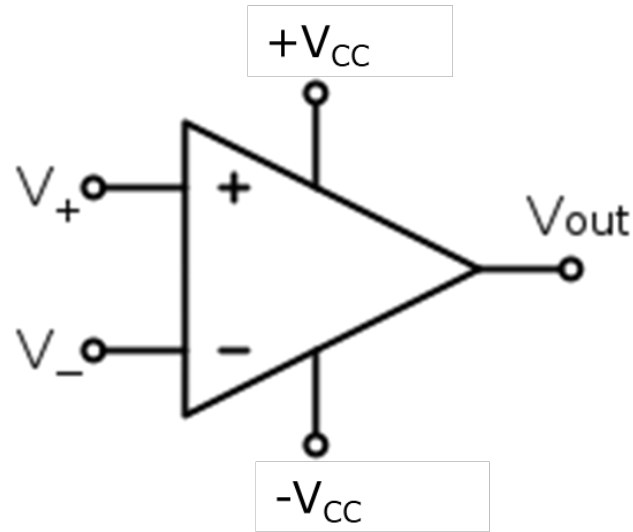


# **CG1111A: Engineering Principles & Practice I**

Tutorial 4: Reflections & Problem Solutions  
(12/13 Oct 2022)



# Comparator



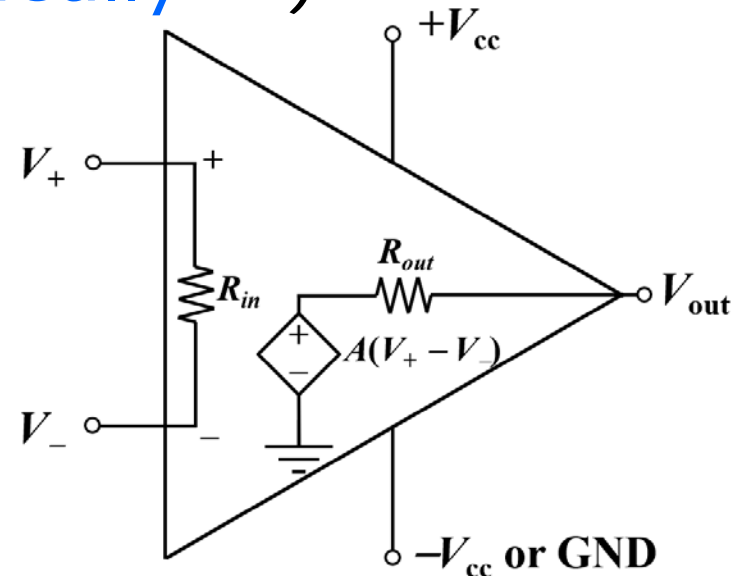
- The comparator is an electronic **decision-making** circuit that makes use of an op-amp's very high gain in its **open-loop state** (i.e., there is no feedback resistor)

# Op-Amp as a Comparator

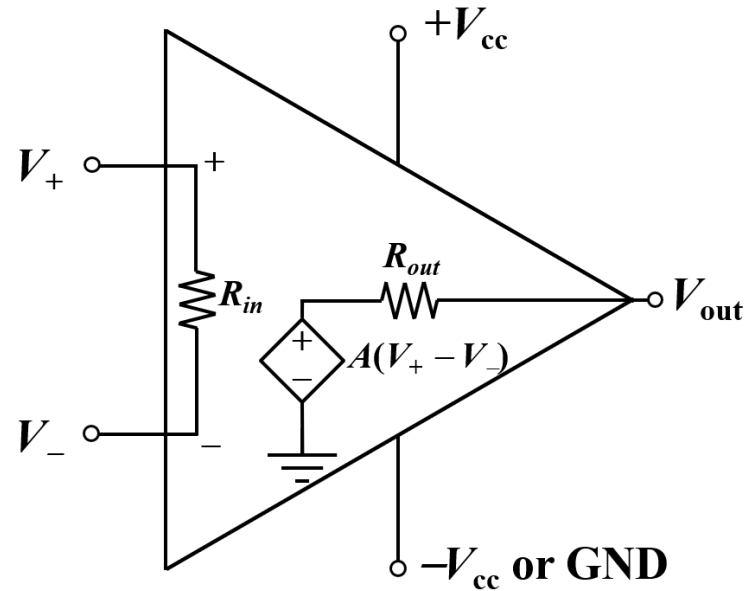
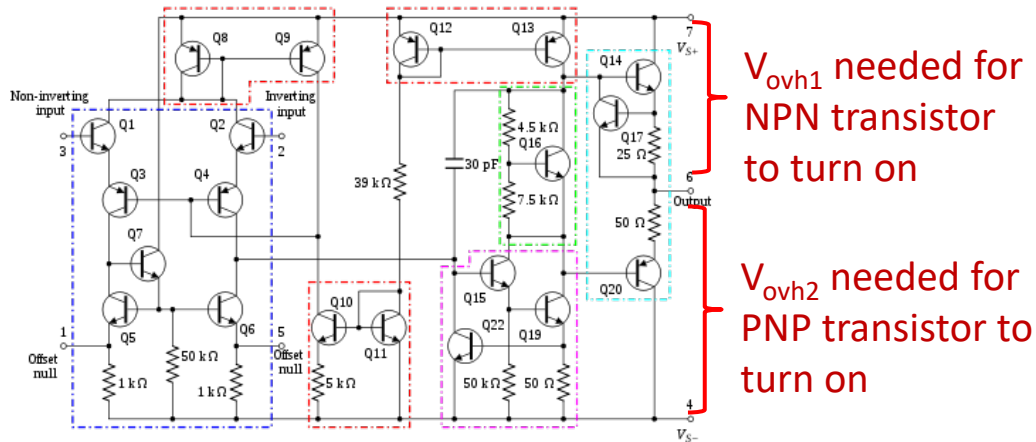
## – How It Works

Recall that for op-amp:

- The difference between the two inputs is amplified as ' $A(V_+ - V_-)$ ' at the output
- The **open-loop** voltage gain ('A') of the op-amp is very high (**ideally  $\infty$** )
- Even if there is a very small difference between the inputs, the high 'A' will pull the output to "**saturation**"



# What Are Saturation Voltages?



- If  $V_+ > V_-$ :

$$V_{out} = V_{CC} - V_{ovh1}$$

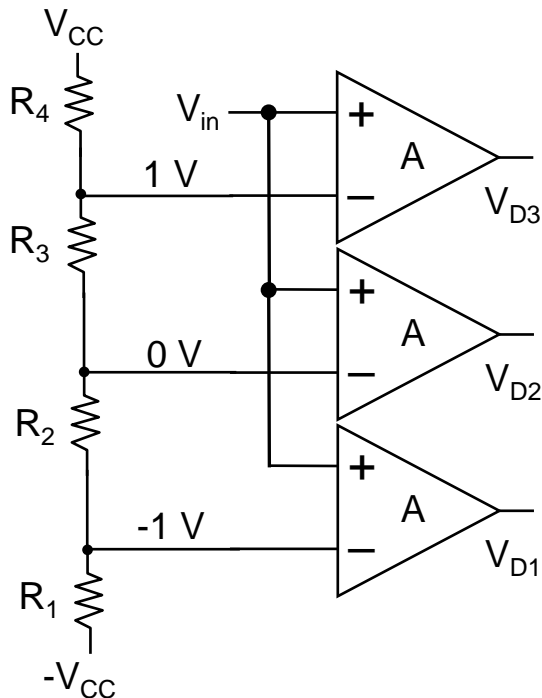
- If  $V_- > V_+$ :

$$V_{out} = \begin{cases} -V_{CC} + V_{ovh2} & \text{if dual power supply} \\ V_{ovh2} & \text{if single power supply} \end{cases}$$

- $V_{ovh1}$  &  $V_{ovh2}$  are the **voltage headrooms** from the **supply rails** ( $V_{CC}$ ,  $-V_{CC}$ , or GND) needed to sustain proper **output transistor turn-on voltage**, and it varies between 0.05 to 1.5 V depending on the **output current**

# Common Application of Comparator

- The comparator is ideal for converting analog signals to **digital signals** at certain threshold values

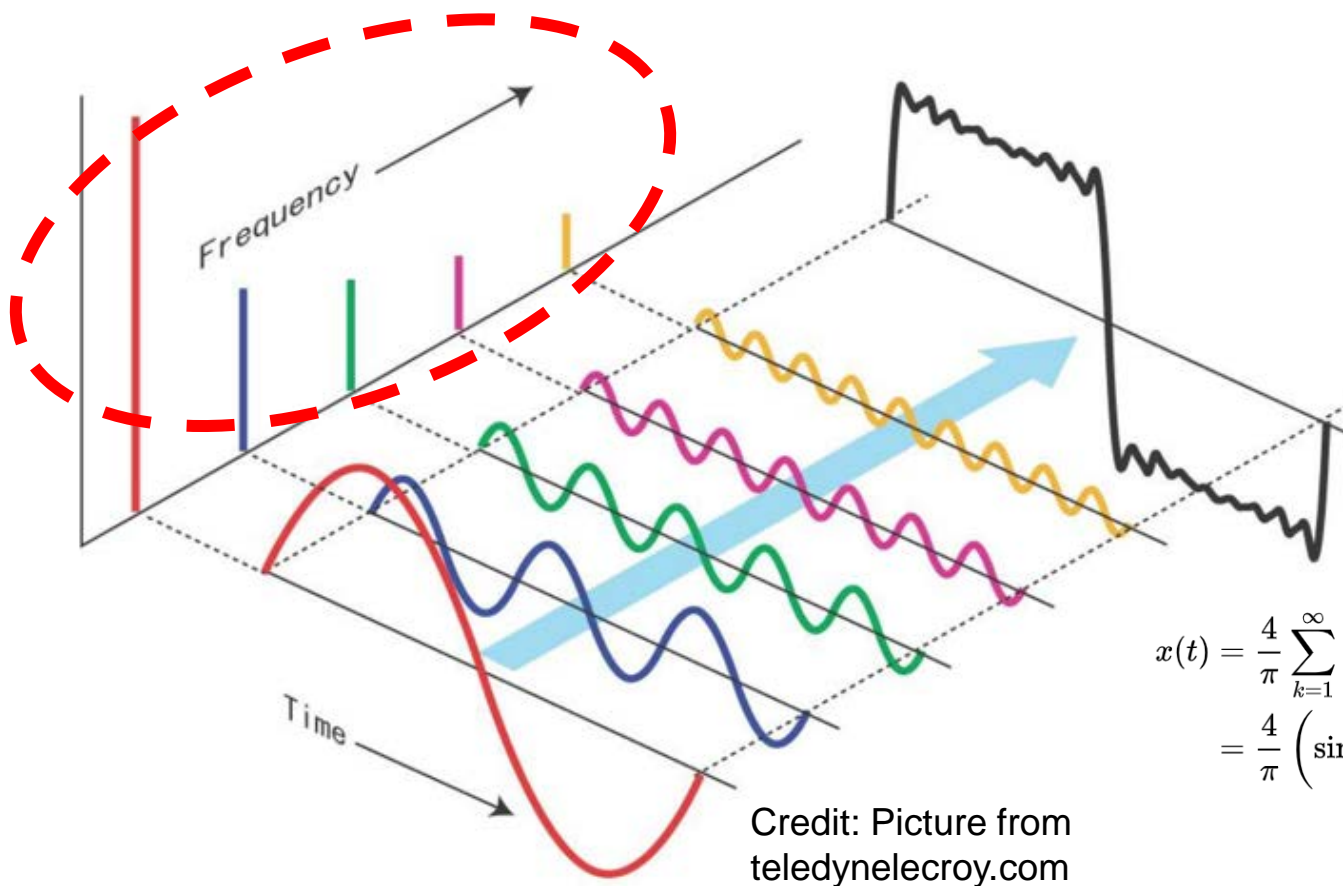


| $V_{in}$                            | $V_{D3}$ | $V_{D2}$ | $V_{D1}$ | ADC |
|-------------------------------------|----------|----------|----------|-----|
| $V_{in} < -1\text{ V}$              | L        | L        | L        | 00  |
| $-1\text{ V} < V_{in} < 0\text{ V}$ | L        | L        | H        | 01  |
| $0\text{ V} < V_{in} < 1\text{ V}$  | L        | H        | H        | 10  |
| $V_{in} > 1\text{ V}$               | H        | H        | H        | 11  |

# Spectral Analysis

- Any function of time can be described as a **sum of sinusoidal waves**, each with different amplitudes and frequencies
- **Spectral analysis** studies the distribution of a signal's frequency components
- The plot of a signal's frequency components and their corresponding magnitudes is called "**frequency spectrum**"

