# ELEC6089 High Voltage Insulation Systems Assignment 1 HV AC 275kV Bushing Design

Thomas J. Smith, David Mahmoodi, Brendan Hickman, Patrick P. L. Fong

University of Southampton

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#### Abstract

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#### 1 Introduction

The design of electrical equipment always involves an aspect of insulation design. For the safe and efficient operation of electrical equipment it is necessary to have an electrical circuit and a means of isolating this circuit from the surrounding environment [1]. Power systems contain a complex structure of generators, transmission lines, transformers, switchgear and more. All of these different devices require an appropriately selected insulation material in order to isolate the mechanical casings and support structures from the high voltage components [2].

The purpose of this report is to describe the design and simulation of a high voltage bushing. Bushings are an integral part of power system insulation. IEEE standard C57.19.00 describes a bushing as "an insulating structure, including a through conductor or providing a central passage for such a conductor, with provision for mounting on a barrier, conducting or otherwise, for the purpose of insulating the conductor from the barrier and conducting current from one side of the barrier to the other." [3]. Bushings are required for situations such as connecting the external conductor to the internal windings of a transformer through the walls of the metal oil tank. The walls of the transformer housing will be grounded, but need to be shielded from the incoming high voltage conductor, hence the use of an insulating bushing [1]. An example of this application can be seen in figure 1, as 400kV grid conductors enter an oil filled transformer casing. The shedding on the outer cylinder can be seen in figure 1 which helps increase electrical strength in wet conditions [1].





(a) Transformer wall connection

(b) Wide view

Figure 1: High Voltage Bushings on the 400kV Transformers at Staythorpe CCGT Power Station, Newark, UK (Taken by TJS)

### 2 Overview of Grading Methods

Electric field stress control is important in the design of many power system elements, especially cable terminations and bushings [2]. Failure of a bushing can damage the power transformer it is protecting, which can be an expensive mistake [1]. Bushings are required to withstand Electrical, Mechanical and Thermal stresses as defined in the IEEE standard C57.19.00 [3]. The design of the bushing is largely determined by the insulation material chosen and the resolution of these conflicting sources of stress. A good bushing design has insulation that can withstand the applied voltage and thermal characteristics appropriate for the current carried by the conductor [4].

The problem grading methods attempt to resolve is laid out in figure 2. The grounded transformer casing is shown in light grey which is perpendicular to the bushing insulation shown in dark grey and the high voltage conductor in white. The top of the bushing is exposed to air, while the other side is exposed to transformer oil. Conducting a numerical analysis or simulation would show that the conductor surface within the plane of the transformer casing and at the points marked by red crosses would experience high electric field stress. The bushing insulation is designed to withstand the high electric field between the conductor and the transformer casing, however at the points marked with crosses the interface between the solid insulation and the air/transformer oil would cause surface discharge leading to relatively low flashover voltages [5]. It is therefore necessary to develop methods of reducing electric field stress to a more uniform distribution for both functional purposes and the economic use of space and materials [2].

#### 2.1 Low Voltage and DC Solutions

There are several methods that can be used dependant upon the application. Low voltage solutions include internal and external screening electrodes, while resistive stress control can be used for DC applications.

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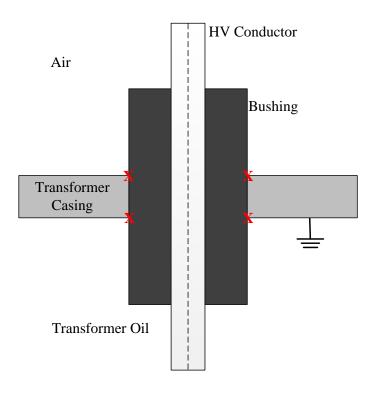


Figure 2: The Bushing Problem

#### 2.2 Capacitive Grading

Capacitive grading was first proposed by R.Nagel of Siemens in a German paper published in 1906 [4]. The value of this type of arrangement was quickly recognised, and is now industry standard practice for AC bushing designs for 25kV - 1500kV applications [2]. The general concept of the design is illustrated in figure 4, showing the isolated foils inserted inside the solid bushing insulation. Shown in red in figure 4 is the potential field with no grading, and in blue with the isolated conductive foils inserted. It shows that the whole dielectric is much more evenly stressed with the capacitive grading method.

