

# Filter Design Assignment

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## Contents

<b>1</b>	<b>First Filter Specifications</b>	<b>2</b>
1.1	Un-normalized Discrete Time Filter Specifications . . . . .	2
1.2	Normalized Digital Filter Specifications . . . . .	2
1.3	Analog Filter Specifications . . . . .	2
1.4	Frequency transformation to be employed . . . . .	2
1.5	Frequency transformed lowpass analog filter specifications . . . . .	2
1.6	The analog Low pass Transfer Function . . . . .	3
1.7	The Analog BandPass Transfer Function . . . . .	3
1.8	The Discrete Time Filter Transfer Function . . . . .	4
1.9	Direct Form 2 Realization of the Discrete Filter . . . . .	5
1.10	FIR Filter Transfer Function to get the same specifications . . . . .	5
<b>2</b>	<b>Second Filter Specifications</b>	<b>7</b>
2.1	Un-normalized Discrete Time Filter Specifications . . . . .	7
2.2	Normalized Digital Filter Specifications . . . . .	7
2.3	Analog Filter Specifications . . . . .	7
2.4	Frequency transformation to be employed . . . . .	7
2.5	Frequency transformed lowpass analog filter specifications . . . . .	8
2.6	The analog Low pass Transfer Function . . . . .	8

# 1 First Filter Specifications

## 1.1 Un-normalized Discrete Time Filter Specifications

- Sampling Frequency ( $f_s$ ) = 140kHz
- $B_L = 9.4kHz$
- $B_H = 14.4kHz$
- Monotonic Passband (Butterworth)

## 1.2 Normalized Digital Filter Specifications

- $\omega_{p1} = \frac{9.4}{140} 2\pi = 0.4219$
- $\omega_{p2} = \frac{14.4}{140} 2\pi = 0.6463$
- $\omega_{s1} = \frac{8.4}{140} 2\pi = 0.3770$
- $\omega_{s2} = \frac{15.4}{140} 2\pi = 0.6912$

## 1.3 Analog Filter Specifications

- $\Omega_{p1} = \tan(\frac{\omega_{p1}}{2}) = 0.2141$
- $\Omega_{p2} = \tan(\frac{\omega_{p2}}{2}) = 0.3349$
- $\Omega_{s1} = \tan(\frac{\omega_{s1}}{2}) = 0.1908$
- $\Omega_{s2} = \tan(\frac{\omega_{s2}}{2}) = 0.3600$

## 1.4 Frequency transformation to be employed

$$s_L = \frac{s^2 + \Omega_0^2}{Bs} \quad (1)$$

with  $B = \Omega_{p2} - \Omega_{p1} = 0.1208$  and  $\Omega_0 = \sqrt{\Omega_{p1}\Omega_{p2}} = 0.2678$   
This translates to

$$\Omega_L = \frac{\Omega^2 - \Omega_0^2}{B\Omega} \quad (2)$$

## 1.5 Frequency transformed lowpass analog filter specifications

From 2

- $\Omega_{Lp} = 1$
- $\Omega_{Ls} = \min(\Omega_{Ls1}, \Omega_{Ls2}) = 1.3321$

## 1.6 The analog Low pass Transfer Function

```
H_s_L =

              1
-----
0.4533 s^11 + 3.423 s^10 + 12.92 s^9 + 32.07 s^8 + 57.98 s^7 + 80.04 s^6 + 86.01 s^5 + 71.95 s^4 + 45.95 s^3 + 21.38 s^2 + 6.539 s + 1

Continuous-time transfer function.
```

