frac{1}{2}} - u_{i-\frac{1}{2}}) + \frac{\mu}{\Delta r^2} (u_{i-\frac{1}{2}} - 2u_i + u_{i+\frac{1}{2}})$$

multiplying by $2 \Delta r$ and re-arranging, we get, (assuming explicit time discretization).

$$p_i^{n+1} = \frac{2 \Delta r p}{\Delta t} (u_i^{n+1} - u_i^n) + p_i^n (u_{i+\frac{1}{2}}^n - u_{i-\frac{1}{2}}^n) - \frac{\mu}{r_i} (u_{i+\frac{1}{2}}^n - u_{i-\frac{1}{2}}^n) - \frac{2 \mu}{\Delta r} (u_{i-\frac{1}{2}}^n - 2u_i^n + u_{i+\frac{1}{2}}^n) + p_{i+1}^{n+1}$$


>> Applying B.C.s for the first grid point ($i=1$) to the continuity formulation, we have

$$u_{i+\frac{1}{2}} = \frac{u_{in} \left(\frac{1}{\Delta r} - \frac{1}{r_i} \right)}{\left(\frac{1}{r_i} + \frac{1}{\Delta r} \right)}$$

and we know $u_{in} = \frac{\dot{m}}{2 \pi h r_0}$

so that we have

$$u_{i+\frac{1}{2}} = \frac{\dot{m} \left(\frac{1}{\Delta r} - \frac{1}{r_i} \right)}{2 \pi h r_0 \left(\frac{1}{r_i} + \frac{1}{\Delta r} \right)}$$

at some ghost point


>> And for the momentum formulation we have that at the last grid point ($i=n$)

Q2C | cont'd.

$$P_n^{n+1} = \frac{2\Delta r \rho}{\Delta t} (u_n^{n+1} - u_n^n) + \rho u_n^n (u_{n+\frac{1}{2}}^n - u_{n-\frac{1}{2}}^n) - \frac{\mu}{r_n} (u_{n+\frac{1}{2}}^n - u_{n-\frac{1}{2}}^n) \\ - \frac{2\mu}{\Delta r} (u_{n+\frac{1}{2}}^n - 2u_n^n + u_{n-\frac{1}{2}}^n) + P_{out}^{n+1}$$

also at the first grid point ($i=1$) we will have the velocity terms as

$$P_1^{n+1} = \frac{2\Delta r \rho}{\Delta t} (u_1^{n+1} - u_1^n) + \rho u_1^n (u_{1+\frac{1}{2}}^n - u_{in}^n) - \frac{\mu}{r_1} (u_{1+\frac{1}{2}}^n - u_{in}^n) \\ - \frac{2\mu}{\Delta r} (u_{in}^n - 2u_1^n + u_{1+\frac{1}{2}}^n) + P_{1+1}^{n+1}$$

These eqns in boxes are used in our fortran90 code and the results is shown below;

>> From the below plot comparison between the solution gotten using finite volume and finite difference method, one can hypothetically guess that finite ^{difference} ~~volume~~ method is more suited for this problem. But this needs further verification using an ~~exact~~ analytical solution, and comparing the error norms between the two methods.

```

!*****Begin Header*****
!This program was written by Godswill Ezeorah, Student Number: 501012886 on July 07, 2021.
!This program solves a Navier-Stokes equation using finite difference method
!and was written as a solution to AE8112 PS4 q2
!*****End Header*****

program Navier_Stokes
    implicit none
    DOUBLE PRECISION, DIMENSION(:), ALLOCATABLE :: ri, P, U, Uo
    DOUBLE PRECISION, PARAMETER :: h=0.5, rin=0.01, rout=0.11, Pout=0, Patm=101325
    DOUBLE PRECISION, PARAMETER :: rho=1.2, mu=1.84D-5, Pi=4*atan(1.0)
    DOUBLE PRECISION :: mdot, t, dt, dr, r, rp, rn, aa, ab, ac, ad, u1, uo1
    DOUBLE PRECISION :: rh
    INTEGER :: n, i
    open(1, file = 'PS4_Q2c_withMu.txt', status = 'unknown')
    !Variable initialization and definition
    t=0.01
    n=100 !Number of control volumes
    ALLOCATE(ri(n), P(n), U(n), Uo(n))
    dr = (rout-rin)/n
    dt = 0.01 !time step
    Uo = 0

    do while (t <= 1)
        t = t+dt
        r=rin
        mdot = (10D-5)*(exp(2*t)-1)
        do i = 1, n !This loop solves velocity using our Continuity formulation
            rp = r+dr
            rh = r+dr/2
            if (i==1) then !for first grid point
                U(i)=mdot*(1/dr-1/rh)/((2*pi*h*(rin-dr/2))*(1/rh+1/dr))
            else !for all other grid points
                U(i)=U(i-1)*(1/dr-1/rh)/(1/rh+1/dr)
            end if
            ri(i)=r
            r=r+dr
        end do
        r=rout
        do i = n, 1, -1 !This loop solves pressure backward using our momentum formulation
            rn = r-dr
            rh = r-dr/2
            aa = (2*rho*dr)*((U(i)+U(i-1))/2-(Uo(i)+Uo(i-1))/2)/dt
            ab = rho*((Uo(i)+Uo(i-1))/2)*(Uo(i)-Uo(i-1))
            ac = mu*(Uo(i)/r-Uo(i-1)/rn)

