# APPENDIX A

# THE DELTA-SIGMA TOOLBOX

#### **Getting Started**

Go to http://www.mathworks.com/matlabcentral/fileexchange/ and search for delsig. Download and install the delsig.zip file. Add the delsig directory to the MATLAB path. To improve simulation speed, compile the simulateDSM.c file by typing mex simulateDSM.c at the MATLAB prompt. Do the same for simulateMS.c.

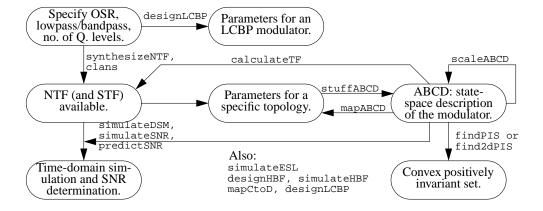
The Delta-Sigma Toolbox requires the Signal Processing Toolbox and the Control Systems Toolbox; the clans and designPBF functions also require the Optimization Toolbox.

The following conventions are used throughout the Delta-Sigma Toolbox:

- Frequencies are normalized; f = 1 corresponds to the sampling frequency,  $f_s$ .
- Default values for function arguments are shown following an equals sign in the parameter list. To use the default value for an argument, omit the argument if it is at the end of the list, otherwise use NaN (not-a-number) or [] (the empty matrix) as a place-holder.
- The loop filter of a general delta-sigma modulator is described with an *ABCD* matrix. See "Modulator Model Details" on page 35 for a description of this matrix.

# **Demonstrations and Examples**

dsdemo1	Demonstration of the synthesizeNTF function. Noise transfer function syn-
	thesis for a 5 <sup>th</sup> -order lowpass modulator, both with and without optimized
	zeros, plus an 8 <sup>th</sup> -order bandpass modulator with optimized zeros.
dsdemo2	Demonstration of the simulateDSM, predictSNR and simulateSNR func-
	tions: time-domain simulation, SNR prediction using the describing function
	method of Ardalan and Paulos, spectral analysis and signal-to-noise ratio cal-
	culation. Lowpass, bandpass, multi-bit lowpass examples are given.
dsdemo3	Demonstration of the realizeNTF, stuffABCD, scaleABCD and mapABCD
	functions: coefficient calculation and dynamic range scaling.
dsdemo4	Audio demonstration of MOD1 and MOD2 with sinc <sup>n</sup> decimation.
dsdemo5	Demonstration of the simulateMS function: simulation of the element se-
	lection logic of a mismatch-shaping DAC.
dsdemo6	Demonstration of the designHBF function. Hardware-efficient halfband fil-
	ter design and simulation.
dsdemo7	Demonstration of the findPIS function: positively-invariant set computa-
	tion.
dsexample1	Discrete-time modulator design example.
dsexample2	Continuous-time lowpass modulator design example.



**Figure A.1** Flowchart of key  $\Delta\Sigma$  Toolbox functions.

#### **Key Functions**

```
ntf = synthesizeNTF(order=3,R=64,opt=0,H_inf=1.5,f0=0)
                                                                           page 7
ntf = class(order=4, R=64, Q=5, rmax=0.95, opt=0)
                                                                           page 8
ntf = synthesizeChebyshevNTF (order=3, R=64, opt=0, H_inf=1.5, f0=0) page 9
Synthesize a noise transfer function.
[v, xn, xmax, y] = simulateDSM(u, ABCD, nlev=2, x0=0)
                                                                          page 10
[v, xn, xmax, y] = simulateDSM(u, ntf, nlev=2, x0=0)
Simulate a delta-sigma modulator with a given input.
[snr,amp] = simulateSNR(ntf,OSR,amp=...,
                            f0=0, nlev=2, f=1/(4*R), k=13)
                                                                          page 11
Determine the SNR vs. input amplitude curve by simulation.
[a,g,b,c] = realizeNTF(ntf,form='CRFB',stf=1)
                                                                          page 12
Convert a noise transfer function into coefficients for the specified topology.
ABCD = stuffABCD(a,g,b,c,form='CRFB')
                                                                          page 13
Calculate the ABCD matrix given the parameters of the specified topology.
[a,q,b,c] = mapABCD (ABCD, form='CRFB')
                                                                          page 13
Convert the ABCD matrix into the parameters of the specified topology.
[ABCDs, umax] = scaleABCD(ABCD, nlev=2, f=0, xlim=1, ymax=nlev+2)
                                                                          page 14
Perform dynamic range scaling on a delta-sigma modulator described by ABCD.
[ntf,stf] = calculateTF(ABCD,k=1)
                                                                          page 15
Calculate the NTF and STF of a delta-sigma modulator described by the given
ABCD matrix, assuming a quantizer gain of k.
[sv,sx,sigma_se,max_sx,max_sy] =
    simulateMSv, mtf, M=16, d=0, dw=[1-], sx0=[0-])
                                                                          page 16
Simulate the element-selection logic of a mismatch-shaping DAC.
```

#### **Functions for Continuous-Time Systems**

```
[ABCDc,tdac2]= realizeNTF_ct(ntf,form='FB',tdac,ordering=[1:n], bp=zeros(-),ABCDc) page 18
```

Realize an NTF with a continuous-time loop filter.

```
[sys, Gp] = mapCtoD(sys_c,t=[0 1],f0=0) page 19
```

Map a continuous-time system to a discrete-time system whose impulse response matches the sampled pulse response of the original continuous-time system. See dsexample2.

```
H = \text{evalTFP}(Hs, Hz, f) page 20
```

Compute the value of the product of the continuous-time transfer function  $H_s$  and the discrete-time transfer function  $H_z$  at frequencies f. Use this function to evaluate the signal transfer function of a CT  $\Delta\Sigma$  ADC system.

#### **Functions for Quadrature Systems**

```
ntf = synthesizeQNTF(order=3,OSR=64,f0=0,NG=-60,ING=-20) page 21 Synthesize a noise transfer function for a quadrature delta-sigma modulator.
```

$$[v, xn, xmax, y] = simulateQDSM(u, ABCD|ntf, nlev=2, x0=0)$$
 page 22 Simulate a quadrature delta-sigma modulator with the given input.

Convert a quadrature noise transfer function into a complex ABCD matrix for the specified structure.

Calculate the noise and signal transfer functions of a quadrature modulator.

```
[sv,sx,sigma_se,max_sx,max_sy]=
    simulateQESL(v,mtf,M=16,sx0=[0-])
page 26
```

Simulate the Element Selection Logic of a quadrature differential DAC.

Note: simulateSNR works for a quadrature modulator if given a complex NTF or ABCD matrix; simulateDSM can also be used for a quadrature modulator if given an ABCDr matrix and a 2-element nlev vector.

# **Specialty Functions**

[f1, f2, info] = designHBF (fp=0.2, delta=1e-5, debug=0) Design a Saramäki half-band filter for use in a decimation or interpolation filter.	page 27
y = simulateHBF(x, f1, f2, mode=0) Simulate a Saramäki half-band filter in the time domain.	page 29
[C, e, x0] = designPBF (N, M, pb, pbr, sbr, ncd, np, ns, fmax) Design a symmetric polynomial-based filter (PBF) according to Hunter's method.	page 30
[snr,amp,k0,k1,sigma_e2 = predictSNR(ntf,OSR=64,amp=,f0=0) Predict the SNR vs. input amplitude curve using the describing function method.	page 31
<pre>[s,e,n,o,Sc] = findPIS(u,ABCD,nlev=2,options) Find a convex positively-invariant set for a delta-sigma modulator.</pre>	page 32
[data, snr] = findPattern(N=1024,OSR=64,ntf,ftest,Atest, f0=0,nlev=2,quadrature=0,dbg=0)  Create a length-N data record which has good spectral properties when repeated.	page 34

#### **Utility Funtions**

# **Delta-Sigma Utility**

```
mod1, mod2
```

Set the ABCD matrix, NTF and STF of the standard 1st- and 2nd-order modulators.

```
snr = calculateSNR(hwfft,f,nsig=1)
```

Estimate the SNR given the in-band bins of a windowed FFT and the location of the input.

```
[A B C D] = partitionABCD(ABCD, m)
```

Partition ABCD into A, B, C, D for an *m*-input state-space system.

```
H_{inf} = infnorm(H)
```

Compute the infinity norm (maximum absolute value) of a z-domain transfer function.

```
y = impL1(ntf, n=10)
```

Compute n points of the impulse response from the comparator output back to the comparator input for the given NTF.

```
y = pulse(S, tp=[0 1], dt=1, tfinal=10, nosum=0)
```

Compute the sampled pulse response of a continuous-time system.

```
sigma_H = rmsGain(H, f1, f2)
```

Compute the root mean-square gain of the discrete-time transfer function H in the frequency band  $[f_1, f_2]$ .