Figure 1: Analog Low Pass Transfer Function

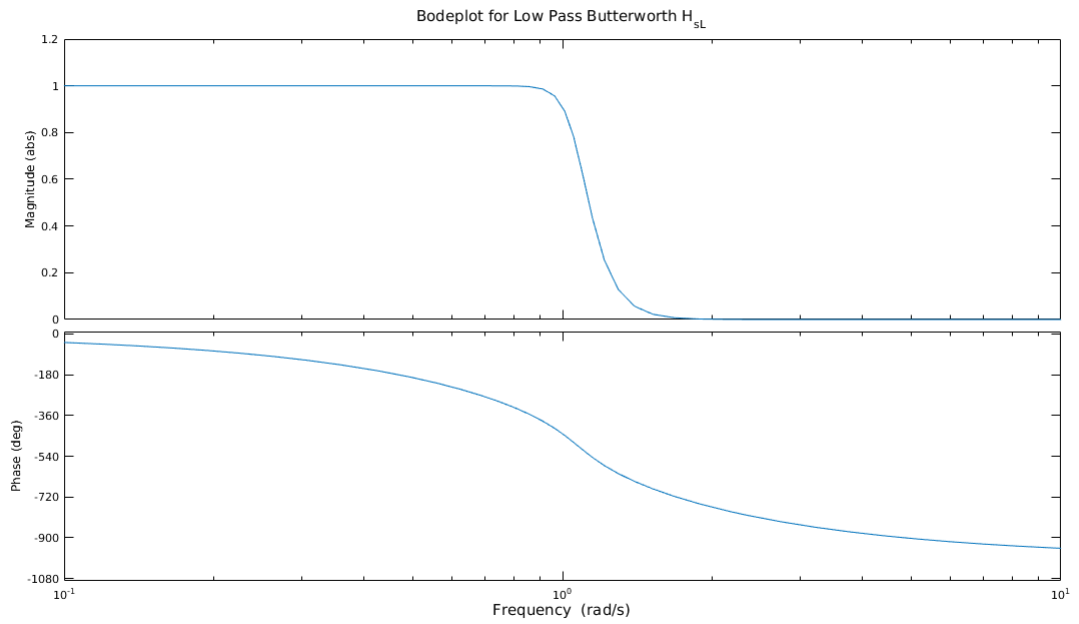


Figure 2: Analog Low Pass Bode plot

## 1.7 The Analog BandPass Transfer Function

```
H_s_bp =

              7.959e-11 s^11
-----
0.4533 s^22 + 0.4133 s^21 + 0.5459 s^20 + 0.3528 s^19 + 0.2621 s^18 + 0.1301 s^17 + 0.0689 s^16 + 0.02732 s^15 + 0.01122 s^14
+ 0.003626 s^13 + 0.001198 s^12 + 0.0003179 s^11 + 8.587e-05 s^10 + 1.864e-05 s^9 + 4.135e-06 s^8 + 7.222e-07 s^7 + 1.306e-07 s^6
+ 1.768e-08 s^5 + 2.554e-09 s^4 + 2.465e-10 s^3 + 2.735e-11 s^2 + 1.485e-12 s + 1.168e-13

Continuous-time transfer function.
```