The insulation is stressed in both a radial and axial direction, which sum to give the tangential field. The radial component  $E_r$  can cause breakdown of the insulating material, while the axial component  $E_z$  can cause surface discharge along the boundary [6]. These can be seen in green in figure 4. These sum up to give the tangential field  $E_t$ .

The most widely used method used to choose the dimensions and locations of the foils is double sided capacitive grading, of which there are two variants [6]. Before the distinction is made between the two, it is first necessary to introduce some terms. Firstly, The radius of the foil referenced from the centre of the conductor is termed  $r_n$ . The spacing between each foil is defined in equation 1.

$$S_n = r_n - r_{n-1} \tag{1}$$

Additionally, the length of each foil is referred to as  $l_n$  and the difference in length on the right and left side between each foil is termed  $b_{ln}$  and  $b_{rn}$ . Symmetric double sided capacitive grading is achieved

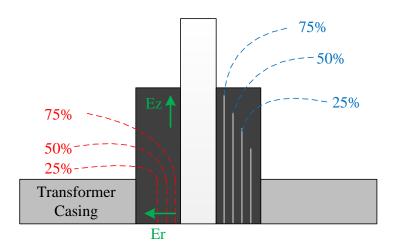


Figure 3: Field Distribution both without capacitive grading (shown in red) and with capacitive grading (shown in blue), modified from [2]

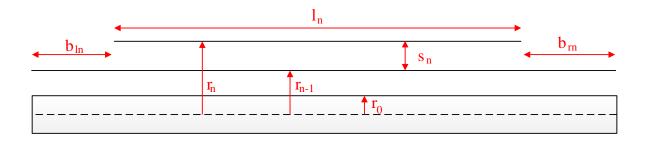


Figure 4: Symbols for calculating capacitive grading, modified from [6]

when  $b_{ln} = b_{rn}$  [6]. The total number of foils in the system is N. Also note that subscript n denotes the outermost foil.

The radial spacing and dimension of each foil is determined in the following derivation, which has been verified and modified from [5]. When a conductor is surrounded by concentric foils of dielectric constant  $\epsilon$  that is much greater than  $\epsilon_0$ , the system can be treated as a set of coaxial cylindrical capacitor units connected in series. In this derivation, the simplest boundary condition is assumed, that is the mean value of the radial field  $E_r$  remains constant within the foils. The foils are assumed to be of equal thickness, denoted by  $\delta$ . Each of the foils forms a coaxial capacitor stressed by the equal voltage  $\Delta V = E_r \delta$  providing all capacitances are equal. The capacitance of each foil is equal providing  $C_n = C_{n-1} = C_0$  where equation 2 gives the value of each capacitance.

$$C_n = \frac{2\pi\epsilon l_{n-1}}{\ln(\frac{r_{n-1}}{r_n})} \tag{2}$$

This can be expanded as in equation 3.

$$\frac{l_n}{ln(\frac{r_{n-1}}{r_n})} = \frac{l_{n-1}}{ln(\frac{r_{n-2}}{r_{n-1}})} = \frac{l_1}{ln(\frac{r_0}{r_1})}$$
(3)

An approximate solution for thin foils can then be found. Under the thin foil assumption,  $r_1 = r_0 + S_n$  and  $\frac{\delta}{r_n} << 1$  even for the smallest radii of the inner conductor. Equation 4 allows the simplification of equation 3 to equation 5.

