

Laki To Tambora

A study of ice cores

Thea Quistgaard

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Figure 1: J. M. W. Turner: *The Eruption of the Soufriere Mountains*

Darkness

I had a dream, which was not all a dream.
The bright sun was extinguish'd, and the stars
Did wander darkling in the eternal space,
Rayless, and pathless, and the icy earth
Swung blind and blackening in the moonless air;
Morn came and went—and came, and brought no day.

Lord Byron (1788–1824)

Acknowledgments

I would like to thank potatoes. They are great.

ABSTRACT

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Abstract

Todo list

INTRO: References missing in entire section	1
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ICE-DENS: Figure out where this comes from.	9
ICE-DIFF: Describe how to solve for sigma.	11
ICE-DIFF: DESCRIBE HOW TO SOLVE FOR SIGMA and a discussion of the ice diffusion constant(ice diffusivity?).	12
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SIGNAL-BACKDIFF: RETHINK THIS PART. DO NOT USE TIME ON ALL THE CALCULATIONS. WRITE THE GENERAL IDEAS OF THE METHODS AND STATE HOW TO CALCULATE/- COMPUTE. SMALL CODE SNIP TO GIVE GENERAL IDEA.	29
SIGNAL-MEM: Write this entire section - maybe not necessary? Maybe use in reconstruction of missing data...	34
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Chapter 1

Introduction

This is an amazing introduction that shows that I know all the stuff that I have done in my thesis. I am clever clever clever.

1.1 Laki and Tambora in Recorded History

In the not-so-distant past two volcanic horizons have been of great importance for this thesis, namely the Laki eruption in 1783 and the Tambora eruption of 1815. Interestingly, these eruptions have not only impacted the geophysical world, but has left their footprints on the history of Man in politics[REFERENCE], sociology[REFERENCE], arts[REFERENCE] and philosophy[REFERENCE]. On the eighth day of June in 1783 a volcanic fissure located in the southern part of Iceland was central for a global climatic change. The fissure Lakagígar or more commonly known as Laki refering to the central mountain, erupted with violent phreagomagmatic explosions due to the basalt magma being exposed to ground water. The eruption was given a Volcanic Explosivity Index(VEI) of 4, corresponding to the magnitude of the much later 2010 Eyjafjallajökull Icelandic eruption. For the next eight months the fissure continued to emit great amounts of sulfuric aerosols into the atmosphere, resulting locally in Iceland in catastrophic mass famine, due to loss of livestock to poisoning, with up to 25 % of the population dying from starvation and poisoning from the volcanic gasses. Globally, the eruption caused a huge amount of sulfur dioxide to be spewed into the northern hemisphere which led to a global drop in temperatures and a generally more extreme climate. In the European regions the following summer was much warmer than usual with many thunderstorms to follow. The winter of 1783-

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84 was subsequently extreme, with long periods of continuous frost. In France the late 1780's were marked by several years with droughts in the summer and frost in the winter, which contributed greatly to a rise in poverty and famine, and creating a greater division between the people and the rulers. Along with a growing dismay and distrust in the ruling forces the climatic changes due to Laki and a number of other climatic disruptions the French political situation finally climaxed in the French revolution of 1789. [REFERENCES!!!!]

32 years later on April 5 in 1815 an even more powerful eruption ensued: the eruption of Mount Tambora on the, now, Indonesian island Sumbawa. This eruption had a Volcanic Explosivity Index of 7, which makes it the most powerful in the recorded history of humankind. Considering that the VEI is defined as a logarithmic scale - at least for indices larger than VEI-3 - the Tambora eruption, though located just south of the Equator, impacted the entire globe as well as the European continent in at least the same magnitude as the 32 years prior Laki eruption. Locally, it was estimated to cause at least 10,000 direct deaths and many tens of thousands more due to sulfur dioxide poisoning, famine and disease. In many contexts the year of 1816 following the event became known as "*The Year Without a Summer*", as the ashes from the eruption column dispersed across the world and lowered global temperatures. This significant climate change though was not just a consequence of the Tambora eruption, but was pushed by a number of climatic forcings, some due to several previous volcanic activities around the globe. Combined, these effects coincided in a drop in global temperature by about 0.4 to 0.7 °C. This climatic change affected the entire globe by disrupting the Indian monsoons, causing a number of failed harvests, laying ground to severe typhus epidemics in southeast Europe and destroying crops and causing potato, oat and wheat harvest failure, especially in Ireland. Since the eruption had so severe consequences for the day to day lives of many people, the aftermath all around the world has been one of the greatest documented in recorded time, with a clear impact on the works of many artists, among them Lord Byron and J. M. W. Turner[REFERENCES!!!!]. Although both eruptions caused many a tragedy, there is beauty in using these events as volcanic horizons in ice core records. Given the severity of both eruptions, they have been so well documented in historical records that they make up solid and certain pillars in developing a temporal map of the past life of our ever so active earth. For that and for their brutal beauty they will remain in human history for a great while to come.

1.2 A Rare Gem of Knowledge

1.3 The Importance of Mapping Paleotemperature and -climate

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Chapter 2

The theory of ice cores

2.1 Water Isotopes and δ -notation

A corner stone in ice core analysis, which helps lay the basis for paleo climate research, is through measurements of the isotopic composition of the water - or that of the encapsulated air in bubbles - which makes up the ice cores. Water isotopes are sensitive to temperature changes and can thus be used as a proxy for paleo temperature along with being used as dating parameters, since the annual cycles often are detectable in water isotope data.

δ notation and water isotopes

Water isotopic ratios, i.e. the ratio of the minority isotope, H_2^{18}O or H_2^{17}O ($^2\text{H}_2\text{O}$), compared to the majority isotope, H_2^{16}O ($^1\text{H}_2\text{O}$), are used to report the quantities of isotopes in a sample relative to the ratio of a given reference water sample. This is commonly expressed in the δ -notation as:

$$\delta^i = \frac{{}^iR_{\text{sample}}}{{}^iR_{\text{reference}}} - 1 \quad (2.1)$$

where $^{18}R = \frac{n_{^{18}\text{O}}}{n_{^{16}\text{O}}}$, $^2R = \frac{n_{^2\text{H}}}{n_{^1\text{H}}}$ and $^{17}R = \frac{n_{^{17}\text{O}}}{n_{^{16}\text{O}}}$. Here n is the abundance of the given isotope.