Figure 3: Analog Band Pass Transfer Function

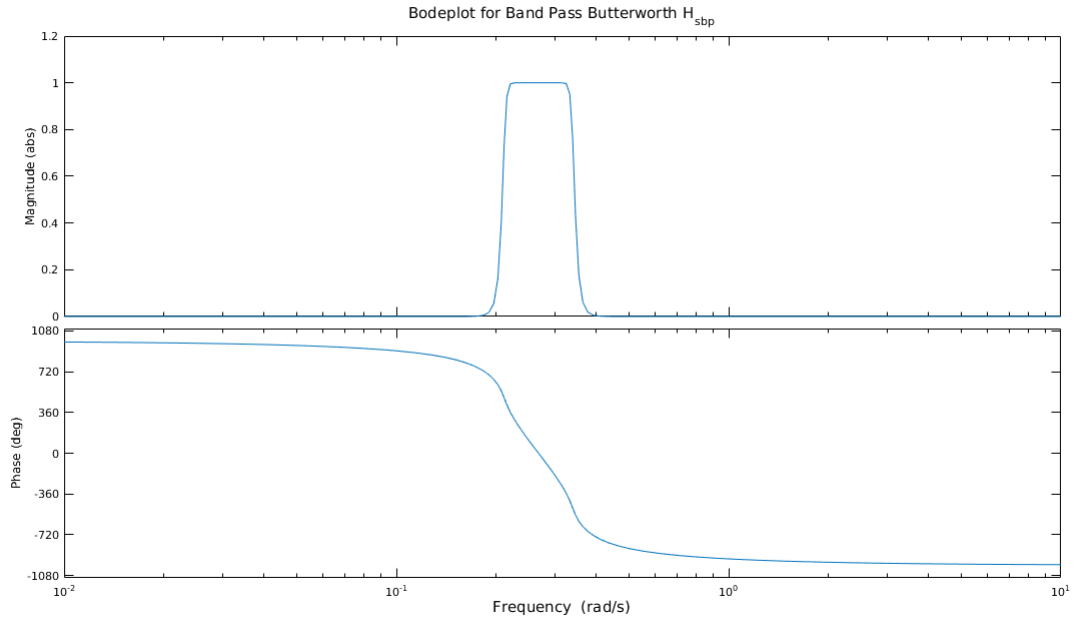


Figure 4: Analog Band Pass Bode Plot

## 1.8 The Discrete Time Filter Transfer Function

```
H_z_bp_actual =

3.506e-11 + 2.132e-14 z^-1 - 3.86e-10 z^-2 + 2.501e-12 z^-3 + 1.916e-09 z^-4 + 4.729e-11 z^-5 - 5.919e-09 z^-6 + 2.983e-10 z^-
-7 + 1.099e-08 z^-8 + 9.459e-10 z^-9 - 1.746e-08 z^-10 + 1.368e-09 z^-11 + 1.487e-08 z^-12 + 1.062e-09 z^-13 - 1.23e-08 z^-14
+ 4.184e-10 z^-15 + 5.588e-09 z^-16 + 7.458e-11 z^-17 - 1.951e-09 z^-18 + 5.372e-12 z^-19 + 3.847e-10 z^-20 + 9.726e-14 z^-21
- 3.506e-11 z^-22

.....

1 - 17.59 z^-1 + 150 z^-2 - 824.9 z^-3 + 3279 z^-4 - 1.002e04 z^-5 + 2.444e04 z^-6 - 4.874e04 z^-7 + 8.081e04 z^-8 - 1.126e05 z^-9
+ 1.329e05 z^-10 - 1.333e05 z^-11 + 1.139e05 z^-12 - 8.269e04 z^-13 + 5.083e04 z^-14 - 2.627e04 z^-15 + 1.129e04 z^-16
- 3966 z^-17 + 1112 z^-18 - 239.7 z^-19 + 37.36 z^-20 - 3.754 z^-21 + 0.1829 z^-22

Sample time: 7.1429e-06 seconds
Discrete-time transfer function.
```