# **General Utility**

```
dbv(), dbp(), undbv(), undbp(), dbm(), undbm()
```

The dB equivalent of voltage/power quantities, and their inverse functions.

```
window = ds_hann(N)
```

A Hann window of length N. Unlike MATLAB's original hanning function, ds\_hann does not smear tones which are located exactly in an FFT bin (i.e. tones having an integral number of cycles in the given block of data). MATLAB 6's hanning (N, 'periodic') function and MATLAB 7's hann (N, 'periodic') function are the same as ds\_hann (N).

```
mag = zinc(f, n=64, m=1)
```

Calculate the magnitude response of a cascade of m sinc<sub>n</sub> filters at frequencies f.

# **Graphing Utility**

```
plotPZ(H,color='b',markersize=5,list=0)
```

Plot the poles and zeros of a transfer function.

```
plotSpectrum(X, fin, fmt)
```

Plot a smoothed spectrum.

```
figureMagic(xRange, dx, xLab, yRange, dy, yLab, size)
```

Performs a number of formatting operations for the current figure, including axis limits, ticks and labelling.

```
printmif(file, size, font, fig)
```

Print a figure to an Adobe Illustrator file and then use ai2mif to convert it to FrameMaker MIF format. ai2mif is an improved version of the function of the same name originally written by Deron Jackson <djackson@mit.edu>.

```
[f,p] = logsmooth(X,inBin,nbin)
```

Smooth the FFT X, and convert it to dB. See also bplogsmooth and bilogplot.

# synthesizeNTF

**Synopsis:** ntf = synthesizeNTF (order=3, OSR=64, opt=0, H\_inf=1.5, f0=0) Synthesize a noise transfer function (NTF) for a delta-sigma modulator.

Input	
order	The order of the NTF. order must be even for bandpass modulators.
OSR	The oversampling ratio. OSR is only needed when optimized NTF zeros
	are requested.
opt	A flag used to request optimized NTF zeros.
	opt=0 puts all NTF zeros at band-center.
	opt=1 optimizes the NTF zeros according to the high-OSR limit.
	opt=2 puts at least one zero at band-center, but optimizes the rest.
	opt=3 uses the Optimization Toolbox to optimize the zeros.
H_inf	The maximum out-of-band gain of the NTF. Lee's rule states that
	H_inf<2 should yield a stable modulator with a binary quantizer. Reduc-
	ing H_inf increases the likelihood of success, but reduces the attenuation
	provided by the NTF and thus the theoretical resolution of the modulator.
f0	The center frequency of the modulator. $f_0 \neq 0$ yields a bandpass modu-
	lator; £0=0.25 puts the center frequency at $f_s/4$ .

#### Output

ntf The modulator NTF, given as an LTI object in zero-pole form.

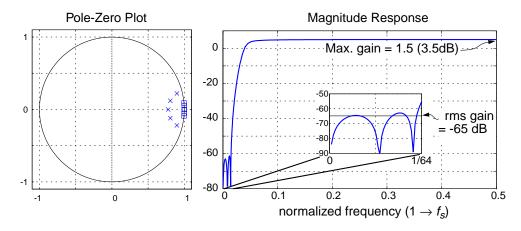
# Bugs

If OSR or H\_inf are low, the NTF is not optimal. Use synthesizeChebyshevNTF instead.

#### Example

Fifth-order lowpass modulator; zeros optimized for an oversampling ratio of 32.

```
>> H = synthesizeNTF(5,32,1) 
Zero/pole/gain: (z-1) (z^2 - 1.997z + 1) (z^2 - 1.992z + 1) (z-0.7778) (z^2 - 1.613z + 0.6649) (z^2 - 1.796z + 0.8549) 
Sampling time: 1
```



# clans

**Synopsis:** ntf = clans (order=4, OSR=64, Q=5, rmax=0.95, opt=0) Synthesize a lowpass NTF using the CLANS (Closed-loop analysis of noise-shaper) methodology [1]. This function requires the Optimization Toolbox.

[1] J. G. Kenney and L. R. Carley, "Design of multibit noise-shaping data converters," *Analog Integrated Circuits Signal Processing Journal*, vol. 3, pp. 259-272, 1993.

#### Input

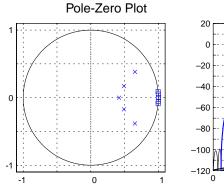
ութաւ	
order	The order of the NTF.
OSR	The oversampling ratio.
Q	The maximum number of quantization levels used by the fed-back quan-
	tization noise. (Mathematically, $Q =   h  _1 - 1$ , i.e. the sum of the ab-
	solute values of the impulse response samples minus 1.) The maximum
	stable input of a $\Delta\Sigma$ modulator is guaranteed to be at least $(n_{lev} - Q)$ .
rmax	The maximum radius for the NTF poles.
opt	A flag used to request optimized NTF zeros.

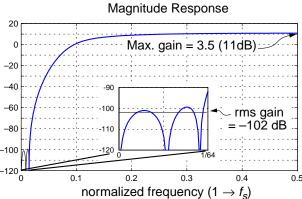
#### Output

ntf The modulator NTF, given as an LTI object in zero-pole form.

#### Example

 $5^{th}$ -order lowpass modulator; time-domain noise gain of 5, zeros optimized for OSR = 32. >> H= clans (5, 32, 5, .95, 1)





# synthesize Chebyshev NTF

**Synopsis:** ntf = synthesizeChebyshevNTF (order, OSR, opt, H\_inf, f0) Obtain a noise transfer function (NTF) in which has equiripple magnitude in the passband. synthesizeChebyshevNTF creates NTFs which are no better than synthesizeNTF, except when OSR or H\_inf are low.

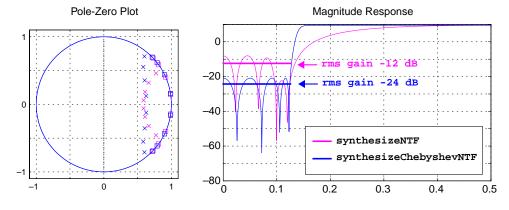
#### **Input and Output**

Same as ssynthesizeNTF, except that the opt argument is not supported yet.

#### **Examples**

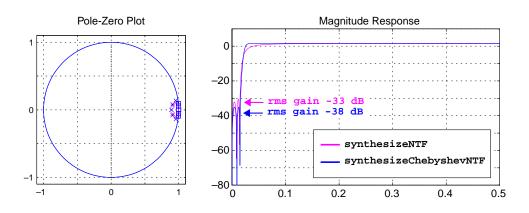
Compare the NTFs created by synthesizeNTF and synthesizeChebyshevNTF when OSR is low:

```
>> OSR = 4; order = 8; H_inf = 3;
>> H1 = synthesizeNTF(order,OSR,1,H_inf);
>> H3 = synthesizeChebyshevNTF(order,OSR,1,H_inf);
```



#### Repeat for H\_inf low:

```
>> OSR = 32; order = 5; H_inf = 1.2;
>> H1 = synthesizeNTF(order,OSR,1,H_inf);
>> H3 = synthesizeChebyshevNTF(order,OSR,1,H_inf);
```



# simulateDSM

Synopsis: [v, xn, xmax, y] = simulateDSM(u, ABCD|ntf, nlev=2, x0=0) Simulate a delta-sigma modulator with a given input. For maximum speed, make sure that the compiled mex file is on your search path by typing which simulateDSM at the MATLAB<sup>TM</sup> prompt.