Besides the isotopic quantities $\delta^{17}\text{O}$, $\delta^{18}\text{O}$ and $\delta^2\text{H} = \delta\text{D}$, both deuterium excess and $\Delta^{17}\text{O}$, known as ^{17}O excess, can be of interest. Deuterium excess is usually used as a measure of the kinetic fractionation processes, taking place in the water vapor formation of polar precipitation, giving an indicator of the conditions during precipitation formation, and thus giving a pointer to the source of the water vapor. Like deuterium excess ^{17}O is sensi-

tive to kinetic fractionation, but much less sensitive to equilibrium fractionation than both δD and $\delta^{18}O$. Along with being nearly insensitive to temperature (REFERENCES), these robustness factors leads to ^{17}O being usable as an independent parameter to be used to reveal the ways of the complicated mixing effects of fractionation due to evaporation, transportation, formation and deposition.

2.2 Diffusion and Densification

Throughout the firn column the important processes of diffusion and densification takes places. Both processes need to be well understood and examined when analyzing ice core data, as diffusion and densification play a large role in thinning of annual layers due to compression of snow to ice and in washing out the measured signals through diffusion in the firn.

2.2.1 Densification

Densification is the process of compression of snow to ice. It plays an important role in the annual layer thickness in the data as snow will be compressed to a smaller volume under pressure from the firn column above until it reaches a solid ice state with a, almost, constant density.

Commonly three stages of densification are described in the firn column. The first stage is between the initial precipitated snow density and the 'critical density' at $0.55 \frac{Mg}{m^3}$, the second stage is between critical density and the close-off density at $0.82 - 0.84 \frac{Mg}{m^3}$, and the third stage is from close-off and all the way through the ice.

At the first stage the densification is mostly due to grain settling and packing and the densification rate is very rapid. At the second stage, the snow is close to isolating air bubbles. At the third stage, the dominating densification taking place is by the compression of air bubbles.

For these three stages it is of interest to develop a depth-density profile, which is dependent on snow accumulation rate and temperature. The focus is on developing an empirical model for the first and second stages of densification, as they are the most dramatic sections of the firn column considering densification and diffusion.

A number of different densification models have been developed (REFERENCES), and in this thesis will be presented the ones used for the analysis.

Herron Langway Empirical Model

Sorge's law(REFERENCES) assumes that the relation between snow density ρ and depth h is invariant with time, given a constant snow accumulation and temperature. Furthermore, annual layer thinning by plastic flow is ignored. Densification of firn, which can be described as the proportional change in air space, is linearly related to change in stress due to the weight of the overlying snow(REFERENCES):

$$\frac{d\rho}{\rho_i - \rho} = \text{const.} \rho dh \quad (2.2)$$

By integration, this implies a linear relation between $\ln \left[\frac{\rho}{\rho_i - \rho} \right]$ and h .

When considering real data, analysis shows that $\ln \left[\frac{\rho}{\rho_i - \rho} \right]$ vs h . plots have two linear segments(EXAMPLE), corresponding to the first and second stages of densification, with separation of segments at $\rho = 0.55$ and $\rho = 0.8$. These segments on the plots will yield two different slopes with slope constants:

$$C = \frac{d \ln \left[\frac{\rho}{\rho_i - \rho} \right]}{dh}, \rho < 0.55 \quad (2.3a)$$

$$C' = \frac{d \ln \left[\frac{\rho}{\rho_i - \rho} \right]}{dh}, 0.55 < \rho < 0.8 \quad (2.3b)$$

To find the densification rate, $\frac{d\rho}{dt}$, substitute $\frac{dh}{dt} = \frac{A}{\rho} \rightarrow dt = \frac{\rho}{A} dh$ and use the differentiation $\frac{\partial}{\partial t} \left[\ln \left[\frac{x(t)}{k-x(t)} \right] \right] = \frac{k \frac{dx}{dt}}{(k-x(t))x(t)}$

$$\begin{aligned} C &= \frac{\rho}{A} \frac{d \ln \left[\frac{\rho}{\rho_i - \rho} \right]}{dt} \\ &= \frac{\rho}{A} \frac{\rho_i}{\rho(\rho_i - \rho)} \frac{d\rho}{dt} \\ &= \frac{1}{A} \frac{\rho_i}{\rho_i - \rho} \frac{d\rho}{dt} \end{aligned}$$

leading to

$$\frac{d\rho}{dt} = \frac{CA}{\rho_i} (\rho_i - \rho) \quad (2.4a)$$

$$\frac{d\rho}{dt} = \frac{C'A}{\rho_i} (\rho_i - \rho) \quad (2.4b)$$

To continue from here two assumptions are made. The first is that the temperature and the accumulation rate dependencies may be separated, and that they thereby have no inter-correlation. The second is that the rate equations may be written as:

$$\frac{d\rho}{dt} = k_0 A^a (\rho_i - \rho), \rho < 0.55 \quad (2.5a)$$

$$\frac{d\rho}{dt} = k_1 A^b (\rho_i - \rho), 0.55 < \rho < 0.8 \quad (2.5b)$$

where k_0 and k_1 are Arrhenius type rate constants which are only temperature dependent, and a and b are constants determining the significance of the accumulation rate and are dependent on the densification mechanisms. a and b may be determined by comparing slopes for densification at different sites of nearly equivalent conditions as:

$$a = \frac{\ln\left(\frac{C_1}{C_2}\right)}{\ln\left(\frac{A_1}{A_2}\right)} + 1 \quad (2.6)$$

and equivalently for b , with C'_1 and C'_2 .

k_0 and k_1 can be estimated by observing values of k at different temperatures and plotting $\ln(k)$ versus temperature - a so-called Arrhenius plot (REFERENCES) - to find A and E_a in equations:

$$k = A e^{-\frac{E_a}{k_B T}} = A e^{-\frac{E_a}{RT}} \quad (2.7)$$

$$\ln(k) = \ln(A) - \frac{E_a}{R} \frac{1}{T}$$

leading to values of k_0 and k_1 of:

$$k_0 = 11e^{-\frac{10160}{RT}} \quad (2.8a)$$

$$k_1 = 575e^{-\frac{21400}{RT}} \quad (2.8b)$$

Depth-density and depth-age calculations

Assuming that temperature, annual accumulation rate and initial snow density are known, the following calculations can be made:

- Density at depth h , $\rho(h)$
- Depth at pore close-off, $\rho = 0.55$

- Depth-age relationship from surface to pore close-off (stage 1 and 2).