Figure 5: Discrete Time Band Pass Transfer Function

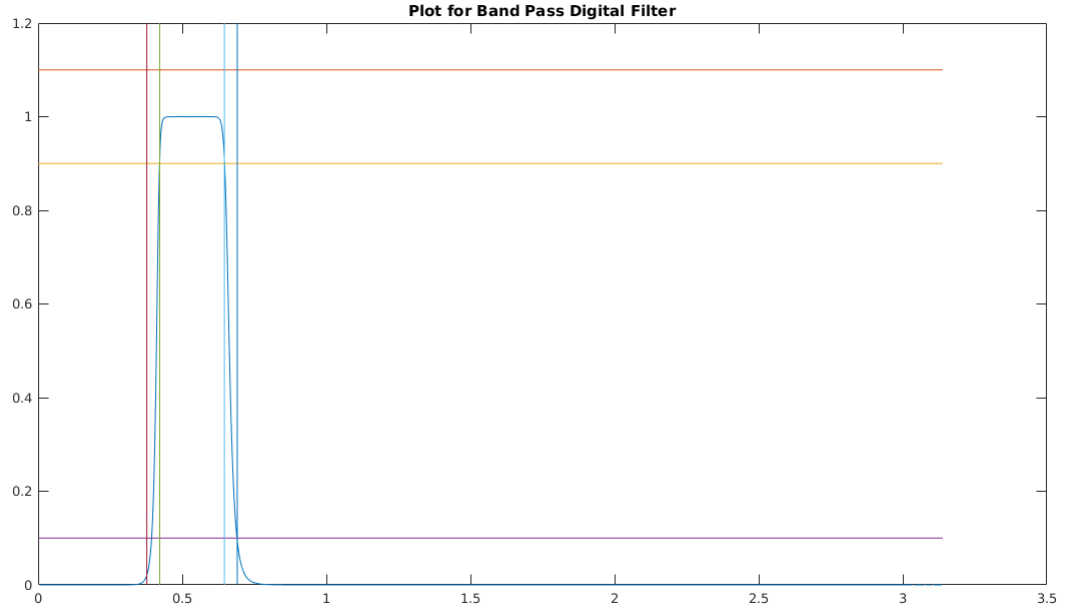


Figure 6: Frequency Magnitude Response of Discrete Time Band Pass Filter

## 1.9 Direct Form 2 Realization of the Discrete Filter

## 1.10 FIR Filter Transfer Function to get the same specifications

Given that  $\delta = 0.1$ , we get

$$A = -20\log_{10}(\delta) = -20\log_{10}(0.1) = 20$$

For  $A < 21$  we get  $\alpha = 0$  and hence  $\beta = 0$ . Also we have  $\Delta\omega = w_s - w_p$ . We then compute

$$N \geq \frac{A - 8}{2 * 2.285 * \Delta\omega} = 58.507$$

Therefore we choose

$$N = 59$$

.

But with  $N = 59$  the resulting FIR doesn't meet all the specifications. Here is the plot for the same

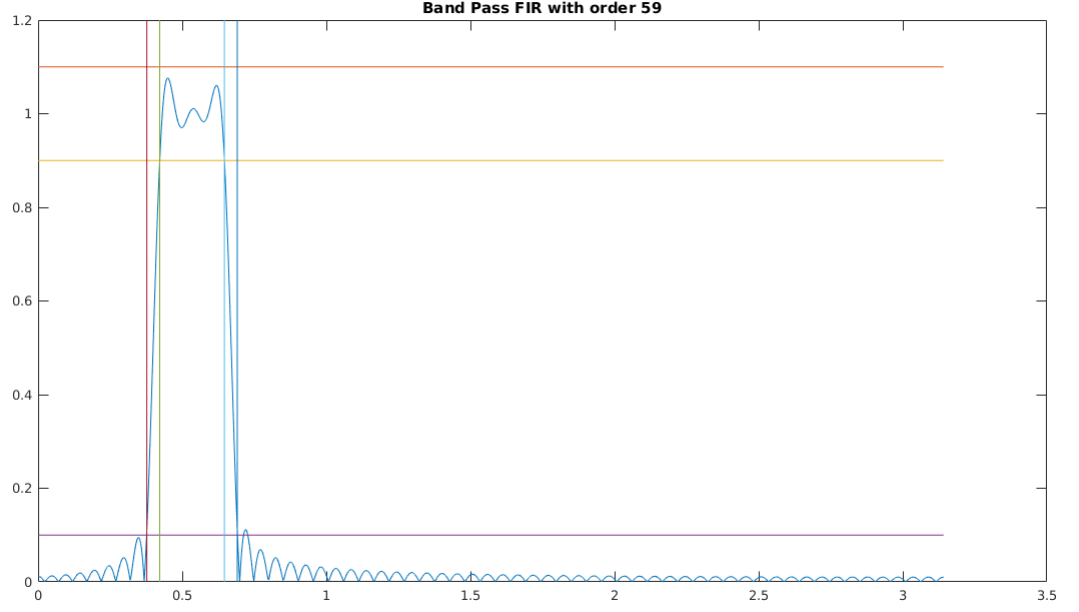


Figure 7: Order 59 FIR Band Pass

On increasing  $N$  to  $N = 63$ , we get an FIR that meets the specifications.