$$ln(\frac{r_n}{r_{n-1}}) = ln\frac{1}{1 - (\frac{\delta}{r_n})} \approx \frac{\delta}{r_n} \tag{4}$$

$$l_n r_n \approx l_{n-1} r_{n-1} \approx \dots \approx l_0 r_0 \tag{5}$$

The two methods for solving the recursive equation in equation 5 is through either radial or axial grading [6]. In radial grading, the spacing of the foils  $S_n$  is assumed to be constant. This means the length of the foils decreases as it it approaches the outer foils of the bushing. Equation 6 gives the method to calculate  $S_n$  which can then be used in the recursive equation 7, which is a simple form of equation 5.

$$S_n = \frac{Outer Diameter - Conductor Diameter}{N-1} \tag{6}$$

$$l_{n+1} = l_n \frac{r_n}{r_n + S_n} \tag{7}$$

In the axial grading method, the length of each foil is assumed to decay by a constant value with each foil, and the radius at which it is placed is determined by a similar iterative formula. Radial grading better suits the purposes of this paper, since there is no requirement to assume the length of the final foil.

TS - We could derive the recursive equation for axial grading given an assumption of the final foil length here.

### 3 Design Details

The reference model for this project is shown in figure 5. The reference design is a paper impregnated with oil bushing with 21 aluminium foils of  $100\mu m$ . One side of the bushing is exposed to air, the other to oil, similar to a transformer bushing. The diameter of the conductor is 100mm, the bushing diameter is 300mm. The length of the first foil is 5000mm long, and fixed 2mm into the bushing at the conductor voltage. The outer foil is also set 2mm inside the bushing and is directly connected to the earthed flange. The conductor is used at 275kV AC voltage, and the design is known to be flawed.

A Matlab script was developed to take a required number of foils, and the inner and outer dimensions of the bushing, to calculate the radial location and length of each foil using the radial grading method as described in section 2.2. This script was built to be easily customisable for any number of foils and any initial values, to cater for the calculation of improved designs. It automatically outputs

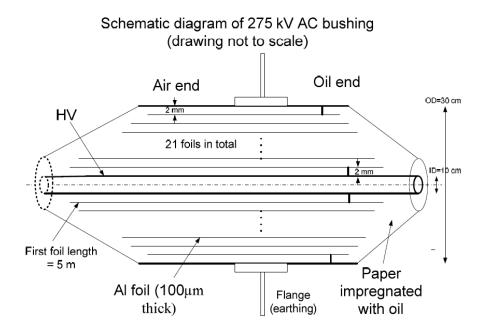


Figure 5: The reference problem taken from [7]

data in a form for direct input into the COMSOL model, and auto-updates a LATEXfile containing the data in table 1. Finally, the script plots the calculated foil positions in a crude graph shown in figure 6. Particularly in figure 6(b) the decay shape can be observed as expected. This allows a quick verification of the scripts accuracy before proceeding to simulation.

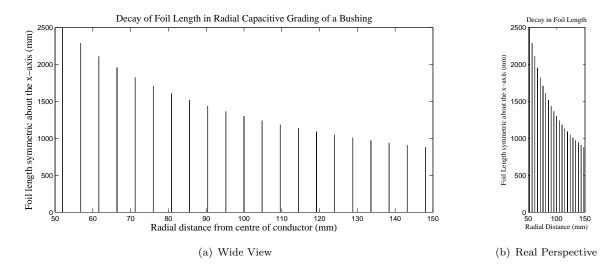


Figure 6: Representation of foil radial position and length

## 4 Modelling Results

Electric field modelling.

Table 1: Radial Grading Calculations Results

Radius(mm)	Length(mm)
52.00	5000.00
56.80	4577.46
00.00	,,,
61.60	4220.78
66.40	3915.66
71.20	3651.69
76.00	3421.05
80.80	3217.82
85.60	3037.38
90.40	2876.11
95.20	2731.09
100.00	2600.00
104.80	2480.92
109.60	2372.26
114.40	2272.73
119.20	2181.21
124.00	2096.77
128.80	2018.63
133.60	1946.11
138.40	1878.61
143.20	1815.64
148.00	1756.76

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### 5 Discussion of Results

Comparison and discussion (Suggestions on improvement).