# Spectral Analysis

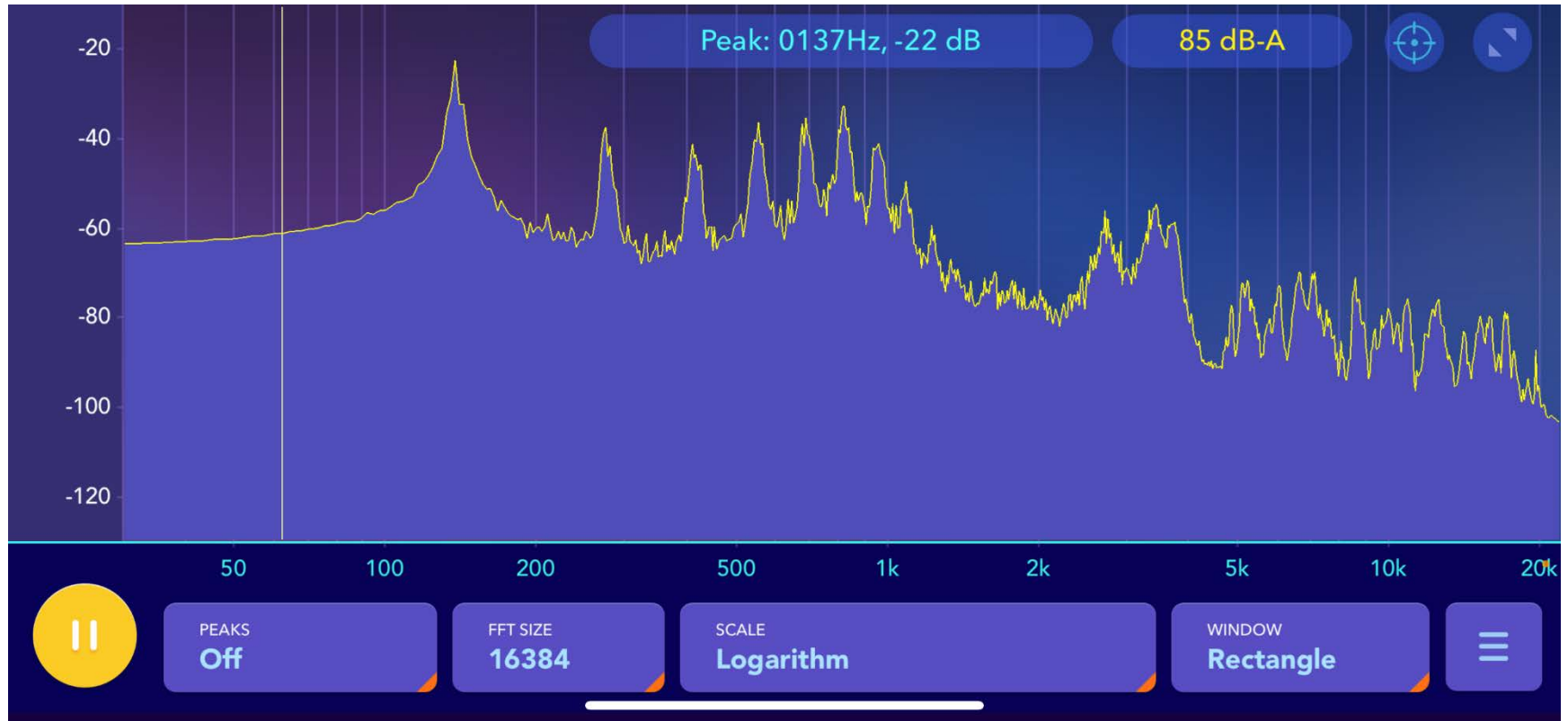


Mathematically, it can be represented using Fourier expansion:

$$\begin{aligned} x(t) &= \frac{4}{\pi} \sum_{k=1}^{\infty} \frac{\sin(2\pi(2k-1)ft)}{2k-1} \\ &= \frac{4}{\pi} \left( \sin(\omega t) + \frac{1}{3} \sin(3\omega t) + \frac{1}{5} \sin(5\omega t) + \dots \right) \end{aligned}$$

- We are analysing a signal in the **frequency domain**
- A square wave can be decomposed into an **infinite sum** of **sinusoidal** waves

# Example of Frequency Spectrum



The frequency spectrum of a particular audio tone



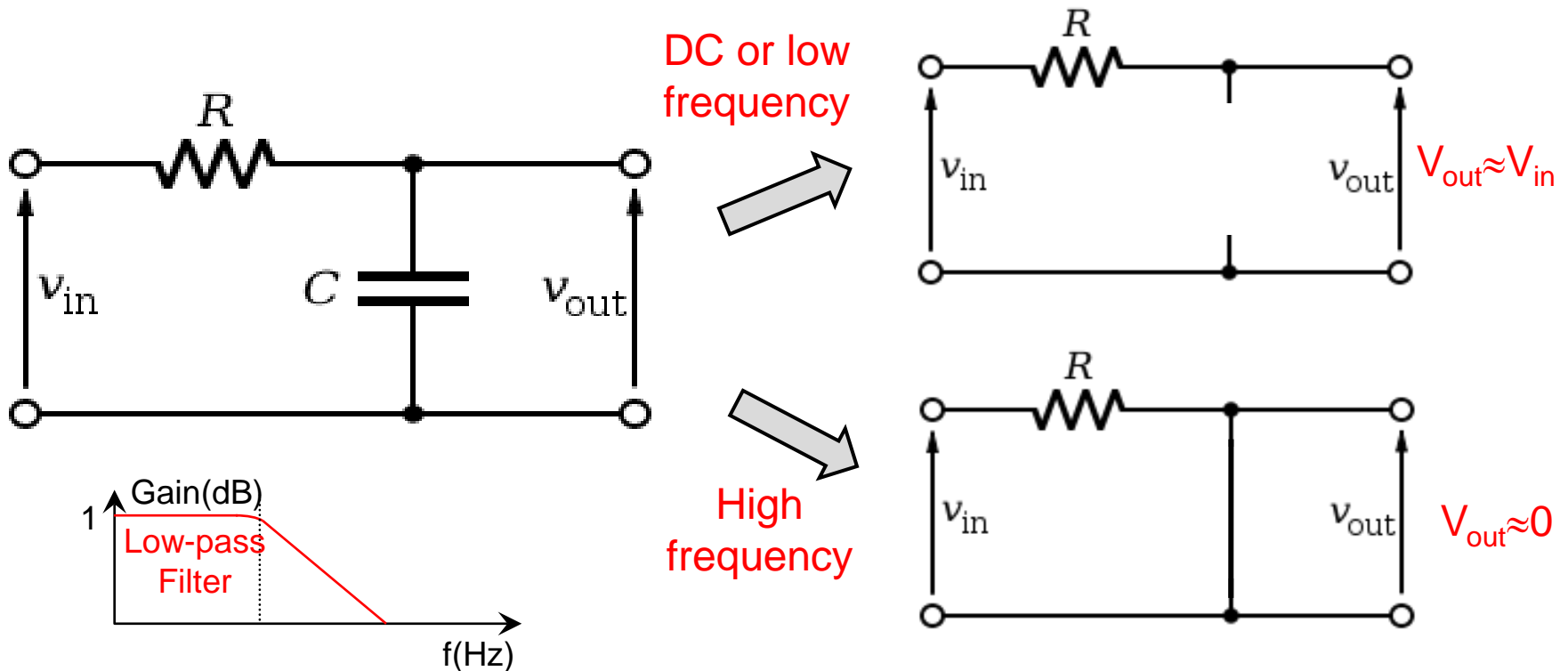
# Filter

- A filter is a device or process that removes some unwanted components or features from a signal
- Examples:
  - Removing the noise from measured ECG signal using a filter to help a doctor understand the heart better



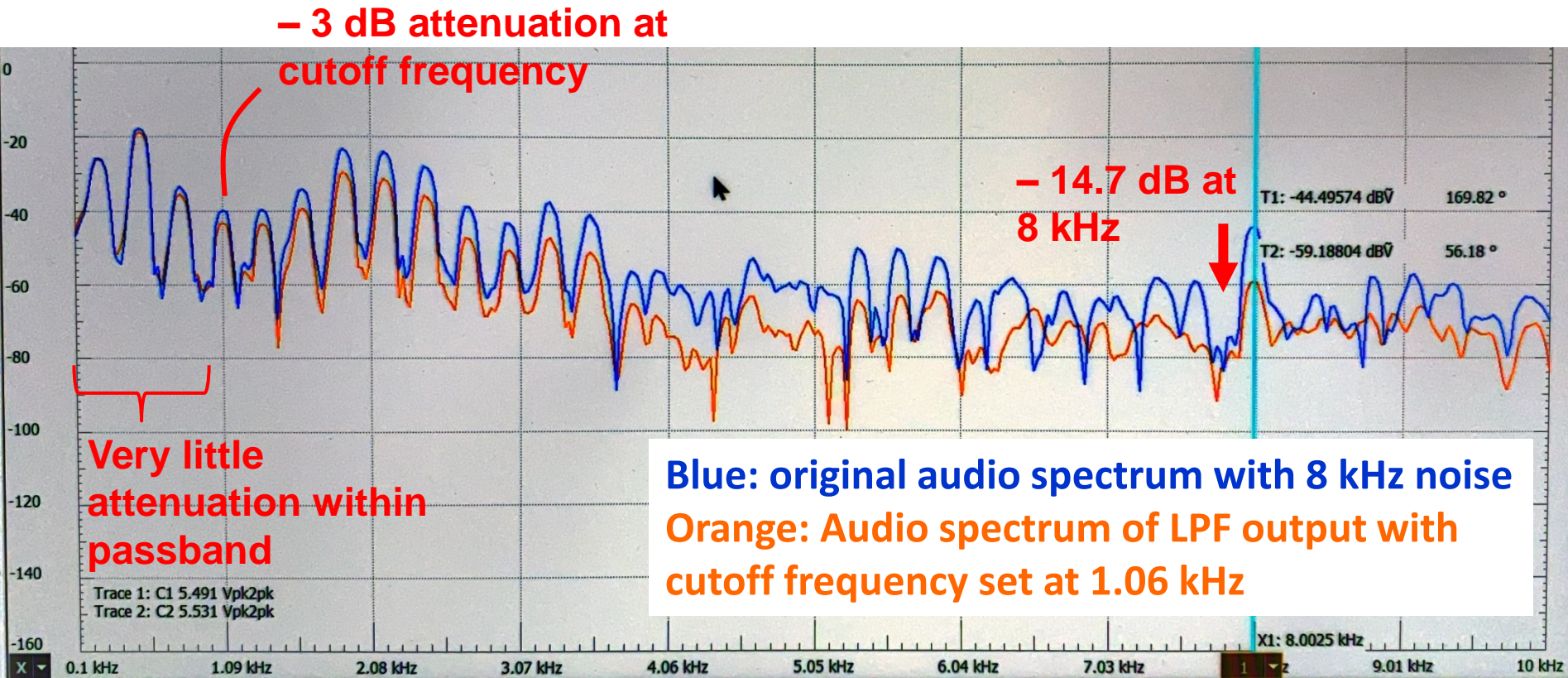
- Removing some frequencies or frequency bands from an audio signal

# Passive Low-Pass Filter



- Capacitor impedance is given as  $1/(j\omega C)$
- At **low** frequency or DC, **capacitor** behaves like **open** circuit
- At **high** frequency, **capacitor** behaves like **short** circuit
- **Allow low** frequency signal to pass through and **reject high** frequency signal  $\Rightarrow$  **Low-pass filter**

# Filters Can Help Suppress (Attenuate) Undesirable Frequencies



## Note:

The above spectrum is plotted in **linear** scale; usual practice is to plot in **logarithmic** scale if plotted over wide frequency range

# Power Gain in decibels (dB)

- The **Voltage Amplification ( $A_v$ )** or **Gain** of a voltage amplifier/filter is given by:

$$A_v = \frac{V_{\text{out}}}{V_{\text{in}}}$$

- The **voltage gain** is commonly expressed in terms of the resulting **power gain** in **dB**:

$$\begin{aligned} \text{Power Gain (dB)} &= 10 \log_{10} \left( \frac{P_{\text{out}}}{P_{\text{in}}} \right) \text{ dB} \\ &\quad \text{(Under certain conditions, to be explained in Q1)} \quad \curvearrowright \\ &= 10 \log_{10} \left( \frac{V_{\text{out}}}{V_{\text{in}}} \right)^2 \text{ dB} = 20 \log_{10} \left| \frac{V_{\text{out}}}{V_{\text{in}}} \right| \text{ dB} \end{aligned}$$

# Frequency Response

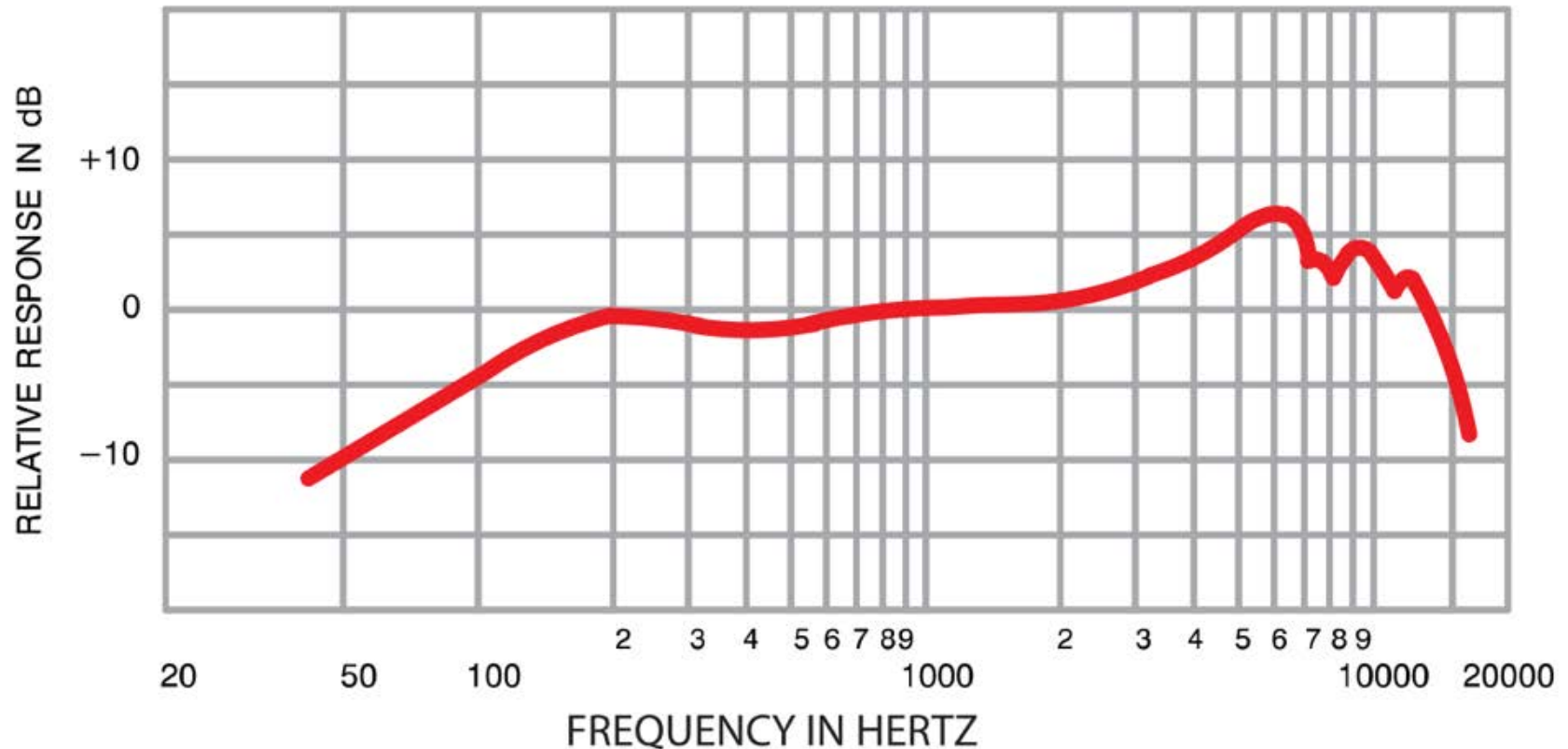
- It is the quantitative measure of the output spectrum of a system or device in response to a stimulus, and is used to characterize the dynamics of the system
  - Frequency in logarithmic scale: horizontal x-axis