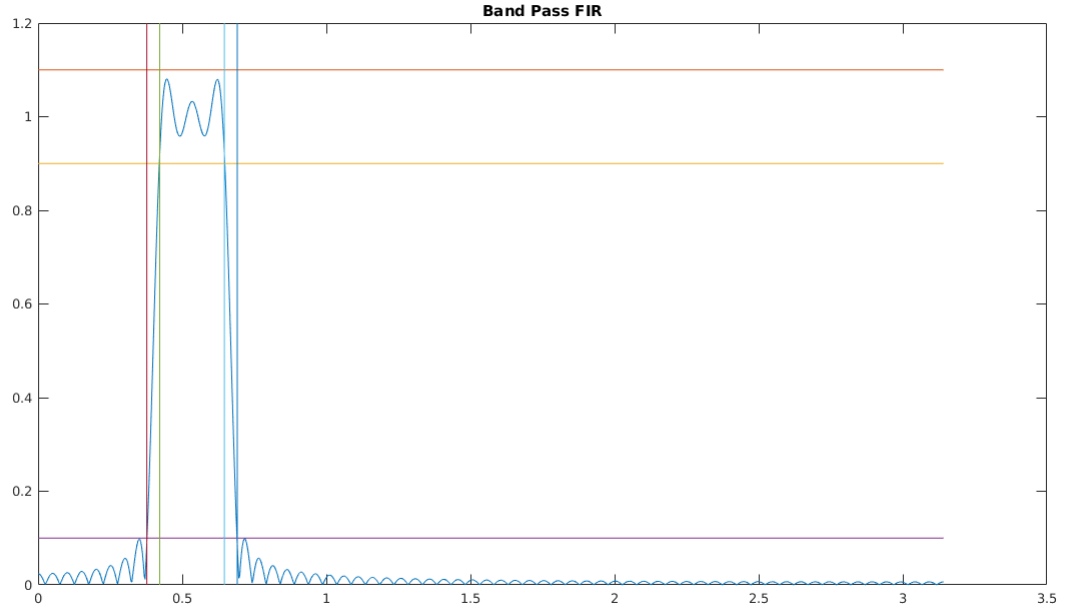


Figure 8: Order 63 FIR Band Pass

$$\begin{aligned}
 H_{fir_{bp}} = & 0.010699z^{-59} + 0.0099216z^{-58} + 0.0061769z^{-57} + 0.00067888z^{-56} + -0.0047345z^{-55} + \\
 & -0.0083073z^{-54} + -0.0090412z^{-53} + -0.0070586z^{-52} + -0.0035005z^{-51} + 1.5549e-17z^{-50} + \\
 & 0.0020437z^{-49} + 0.0020753z^{-48} + 0.0006074z^{-47} + -0.0010474z^{-46} + -0.0014292z^{-45} + 0.00031922z^{-44} + \\
 & 0.0039434z^{-43} + 0.0080615z^{-42} + 0.010683z^{-41} + 0.010067z^{-40} + 0.0055652z^{-39} + -0.0019308z^{-38} + \\
 & -0.010166z^{-37} + -0.016293z^{-36} + -0.017965z^{-35} + -0.014297z^{-34} + -0.0062993z^{-33} + 0.0034278z^{-32} + \\
 & 0.011658z^{-31} + 0.015779z^{-30} + 0.014805z^{-29} + 0.009742z^{-28} + 0.0031172z^{-27} + -0.0021396z^{-26} +
 \end{aligned}$$