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#### 6 Conclusions

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## A Individual Contributions

Team Member	Contribution
Thomas J. Smith	
23914254	
David Mahmoodi	
99999999	
Brendan Hickman	
99999999	
Patrick P. L. Fong	
99999999	

# B Meeting Minutes

## B.1 Meeting 1 - Kick-off Meeting

Purpose	ELEC6089 Bushing Design Kick Off Meeting	
Date and Time	Thursday 20th February 13:30	
Venue	GDP Lab Zepler Building, Highfield Campus	
Participants	TS (Thomas Smith), DM (David Mahmoodi), BH (Brendan	
Participants	Hickman), PF (Patrick Fong)	
Apologies	None	
	Review what we understand of the project so far.	
Agenda	Understand the tasks required.	
	Agree expectations of work and schedule.	
	Agree date and agenda of next meeting.	

### B.1.1 Minutes of the Meeting

ID	Subject	Notes and Discussion	Action
1.0	Research prior	BH uploaded the course text to the Facebook work-	ALL A1.0
	to the meeting	ing group which has a section on stress control by	
		floating screens. TS uploaded a project from KTH	
		university that had similar guidelines and had a	
		useful description to compound the lecturenotes for	
		the module. All agreed to research the topic fur-	
		ther and read these sections by the next meeting	
2.0	Current	The group discussed the task at hand. We need	-
	understanding	to design the bushing using the iterative formu-	
	of task	las from the lectures and then build a COMSOL	
		model. The design must be either radial or axial	
		in grading method.	
3.0	Work	The group tried to identify the work to complete.	-
	Breakdown	This includes research into field design and grading	
		methods, calculating the bushing design, simulat-	
		ing and report writing. None of these tasks can be	
		completed in parallel, and all need the previous in	
		order to complete the task. Hence each member	
		needs to research, and have knowledge of the de-	
		sign and simulation process. It will become clearer	
		who will be assigned responsibility for what shortly.	
		Currently, remain with all needing to complete re-	
		search	
4.0	Next Meeting	First meeting with G. Chen in 2 weeks, Tuesday	-
		4th March. Before then have a first model and have	
		begun verification. Have group Latex template for	
		collaboration, good layout and presentation marks.	
		Use Github. Next meeting on Wednesday 26th.	

#### B.1.2 Action List

ID	Action	Comments	Status
A1.0	Research	All to start research. Make notes of all sources. At	Open 20th Feb
		least reviewed the lecture notes and Kuffel.	

Next Meeting: 26th Feb 2014, Location & Time TBA

## B.2 Meeting 2 - Progress Meeting

Purpose	ELEC6089 Bushing Design Progress Meeting	
Date and Time	Wednesday 26th February 11:30	
Venue	GDP Lab Zepler Building, Highfield Campus	
Participants	TS (Thomas Smith), DM (David Mahmoodi), BH (Brendan	
r ai ticipants	Hickman)	
Apologies	PF (Patrick Fong)	
	Review research progress.	
Agenda	Clarify project understanding.	
	Start design task.	
	Identify further work.	

#### B.2.1 Minutes of the Meeting

ID	Subject	Notes and Discussion	Action
1.0	Research	The present team members discussed the task in	ALL A1.0
	update	the context of Kuffel and KTH research. Agreed	
		on bushing definitions and the theory behind ca-	
		pacitive grading. Also took time to verify that the	
		lecture notes matched the explanation in Kuffel.	
		Kuffel pages are 235-241. Also discussed why the	
		capacitors were added, and established the itera-	
		tive formula to use. All should continue to gain a	
		firmer grounding of the required theory	
2.0	Github and	TS ran the present through the report template,	-
	IAT <sub>E</sub> X	what was required and how to use the distributed	
		revision control system Git as hosted on GitHub.	
		This should make collaboration much easier than	
		using just our facebook group page.	