#### Input

u	The input sequence to the modulator, given as a $m \times N$ matrix, where $m$
	is the number of inputs (usually 1). Note that full-scale corresponds to
	an input of magnitude nlev-1.
ABCD	A state-space description of the modulator loop filter.
ntf	The modulator NTF, given in zero-pole form. The modulator STF is
	assumed to be unity.
nlev	The number of levels in the quantizer. Multiple quantizers are indicated
	by making nlev a column vector.
x0	The initial state of the modulator.

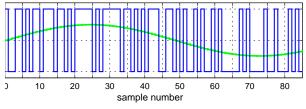
#### Output

Gutput	
V	The samples of the output of the modulator, one for each input sample.
xn	The internal states of the modulator, one for each input sample, given as
	an $n \times N$ matrix.
xmax	The maximum absolute values of each state variable.
У	The samples of the quantizer input, one per input sample.

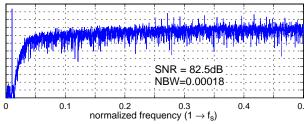
#### **Example**

Simulate a 5<sup>th</sup>-order binary lowpass modulator with a half-scale sine-wave input and plot its output in the time and frequency domains.

```
>> OSR = 32; H = synthesizeNTF(5,OSR,1)}
>> N = 8192; fB = ceil(N/(2*OSR));}
>> f=85; u = 0.5*sin(2*pi*f/N*[0:N-1]);}
>> v = simulateDSM(u,H);
```



```
t = 0:85;
stairs(t, u(t+1),'g');
hold on;
stairs(t,v(t+1),'b');
axis([0 85 -1.2 1.2]);
ylabel('u, v');
```



# **simulateSNR**

Simulate a delta-sigma modulator with sine wave inputs of various amplitudes and calculate the signal-to-noise ratio (SNR) in dB for each input.

#### Input

g, given in zero-pole form.
iption of the modulator loop filter, or the name of a
input signal as its sole argument.
atio.
g the amplitudes to use. Defaults to [-120 -11020
dB, where 0 dB means a full-scale (peak value =
e.
y of the modulator.
ls in the quantizer. Multiple quantizers are indicated
vector.
adjusted to be an FFT bin.
points used for the FFT is $2^k$ .
at the system being simulated is quadrature. This flag
if either ntf or ABCD are complex.
Is in the quantizer. Multiple quantizers are indicated elector.  Adjusted to be an FFT bin.  A points used for the FFT is 2 <sup>k</sup> .  At the system being simulated is quadrature. This flat

#### Output

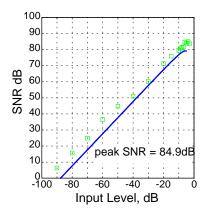
A row vector containing the SNR values calculated from the simulations.

A row vector listing the amplitudes used.

### Example

Compare the SNR vs. input amplitude curve determined by the describing function method of Ardalan and Paulos with that determined by simulation for a 5<sup>th</sup>-order modulator.

```
>> OSR = 32; H = synthesizeNTF(5,OSR,1)
>> [snr_pred,amp] = predictSNR(H,OSR);
>> [snr,amp] = simulateSNR(H,OSR);
```



```
plot(amp,snr_pred,'b',amp,snr,'gs');
grid on;
figureMagic([-100 0], 10, 2, ...
    [0 100], 10, 1);
xlabel('Input Level, dB');
ylabel('SNR dB');
s=sprintf('peak SNR = %4.1fdB\n',...
    max(snr));
text(-65,15,s);
```

# realizeNTF

**Synopsis:** [a,g,b,c] = realizeNTF (ntf,form='CRFB',stf=1) Convert an NTF into a set of coefficients for a particular modulator topology.

#### Input

ութաւ	
ntf	The modulator NTF, given in zero-pole form (i.e. a zpk object).
form	A string specifying the modulator topology.
	CRFB Cascade-of-resonators, feedback form.
	CRFF Cascade-of-resonators, feedforward form.
	CIFB Cascade-of-integrators, feedback form.
	CIFF Cascade-of-integrators, feedforward form.
	D Any of the above, but the quantizer is delaying.
	Structures are described in "Modulator Model Details" on page 35.
stf	The modulator STF, specified as a zpk object. Note that the poles of the
	STF must match those of the NTF in order to guarantee that the STF can
	be realized without the addition of extra state variables.

#### Output

Juipui	
a	Feedback/feedforward coefficients from/to the quantizer $(1 \times n)$ .
g	Resonator coefficients $(1 \times \lfloor n/2 \rfloor)$ .
b	Feed-in coefficients from the modulator input to each integrator
	$(1\times(n+1))$ .
С	Integrator inter-stage coefficients. $(1 \times n)$ . In unscaled modulators, c is
	all ones.

#### Example

Determine the coefficients for a 5<sup>th</sup>-order modulator with the cascade-of-resonators structure, feedback (CRFB) form.

# See Also

Use realizeNTF\_ct (page 18) to realize an NTF with a continuous-time loop filter.

# **stuffABCD**

Synopsis: ABCD = stuffABCD(a,g,b,c,form='CRFB')

Calculate the ABCD matrix given the parameters of a specified modulator topology.

#### Input

a	Feedback/feedforward coefficients from/to the quantizer.
g	Resonator coefficients.

b Feed-in coefficients from the modulator input to each integrator.

c Integrator inter-stage coefficients.

form See realizeNTF on page 12 for a list of supported forms and "Sup-

ported Modulator Topologies" on page 36 for block diagrams of them.

#### Output

ABCD A state-space description of the loop filter.

# mapABCD

**Synopsis:** [a,g,b,c] = mapABCD (ABCD, form='CRFB')

Calculate the parameters for a specified modulator topology, assuming ABCD fits that topology.

#### Input

ABCD	A state-space desc	ription of the mod	lulator loop filter.
------	--------------------	--------------------	----------------------

form See realizeNTF on page 12 for a list of supported structures.

#### Output

a Feedback/feedforward coefficients from/to the quantizer.

g Resonator coefficients.

b Feed-in coefficients from the modulator input to each integrator.

c Integrator inter-stage coefficients.

# scaleABCD

Scale the ABCD matrix so that the state maxima are less than a specified limit. The maximum stable input is determined as a side-effect of this process.

#### Input

ABCD A state-space description of the modulator loop filter.

nlev The number of levels in the quantizer.

f The normalized frequency of the test sinusoid. xlim The limit on the states. May be given as a vector.

ymax The threshold for judging modulator stability. If the quantizer input ex-

ceeds ymax, the modulator is considered to be unstable.

Output

ABCDs The scaled state-space description of the modulator loop filter.

umax The maximum stable input. Input sinusoids with amplitudes below this

value should not cause the modulator states to exceed their specified lim-

its.

# calculateTF

**Synopsis:** [ntf, stf] = calculateTF (ABCD, k=1) Calculate the NTF and STF of a delta-sigma modulator.

#### Input

ABCD A state-space description of the modulator's loop filter.

k The quantizer gain to assume.

#### Output

ntf The modulator NTF, given as an LTI system in zero-pole form. stf The modulator STF, given as an LTI system in zero-pole form.

#### **Example**

Static gain.