1. stage of densification: Depth-density profile:

$$\rho(h) = \frac{\rho_i Z_0}{1 + Z_0} \quad (2.9)$$

where $Z_0 = e^{\rho_i k_0 h + \ln\left[\frac{\rho_0}{\rho_i - \rho_0}\right]}$. In this segment, the depth-density is independent of accumulation rate. The critical density depth can be calculated as:

$$h_{0.55} = \frac{1}{\rho_i k_0} \left[\ln \left[\frac{0.55}{\rho_i - 0.55} \right] - \ln \left[\frac{\rho_0}{\rho_i - \rho_0} \right] \right] \quad (2.10)$$

and the age at close-off depth as:

$$t_{0.55} = \frac{1}{k_0 A} \ln \left[\frac{\rho_i - \rho_0}{\rho_i - 0.55} \right] \quad (2.11)$$

2. stage of densificaion: The depth-density profile

$$\rho(h) = \frac{\rho_i Z_1}{1 + Z_1} \quad (2.12)$$

ICE-DENS: Figure out where this comes from.

where $Z_1 = e^{\rho_i k_1 (h - h_{0.55}) - \frac{1}{A^{0.5}} + \ln\left[\frac{0.55}{\rho_i - 0.55}\right]}$. The age of firn at a given density ρ :

$$t_\rho = \frac{1}{k_1 A^{0.5}} \ln \left[\frac{\rho_1 - 0.55}{\rho_1 - \rho} \right] \quad (2.13)$$

An estimate of the mean annual accumulation rate can be made from the slope C' and the mean annual temperature:

$$A = \left(\frac{\rho_i k_1}{C'} \right)^2 \quad (2.14)$$

2.2.2 Diffusion

In Firn

Diffusion describes the attenuation of a given signal, e.g. a water isotopic signal, due to vapor phase diffusion in the porous firn column. This process takes place in the air pockets of the material from time of deposition to pore close-off. Commonly, firn is divided into three densification zones based on the dominant densification physics in the given zone [7, Herron and Langway, 1980], see section 2.2.1. To develop accurate knowledge of paleo climate

and temperatures it is of great importance to understand this process, as a reconstruction of the part of the signal lost will reveal finer details in the signal and thus a more detailed knowledge of past times. Diffusion can be described through Fick's 2nd law, which describes the change in concentration of a substance with time, due to diffusion:

$$\frac{\partial \phi}{\partial t} = D(t) \frac{\partial^2 \phi}{\partial z^2} - \dot{\epsilon}_z(t) z \frac{\partial \phi}{\partial z} \quad (2.15)$$

If we say the diffusion is focused on water isotopes, then we can approximate the water isotopic signal with the concentration, $\phi \approx \delta$, so:

$$\frac{\partial \delta}{\partial t} = D(t) \frac{\partial^2 \delta}{\partial z^2} - \dot{\epsilon}_z(t) z \frac{\partial \delta}{\partial z} \quad (2.16)$$

Through attenuation with depth and time due to diffusion there is a loss of information. But the diffusion constant and the vertical strain rate $\dot{\epsilon}_z(t)$ in Fick's 2nd law are dependent on temperature and accumulation on site, this information loss process can be used to infer temperature of firn and accumulation on site. The solution of Eq. 2.16 can be found by deconvolution. The attenuated, directly measured, isotopic signal, $\delta(z)$, can be described as the convolution between the initial isotopic signal, $\delta'(z)$, and a Gaussian filter, $\mathcal{G}(z)$, multiplied by the thinning function, $S(z)$, which describes the total thinning of a given layer at depth z due to the vertical strain from the above firn column.:

$$\delta(z) = S(z) [\delta'(z) * \mathcal{G}(z)] \quad (2.17)$$

where

$$S(z) = e^{\int_0^z \dot{\epsilon}_z(z') dz'} \quad (2.18)$$

and

$$\mathcal{G}(z) = \frac{1}{\sigma \sqrt{2\pi}} e^{-\frac{z^2}{2\sigma^2}} \quad (2.19)$$

In the gaussian filter, the variance σ^2 is referred to commonly as the diffusion length: the distance a water molecule is displaced along the z-axis. This quantity is directly related to both $D(t)$ and $\dot{\epsilon}_z(t)$ (the strain rate being approximately proportional to the densification rate in the column). Thus an accurate estimate of the diffusion length is crucial for describing the diffusion process. The change of diffusion length over time is given as

$$\frac{d\sigma^2}{dt} - 2\dot{\epsilon}_z(t)\sigma^2 = 2D(t) \quad (2.20)$$

given by [8, Johnsen, 1977], which also states that in the case of firn and assuming a site with little ice flow, the vertical strain rate, can be approximated with a simple strain rate, only dependent on the density and its time evolution:

$$\dot{\epsilon}_z(t) \approx -\frac{d\rho}{dt} \frac{1}{\rho} \quad (2.21)$$

where ρ is the density and $\frac{d\rho}{dt}$ is the densification rate. With this approximation, the solution to the equation for evolution of the diffusion length in the firn column can be found, defined only through density and densification rate, as:

$$\sigma^2(\rho) = \frac{1}{\rho^2} \int_{\rho_0}^{\rho} 2\rho'^2 \left(\frac{d\rho'}{dt} \right)^{-1} D(\rho') d\rho' \quad (2.22)$$

ICE-DIFF: Describe how to solve for sigma.

Certain densities and corresponding depths are of special interest as they indicate a specific stage of the firn and ice column. At top and bottom, we find the two extremum densities of settled snow, $\rho_{\text{snow}} = 330 \frac{\text{kg}}{\text{m}^3}$, and ice, $\rho_{\text{ice}} = 917 \frac{\text{kg}}{\text{m}^3}$. In between these two there are two more densities of importance: the critical density, $\rho_{\text{Cr}} = 550 \frac{\text{kg}}{\text{m}^3}$, describing the transition between the two firn stages (see Section 2.2.1), and the pore close off density, $\rho_{\text{CO}} = 330 \frac{\text{kg}}{\text{m}^3}$, describing the density at which air pockets in firn will seal off from each other to form single bubbles. From the close off density, further densification will be due to compression of these closed off air bubbles until the density reaches ρ_{ice} . If we assume that the diffusion constant, $D(\rho)$, and the densification rate, $\frac{d\rho}{dt}$ are known, then it is possible to give an estimate of the diffusion length profile by integrating from top, at density ρ_0 , to pore close-off depth, ρ_{co} .

In Solid Phase

When firn reaches solid state, below close-off depth, the isotope diffusion is driven not as much by densification any more, but by isotopic gradients within the ice crystal lattice structure. This diffusion process is much slower than the diffusion in vapor phase taking place in firn, and thus does not contribute as much to the information loss and attenuation of the signal. For solid ice, at $\rho \leq \rho_{\text{ice}}$, the diffusion constant is only dependent on temperature, and can be described through an Arrhenius type equation as(ref: RAMSEIER1967, JOHNSENetal2000):

$$D_{\text{ice}} = 9.2 \cdot 10^{-4} e^{-\frac{7186}{T}} \left[\frac{\text{m}^2}{\text{s}} \right] \quad (2.23)$$

The diffusion length in ice is given from the diffusion constant in ice and the thinning function as:

$$\sigma_{\text{ice}}^2(t) = S(t)^2 \int_0^t 2D_{\text{ice}}(t') S(t')^{-2} dt' \quad (2.24)$$

ICE-DIFF: DESCRIBE HOW TO SOLVE FOR SIGMA and a discussion of the ice diffusion constant (ice diffusivity?).