$$\begin{aligned}
& -0.0040068z^{-25} + -0.0023031z^{-24} + 0.0011925z^{-23} + 0.003537z^{-22} + 0.0020435z^{-21} + -0.0042678z^{-20} + \\
& -0.013846z^{-19} + -0.022858z^{-18} + -0.026534z^{-17} + -0.021167z^{-16} + -0.0059818z^{-15} + 0.01592z^{-14} + \\
& 0.038073z^{-13} + 0.05258z^{-12} + 0.052901z^{-11} + 0.036481z^{-10} + 0.0062323z^{-9} + -0.029837z^{-8} + \\
& -0.060854z^{-7} + -0.07654z^{-6} + -0.070733z^{-5} + -0.04374z^{-4} + -0.0026197z^{-3} + 0.040796z^{-2} + \\
& 0.073555z^{-1} + 0.085714z^0 + 0.073555z^1 + 0.040796z^2 + -0.0026197z^3 + -0.04374z^4 + -0.070733z^5 + \\
& -0.07654z^6 + -0.060854z^7 + -0.029837z^8 + 0.0062323z^9 + 0.036481z^{10} + 0.052901z^{11} + 0.05258z^{12} + \\
& 0.038073z^{13} + 0.01592z^{14} + -0.0059818z^{15} + -0.021167z^{16} + -0.026534z^{17} + -0.022858z^{18} + \\
& -0.013846z^{19} + -0.0042678z^{20} + 0.0020435z^{21} + 0.003537z^{22} + 0.0011925z^{23} + -0.0023031z^{24} + \\
& -0.0040068z^{25} + -0.0021396z^{26} + 0.0031172z^{27} + 0.009742z^{28} + 0.014805z^{29} + 0.015779z^{30} + \\
& 0.011658z^{31} + 0.0034278z^{32} + -0.0062993z^{33} + -0.014297z^{34} + -0.017965z^{35} + -0.016293z^{36} + \\
& -0.010166z^{37} + -0.0019308z^{38} + 0.0055652z^{39} + 0.010067z^{40} + 0.010683z^{41} + 0.0080615z^{42} + \\
& 0.0039434z^{43} + 0.00031922z^{44} + -0.0014292z^{45} + -0.0010474z^{46} + 0.0006074z^{47} + 0.0020753z^{48} + \\
& 0.0020437z^{49} + 1.5549e-17z^{50} + -0.0035005z^{51} + -0.0070586z^{52} + -0.0090412z^{53} + -0.0083073z^{54} + \\
& -0.0047345z^{55} + 0.00067888z^{56} + 0.0061769z^{57} + 0.0099216z^{58} + 0.010699z^{59}
\end{aligned}$$

## 2 Second Filter Specifications

### 2.1 Un-normalized Discrete Time Filter Specifications

- Sampling Frequency ( $f_s$ ) = 140kHz
- $B_L = 7.7kHz$
- $B_H = 10.7kHz$
- Monotonic Passband (Butterworth)

### 2.2 Normalized Digital Filter Specifications

- $\omega_{p1} = \frac{7.7}{90}2\pi = 0.3007$
- $\omega_{p2} = \frac{10.7}{90}2\pi = 0.5251$
- $\omega_{s1} = \frac{6.7}{90}2\pi = 0.3456$
- $\omega_{s2} = \frac{11.7}{90}2\pi = 0.4802$

### 2.3 Analog Filter Specifications

- $\Omega_{p1} = \tan(\frac{\omega_{p1}}{2}) = 0.1515$
- $\Omega_{p2} = \tan(\frac{\omega_{p2}}{2}) = 0.2688$
- $\Omega_{s1} = \tan(\frac{\omega_{s1}}{2}) = 0.1745$
- $\Omega_{s2} = \tan(\frac{\omega_{s2}}{2}) = 0.2448$

### 2.4 Frequency transformation to be employed

$$s_L = \frac{s^2 + \Omega_0^2}{Bs} \quad (3)$$

with  $B = \Omega_{p2} - \Omega_{p1} = 0.1208$  and  $\Omega_0 = \sqrt{\Omega_{p1}\Omega_{p2}} = 0.2678$   
This translates to

$$\Omega_L = \frac{\Omega^2 - \Omega_0^2}{B\Omega} \quad (4)$$

## 2.5 Frequency transformed lowpass analog filter specifications

From 4

- $\Omega_{Lp} = 1$
- $\Omega_{Ls} = \min(\Omega_{Ls1}, \Omega_{Ls2}) = 1.3321$

## 2.6 The analog Low pass Transfer Function

$$H_{analog}(s_L) = \frac{1}{0.4533s^{11} + 3.423s^{10} + 12.92s^9 + 32.07s^8 + 57.98s^7 + 80.04s^6 + 86.01s^5 + 71.95s^4 + 45.95s^3 + 21.38s^2}$$