Realize a 5<sup>th</sup>-order modulator with the cascade-of-resonators structure, feedback form. Calculate the ABCD matrix of the loop filter and verify that the NTF and STF are correct.

```
>> H = synthesizeNTF(5,32,1)
Zero/pole/gain:
(z-1) (z^2 - 1.997z + 1) (z^2 - 1.992z + 1)
_____
(z-0.7778) (z^2 - 1.613z + 0.6649) (z^2 - 1.796z + 0.8549)
Sampling time: 1
>> [a,g,b,c] = realizeNTF(H)
a = 0.0007 0.0084 0.0550 0.2443 0.5579
g = 0.0028 \quad 0.0079
b = 0.0007  0.0084  0.0550  0.2443  0.5579  1.0000
c = 1 1 1 1
>> ABCD = stuffABCD(a,q,b,c)
ABCD =

    0
    0
    0
    0.0007
    -0.0007

    0000
    -0.0028
    0
    0.0084
    -0.0084

    0000
    0.9972
    0
    0.0633
    -0.0633

1.0000
1.0000 1.0000 -0.0028
1.0000 1.0000 0.9972
    0 0 1.0000 1.0000 -0.0079 0.2443 -0.2443
            0 1.0000 1.0000 0.9921 0.8023 -0.8023
            0
                     0
                          0 1.0000
                                            1.0000
>> [ntf,stf] = calculateTF(ABCD)
Zero/pole/gain:
(z-1) (z^2 - 1.997z + 1) (z^2 - 1.992z + 1)
  ._____
(z-0.7778) (z^2 - 1.613z + 0.6649) (z^2 - 1.796z + 0.8549)
Sampling time: 1
Zero/pole/gain:
```

# **simulateMS**

```
Synopsis: [sv,sx,sigma_se,max_sx,max_sy]
```

= simulateMS(v, mtf, M=16, d=0, dw=[1-], sx0=[0-])

Simulate an *M*-element DAC using mismatch-shaping transfer function *mtf*.

#### Reference

max\_sx

max\_sy

R. Schreier and B. Zhang "Noise-shaped multibit D/A convertor employing unit elements," *Electronics Letters*, vol. 31, no. 20, pp. 1712-1713, Sept. 28 1995.

#### Input

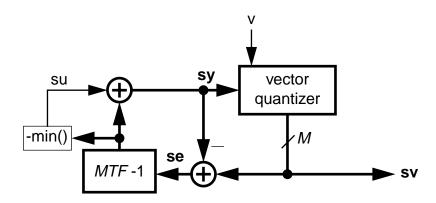
input	
V	A vector containing the number of elements to enable. Note that the
	output of simulateDSM must be offset and scaled in order to be used
	here as v must be in the range $[0, \sum_{i}^{M} dw(i)]$ .
mtf	The mismatch-shaping transfer function, given in zero-pole form.
M	The number of DAC elements.
d	Dither uniformly distributed in $[-d,d]$ is added to the sy input of the
	vector quantizer.
dw	A vector containing the nominal weight associated with each element.
sx0	An $n \times M$ matrix containing the initial state of the element selection logic.
Output	
sv	The selection vector: a vector of zeros and ones indicating which ele-
	ments to enable.
SX	An $n \times M$ matrix containing the final state of the element selection logic.
sigma_se	The rms value of the selection error, $se = sv - sy$ . sigma_se may be used

to analytically estimate the power of in-band noise caused by element mismatch.

The maximum value attained by any state in the ESL.

The maximum value attained by any component of the (un-normalized)

"desired usage" vector sy.

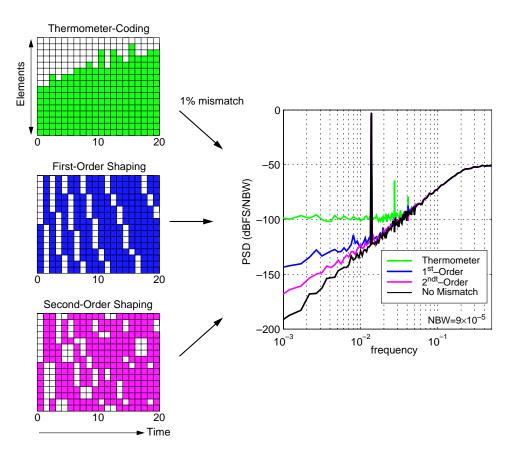


Block diagram of the Element Selection Logic

### Example (cf. dsdemo5)

Compare the usage patterns and example spectra for a 16-element DAC driven with thermometer-coded, 1<sup>st</sup>-order and 2<sup>nd</sup>-order mismatch-shaped data generated by a 3<sup>rd</sup>-order modulator.

```
ntf = synthesizeNTF(3,[],[],4);
M = 16;
N = 2^14;
fin = round(0.33*N/(2*12));
u = M/sqrt(2)*sin((2*pi/N)*fin*[0:N-1]);
v = simulateDSM(u, ntf, M+1);
sv0 = ds\_therm(v, M);
mtf1 = zpk(1,0,1,1);
                                           % First-order shaping
sv1 = simulateMS(v,mtf1,M);
mtf2 = zpk([11], [00], 1, 1);
                                           % Second-order shaping
sv2 = simulateMS(v,mtf2,M);
ue = 1 + 0.01 * randn(M, 1);
                                           % 1% mismatch
dv0 = ue' * sv0;
spec0 = fft(dv0.*ds_hann(N))/(M*N/8);
plotSpectrum(spec0, fin, 'g');
```



# realizeNTF\_ct

Realize a noise transfer function (NTF) with a continuous-time loop filter.

#### Input

ntf The modulator NTF, specified as an LTI object in zero-pole form.

form A string specifying the modulator topology.

FB Feedback form.
FF Feedforward form.

tdac The timing for the feedback DAC(s). If  $tdac(1) \ge 1$ , direct feedback

terms are added to the quantizer. Multiple timings (one or more per integrator) for the FB topology can be specified by making tdac a cell array,

e.g.

 $tdac = \{[1,2]; [1 2]; [0.5 1], [1 1.5]; [];\}$ 

ordering A vector specifying which NTF zero-pair to use in each resonator. De-

fault is for the zero-pairs to be used in the order specified in the NTF.

bp A vector specifying which resonator sections are bandpass. The default

(zeros(...)) is for all sections to be lowpass.

ABCDc The loop filter structure, in state-space form. If this argument is omitted,

ABCDc is constructed according to form.

#### Output

ABCDc A state-space description of the CT loop filter.

tdac2 A matrix with the DAC timings, one for each input, including ones that

were automatically added.

#### **Example**

Realize the NTF with a CT system (cf. the example on page 19).

```
>>  ntf = zpk([1 1],[0 0],1,1);
>> [ABCDc,tdac2] = realizeNTF_ct(ntf,'FB')
ABCDc =
                1.0000 -1.0000
    0
1.0000
                     0 -1.5000
             0
    0
      1.0000
                      0
                          0.0000
tdac2 =
-1
     -1
0
      1
```

# mapCtoD

**Synopsis:** [sys, Gp] = mapCtoD(sys\_c, t=[0 1], f0=0)

Map a MIMO continuous-time system to a SIMO discrete-time equivalent. The criterion for equivalence is that the sampled pulse response of the CT system must be identical to the impulse response of the DT system. I.e. if  $y_c$  is the output of the CT system with an input  $v_c$  taken from a set of DACs fed with a single DT input  $v_c$ , then  $v_c$ , the output of the equivalent DT system with input  $v_c$  satisfies  $v_c$  are characterized by rectangular impulse responses with edge times specified in the  $v_c$  matrix.

#### Input

Input	
sys_c	The LTI description of the CT system.
t	The edge times of the DAC pulse used to make CT waveforms from DT
	inputs. Each row corresponds to one of the system inputs; [-1 -1]
	denotes a CT input. The default is [0 1] for all inputs except the first,
	which is assumed to be a CT input.
f0	The frequency for which the Gp filters' gains are to be set to unity. De-
	fault 0 (DC).

### Output

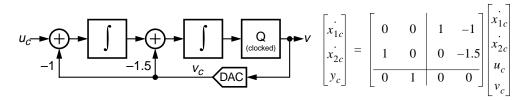
sys	The LTI description for the DT equivalent.
Gp	The mixed CT/DT prefilters which form the samples fed to each state for
	the CT inputs.

#### Reference

R. Schreier and B. Zhang, "Delta-sigma modulators employing continuous-time circuitry," *IEEE Transactions on Circuits and Systems I*, vol. 43, no. 4, pp. 324-332, April 1996.