Reconstruction of temperatures

Reconstruction of paleotemperatures can be attempted through a number of various techniques (REFERENCES). For precise and accurate results, the single isotopologue diffusion methods have proven useful (REFERENCES).

As is known, convolution in time domain is equal to multiplication in the frequency domain. According to equation (2.17), the transfer function to the frequency domain, will be the Fourier transform of the Gaussian filter:

$$\mathcal{F}[\mathcal{G}(z)] = \hat{\mathcal{G}} = e^{-\frac{k^2 \sigma^2}{2}}, \quad k = 2\pi f = \frac{2\pi}{\Delta} \quad (2.25)$$

where Δ is the discrete sampling size. This filter keeps larger wavelength frequencies (> 50 cm) unaltered but attenuates short wavelengths (< 20 cm) heavily, which is exactly the effect of diffusion on the isotopic signal. An estimate of the diffusion length σ^2 can be made from the power spectral density (PSD) of an isotopic time series. In the frequency domain a PSD composed of an initial signal, a filter function and a noise term is given by:

$$P_s = P_0(k) e^{-k^2 \sigma^2} + |\hat{\eta}(k)|^2, \quad f \in [0, f_{Nq}] \quad (2.26)$$

where the diffused and noise-affected signal, P_s , is equal to the original signal, $P_0(k)$, times a filter, $e^{-k^2 \sigma^2}$ (our previously inspected Gaussian filter), plus a noise term, $|\hat{\eta}(k)|^2$, over a frequency space ranging from zero to the Nyquist frequency, f_{Nq} . The Nyquist frequency is dependent on the sampling resolution by $f_{Nq} = \frac{1}{2\Delta}$. The noise term, often categorized as white noise, but red noise is also seen in isotopic signals (REFERENCES), is given as

$$|\hat{\eta}(k)|^2 = \frac{\sigma_n^2 \Delta}{|1 - a_1 e^{ik\Delta}|^2} \quad (2.27)$$

ICE-TEMP: Describe an autoregressive process

Equation 2.27 describes an autoregressive process of the first order, with a_1 being an AR-1 coefficient.

The spectral estimate of the time series, \mathbb{P}_s , can be computed via a number of different numerical schemes, here Burg's method will be used, REFERENCES.

To determine the diffusion length a fit to these estimated spectral data, P_s , is found through for example a least square optimization, from which the parameters P_0 , σ , a_1 , σ_η^2 can be estimated.

The diffusion length σ^2 can be calculated by least-square minimization of the misfit between \mathbb{P}_s and P_s .

This estimated diffusion length needs to be corrected: the obtained $\hat{\sigma}^2$ is affected by two further diffusion processes, taking place respectively in the ice and in the experimental sampling:

- **Sampling diffusion:** This diffusion is due to the sampling method. Sampling at a certain discrete resolution - be it discrete sections or resolution in CFA system due to step or impulse response - gives an additional diffusion length of

$$\sigma_{dis} = \frac{2\Delta^2}{\pi^2} \ln\left(\frac{\pi}{2}\right) \quad (2.28)$$

- **Ice diffusion** When below the close-off depth, a correction for the ice diffusion must also be made.

So to obtain the actual diffusion length from the raw data, both the sampling and the ice diffusion need to be subtracted from σ^2 , and a scaling factor due to thinning from the strain must be introduced:

$$\sigma_{firn}^2 = \frac{1}{S(z)^2} \hat{\sigma}_{firn}^2 = \frac{\hat{\sigma}^2 - \sigma_{dis}^2 - \sigma_{ice}^2}{S(z)^2} \quad (2.29)$$

Now, from the obtained estimate of the firn diffusion length, a temperature estimate can be made by numerically finding the root of:

$$\left(\frac{\rho_{co}}{\rho_i}\right)^2 \sigma^2(\rho = \rho_{co}, T(z), A(z)) - \sigma_{firn}^2 = 0 \quad (2.30)$$

NOTE: Annual spectral signals appearing as peaks in the PSD, can influence the estimate of diffusion lengths. This can be taken into account by introducing a weight function omitting the annual signal from the PSD:

$$w(f) = \begin{cases} 0, & f_\lambda - df_\lambda \leq f \leq f_\lambda + df_\lambda \\ 1, & f < f_\lambda - df_\lambda, f > f_\lambda + df_\lambda \end{cases} \quad (2.31)$$

2.3 The Community Firn Model

The Community Firn Model (CFM) is an open-source modular Python framework for firn-modelling. It was first developed by [17, Stevens et al, 2020] and later adapted to a different version with a focus on water isotopic diffusion by [4, Gkinis et al, 2019] under the name Iso-CFM, the latter version used in this thesis. The original CFM is modular, meaning that, firstly, it is easy to choose which physical processes should be included in the modelling, and, secondly, it allows for the user to develop new modules that can easily be integrated in the framework, which is what [4] utilized in their work on the Iso-CFM. The main focus of the CFM is on modelling the evolution of firn density and temperature using a Lagrangian (firn parcel-following) grid, where each parcel (model volume) represents a layer of firn with uniform properties. This is carried out by first assuming that the accumulation rate at the site under consideration is constant and that the firn-density profile is in a steady state (Sorge’s law). The densification rate is computed at each step in the model, using any of the given previously published firn-densification models, provided in the modules, and the firn density is updated in each time step. Following, the firn temperature evolution is computed through a coupled heat-diffusion model, by the use of a finite-volume method, [14, Patankar, 1980]. The model then proceeds by adding a new layer on top of the simulated firn column, described by the provided input parameters (temperature, accumulation rate, density), and the bottom volume of the grid is removed. The user starts by specifying input parameters (firn-densification physics, time-step size, surface boundary conditions and more) in a .json file. A model run is then started by a ”spin-up” which determines a steady state model used as the initial condition for the main model run. Thus, for the initial model, a steady state analytic firn-densification Herron-Langway model [7] is used to calculate depth-density and depth-age profiles, using the forced steady state parameters temperature, T_0 and accumulation, \dot{b}_0 . Then stepping forward one time step, it uses the specified densification model to evolve the firn in time. An in depth description of the entire CFM can be found in [17, Stevens et al.].