ID	Subject	Notes and Discussion	Action
3.0	Grading	DM left the meeting at this point to read the lec-	PF & DM
	Methods	ture notes. DA will also perform the grading and	A2.0
		we can then use this to idependently verify the de-	
		sign. TS and BH started on axial grading method.	
		Both wrote matlab code to calculate spacings. The	
		results were the same, hence reasonable level of	
		confidence of validity.	
4.0	Remaining	BH and TS identified the remaining work for ac-	-
	work	tioning. The report has an introduction which re-	
		quires review. Sections on Grading methods (why	
		grade? LV solutions using electrodes, DC solution	
		using resistivity, AC capacitive grading), AC grad-	
		ing types (discussion of axial and radial compo-	
		nents of tangential fields, radial and axial deriva-	
		tion) and section on the design details (iterative	
		formula, Matlab calculations, visio diagrams). The	
		design must be built in COMSOL which represents	
		significant work to understand COMSOL. Proba-	
		bly want to simulate a non-graded bushing as a	
		baseline for discussion. Aiming to do both radial	
		and axial grading simulations. Then discuss.	
5.0	Assignment of	BH and PF have a key deadline on tuesday 4th	TS & DA A3.0
	work	March hence largely unavailable until then. TS and	A4.0
		DM to get started on tasks. Try and get simula-	
		tions done before meeting with GC.	
4.0	Next Meeting	First meeting with G. Chen Tuesday 4th March.	-
		Before then have a first model and have begun ver-	
		ification. Next meeting on Prior to this meeting.	

#### B.2.2 Action List

ID	Action	Comments	Status
A1.0	Research	All to start research. Make notes of all sources. At	Open 20th Feb
		least reviewed the lecture notes and Kuffel.	
A2.0	Grading	Other members to perform axial grading calcula-	Open 26th Feb
		tions seperately so that the results can be verified	
		independently	
A3.0	COMSOL	Gain an understanding of COMSOL and attempt	Open 26th Feb
		some simulations.	
A4.0	Reporting	Continue to document progress in the report.	Open 26th Feb

#### C Code Listings

```
%% ELEC6089 High Volatage Insulation Design - Bushing Design
\%\% Calculates the lengths of each foil layer - Radial grading
%% Author - TJS and BH
%% date - 26/02/2014
\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)\(\lambda\)
N = 21
                                                  %Number of foils
length = zeros(N, 1) %initiate vectors
radius = zeros(N, 1)
                                                  %set inner radius
radius(1) = 52
length(1) = 5000
                                                 %first foil length
radius(N) = 148
                                              %outer foil radius
spacing = (radius(21)-radius(1))/(N-1) %even spacing of foils
%calculate each foil radius and length - from Kuffel and Lecture Notes
for i = 2: N
         radius(i) = radius(i-1)+spacing
         length(i) = (length(i-1)*radius(i-1))/radius(i)
%Plot a graph to indicate validity
lengthhalved = length/2 %half lengths to index from center
bar(radius, lengthhalved, 0.01) %plot bars with radius
%Write values to .tex file for reference in text.
FID = fopen('RadialVals21.tex', 'w');
fprintf(FID, '\\begin{table}[!htb]\n');
fprintf(FID, '\\caption{Radial Grading Calculations Results}\n');
fprintf(FID, '\\label{table:radialvals}\n');
fprintf(FID, '\\begin{center}\n');
fprintf(FID, '\\begin{tabular}{cc}\n');
fprintf(FID, '\\toprule\n');
fprintf(FID, '\\textbf{Radius(mm)} & \\textbf{Length(mm)} \\\\ \\toprule\n');
for k=1:N
          fprintf(FID, '%4.2f & %4.2f \\\\ ', radius(k), length(k));
         fprintf(FID, '\n');
end
fprintf(FID, '\\bottomrule\n');
fprintf(FID, '\\end{tabular}\n');
fprintf(FID, '\\end{center}\n');
fprintf(FID, '\\end{table}\n');
fclose(FID);
%For easy plotting in COMSOL
z = zeros(\bar{N}, 1)
r = zeros(N, 1)
zoffset = 1000
roffset = 0
r = radius + roffset
z = zoffset + ((length(1) - length)/2)
```