#### Example

Map the standard second-order CT modulator shown below to its DT equivalent and verify that the NTF is  $(1-z^{-1})^{2}$ .



```
>> LFc = ss([0 0;1 0], [1 -1;0 -1.5], [0 1], [0 0]);
>> tdac = [0 1];
>> [LF,Gp] = mapCtoD(LFc,tdac);
>> ABCD = [LF.a LF.b; LF.c LF.d];
>> H = calculateTF(ABCD)

Zero/pole/gain:
(z-1)^2
-----
z^2
Sampling time: 1
```

# **evalTFP**

#### Synopsis: H = evalTFP(Hs, Hz, f)

Use this function to evaluate the signal transfer function of a continuous-time (CT) system. In this context Hs is the open-loop response of the loop filter from the u input and Hz is the closed-loop noise transfer function.

#### Input

Hs	A continuous-time transfer function in zpk form.
Hz	A discrete-time transfer function in zpk form.
f	A vector of frequencies.

#### Output

```
H The value of H_s(j2\pi f)H_z(e^{j2\pi f}).
```

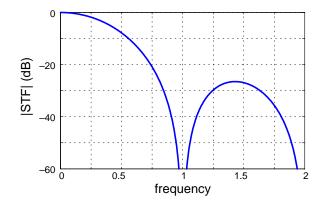
#### See Also

evalMixedTF is a more advanced version of this function which is used to evaluate the individual feed-in transfer functions of a CT modulator.

#### Example

Plot the STF of the 2<sup>nd</sup>-order CT system depicted on page 19.

```
Ac = [0 0; 1 0];
Bc = [1 -1; 0 -1.5];
Cc = [0 1];
Dc = [0 0];
LFc = ss(Ac, Bc, Cc, Dc);
L0c = zpk(ss(Ac,Bc(:,1),Cc,Dc(1)));
tdac = [0 1];
[LF,Gp] = mapCtoD(LFc,tdac);
ABCD = [LF.a LF.b; LF.c LF.d];
H = calculateTF(ABCD);
% Yields H=(1-z^-1)^2
f = linspace(0,2,300);
STF = evalTFP(L0c,H,f);
plot(f,dbv(STF));
```



# synthesizeQNTF

```
Synopsis: ntf = synthesizeQNTF(order=3,OSR=64,f0=0,f0=-60,ING=-20, n_im=order/3)
```

Synthesize a noise transfer function (NTF) for a quadrature delta-sigma modulator.

# Input order

OSR	The oversampling ratio.
f0	The center frequency of the modulator.
NG	The rms in-band noise gain (dB).
ING	The rms image-band noise gain (dB).
n_im	Number of image-band zeros.

The order of the NTF.

#### Output

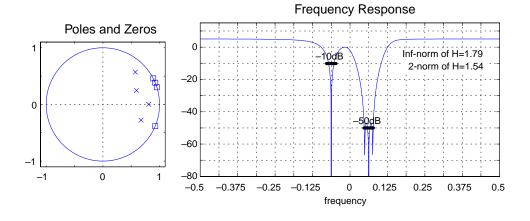
ntf The modulator NTF, given as an LTI object in zero-pole form.

#### Bugs

ALPHA VERSION. This function uses an experimental ad hoc method that is neither optimal nor robust.

#### **Example**

Fourth-order, , bandpass NTF with an rms in-band noise gain of  $-50~\mathrm{dB}$  and an image-band noise gain of  $-10~\mathrm{dB}$ .



# **simulateQDSM**

**Synopsis:** [v, xn, xmax, y] = simulateQDSM(u, ABCD|ntf, nlev=2, x0=0) Simulate a quadrature delta-sigma modulator with a given input. For improved simulation speed, use simulateDSM with a 2-input/2-output ABCDr argument as indicated in the example in mapQtoR on page 24.

#### Input

u	The input sequence to the modulator, given as a $1 \times N$ row vector. Full-
	scale corresponds to an input of magnitude $nlev - 1$ .
ABCD	A state-space description of the modulator's loop filter.
ntf	The modulator NTF, given in zero-pole form.
nlev	The number of levels in the quantizer. Multiple quantizers are indicated
	by making nlev a column vector.
x0	The initial state of the modulator.
Output	
v	The samples of the output of the modulator, one for each input sample.
	The internal states of the moduleton one for each input semale, given as

The internal states of the modulator, one for each input sample, given as an  $n \times N$  matrix.

The maximum absolute values of each state variable.

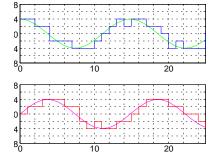
The samples of the quantizer input, one per input sample.

#### **Example**

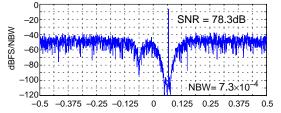
Simulate a 4<sup>th</sup>-order 9-level quadrature modulator with a half-scale sine-wave input and plot its output in the time and frequency domains.

```
nlev = 9; f0 = 1/16; osr = 32; M = nlev-1;
ntf = synthesizeQNTF(4,osr,f0,-50,-10);
N = 64*osr; f = round((f0+0.3*0.5/osr)*N)/N;
u = 0.5*M*exp(2i*pi*f*[0:N-1]);
v = simulateQDSM(u,ntf,nlev);
```

```
t = 0:25;
subplot(211)
plot(t, real(u(t+1)),'g');
hold on;
stairs(t,real(v(t+1)),'b');
figureMagic(...)
ylabel('real');
```



```
spec = fft(v.*ds_hann(N))/(M*N/2);
spec = [fftshift(spec) spec(N/2+1)];
plot(linspace(-0.5,0.5,N+1), dbv(spec))
figureMagic([-0.5 0.5],1/16,2, [-120 0],10
ylabel('dBFS/NBW')
[f1 f2] = ds_f1f2(osr,f0,1);
fb1 = round(f1*N); fb2 = round(f2*N);
fb = round(f*N)-fb1;
snr = calculateSNR(spec(N/2+1+[fb1:fb2]),f
text(f,-10,sprintf('SNR = %4.1fdB\n',snr)
text(0.25, -105, sprintf('NBW=%0.1e',1.5/N)
```



# realizeQNTF

**Synopsis:** ABCD = realizeQNTF(ntf, form='FB', rot=0, bn)

Convert a quadrature NTF into an ABCD matrix for the specified structure.

#### Input

ntf A zpk object specifying the modulator's NTF.
form A string specifying the modulator topology.

FB Feedback

 $\begin{array}{c} {\tt PFB} \ Parallel \ feedback \\ {\tt FF} \ Feedforward \end{array}$ 

PFF Parallel feedforward

rot = 1 means rotate states to make as many coefficients as possible real.

bn The coefficient of the auxiliary DAC for form = 'FF'.

#### Output

ABCD State-space description of the loop filter.

#### **Example**

Determine coefficients for the parallel feedback (PFB) structure.

```
>> ntf = synthesizeQNTF(5, 32, 1/16, -50, -10);
>> ABCD = realizeQNTF(ntf,'PFB',1)
ABCD =
Columns 1 through 4
0.8854+0.4648i
                     0
                                     0
                                                      0
               0.9547+0.2974i
0.0065+1.0000i
                                     0
                                                      0
    0
                 0.9715+0.2370i 0.9088+0.4171i
                                                      0
    0
                                 0.8797+0.4755i 0.9376+0.3477i
                     0
    0
                     0
                                     0
                                                     0
    0
                     0
                                     0
                                                -0.9916-0.1294i
Columns 5 through 7
         0.0025
    0
                                 0.0025+0.0000i
    0
                     0
                                 0.0262+0.0000i
    0
                     0
                                 0.1791+0.0000i
    0
                     0
                                 0.6341+0.0000i
0.9239-0.3827i
                                 0.1743+0.0000i
                    0
-0.9312-0.3645i
                    0
                                     0
```

# mapQtoR

**Synopsis:** ABCDr = mapQtoR(ABCD)

Convert a quadrature matrix into its real (IQ) equivalent.