2.3.1 Iso-CFM

The Iso-CFM building on the Community Firn Model, is a tool for estimating firn diffusion rates of water isotopes, $\delta^{18}\text{O}$, $\delta^{17}\text{O}$ and δD , developed by [5, Gkinis et al., 2021] for use in [5]. It requires two main inputs, temperature and accumulation rate, and no prior knowledge of the isotopic signal is required. The model provides computation of the diffusion lengths for the mentioned

water isotopes. As previously discussed, the diffusion lengths are a metric for the smoothing a signal has undergone and can, along with deconvolution techniques also discussed in this thesis, be used to reconstruct some of the signal that has been otherwise attenuated.

Firn Diffusivity

The Iso-CFM framework contains a number of different new modules added to the CFM. A specific module for calculation of the firn diffusivity, $D(\rho(z))$, is provided, containing several different methods for the calculations of the individual parameters contained in the calculation of the diffusivity constant, using the formulation in [10, Johnsen et al., 2000]:

$$D_i(z) = \frac{m p D_{\text{air}}}{R T(z) \alpha_{s/v}^i \tau(z)} \left(\frac{1}{\rho(z)} - \frac{1}{\rho_{\text{ice}}} \right) \quad (2.32)$$

with $i \in \text{O}^{18}, \text{O}^{17}, \text{D}$ representing the three different types of water isotopic ratios generally examined. The different terms in 2.32 each describes the following:

m : molecular weight in [kg]

$R = 8.314478 \left[\frac{\text{m}^3 \text{Pa}}{\text{K mol}} \right]$: molar gas constant

T Temperature [K]

p : saturation vapor pressure over ice in [Pa]

The saturation vapor pressure over ice can be calculated in two different ways, as in [?, Murphy & Koop 2005]:

$$p = \exp \left(28.9074 - \frac{6143.7}{T} \right) \quad (2.33)$$

$$p = \exp \left(9.5504 - \frac{5723.265}{T} + 3.530 \ln(T) - 0.0073 T \right) \quad (2.34)$$

where Eq. 2.34 takes the temperature dependence of the latent heat of sublimation of ice into account when integrating the Clausius-Clapeyron equation. A third expression is presented in [9, Johnsen et al., 2000] as:

$$p = 3.454 \cdot 10^{12} \exp \left(\frac{-6133}{T} \right) \quad (2.35)$$

which will be the one used for analytical calculations of diffusion length in this project.

D_{air} : diffusivity of water vapor in air,

calculated from $P_0 = 1\text{Atm}$, $T_0 = 273.15\text{K}$, T temperature in [K] and P ambient pressure in [Atm], as in [?, Hall and Prupacher, 1976]:

$$D_{\text{air}} = 2.1 \cdot 10^{-5} \left(\frac{T}{T_0} \right)^{1.94} \left(\frac{P_0}{P} \right) \quad (2.36)$$

From [?, Merlivat, 1978] the additional diffusivity of water isotopes ratios for ^{18}O and ^2H vapor were defined as

$$D_{\text{air}^2\text{H}} = \frac{D_{\text{air}}}{1.0251} \quad (2.37)$$

$$D_{\text{air}^{18}\text{O}} = \frac{D_{\text{air}}}{1.0285} \quad (2.38)$$

$\alpha_{s/v}^i$: solid-to-vapour fractionation factor. $i = ^{18}\text{O}$, D, ^{17}O ,

For both $\alpha_{s/v}^{18}$ and $\alpha_{s/v}^2$ there are multiple options for parameterisation of the fractionation factor. Considering $\alpha_{s/v}^{18}$, one can choose between [?, Majoube 1971] and [?, Ellehøj et al., 2013], respectively as:

$$\ln(\alpha_{s/v}^{18}) = \frac{11.839}{T} - 28.224 \cdot 10^{-3} \quad (2.39)$$

and

$$\ln(\alpha_{s/v}^{18}) = 0.0831 - \frac{49.192}{T} + \frac{8312.5}{T^2} \quad (2.40)$$

For $\alpha_{s/v}^2$ the parameterisation from [?, Merlivat and Nief, 1967], [?, Ellehøj et al., 2013] or [?, Lamb et al., 2017], respectively as:

$$\ln(\alpha_{s/v}^2) = \frac{16288}{T^2} - 9.45 \cdot 10^{-2}, \quad (2.41)$$

$$\ln(\alpha_{s/v}^2) = 0.2133 - \frac{203.1}{T} + \frac{48888}{T^2} \quad (2.42)$$

or

$$\ln(\alpha_{s/v}^2) = \frac{13525}{T^2} - 5.59 \cdot 10^{-2}. \quad (2.43)$$

The parameterisation of the fractionation factor related to the ^{17}O water isotopic ratios is based on [?, Barkan and Luz, 2005] as $\alpha_{s/v}^{17} = 0.529\alpha_{s/v}^{18}$. For a comparison of the different parameterisations see [?, Gkinis et al., 2021]. The default choices in the iso-CFM modules is [?, Majoube 1971] for $\alpha_{s/v}^{18}$ and [?, Merlivat and Nief, 1967] for $\alpha_{s/v}^2$

τ : firn tortuosity

In [10, Johnsen et al., 2000] a parameterisation of the firn tortuosity was presented as:

$$\frac{1}{\tau} = \begin{cases} 1 - b_\tau \left(\frac{\rho}{\rho_{\text{ice}}} \right)^2, & \rho \leq \frac{\rho_{\text{ice}}}{\sqrt{b_\tau}} \\ 0, & \rho > \frac{\rho_{\text{ice}}}{\sqrt{b_\tau}} \end{cases} \quad (2.44)$$

where $b_\tau = 1.3$ and $\rho_{\text{ice}} = 917 \frac{\text{kg}}{\text{m}^3}$, implying for $\frac{1}{\tau} = 0$ a close-off density of $\rho_{\text{CO}} = 804.3 \frac{\text{kg}}{\text{m}^3}$. This close-off density refers to the density at the depth where diffusive fluxes stop and $\frac{D_{\text{air}}}{D_{\text{eff}}} \rightarrow \infty$. Different parameterisations have been suggested, some defined from the total porosity, but for this project, the expression used is the one given in Eq. 2.44.