```

```

ad = 2*mu*(Uo(i-1)-(Uo(i)+Uo(i-1))+Uo(i))/dr
if ( i == n ) then      !for last grid point
    P(i) = aa+ab-ac-ad+Pout
elseif ( i >= 2 ) then !for all other grid points
    P(i) = aa+ab-ac-ad+P(i+1)
else                    !for first grid point
    u1=(10D-5)*(exp(2*t)-1)*(2*pi*h*(rin-dr/2))
    uo1=(10D-5)*(exp(2*(t-dt))-1)*(2*pi*h*(rin-dr/2))
    aa = (2*rho*dr)*((U(i)+U1)/2-(Uo(i)+Uo1)/2)/dt
    ab = rho*((Uo(i)+Uo1)/2)*(Uo(i)-Uo1)
    ac = mu*(Uo(i)-Uo1)/rh
    ad = 2*mu*(Uo1-(Uo(i)+Uo1)+Uo(i))/dr
    P(i) = aa+ab-ac-ad+P(i+1)
end if
r=r-dr
end do
Uo = U
end do

!Printing results
do i = 1, n
    write(1,*) ri(i), P(i)+Patm
end do
print *, 'Velo. Diff',U(1)-U(n)
print *, 'press. Diff',P(1)-P(n)
write(*,2) 'Radius =', ri
write(*,1) '(Pressure - Patm) =', P
write(*,2) 'Velocity =', U
1 format(a20,100E10.3)
2 format(a11,100f7.3)
close (1)
end program Navier_Stokes

```

(Pressure - Patm) = 0.103E-02 0.824E-03 0.781E-03 0.735E-03 0.690E-03 0.648E-03 0.608E-03 0.571E-03 0.537E-03 0.506E-03 0.478E-03 0.452E-03 0.428E-03 0.405E-03 0.385E-03 0.366E-03 0.348E-03 0.332E-03 0.316E-03 0.302E-03 0.288E-03 0.276E-03 0.264E-03 0.253E-03 0.242E-03 0.232E-03 0.223E-03 0.214E-03 0.206E-03 0.198E-03 0.190E-03 0.183E-03 0.176E-03 0.169E-03 0.163E-03 0.157E-03 0.151E-03 0.146E-03 0.140E-03 0.135E-03 0.131E-03 0.126E-03 0.121E-03 0.117E-03 0.113E-03 0.109E-03 0.105E-03 0.101E-03 0.976E-04 0.941E-04 0.907E-04 0.874E-04 0.842E-04 0.812E-04 0.782E-04 0.753E-04 0.726E-04 0.699E-04 0.672E-04 0.647E-04 0.622E-04 0.598E-04 0.574E-04 0.552E-04 0.530E-04 0.508E-04 0.487E-04 0.467E-04 0.447E-04 0.427E-04 0.408E-04 0.390E-04 0.372E-04 0.354E-04 0.337E-04 0.320E-04 0.304E-04 0.288E-04 0.272E-04 0.257E-04 0.242E-04 0.227E-04 0.213E-04 0.199E-04 0.185E-04 0.172E-04 0.159E-04 0.146E-04 0.133E-04 0.121E-04 0.109E-04 0.970E-05 0.854E-05 0.740E-05 0.628E-05 0.518E-05 0.411E-05 0.305E-05 0.202E-05 0.999E-06

Comparison of Finite Volume and Finite Difference Method