- Power Gain in decibels (dB): vertical y-axis  
To describe a change in output power over the whole frequency range

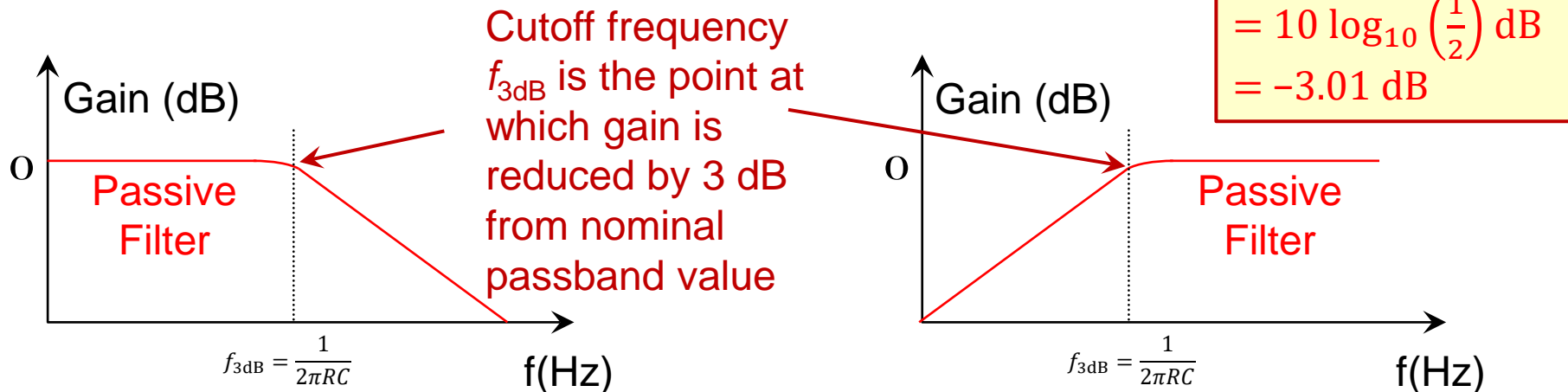
$$\text{Power Gain in dB } (f) = 20 \log_{10} |A_v(f)|$$

# Example of a Microphone's Frequency Response Graph



# Cut-off Frequency

- In filters, the cut-off frequency characterizes a “boundary” between a **passband** and a **stopband**
- It is defined as the frequency at which the **output power** is reduced by **half** compared to the nominal passband value
- In **dB scale**, this is equivalent to the nominal passband value reduced by about 3 dB

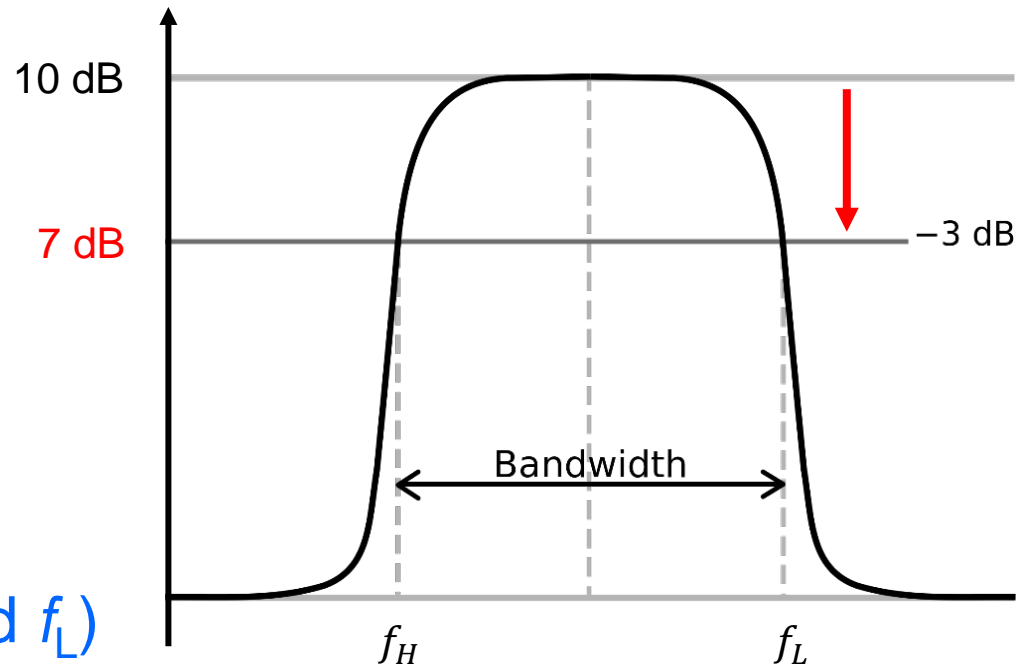




# Cut-off Frequency: $-3$ dB Point (i.e., Half-power Point)

## ■ **Graphical** approach:

- Find the passband gain from the magnitude vs frequency plot
- Subtract 3 dB from the passband gain and draw a horizontal line on the plot
- Identify the points where this horizontal line intercepts the plot
- The frequencies corresponds to these intercepts are the cut-off frequencies ( $f_H$  and  $f_L$ )





# Cut-off Frequency: $-3$ dB Point (i.e., Half-power Point)

- Quantitative approach  
(for first-order filters):

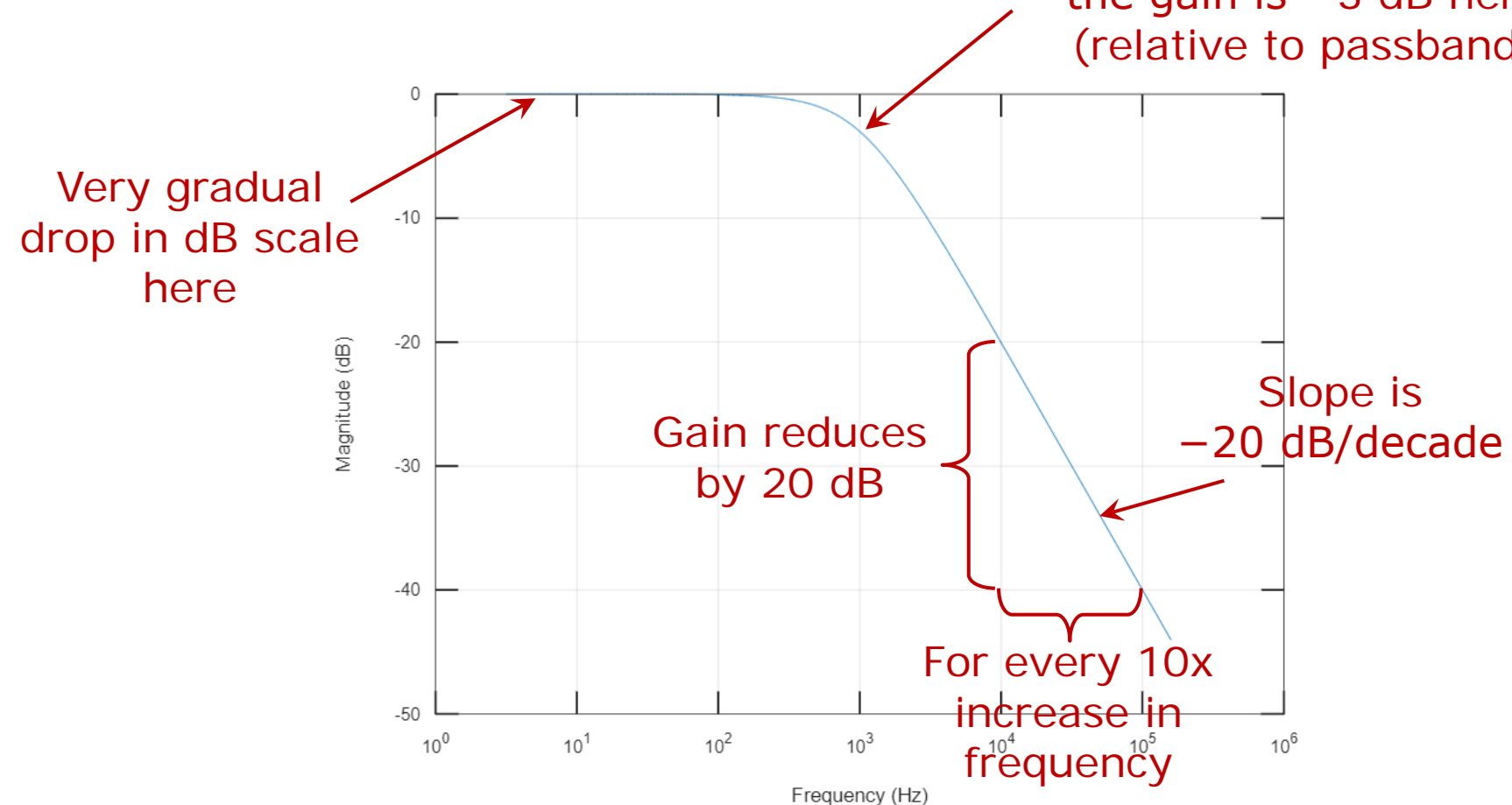
$$f_H = \frac{1}{2\pi R_H C_H}, \quad f_L = \frac{1}{2\pi R_L C_L}$$

# First-order Low-Pass Filter

- Slope after cut-off frequency

$\approx -20$  dB/decade

If cut-off frequency is 1 kHz,  
the gain is  $-3$  dB here  
(relative to passband)



# Passive Low-Pass Filter

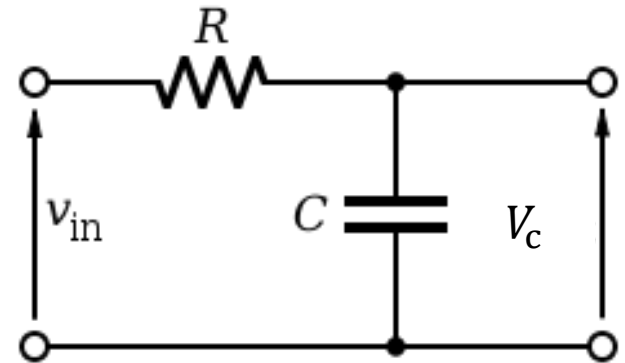
- Using voltage divider rule to find the voltage gain:

$$\rightarrow V_c = \left[ \frac{\frac{1}{j\omega C}}{\frac{1}{j\omega C} + R} \right] V_{in}$$

$$\rightarrow \frac{V_c}{V_{in}} = \left[ \frac{\frac{1}{j\omega C}}{\frac{1}{j\omega C} + R} \right] = \left[ \frac{1}{1 + jR\omega C} \right] = \frac{1 \angle 0^\circ}{\sqrt{1^2 + (R\omega C)^2} \angle \theta^\circ}$$

$$\rightarrow \left| \frac{V_c}{V_{in}} \right| = \left[ \frac{1}{\sqrt{1 + (R\omega C)^2}} \right]$$

$$\text{Gain in dB} = \underbrace{20 \log_{10} 1}_{\substack{\text{Passband gain} \\ (= 0 \text{ dB})}} - \underbrace{20 \log_{10} \sqrt{1 + (\omega CR)^2}}_{\substack{\text{Change in gain with } \omega \\ (-3 \text{ dB occurs at } f_L = \frac{1}{2\pi RC})}} \text{ dB}$$



# Passive High-Pass Filter

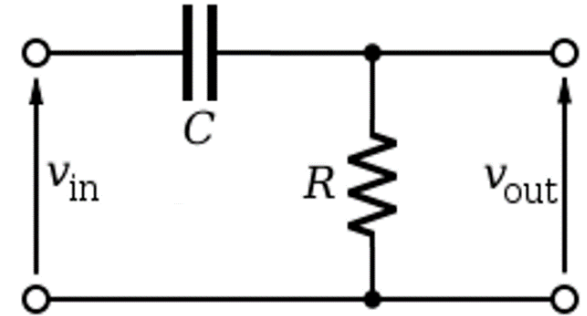
- Using voltage divider rule to find the voltage gain:

$$\rightarrow V_{\text{out}} = \left[ \frac{R}{R + \frac{1}{j\omega C}} \right] V_{\text{in}}$$

$$\rightarrow \frac{V_{\text{out}}}{V_{\text{in}}} = \left[ \frac{R}{R + \frac{1}{j\omega C}} \right] = \left[ \frac{1}{1 - \frac{j}{\omega CR}} \right] = \frac{1 \angle 0^\circ}{\sqrt{1^2 + \left(\frac{1}{\omega CR}\right)^2} \angle \theta^\circ}$$

$$\rightarrow \left| \frac{V_{\text{out}}}{V_{\text{in}}} \right| = \left[ \frac{1}{\sqrt{1 + \left(\frac{1}{\omega CR}\right)^2}} \right]$$

$$\text{Gain in dB} = \underbrace{20 \log_{10} 1}_{\text{Passband gain (} = 0 \text{ dB)}} - \underbrace{20 \log_{10} \sqrt{1 + \left(\frac{1}{\omega CR}\right)^2}}_{\text{Change in gain with } \omega \text{ (-3 dB occurs at } f_H = \frac{1}{2\pi RC})}} \text{ dB}$$