Diffusion Length Profiles

The iso-CFM computes a numerical solution for σ using a time-stepping scheme, as is the case for the original CFM, to estimate the most likely diffusion length profile at a given site. From each time step the CFM computes $\frac{d\rho}{dt}$ and T , and the iso-CFM uses these results to calculate the quantity $\frac{d\sigma^2}{dt}$:

$$\frac{d\sigma^2}{dt} = 2 \left(D(t) - \frac{\sigma^2}{\rho} \frac{d\rho}{dt} \right) \quad (2.45)$$

Eq. 2.45 shows that the diffusion length signal throughout the ice is a result of two processes, opposing each other: the always positive diffusivity term $D(t)$, and the densification process contributing negatively to the change over time, $-\frac{\sigma^2}{\rho} \frac{d\rho}{dt}$. After a certain depth, the densification term comes to dominate and thus the entire equation becomes negative and the value of the diffusion length is decreasing.

Diffusion/densification terms figure. See V. Gkinis 2021.

To simplify the work of this thesis, the numerical module of the CFM and the iso-CFM has not been implemented in the final computations, and the diffusion length profiles referred to in the rest of the project are calculated through an analytical method, using equations derived from Eq. 2.45 analytically. A short walk-through of the derivations will be presented here as they are described in [?, Gkinis et al., 2021]. By substitution of variables rearrangement Eq. 2.45 becomes:

$$\frac{d\sigma^2}{d\rho} + \frac{2\sigma^2}{\rho} = 2 \left(\frac{d\rho}{dt} \right)^{-1} D(\rho) \quad (2.46)$$

which can be converted to integral form:

$$\sigma^2(\rho) = \frac{1}{\rho^2} \int_{\rho_0}^{\rho} 2\rho'^2 \left(\frac{d\rho'}{dt} \right)^{-1} D(\rho') d\rho' \quad (2.47)$$

Then, by using the densification rate parameterisation given in [7, Herron and Langway, 1980], the expression becomes:

$$\frac{d\rho(z)}{dt} = k(T) A^\nu (\rho_{\text{ice}} - \rho(z)), \quad (2.48)$$

where $k(T)$ is an Arrhenius-type densification rate constant, dependent on temperature and densification zone described by:

$$k_0(T) = 0.011 \exp\left(-\frac{10160}{RT}\right), \quad \nu_0 = 1 \quad (2.49)$$

in the upper densification zone, $\rho < 550\rho_{\text{CO}}$. In the lower densification zone, $\rho \geq \rho_{\text{CO}}$, it is described as:

$$k_1(T) = 0.575 \exp\left(-\frac{21400}{RT}\right), \quad \nu_1 = 0.5. \quad (2.50)$$

Using the parameterization of the diffusivity coefficient from Eq. 2.32 and expressing the term $1/\tau = 1 - b_{\text{tau}} \left(\frac{\rho}{\rho_{\text{ice}}}\right)^2$ in densities, the diffusivity coefficient can be described as a function of density:

$$D_i(\rho) = \frac{m p D_{\text{air}}}{R T \alpha_{s/v}^i} \left(1 - b_\tau \left(\frac{\rho}{\rho_{\text{ice}}}\right)^2\right) \left(\frac{1}{\rho} - \frac{1}{\rho_{\text{ice}}}\right). \quad (2.51)$$

By then inserting in Eq. 2.47, defining $\frac{m p D_{\text{air}}}{R T \alpha_{s/v}^i} = \zeta$, and integrating the final analytical equations for the diffusion length in upper and lower densification zones can be obtained:

$$\sigma^2(\rho < \rho_{\text{CO}}) = \frac{\zeta}{\rho^2 k_0 A^{\nu_0} \rho_{\text{ice}}} \left[\rho^2 - \rho_0 - \frac{b_\tau}{2\rho_{\text{ice}}^2} (\rho^4 - \rho_0^4) \right] \quad (2.52)$$

$$\begin{aligned} \sigma^2(\rho \geq \rho_{\text{CO}}) = & \frac{\zeta}{\rho^2 k_1 A^{\nu_1} \rho_{\text{ice}}} \left[\rho^2 - \rho_{\text{Cr}} - \frac{b_\tau}{2\rho_{\text{ice}}^2} (\rho^4 - \rho_{\text{Cr}}^4) \right] \\ & + \frac{\zeta}{\rho^2 k_0 A^{\nu_0} \rho_{\text{ice}}} \left[\rho_{\text{Cr}}^2 - \rho_0 - \frac{b_\tau}{2\rho_{\text{ice}}^2} (\rho_{\text{Cr}}^4 - \rho_0^4) \right] \end{aligned} \quad (2.53)$$

The analytical equations have been used for creating a contour plot of the analytical solutions for σ_{18} at the close-off density, ρ_{CO} .

These analytical equations are used to compute diffusion lengths to compare with the optimal diffusion length estimates computed from the raw data.

Create contour plot
as in Gkinis2021

One could advantageously spend some time and energy on using the iso-CFM to numerically compute the comparison diffusion lengths with different temperature and accumulation forcing to recreate a diffusion length profile corresponding to the largest likelihood at a given drill site. Since the iso-CFM do consist of many different modules all with different possibilities for parameterisation, it is outside the scope of this project to develop a iso-CFM diffusion length estimate. In depth methodology and results from the iso-CFM can be found in [?, Gkinis et al., 2021].

2.4 Temperature Estimation

2.5 ECM and DEP

Electrical conductivity measurements(ECM), dielectric profiling(DEP) and isotopic composition analysis are three distinct ways of analyzing an ice core to examine past temperatures, climate and atmospheric composition. Some of these methods are sensitive to violent volcanic eruptions, which makes it possible to use known eruptions visible in the ice cores as volcanic horizons, and thus making dating of the ice core more precise and absolute.

2.5.1 Electrical Conductivity Measurements

The conductivity of ice arises from the current emerging due to the build-up of space charges in the ice structure. This conductivity can be analyzed by measuring the electrical current(DC) - induced by the electric potential and the acid balance - between two electrodes which are moved along the ice cores length. This current will be connected to the acid impurity concentration (pH), in the form of H_3O^+ concentration, of the ice core. Higher levels of acid impurity concentration are due to volcanic eruptions. Large amounts of volcanic gases, i.e. SO_2 , in the atmosphere oxidizes and combines with water to form acid, i.e. sulphuric acid, which is the washed out of the air due to precipitation. Thus it is made possible to recognize volcanic horizons in ice cores, and - if the location of the eruption is known - from the amount of acid, the magnitude of the eruption can also be estimated.

High acidity of layers containing volcanic fall-out influence the dielectric constant of ice, so that these layers may be a possible explanation to the internal reflection horizons found in radio-echo sounding.