Input

ABCD A complex matrix describing a quadrature system.

Output

ABCDr A real matrix corresponding to ABCD. Each element z in ABCD is re-

placed by a  $2 \times 2$  matrix to make ABCDr. Specifically

$$z \to \begin{bmatrix} x & -y \\ y & x \end{bmatrix}$$
 where  $x = Re(z)$  and  $y = Im(z)$ .

#### **Example**

Replace a call to simulateQDSM with a faster code block using simulateDSM.

```
% v = simulateQDSM(u,ntf,nlev);
ABCD = realizeQNTF(ntf,'FF');
ABCDr = mapQtoR(ABCD);
ur = [real(u); imag(u)];
vr=simulateDSM(ur,ABCDr,nlev*[1;1]);
v = vr(1,:) + li*vr(2,:);
```

# mapRtoQ

**Synopsis:** [ABCDq ABCDp] = mapR2Q(ABCDr)

Map a real ABCDr to a quadrature ABCD. ABCDr has its states paired (real, imaginary) as indicated above in mapQtoR.

Input

ABCDr A real matrix describing a quadrature system.

Output

ABCDq The quadrature (complex) version of ABCDr.

ABCDp The mirror-image system matrix. ABCDp is zero if ABCDr has no quadra-

ture errors.

# calculateQTF

Synopsis: [ntf stf intf istf] = calculateQTF(ABCDr)

Calculate the noise and signal transfer functions for a quadrature modulator.

#### Input

ABCDr

A real state-space description of the modulator's loop filter. I/Q asymmetries may be included in the description. These asymmetries result in non-zero image transfer functions.

#### Output

ntf, stf The noise and signal transfer functions.

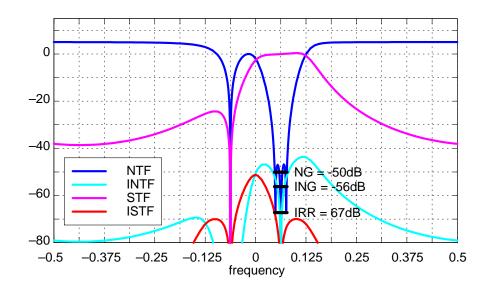
intf, istf The image noise and image signal transfer functions.

All transfer functions are returned as LTI systems in zero-pole form.

#### Example

Examine the effect of mismatch in the first feedback.

```
>> ABCDr = mapQtoR(ABCD);
>> ABCDr(2,end) = 1.01*ABCDr(2,end); % 0.1% mismatch in first feedback
>> [H G HI GI] = calculateQTF(ABCDr);
```



# simulateQESL

```
Synopsis: [sv,sx,sigma_se,max_sx,max_sy]
= simulateQESL(v,mtf,M=16,sx0=[0-])
```

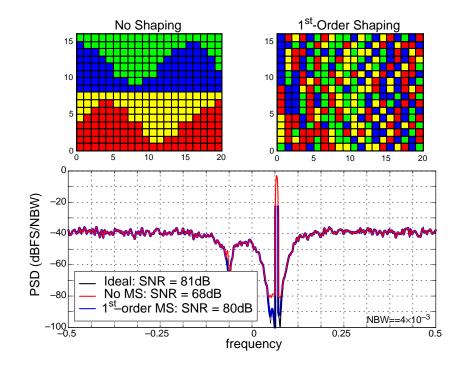
Simulate the element selection logic (ESL) of a quadrature differential DAC.

### Input

V	A vector the digital input values.
mtf	The mismatch-shaping transfer function, given in zero-pole form.
M	The number of elements. There is a total 2 <i>M</i> elements.
sx0	An $n \times M$ matrix whose columns are the initial state of the ESL.
Output	
SV	The selection vector: a vector of zeros and ones indicating which ele-
	ments to enable.
SX	An $n \times M$ matrix containing the final state of the ESL.
sigma_se	The rms value of the selection error, $se = sv = sy$ . sigma_se may be used
	to estimate the power of in-band noise caused by element mismatch.
max_sx	The maximum absolute value attained by any state in the ESL.
max_sy	The maximum absolute value attained by any input to the VQ.

# Example

```
>> mtf1 = zpk(exp(2i*pi*f0),0,1,1);
% First-order complex shaping
>> sv1 = simulateQESL(v,mtf1,M);
```



# designHBF

Synopsis: [f1, f2, info] = designHBF (fp=0.2, delta=1e-5, debug=0)

Design a hardware-efficient linear-phase half-band filter for use in the decimation or interpolation filter associated with a delta-sigma modulator. This function is based on the procedure described by Saramäki [1]. Note that since the algorithm uses a non-deterministic search procedure, successive calls may yield different designs.

[1] T. Saramäki, "Design of FIR filters as a tapped cascaded interconnection of identical subfilters," *IEEE Transactions on Circuits and Systems*, vol. 34, pp. 1011-1029, 1987.

#### Input

fp	Normalized passband cutoff frequency.
delta	Passband and stopband ripple in absolute value.

#### Output

f1,f2	Prototype filter and subfilter coefficients and their canonical-signed digit
	(csd) representation.

info A vector containing the following information data (only set when

debug=1):

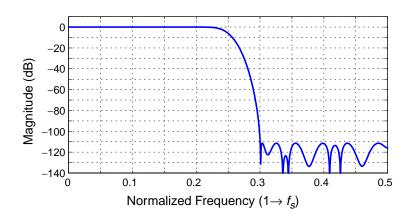
complexity The number of additions per output sample.
n1, n2 The length of the f1 and f2 vectors.
sbr The achieved stop-band attenuation in dB.
phi The scaling factor for the F2 filter.

#### **Example**

Design of a lowpass half-band filter with a cut-off frequency of  $0.2f_s$ , a passband ripple of less than  $10^{-5}$  and a stopband gain less than  $10^{-5}$  (-100 dB).

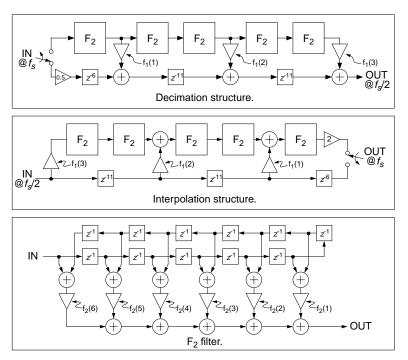
```
>> [f1,f2] = designHBF(0.2,1e-5);
>> f = linspace(0,0.5,1024);
>> plot(f, dbv(frespHBF(f,f1,f2)))
```

A plot of the filter response is shown below. The filter achieves 109 dB of attenuation in the stopband and uses only 124 additions (no true multiplications) to produce each output sample.



The structure of this filter as a decimation or interpolation filter is shown below. The coefficients and their canonical signed-digit (csd) decompositions are

In the csd expansions, the first row contains the powers of two while the second row gives their signs. For example,  $f_1(1) = 0.9453 = 2^0 - 2^{-4} + 2^{-7}$ . Since the filter coefficients use only 3 csd terms, each multiply-accumulate operation shown in the diagram below needs only 3 additions. An implementation of this  $110^{\text{th}}$ -order FIR filter therefore needs only  $3 \times 3 + 5 \times (3 \times 6 + 6 - 1) = 124$  additions at the low  $(f_s/2)$  rate.



# **simulateHBF**

**Synopsis:** y = simulateHBF(x, f1, f2, mode=0)

Simulate a Saramäki half-band filter (see designHBF on page 27) in the time domain.

#### Input

x The input data.

f1, f2 Filter coefficients. f1 and f2 can be vectors of values or struct arrays

like those returned from designHBF.

mode This flag determines whether the input is filtered, interpolated, or decimated according to the following:

O Plain filtering, no interpolation or decimation.

- 1 The input is interpolated.
- The output is decimated, even samples are taken.
- The output is decimated, odd samples are taken.