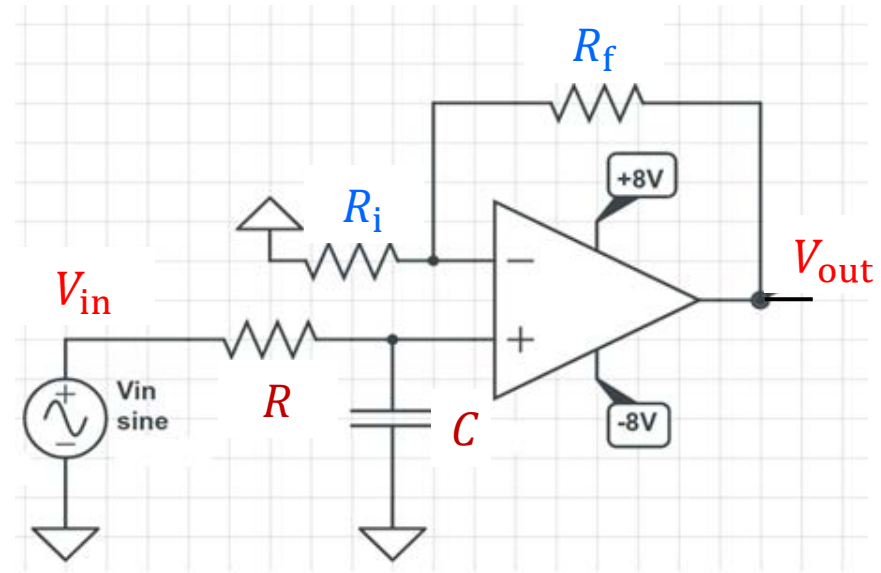


# The Need for Amplifying Signals

- Voltage output from sensors may be in the order of **mV**, e.g., microphone signals
- The sensor voltage output would need to be scaled **before A-to-D conversion** for more accurate measurements (e.g., using Arduino Uno)

# Active Low-Pass Filter

$$\frac{V_{out}}{V_{in}} = \frac{V_{out}}{V_{+}} \times \frac{V_{+}}{V_{in}} = \left(1 + \frac{R_f}{R_i}\right) \frac{V_{+}}{V_{in}}$$



$$\left| \frac{V_{out}}{V_{in}} \right| = \left(1 + \frac{R_f}{R_i}\right) \frac{1}{\sqrt{1 + (R\omega C)^2}}$$

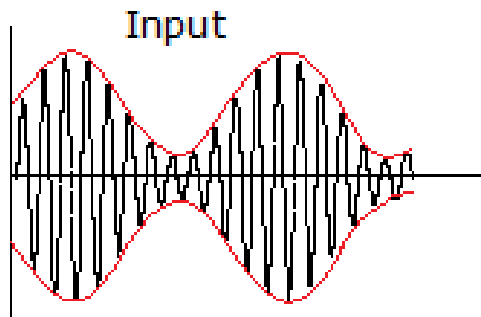
$$\text{Gain in dB} = \underbrace{20 \log_{10} \left(1 + \frac{R_f}{R_i}\right)}_{\text{Passband gain}} - \underbrace{20 \log_{10} \sqrt{1 + (\omega CR)^2}}_{\text{Change in gain with } \omega} \text{ dB}$$

Passband gain  
(= XX dB)

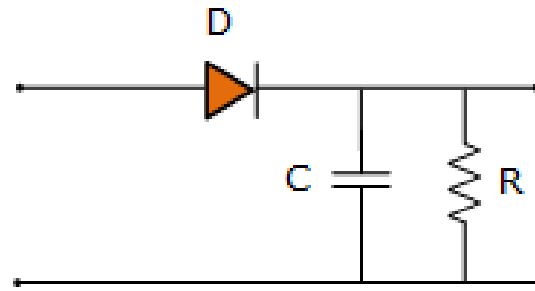
Change in gain with  $\omega$   
(-3 dB from XX dB occurs at  $f_L = \frac{1}{2\pi RC}$ )

# Envelope Detector

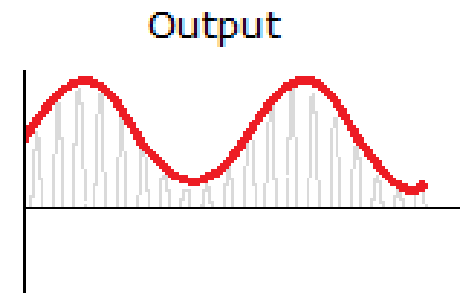
- An envelope detector is an electronic circuit that takes a high-frequency signal as input (**sound**) and provides an output which is the envelope of the original signal
- The capacitor in the circuit stores up charge on the rising edge, and releases it slowly (through the load) when signal falls



(Sound Signal)

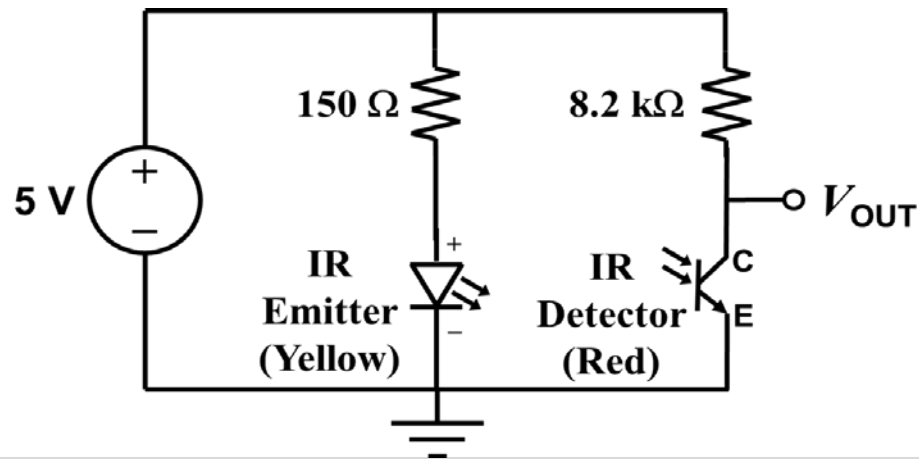


Envelope Detector

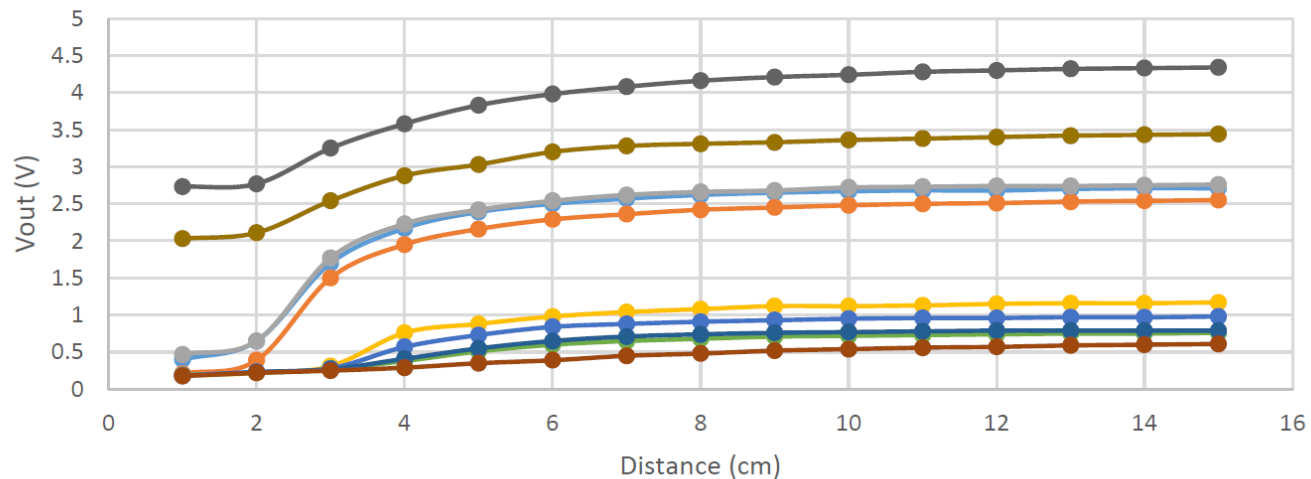


(Envelope of the Input)

# IR Proximity Sensor

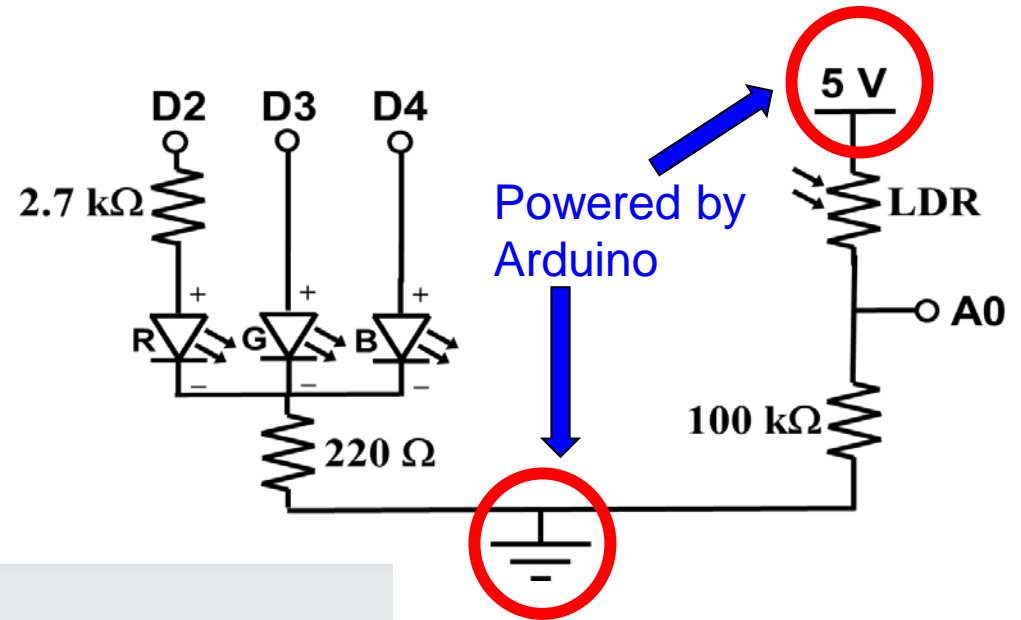
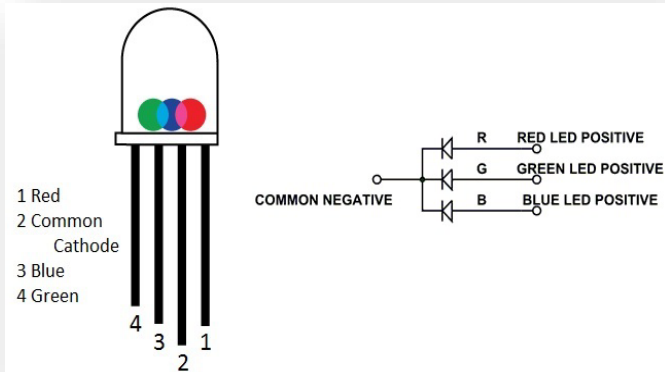


IR Proximity Sensor: Distance vs  $V_{OUT}$   
(10 sets of result from various  
locations/conditions)