ICE-
TEMP.EST: This
entire section needs
to be written

The measured current can then be transformed into acidity by a calibration curve relating the current, in μA , to the acidity, in $\mu\text{equiv. H}_3\text{O}^+$ per kilogram. To find the calibration parameters, the current and the acidity must be measured - the current through the above mentioned method, and the acidity through pH measurements of melted ice core samples. The pH measurements must further be corrected for any CO_2 induced H^+ ions (REFERENCES). The relation between acidity $[\text{H}^+]$ (corrected for CO_2 induced H^+) and current I can be expressed in two ways:

- $[\text{H}^+] = (0.017 I^2 + 1.2) \mu\text{equiv. H}^+/\text{kg}$
without a 50% correction for CO_2 surplus.
- $[\text{H}^+] = (0.045 I^{1.73}) \mu\text{equiv. H}^+/\text{kg}$
with a 50% correction for CO_2 surplus.

The salt concentration in the ice can be estimated from measurements of the specific conductivity σ of the melted samples. The salt contribution hereto can be expressed as:

$$\sigma_s = \sigma - \sigma(\text{H}^+) - \sigma(\text{X}^-) - \sigma(\text{HCO}_3^-) \quad (2.54)$$

where the three later terms correspond to the contributions from H^+ (through pH measurements) and its anions¹, HCO_3^- and any other anions X^- . The anion concentration will be equal to the cation concentration, which in this case is only H^+ concentration. Disregarding low acidity samples, the concentration of HCO_3^- is negligible and thus $\text{concentration}(\text{X}^-) \approx \text{concentration}(\text{H}^+)$. The current is thus heavily influenced on/determined by the H^+ concentration, and thus it is approximated that the salt concentration has no influence on the current readings, which is fortunate, since the ECM method only responds to acidity, and not to salt and ammonia concentrations. This is one of the methods limitations, which the later dielectric profiling method took into account.

2.5.2 Dielectric Profiling

A method was later developed to demonstrate how both acids and salts play a decisive role in the determination of the electrical behavior of ice. The dielectric response of an ice core can be used to determine the total ionic concentration of the core. For ECM the measurements are sensitive to the

²Anions are molecules losing a number of electrons to become negatively charged. Cations are molecules that gain a number of electrons to become positively charged.

fluctuating distance between ice core and electrodes, and after each measurement a fresh piece of ice needs to be prepared to repeat a measurement.

A new dielectric profiling technique (DEP) was developed (REFERENCES) with the advantages over the ECM that no direct contact is needed between the electrodes and the ice, so that the ice can stay in a protective polythene sleeve and the experiment easily can be repeated on the same piece of ice. Together the ice core and the polythene sleeve creates a complete system, where the plastic acts as an electrical blocking layer.

The dielectric response is measured by a sweeping of the AF-LF frequency range for the entire ice-polythene system. At LF the conductivity of the composite system is within a few percentages of the intrinsic behavior of the ice itself. At HF-VHF frequencies it also approximates well enough (REFERENCES).

The measured dielectric parameters are the conductivity of ice at HF-VHF range, denoted σ_∞ where ∞ signifies a frequency much higher than the relaxation frequency, f_r , of the dominant dispersion in the system. Both of these parameters display clear chemical response signals which can be used either alone or in combination with other ice core analysis measurements like ECM and isotope analysis.

If the core under analysis is chemically analyzed for Na^+ , Mg^{2+} , Cl^- , SO_4^{2-} and NO_3^- , a number of important parameters, which can be used to evaluate the response of the dielectric parameters, can be calculated (REFERENCES):

- The salt parameter, which represents the total marine cation concentration calculated with the assumed marine ratios as:

$$[\text{salt}] = 1.05([\text{Na}^+] + [\text{Mg}^{2+}]) \quad (2.55)$$

- XSO_4 , the excess sulphate, which represents the amount the sulphate concentration is above the expected if the salt and sulphate ions were in normal sea salt ratios. Excess sulphate is essentially sulphuric acid, which is the main acidic component of the ice.
- The strong acid content of the ice has been calculated as (assuming no other ions present in significant quantities):

$$[\text{acid}] = [\text{Cl}^-] + [\text{SO}_4^{2-}] + [\text{NO}_3^-] - 1.05([\text{Na}^+] + [\text{Mg}^{2+}]) \quad (2.56)$$

From data, it can be seen that acid and salt concentration peaks clearly affect σ_∞ and f_r (EXAMPLES, REFERENCES). The relationship between salt

and acid, and the two dielectric parameters have been derived through non-linear regression analysis. In PAPER(REFERENCES) the linear responses for the DEP at -22°C were:

$$\sigma_{\infty} = (0.39 \pm 0.01)[\text{salt}] + (1.43 \pm 0.05)[\text{acid}] + (12.7 \pm 0.3) \quad (2.57)$$

with 76.6 % variance

$$f_r = (440 \pm 11)[\text{salt}] + (612 \pm 65)[\text{acid}] + (8200 \pm 400) \quad (2.58)$$

with 68.4 % variance. σ_{∞} is measured in $\mu\text{S/m}$, f_r in Hz and [acid] and [salt] in $\mu\text{Eq/l}$. The total ionic concentration of the ice core is strongly linked to the dielectric parameters, and a regression between the total anion concentration and the dielectric parameters gives:

$$[\text{anions}] = [\text{salt}] + [\text{acid}] = 0.022\sigma_{\infty}^{1.89} + 10^{-6}f_r^{1.61} - 0.2 \quad (2.59)$$

with 86.7 % variance.

The DEP complements the ECM technique by not only reacting to acids alone, as ECM does, but responds to both neutral salts and acids. The acid term is here associated with the DC conductivity, the same way it is also detected by ECM. The dielectric dependence on salts is consistent with the Bjerrum L defect² affecting every one or two salt ions in the ice, indicating that a large fraction of the neutral salt is incorporated into the ice lattice.³ The sensitivity to salt concentrations allows for identifications of periods with major storms and open seas which are also important identifiers for paleo climate research, along with the volcanic eruption detection made possible through the ECM.