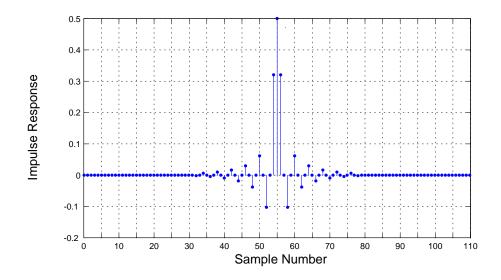
# Output

y The output data.

### Example

Plot the impulse response of the HBF designed on the previous page.

```
>> N = (2*length(f1)-1)*2*(2*length(f2)-1)+1;
>> y = simulateHBF([1 zeros(1,N-1)],f1,f2);
>> stem([0:N-1],y);
>> figureMagic([0 N-1],5,2, [-0.2 0.5],0.1,1)
```



# designPBF

**Synopsis:** [C, e, x0] = designPBF (N,M,pb,pbr,sbr,ncd,np,ns,fmax) Design a symmetric polynomial-based filter (PBF) according to Hunter's method [1]. designPBF requires the Optimization Toolbox.

[1] M. T. Hunter, "Design of polynomial-based filters for continuously variable sample rate conversion with applications in synthetic instrumentation and software defined radio," Ph.D. thesis, University of Florida, 2008.

#### Input

1	
N=10	Number of polynomial pieces.
M=5	Order of the polynomial pieces.
pb=0.25	Passband width. Relative to the input sample rate, the passband is [0, pb]
	and the stopband is $[1-pb,\infty)$ . Use pb = 0.5/OSR where OSR is the
	oversampling ratio of the input.
pbr=0.1	Passband ripple in dB.
sbr=-100	Stobpand ripple in dB.
ncd=0	Number of continuous derivatives. To allow the impulse response itself
	to be discontinuous, use $ncd = -1$ .
np=100	Number of points in the passband.
ns=1000	Number of points in the stopband.
fmax=5	Maximum frequency checked in the stopband.
Outnut	

#### Output

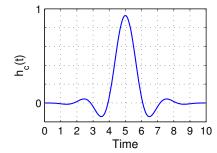
```
N × (M+1) matrix containing the coefficients of the polynomial pieces. Piece i is p_i(x) = C(i,1) + C(i,2)x + C(i,3)x^2 + ... + C(i,M+1)x^M.

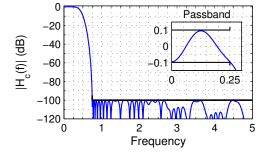
The maximum weighted error. e \le 1 indicates the specs were met. Offset on the polynomial argument, i.e. x = \mu + x0, where \mu \in [0,1].
```

#### Example

Construct a 10-segment PBF using polynomials of order 5 for interpolating signals with an input OSR of 2. Aim for a passband ripple of 0.1 dB and a stopband ripple of  $-100 \, dB$ .

```
[C, e, x0] = designPBF(10, 5, 0.5/2, 0.1, -100);
[hc, t] = impulsePBF(C,20,x0);
subplot(121); plot(t, hc, 'Linewidth', 1);
f = linspace(0,5,1000);
Hc = frespPBF(f,C,x0);
subplot(122); plot(f, dbv(Hc), 'Linewidth', 1);
```





# predictSNR

**Synopsis:** [snr,amp,k0,k1,sigma\_e2] = predictSNR(ntf,OSR=64,amp=...,f0=0) Use the describing function method of Ardalan and Paulos [1] to predict the signal-to-noise ratio (SNR) in dB for various input amplitudes. This method is only applicable to binary modulators.

[1] S. H. Ardalan and J. J. Paulos, "Analysis of nonlinear behavior in delta-sigma modulators," *IEEE Transactions on Circuits and Systems*, vol. 34, pp. 593-603, June 1987.

#### Input

ntf	The modulator	NTF.	given	in zero-	pole form.
-----	---------------	------	-------	----------	------------

OSR The oversampling ratio.

amp A row vector listing the amplitudes to use. amp defaults to

[-120 - 110... - 20 - 15 - 10 - 9 - 8...0] dB, where 0 dB means a full-

scale (peak value = 1) sine wave.

The center frequency of the modulator.

#### Output

snr	A row vector containing the predicted SNRs
amp	A row vector listing the amplitudes used.

k0 A row vector containing the signal gain of the quantizer model.k1 A row vector containing the noise gain of the quantizer model.

sigma\_e2 A row vector containing the mean square value of the noise in the quan-

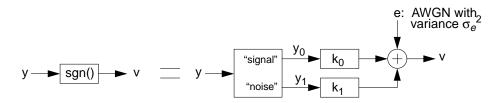
tizer model.

#### **Example**

See the example on page 11.

#### The Quantizer Model

The binary quantizer is modeled as a pair of linear gains and a noise source, as shown in the figure below. The input to the quantizer is divided into signal and noise components which are processed by signal-dependent gains  $k_0$  and  $k_1$ . These components are added to a noise source, which is assumed to be white and to have a Gaussian distribution to produce the quantizer output. The variance  $\sigma_e^2$  of the noise source is also signal-dependent.



# findPIS, find2dPIS (in the PosInvSet subdirectory)

```
Synopsis: [s,e,n,o,Sc] = findPIS(u,ABCD,nlev=2,options)
        [s,e,n,o,Sc] = findPIS(u,ABCD,nlev=2,options)
        options = [dbg=0 itnLimit=2000 expFactor=0.005 N=1000 skip=100]
Find a convex positively-invariant set for a delta-sigma modulator. findPIS requires compilation of the ghull mex file; find2dPIS does not but is limited to second-order systems.
```

This function is an implementation of the method described in [1].

[1] R. Schreier, M. Goodson and B. Zhang "An algorithm for computing convex positively invariant sets for delta-sigma modulators," *IEEE Transactions on Circuits and Systems I*, vol. 44, no. 1, pp. 38-44, January 1997.

#### Input

The input to the modulator. If u is a scalar, the input to the modulator is

constant. If u is a  $2 \times 1$  vector, the input to the modulator may be any

sequence whose samples lie in the range [u(1), u(2)].

ABCD A state-space description of the modulator loop filter.

nlev The number of quantizer levels.

dbg Set dbg=1 to see a graphical display of the iterations.

itnLimit The maximum number of iterations.

expFactor The expansion factor applied to the hull before every mapping operation.

Increasing expFactor decreases the number of iterations but results in

sets which are inflated.

N The number of points to use when constructing the initial guess.

skip The number of time steps to run the modulator before observing the state.

This handles the possibility of transients in the modulator.

qhullArqA The 'A' argument to the qhull program. Adjacent facets are merged if

the cosine of the angle between their normals is greater than the absolute value of this parameter. Negative values imply that the merge operation is performed during hull construction, rather than as a post-processing

step.

qhullArgC The 'C' argument to the qhull program. A facet is merged into its

neighbor if the distance between the facet's centrum (the average of the facet's vertices) and the neighboring hyperplane is less than the absolute value of this parameter. As with the above argument, negative values

imply pre-merging while positive values imply post-merging.

### Output

S	The vertices	of the set	$(dim \times n_v)$ .

e The edges of the set, listed as pairs of vertex indices  $(2 \times n_e)$ .

The normals for the facets of the set  $(dim \times n_f)$ .

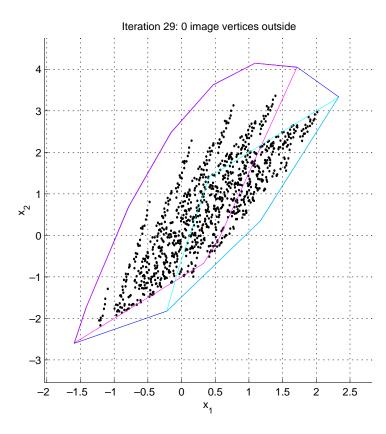
The offsets for the facets of the set  $(1 \times n_f)$ .

Sc The scaling matrix which was used internally to round out the set.