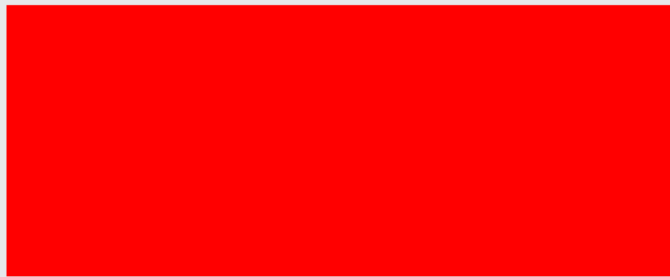




# LDR Colour Sensor



## RGB Calculator



`rgb(255, 0, 0)`

`#ff0000`

`hsl(0, 100%, 50%)`

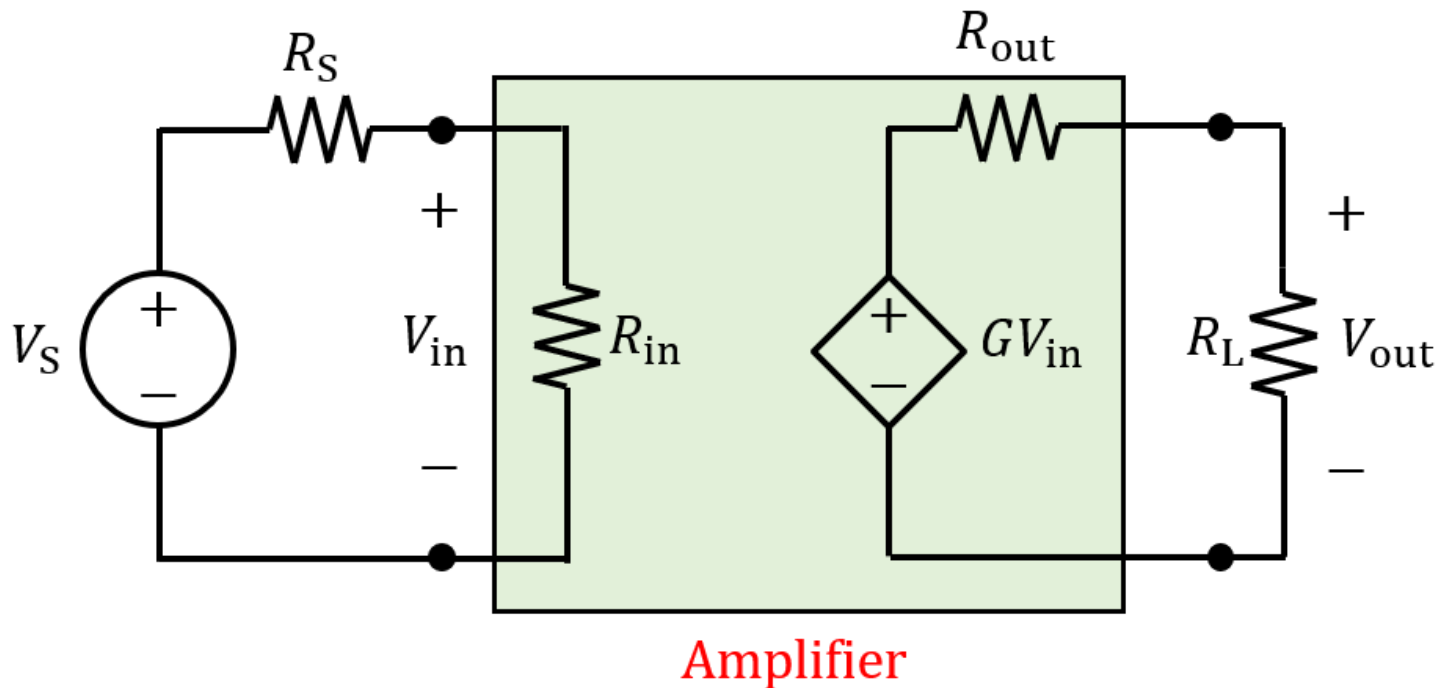


- An RGB colour value is specified with: `rgb(red, green, blue)`
- Each parameter (red, green, and blue) defines the intensity of the colour as an integer between 0 and 255

# Question 1

Show that if  $R_{in} = R_L$ , then the power gain in dB for an amplifier circuit is given by

$$\text{Power gain (dB)} = 20 \log_{10} \left| \frac{V_{out}}{V_{in}} \right| \text{ dB}$$



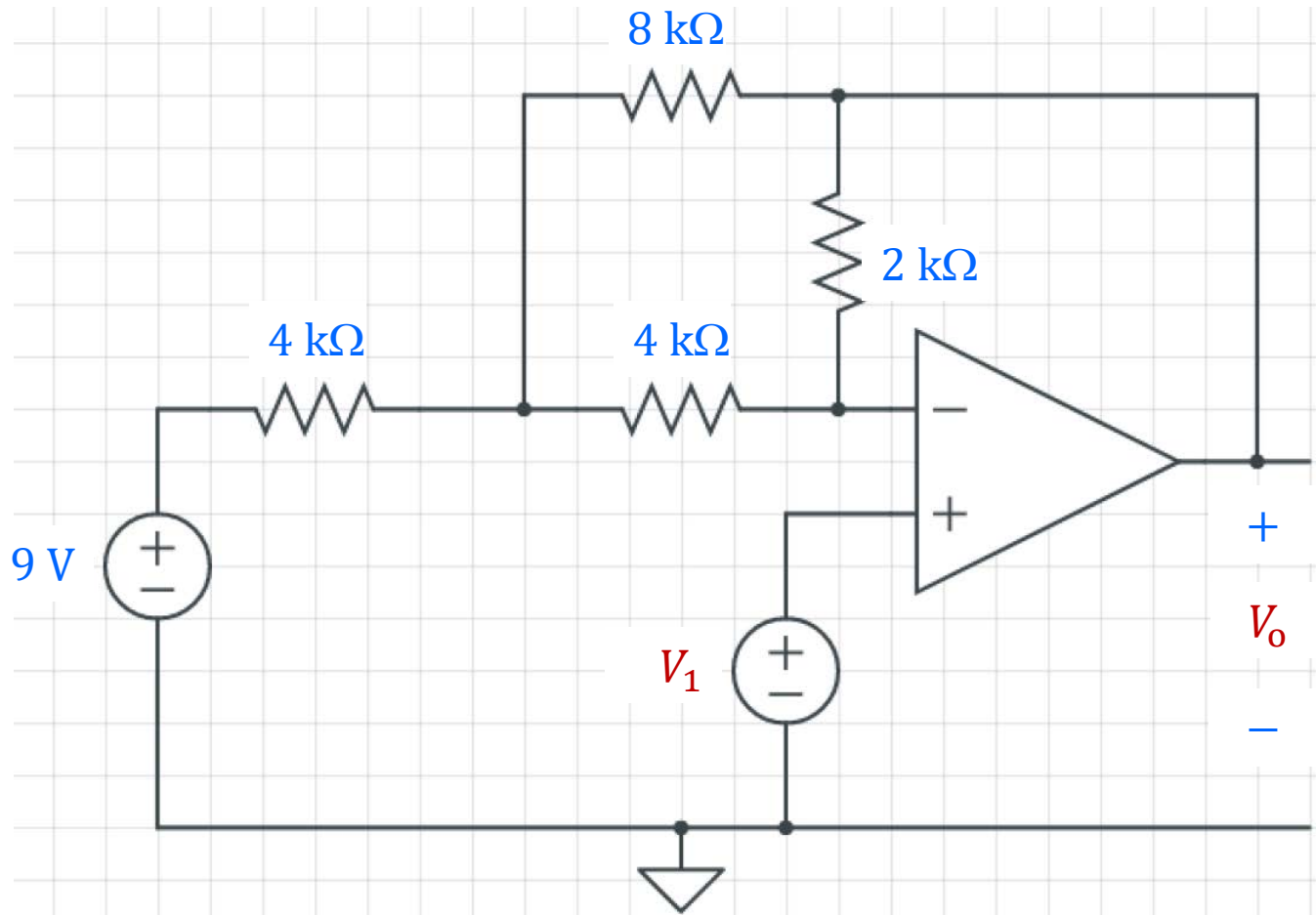
# Question 1

- Power at amplifier's input:  $P_{\text{in}} = \frac{V_{\text{in}}^2}{R_{\text{in}}}$
- Power delivered to load:  $P_{\text{out}} = \frac{V_{\text{out}}^2}{R_L}$
- Power Gain in dB

$$\begin{aligned} &= 10 \log_{10} \left( \frac{P_{\text{out}}}{P_{\text{in}}} \right) \\ &= 10 \log_{10} \left( \frac{V_{\text{out}}}{V_{\text{in}}} \right)^2 + \underbrace{10 \log_{10} \left( \frac{R_{\text{in}}}{R_L} \right)}_{\substack{\text{Equals 0 if} \\ R_{\text{in}} = R_L}} \\ &= 20 \log_{10} \left| \frac{V_{\text{out}}}{V_{\text{in}}} \right| \end{aligned}$$

## Question 2

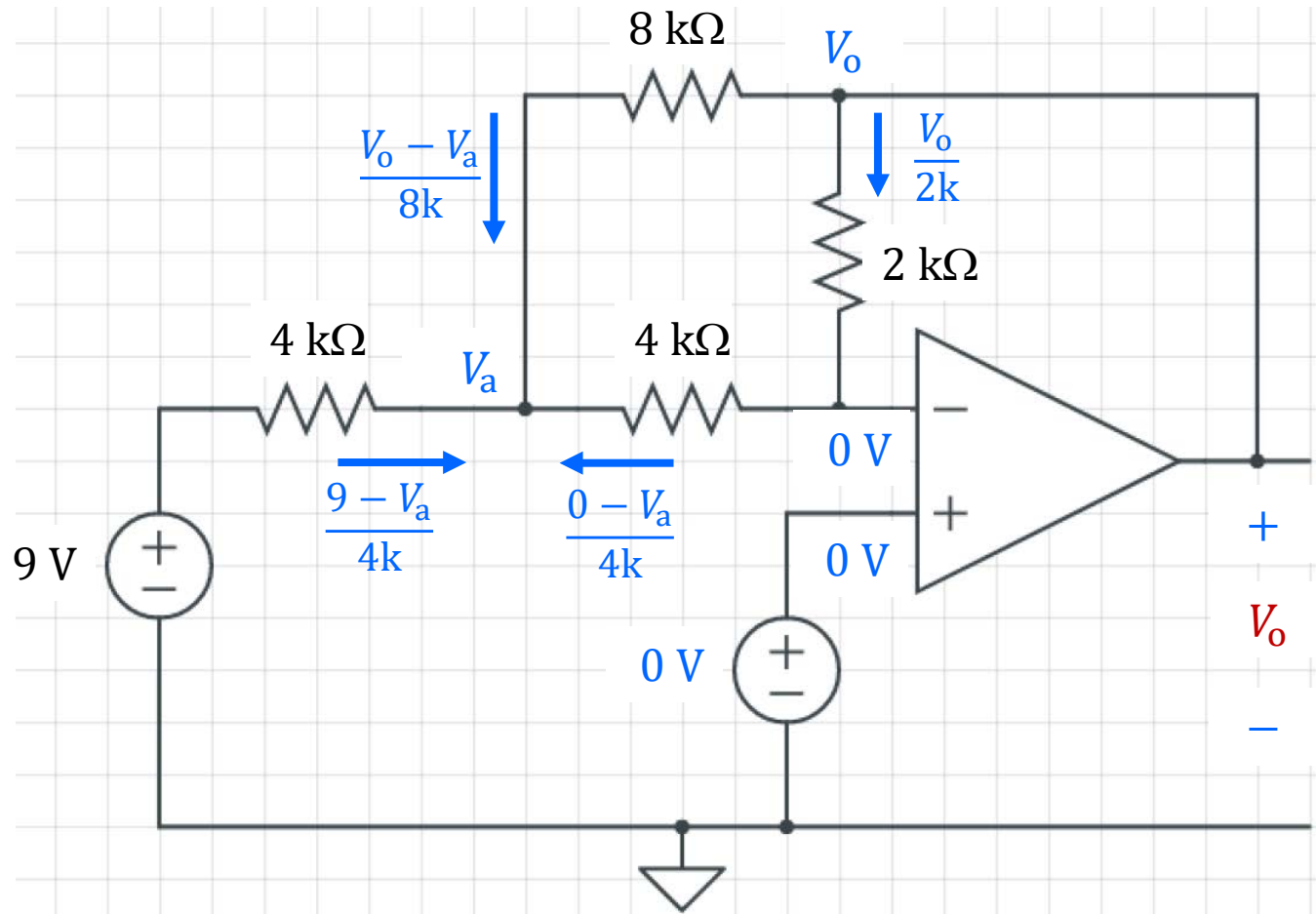
- Calculate  $V_o$  in the circuit if  $V_1 = 0$



# Question 2

$$\frac{9 - V_a}{4k} + \frac{V_o - V_a}{8k} + \frac{0 - V_a}{4k} = 0$$

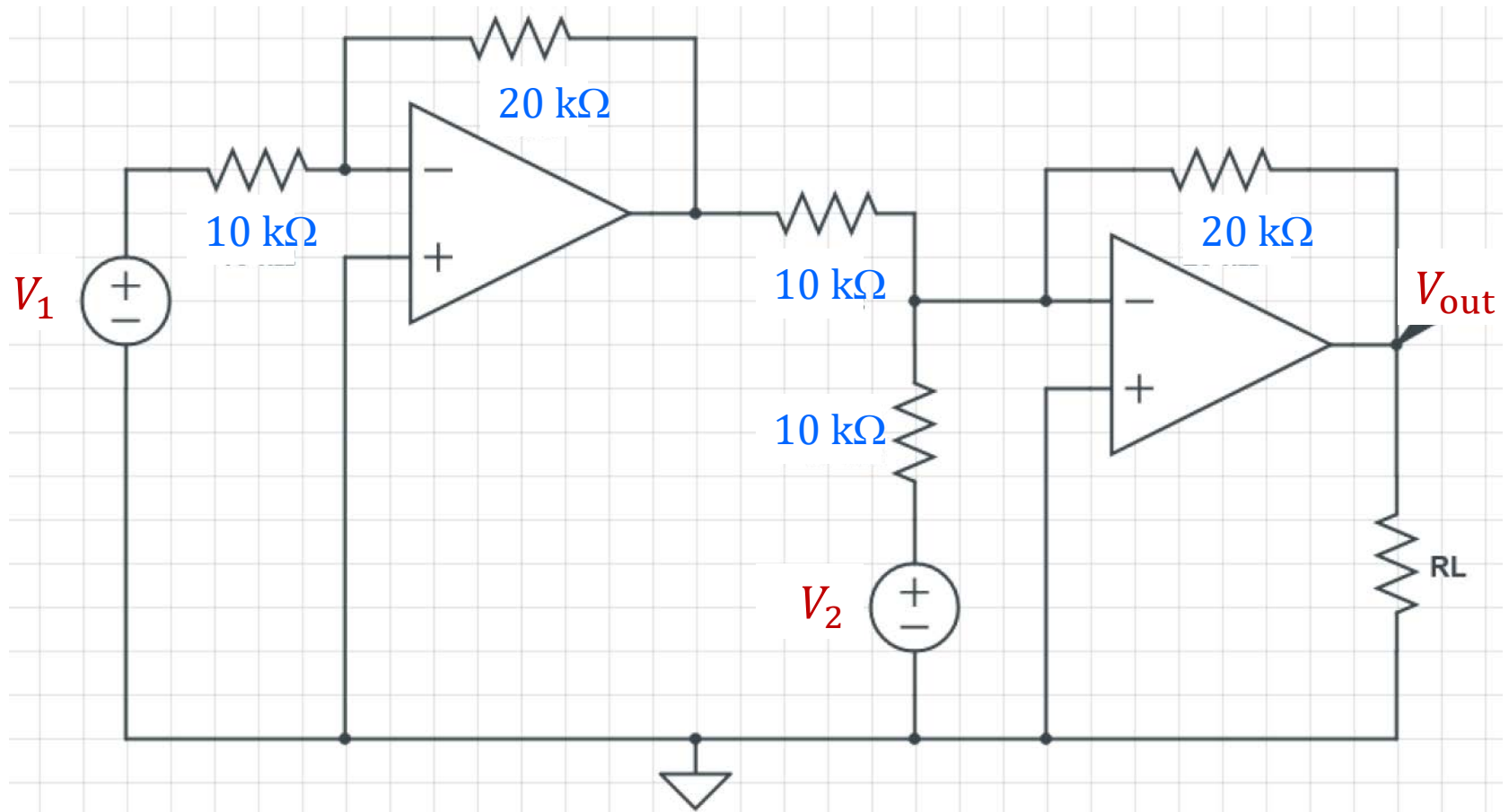
$$\frac{V_o}{2k} + \frac{V_a - 0}{4k} = 0 \rightarrow V_a = -2V_o$$



Solving,  
 $V_o = -1.64 \text{ V}$

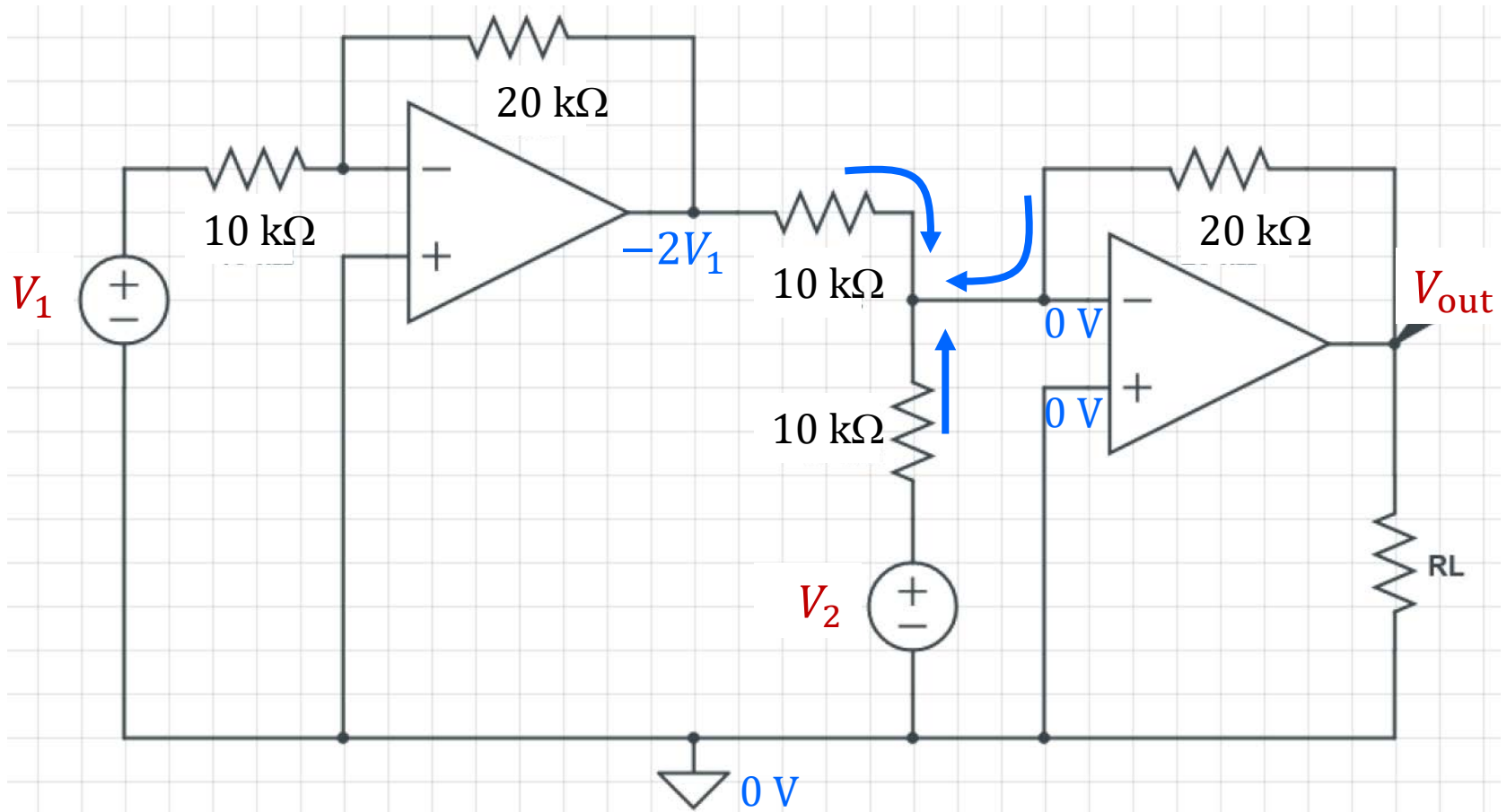
# Question 3

- Find an expression for  $V_{out}$  (in terms of  $V_1$  and  $V_2$ )



# Question 3

$$\frac{-2V_1 - 0}{10k} + \frac{V_2 - 0}{10k} + \frac{V_{out} - 0}{20k} = 0 \rightarrow V_{out} = 4V_1 - 2V_2$$

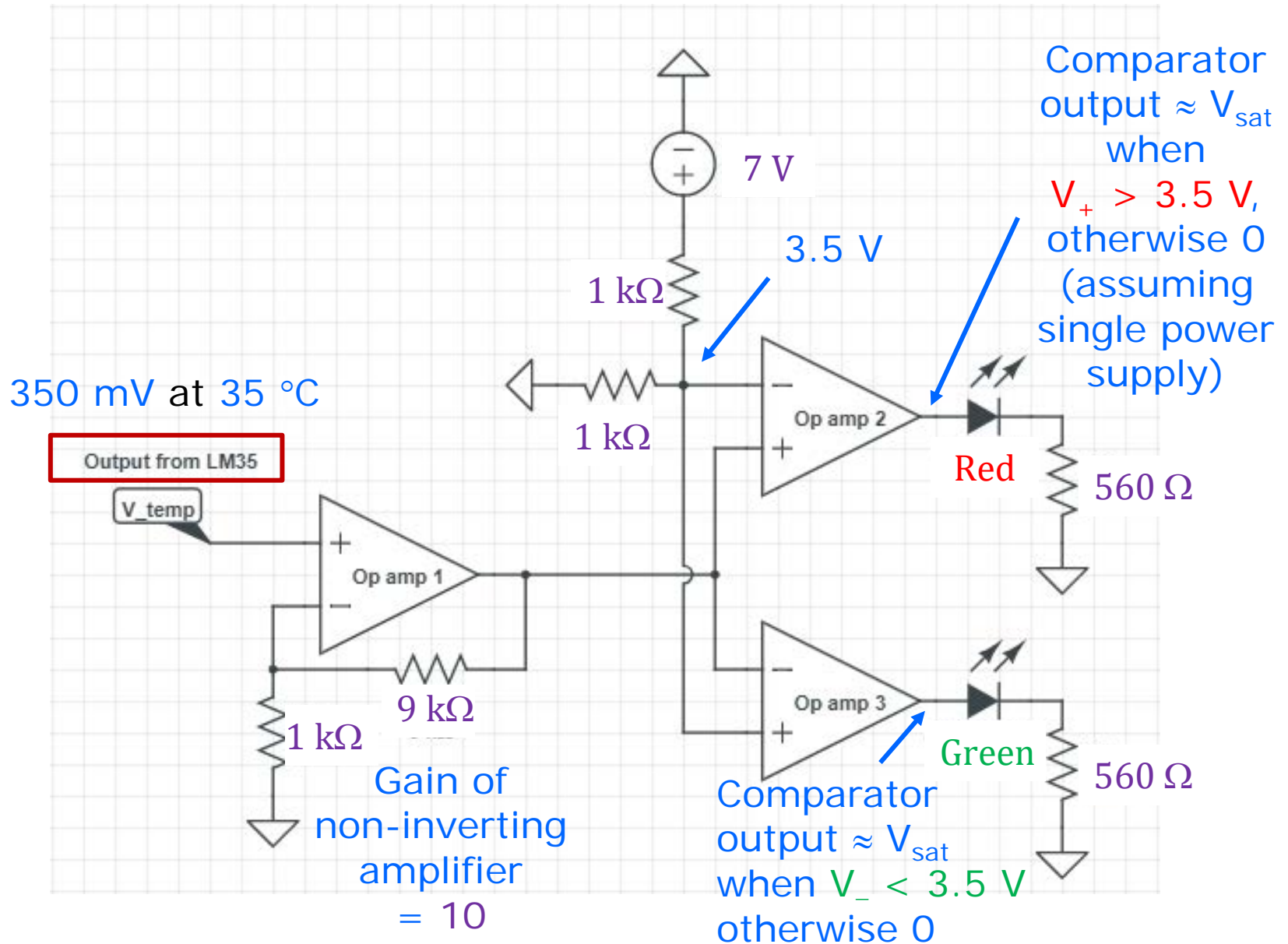


# Question 4

- Design a temperature sensing circuit using LM35 (temperature sensor IC), Op amps, resistors, and LEDs
- LM35 output = 250 mV at 25 °C
- LM35 output varies as 10 mV/°C
- Temperature below 35 °C, GREEN LED on
- Temperature above 35 °C, RED LED on



# Question 4



# Question 4

- Op Amp 1 – closed loop gain of 10
- Op Amps 2 & 3 are comparators with reference voltage of 3.5 V
  - Op Amp 2 – non-inverting comparator
  - Op Amp 3 – inverting comparator
- When output of op-amp 1 is more than 3.5 V (i.e., when temperature > 35 °C), Red LED is turned on
- When output of op-amp 1 is less than 3.5 V (i.e., when temperature < 35 °C), Green LED is turned on

# Question 5

- Suppose:
  - An audio clip: 100-3000 Hz
  - Corrupted with 10 kHz noise
  - Signal very soft
- Desired outcome:
  - Active** LPF with passband gain of 6 dB
  - Suppress** the **10 kHz noise** by 20 dB relative to the passband gain
- What is the **cut-off frequency** of the low-pass filter?

# A Note About –20 dB in Power

- Suppressing the noise by 20 dB is equivalent to reducing its **power** to just **1%** compared to no filtering
- Also equivalent to reducing its **voltage** to just **10%** compared to no filtering

- $10 \log_{10} \left( \frac{P_{\text{noise(filtered)}}}{P_{\text{noise(no filter)}}} \right) = 10 \log_{10}(0.01) = -20 \text{ dB}$

- $20 \log_{10} \left( \frac{V_{\text{noise(filtered)}}}{V_{\text{noise(no filter)}}} \right) = 20 \log_{10}(0.1) = -20 \text{ dB}$

# Question 5

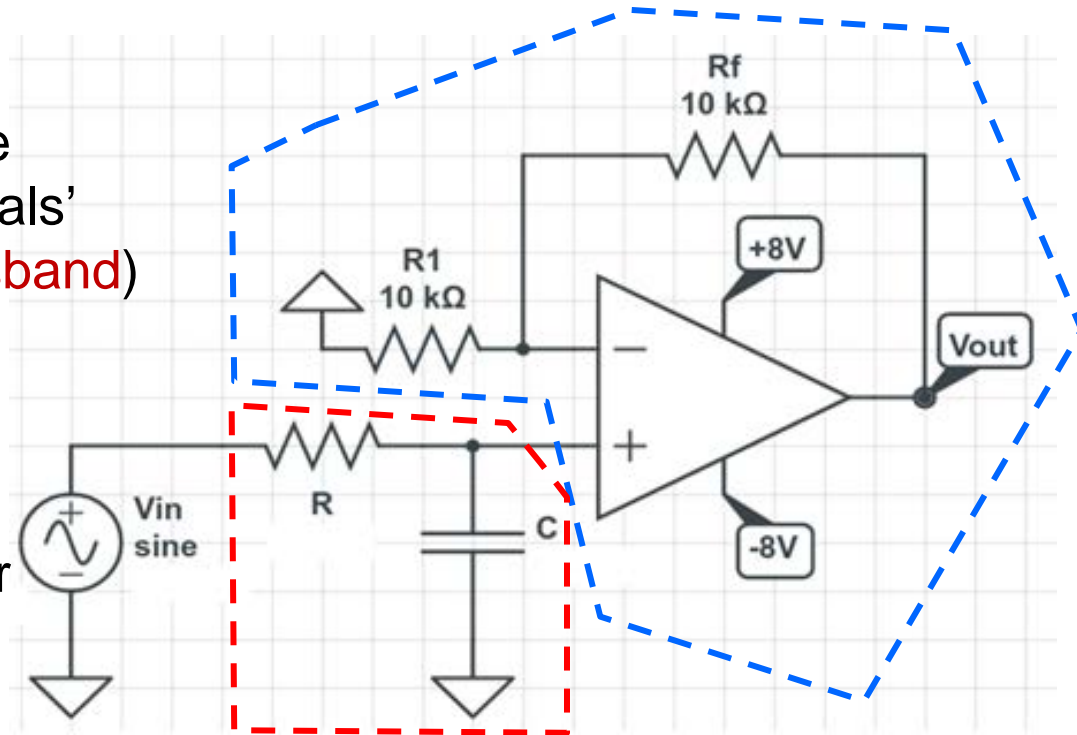
Active low-pass filter  
(i.e., amplifies entire signal while suppressing high frequency signals' power relative to signals in passband)