# Example

Find a positively-invariant set for the second-order modulator with an input of  $1/\sqrt{7}$ .

```
>> ABCD = [
1
      0
            1
                 -1
1
      1
            1
                 -2
0
      1
            0
                  0];
>> s = find2dPIS(sqrt(1/7),ABCD,1)
Columns 1 through 7
-1.5954
          -0.2150
                     1.1700
                                2.3324
                                          1.7129
                                                     1.0904
                                                               0.4672
-2.6019
          -1.8209
                      0.3498
                                3.3359
                                          4.0550
                                                     4.1511
                                                               3.6277
Columns 8 through 11
-0.1582
          -0.7865
                    -1.4205
                               -1.5954
                   -1.7462
2.4785
          0.6954
                              -2.6019
```



# **findPattern**

Use delta-sigma modulation to create a length-*N* data-stream which has good spectral properties when repeated.

#### Input

N The length of the data record.

OSR The oversampling ratio.

NTF The modulator NTF.

ftest The signal frequency. ftest may be a vector.

Atest The target output level as a fraction of full-scale.

f0 The center frequency.

nlev The number of levels in the output data.

quadrature A flag which indicates to use quadrature modulation.

A flag which enables showing the progress of the iterations.

#### Output

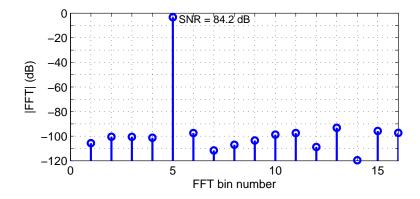
data  $1 \times N$  data record.

snr The in-band signal-to-noise ratio, in dB.

#### **Example**

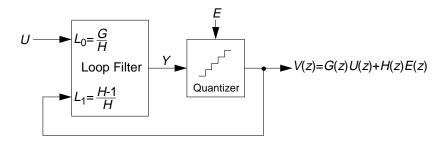
Length-1024 data record containing a -3-dBFS, 5-cycle sine wave with low in-band noise for an oversampling ratio of 32.

```
N = 1024;
osr = 32;
ntf = synthesizeNTF(5,osr,1,1.5);
ftest = 5/N;
Atest = undbv(-3);
[data snr] = findPattern(N,osr,ntf,ftest,Atest);
spec = fft(data)/(N/2);
inband = 0:ceil(N/(2*osr));
lollipop(inband,dbv(spec(inband+1)),'b',2,-120);
```



# **Modulator Model**

A delta-sigma modulator with a single quantizer is assumed to consist of quantizer connected to a loop filter as shown in the diagram below.



#### The Loop Filter

The loop filter is described by an *ABCD matrix*. For single-quantizer systems, the loop filter is a two-input, one-output linear system and ABCD is an  $(n+1) \times (n+2)$  matrix, partitioned into A  $(n \times n)$ , B  $(n \times 2)$ , C  $(1 \times n)$  and D  $(1 \times 2)$  sub-matrices as shown below:

$$ABCD = \left[ \begin{array}{c|c} A & B \\ \hline C & D \end{array} \right] \tag{A.1}$$

The equations for updating the state and computing the output of the loop filter are

$$x(n+1) = Ax(n) + B \begin{bmatrix} u(n) \\ v(n) \end{bmatrix}$$

$$y(n) = Cx(n) + D \begin{bmatrix} u(n) \\ v(n) \end{bmatrix}$$
(A.2)

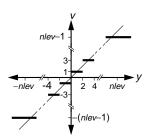
This formulation is sufficiently general to encompass all single-quantizer modulators which employ linear loop filters. The toolbox currently supports translation to/from an ABCD description and coefficients for the following topologies:

CIFB	Cascade-of-integrators, feedback form.
CIFF	Cascade-of-integrators, feedforward form.
CRFB	Cascade-of-resonators, feedback form.
CRFF	Cascade-of-resonators, feedforward form.
CRFBD	Cascade-of-resonators, feedback form, delaying quantizer.
CRFFD	Cascade-of-resonators, feedforward form, delaying quantizer
Stratos	A CIFF-like structure supporting NTF zeros on the unit circle (Jeff Gealow)
DSFB	Double-sampled, feedback (Dan Senderowicz)

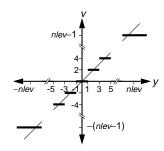
Multi-input and multi-quantizer systems can also be described with an ABCD matrix and Eq. (A.2) will still apply. For an  $n_i$ -input,  $n_o$ -output modulator, the dimensions of the sub-matrices are  $A: n \times n$ ,  $B: n \times (n_i + n_o)$ ,  $C: n_o \times n$  and  $D: n_o \times (n_i + n_o)$ .

# The Quantizer

The quantizer is ideal, producing integer outputs centered about zero. Quantizers with an even number of levels are of the mid-rise type and produce outputs which are odd integers. Quantizers with an odd number of levels are of the mid-tread type and produce outputs which are even integers.

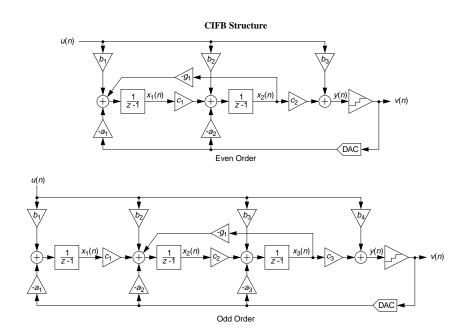


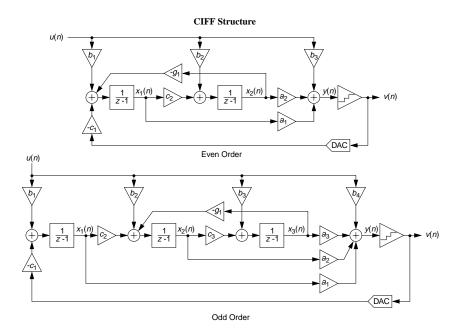
Transfer curve of a quantizer with an even number of levels.

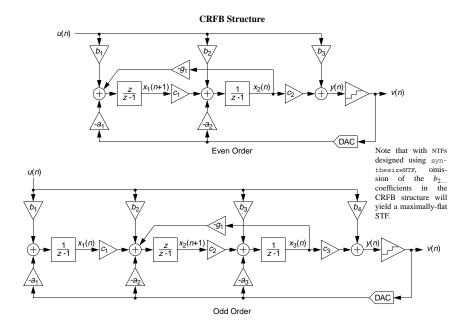


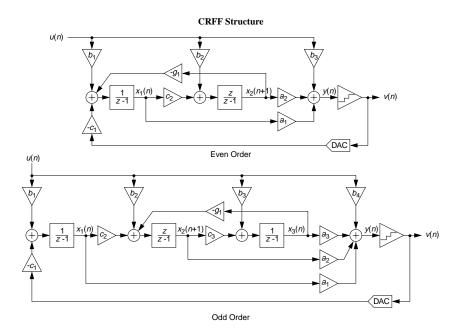
Transfer curve of a quantizer with an odd number of levels.

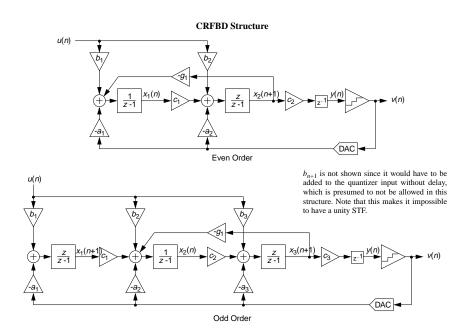
# **Supported Modulator Topologies**

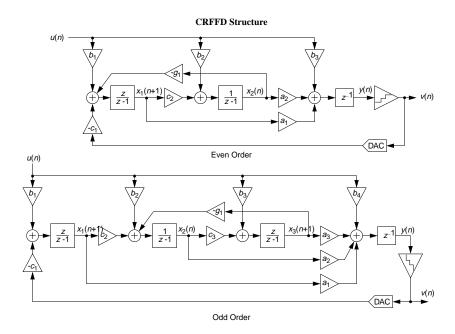












# DSFB Structure (Developed with D. Senderowicz 2014-03)