Blue:

Active gain  
(= 2, i.e., 6 dB)  
due to non-inverting amplifier

Red:

Passive filter's gain due to RC potential divider ( $\omega$ -dependent)



$$\frac{V_{out}}{V_{in}} = \frac{V_{out}}{V_{+}} \times \frac{V_{+}}{V_{in}} = \left(1 + \frac{R_f}{R_1}\right) \frac{V_{+}}{V_{in}} = 2 \left[ \frac{\frac{1}{j\omega C}}{\frac{1}{j\omega C} + R} \right] = \frac{2}{1 + j\omega CR}$$

Hence, gain's magnitude w.r.t.  $\omega = \left| \frac{V_{out}}{V_{in}} \right| = \frac{2}{\sqrt{1 + (\omega CR)^2}}$

# Question 5

$$\text{Gain in dB} = \overbrace{20 \log_{10} 2}^{\text{Passband gain}} - \overbrace{20 \log_{10} \sqrt{1 + (\omega CR)^2}}^{\text{Change in gain with } \omega} \text{ dB}$$

A gain reduction of 20 dB at  $f = 10 \text{ kHz}$  means:

$$\left. -20 \log_{10} \sqrt{1 + (\omega CR)^2} \right|_{f = 10 \text{ kHz}} = -20 \text{ dB}$$

Hence,  $\sqrt{1 + (\omega CR)^2} = 10$  when  $f = 10 \text{ kHz}$

Our low-pass filter needs to have:

$$RC = \frac{\sqrt{10^2 - 1}}{2\pi \times 10000} = 1.584 \times 10^{-4} \text{ s}$$

Choose  
some  $RC$   
combination  
that has this  
value

# Question 5

- Cutoff frequency is the frequency at which the gain decreases by 3 dB from passband gain
- A gain reduction of 3 dB at  $f = f_c$  means:  
$$\left. -20 \log_{10} \sqrt{1 + (\omega CR)^2} \right|_{f = f_c} = -3 \text{ dB}$$
- Hence,  $\sqrt{1 + (\omega CR)^2} = 10^{3/20} = \sqrt{2}$  at  $f = f_c$

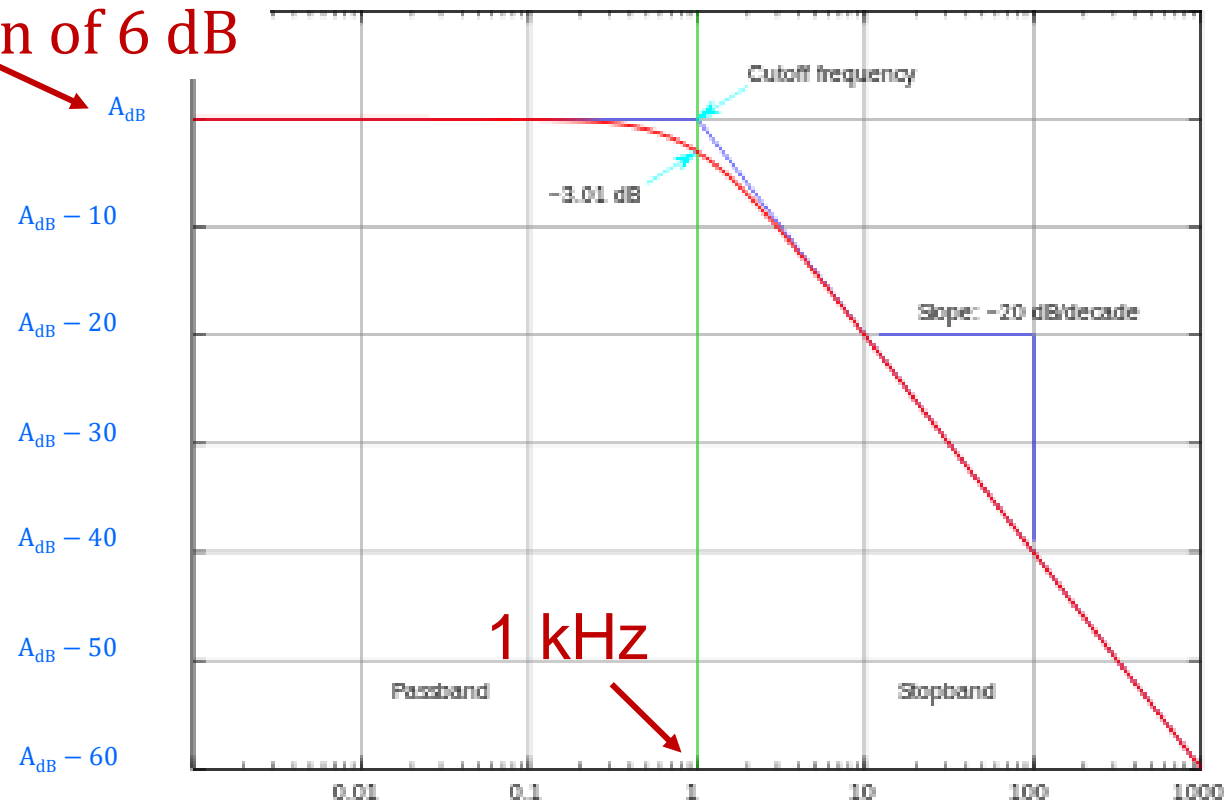
$$\omega CR = 1 \text{ at } f = f_c$$

Since  $\omega = 2\pi f$ , we have  $f_c = \frac{1}{2\pi RC} = \frac{1}{2\pi \times 1.584 \times 10^{-4}} \approx 1 \text{ kHz}$

# Graphical Visualization for Q5

- First-order low-pass filter:  $-20$  dB/decade
- Each horizontal box is "1 decade" ↗

DC gain of 6 dB ↗

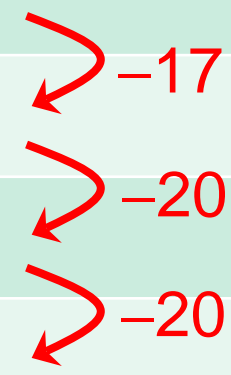


i.e.,  
frequency  
changes by  
10 times



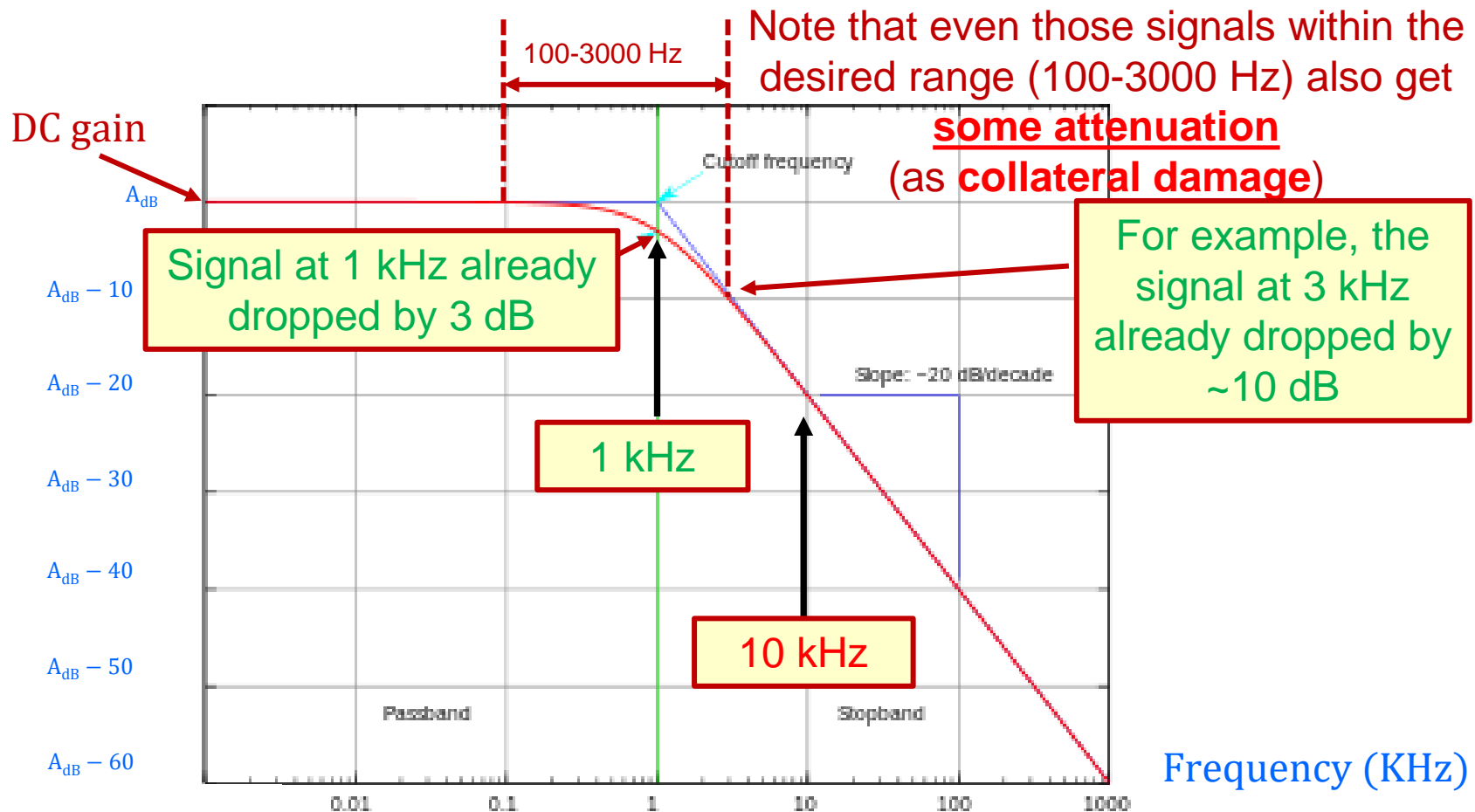
# Why $-20$ dB/decade?

| $f$               | $-20 \log_{10} \sqrt{1 + (\omega CR)^2}$ |
|-------------------|--|
| $f_c$             | $\approx -3$ dB                          |
| $10 \times f_c$   | $\approx -20$ dB                         |
| $100 \times f_c$  | $\approx -40$ dB                         |
| $1000 \times f_c$ | $\approx -60$ dB                         |



# Graphical Visualization for Q5

- If 10 kHz noise has to be reduced by 20 dB, we need to have the cutoff frequency at 1 kHz



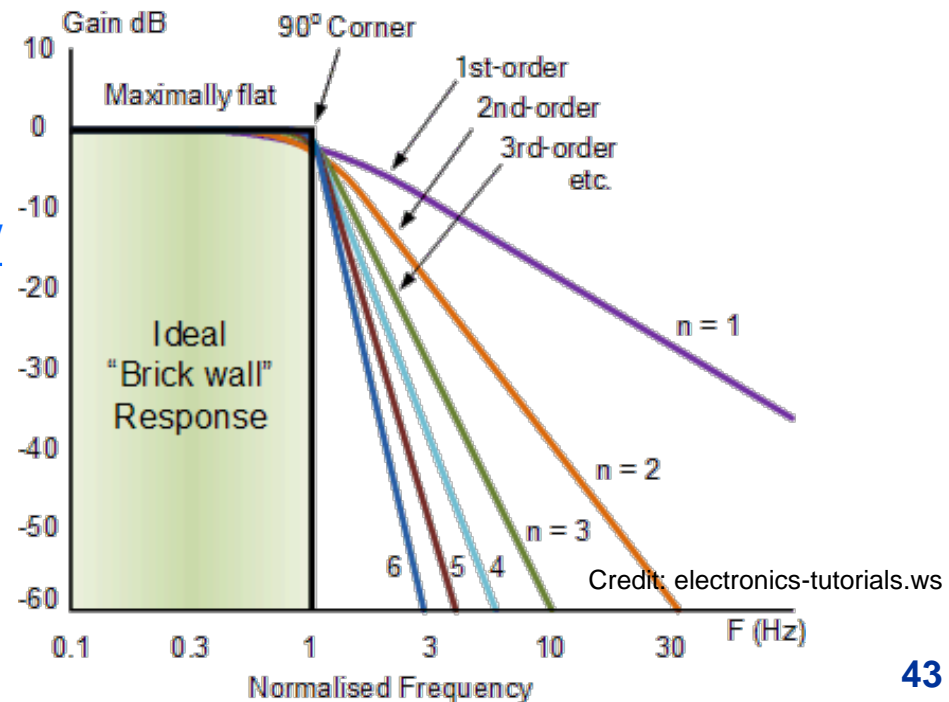
# Extra Points to Note for Q5

For your curiosity only:

As can be seen, with a first-order filter, we also **lose some audio signals** that we desire. How do we improve this?

We can use **higher-order filters**! This allows us to have **sharper attenuation slope**, so that our desired **passband** is not attenuated too much!

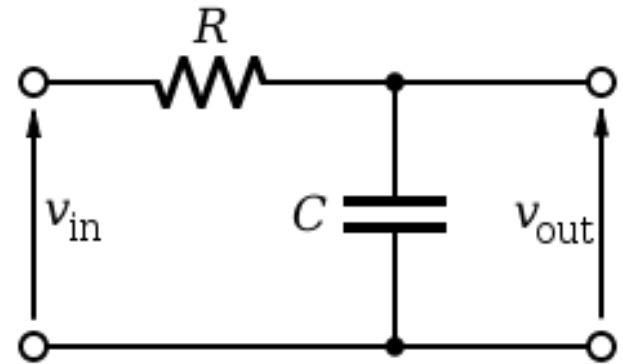
- **2<sup>nd</sup> order**: **40 dB/decade**
  - <http://www.electronics-tutorials.ws/filter/second-order-filters.html>
- **3<sup>rd</sup> order**: **60 dB/decade**
  - <http://www.circuitstoday.com/higher-order-filters>



# Question 6

- Design a passive LPF to suppress **12 kHz** noise by at least **15 dB**

$$\rightarrow V_{\text{out}} = \left[ \frac{\frac{1}{j\omega C}}{\frac{1}{j\omega C} + R} \right] V_{\text{in}}$$



$$\rightarrow \frac{V_{\text{out}}}{V_{\text{in}}} = \left[ \frac{\frac{1}{j\omega C}}{\frac{1}{j\omega C} + R} \right] = \left[ \frac{1}{1 + jR\omega C} \right] = \frac{1 \angle 0^\circ}{\sqrt{1^2 + (R\omega C)^2} \angle \theta^\circ}$$

$$\rightarrow \underbrace{\left| \frac{V_{\text{out}}}{V_{\text{in}}} \right|}_{\text{Magnitude}} = \left[ \frac{1}{\sqrt{1 + (R\omega C)^2}} \right] \rightarrow \underbrace{20 \log_{10} 1}_{\text{Passband gain (} = 0 \text{ dB)}} - \underbrace{20 \log_{10} \sqrt{1 + (R\omega C)^2}}_{\text{Change in gain with } \omega \text{ (we want } -15 \text{ dB at } 12 \text{ kHz)}} \text{ dB}$$

## Question 6

A gain reduction of 15 dB at  $f=12$  kHz means:

$$\left. -20 \log_{10} \sqrt{1 + (\omega CR)^2} \right|_{f = 12 \text{ kHz}} = -15 \text{ dB}$$

Hence,  $\sqrt{1 + (\omega CR)^2} = 10^{15/20}$  when  $f = 12$  kHz

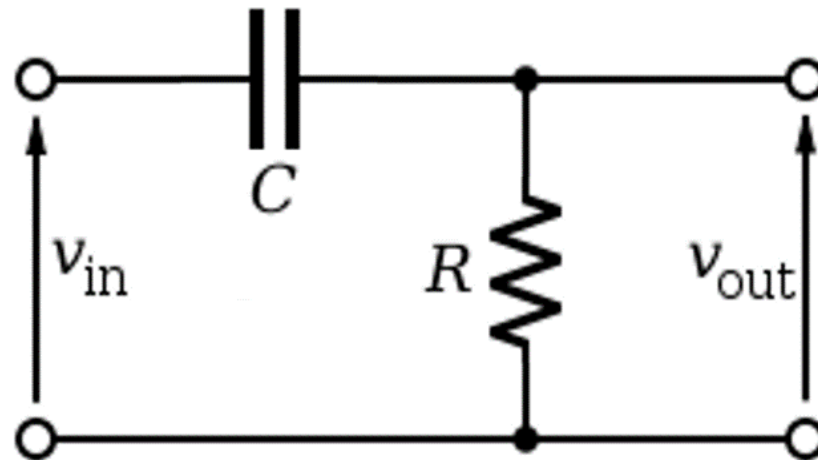
Our low-pass filter needs to have:

$$RC = \frac{\sqrt{10^{(15/20)^2} - 1}}{2\pi \times 12000} = 73.4 \text{ } \mu\text{s}$$

If we choose  $C = 10$  nF, we get  $R = 7.34$  k $\Omega$

# Question 7

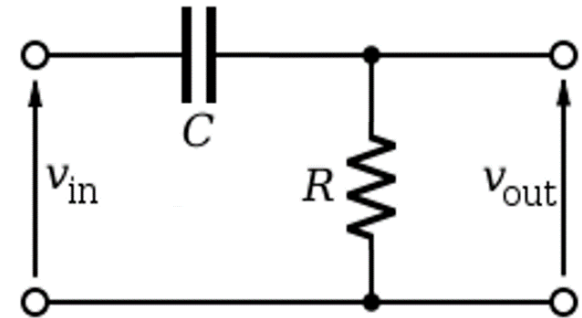
For the following passive first-order **high-pass filter**, show that its **cutoff frequency** is given by  $f_H = \frac{1}{2\pi CR}$



# Question 7

- Using **voltage divider rule** to find the **voltage gain**:

$$\rightarrow V_{\text{out}} = \left[ \frac{R}{R + \frac{1}{j\omega C}} \right] V_{\text{in}}$$



$$\rightarrow \frac{V_{\text{out}}}{V_{\text{in}}} = \left[ \frac{R}{R + \frac{1}{j\omega C}} \right] = \left[ \frac{1}{1 - \frac{j}{\omega CR}} \right] = \frac{1 \angle 0^\circ}{\sqrt{1^2 + \left( \frac{1}{\omega CR} \right)^2} \angle \theta^\circ}$$

$$\rightarrow \left| \frac{V_{\text{out}}}{V_{\text{in}}} \right| = \left[ \frac{1}{\sqrt{1 + \left( \frac{1}{\omega CR} \right)^2}} \right] \rightarrow \underbrace{20 \log_{10} 1}_{\text{Passband gain (} = 0 \text{ dB)}} - \underbrace{20 \log_{10} \sqrt{1 + \left( \frac{1}{\omega CR} \right)^2}}_{\text{Change in gain with } \omega \text{ (-3 dB occurs at } f_H \text{)}} \text{ dB}$$

Magnitude

## Question 7

A gain reduction of 3 dB at  $f = f_H$  means:

$$\left. -20 \log_{10} \sqrt{1 + \left( \frac{1}{\omega CR} \right)^2} \right|_{f=f_H} = -3 \text{ dB}$$

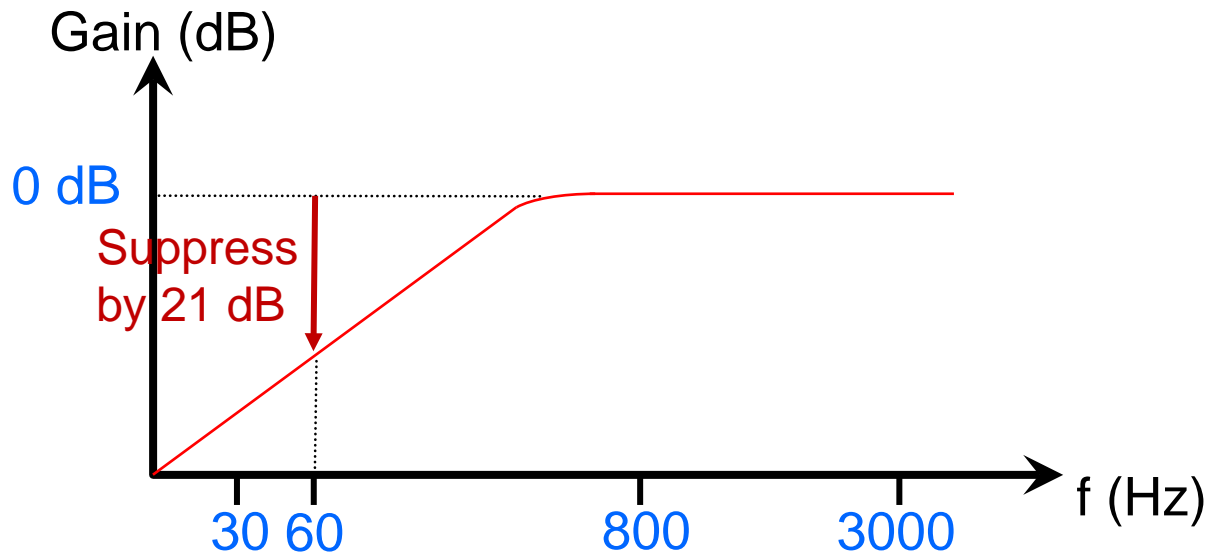
Hence,  $\sqrt{1 + \left( \frac{1}{\omega CR} \right)^2} = 10^{3/20} = \sqrt{2}$  at  $f = f_H$ ,

which gives  $\frac{1}{\omega CR} = \frac{1}{2\pi f_H CR} = 1 \rightarrow f_H = \frac{1}{2\pi CR}$



# Question 8

- Low frequency humming from the airplane's engine: 30 – 60 Hz
- Electronic dance music: 800 – 3000 Hz
- Design a high-pass filter to suppress the humming by at least 21 dB



# Question 8

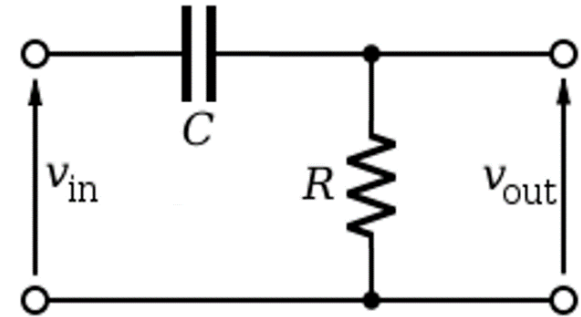
- We will focus on the **passive** filter. If need be, a non-inverting amplifier can be cascaded to boost the gain.

$$\left| \frac{V_{\text{out}}}{V_{\text{in}}} \right| = \left[ \frac{1}{\sqrt{1 + \left( \frac{1}{\omega CR} \right)^2}} \right]$$

$$\rightarrow 20 \log_{10} 1 - 20 \log_{10} \sqrt{1 + \left( \frac{1}{\omega CR} \right)^2} \text{ dB}$$

Passband gain  
(= 0 dB)

Change in gain with  $\omega$   
(we want **-21 dB** at **60 Hz**)



## Question 8

Hence,

$$-20 \log_{10} \sqrt{1 + \left( \frac{1}{\omega CR} \right)^2} \Big|_{f=60 \text{ Hz}} = -21 \text{ dB}$$

$$\sqrt{1 + \left( \frac{1}{\omega CR} \right)^2} = 10^{21/20} \text{ when } f = 60 \text{ Hz,}$$

$$\text{which gives } \frac{1}{\omega CR} = \frac{1}{2\pi(60)CR} = 11.176$$

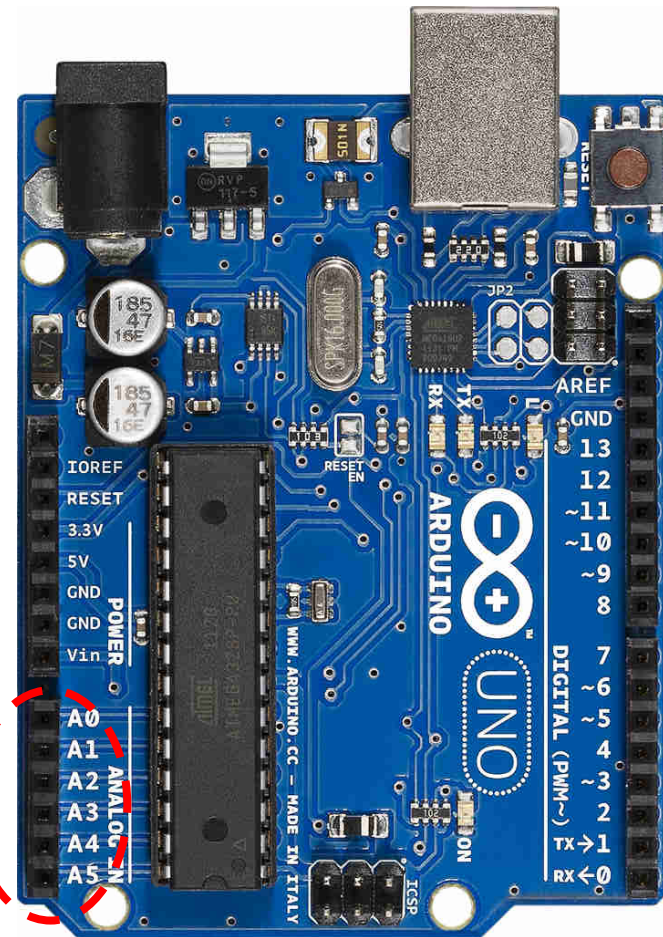
$$\text{Cutoff frequency of filter} = \frac{1}{2\pi CR} = 670.5 \text{ Hz}$$

# Question 9

- Pressure sensor:  $p = 250 \left( \frac{V_{out}}{V_{cc}} \right) - 25$ , where  $V_{cc} = 5 \text{ V}$
- Max pressure in setup: 10 PSI
- How to amplify signal before sampling to make good use of Arduino Uno's ADC input range of 0 – 5 V for better accuracy?

ADC input  
range: 0 – 5 V

ADC Output:  
0 – 1023



# Question 9

- Since max pressure is 10 PSI, we have

$$10 = 250 \left( \frac{V_{\text{out}}}{5} \right) - 25$$

- Solving, we get max  $V_{\text{out}} = 0.7 \text{ V}$
- To make good use of the ADC's input range of  $0 - 5 \text{ V}$ , we need a gain of  $\frac{5}{0.7} = 7.14$
- We can pick a non-inverting amplifier with

$$\frac{R_f}{R_i} = 7.14 - 1 = 6.14$$

# Question 10

- HIH-4030 humidity sensor IC chip
- $V_{\text{out}}$  varies by 30.68 mV/RH% change
- At 0% RH,  $V_{\text{out}} = 0.958 \text{ V}$
- Design a humidity sensing circuit using HIH-4030, op-amp, and Arduino Uno

# Question 10

- At 100% RH,  $V_{\text{out}} = 0.958 \text{ V} + 0.03068 \times 100 = 4.026 \text{ V}$
- We can amplify  $V_{\text{out}}$  to the range of  $0 - 5 \text{ V}$  before sampling it using Arduino Uno, using a non-inverting amplifier with a gain of  $\frac{5}{4.026} = 1.242$