2.6 Dating of Ice Cores Through Volcanic Horizons

Throughout the history of the earth a number of different geophysical events have left their mark on the geological and glaciological records we use to steal a glance into the past. When considering ice core records, there are few as visible - both to the eye and in measured data - than volcanic eruptions. It is widely

³A Bjerrum defect is a crystallographic defect specific to ice, partly responsible for the electrical properties of ice. Usually a hydrogen bond will normally have one proton, but with a Bjerrum defect it will have either two protons (D defect) or no proton (L defect).(REFERENCES)

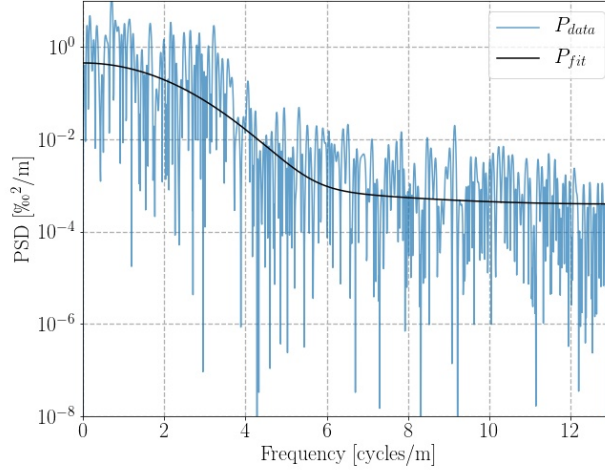


Figure 2.1: This is a great figure.

known [REFERENCE] that eruptions above a certain scale have the possibility to change not only the atmospheric composition, due to the heavy amount of volcanic material slung into the air, but also the ability to impact the climate in the years following an enormous eruption. Through electrical conductivity measurements it is possible to observe the very clear effects of some volcanic events in ice cores. Particles from the eruption are quickly transported from the source, since the atmospheric airflow will scatter the particles all over the atmosphere at a relatively high speed. Thus the dust(particle) and ECM signals pick up the volcanic signal faster than for example the isotopic signals. The isotopic signal reacts much slower, as it must be subjected to a change in global - and then following local - temperature, which might first show after a number of years. Thus ECM, DEP and dust measurements are good records to use for dating ice cores. Some eruptions are only great enough to show in ice cores located close to the volcanic source [REFERENCE], while others are of a magnitude impacting the entire globe, thus showing in almost all ice core records. These volcanic horizons are specifically good for synchronizing records, which is essential for developing knowledge about the geographically varying climate, temperatures and hemispherical dependency of the past. For this thesis the volcanic horizons are especially important for developing

2.6.1 Laki and Tambora in Data

Chapter 3

Isotopic Data: Laki to Tambora as seen in N Ice Cores.

3.1 Selection of Data

3.1.1 AWI B-cores

3.1.2 Crete and Surrounding Alphabet Cores

3.2 Data Specifications

Chapter 4

Signal Restoration and Peak Detection

The data obtained through various experimental measurements are easily compared with a time series, as they typically show some quantity measured all along the depth of an ice core. This depth is often, at short intervals, treated as a regular linear time series thus making it possible to use some of the known signal analysis methods. Of course, when considering the entirety of an ice core, the linearity disappears as thinning and compression makes the depth series non linear. But when considering short lengths of core it is possible to estimate a linearity, assuming conformity in this specific layer.

4.1 Back Diffusion

Due to diffusion in firn and ice, some of the water isotopic signal is lost. Some of this signal can be restored by investigating the diffusion process, and through filtering and deconvolution techniques(REFERENCES). For the data of this thesis two different restoration techniques are presented: a spectral method, determining the effect of mixing and diffusion as a spectral filter(REFERENCES), and a kernel restoration method much like the ones used to restore pixel resolution in images (REFERENCES).

4.1.1 Spectral Analysis

Power Spectral Densities

A very useful tool for analyzing signals exhibiting oscillatory effects is analysis of the signals power spectrum. Instead of considering the signal in time, it is

transformed to the spectral domain, where it is possible to obtain an estimate of both the signal and the underlying noise. This is crucial for enhancing the signal and filtering away noise. But to be able to examine these effects, first the data must be transformed. A range of different methods may be used to compute the frequency transform of the depth series, here I present the three I have been working with. Since the data are discrete and experimental, I will be presenting the discrete and applicable mathematical models.

When considering a signal, it may be of interest to investigate how the energy of said signal is distributed with frequency. The total power is defined as:

$$\text{Total Power} = \int_{-\infty}^{\infty} |X(\tau)|^2 d\tau. \quad (4.1)$$

Using Parseval's theorem (REFERENCE) (assuming that the signal has a finite total energy), the power of the signal can alternatively be written as

$$\int_{-\infty}^{\infty} |X(\tau)|^2 d\tau = \int_{-\infty}^{\infty} |\tilde{X}(f)|^2 df \quad (4.2)$$

where $\tilde{X}(f)$ is the spectral (Fourier) transform of the signal, from time to frequency domain, defined as:

$$\tilde{X}(f) = \int_{-\infty}^{\infty} X(\tau) e^{2\pi i f \tau} d\tau \quad (4.3)$$

and the inverse spectral (Fourier) transform, from frequency to time domain, defined as:

$$X(t) = \int_{-\infty}^{\infty} \tilde{X}(f) e^{-2\pi i f \tau} df. \quad (4.4)$$

Both $X(t)$ and $\tilde{X}(f)$ represent the same function, just in different variable domains. Often, the angular frequency ω is used instead, with the relation between ω and f being $\omega \equiv 2\pi f$, giving the Fourier and inverse Fourier transforms as:

$$\begin{aligned} \tilde{X}(\omega) &= \int_{-\infty}^{\infty} X(t) e^{i\omega\tau} d\tau \\ X(\tau) &= \int_{-\infty}^{\infty} \tilde{X}(\omega) e^{-i\omega\tau} d\omega \end{aligned} \quad (4.5)$$

From Equation 4.2 we can interpret the integrand on the right hand side $|\tilde{X}(f)|^2$ as a density function, describing the energy per unit frequency. This

is a property which is able to reveal much information about the considered signal, and it is useful to define this as the (one-sided) Power Spectral Density:

$$P_X(f) \equiv |\tilde{X}(f)|^2 + |\tilde{X}(-f)|^2 \quad 0 \leq f < \infty \quad (4.6)$$

This entity ensures that the total power is found just by integrating over $P_X(f)$ from 0 to ∞ . When the function is purely real, the PSD reduces to $P_X(f) = 2|\tilde{X}(f)|^2$.

In the above the transform used to define the PSD was presented as the Fourier transform. When working with discrete data, as is very common when analyzing real world data, there are a number of different ways of estimating the PSD. In the following three different methods will be presented, all used in this thesis.

RETHINK THIS PART. DO NOT USE TIME ON ALL THE CALCULATIONS. WRITE THE GENERAL IDEAS OF THE METHODS AND STATE HOW TO CALCULATE/COMPUTE. SMALL CODE SNIP TO GIVE GENERAL IDEA.

SIGNAL-BACKDIFF: RETHINK THIS PART. DO NOT USE TIME ON ALL THE CALCULATIONS. WRITE THE GENERAL IDEAS OF THE METHODS AND STATE HOW TO CALCULATE/-COMPUTE. SMALL CODE SNIP TO GIVE GENERAL IDEA.

Discrete and Fast Fourier Transform

The definition of the continuous Fourier transform and its inverse was presented in the above. The Fourier transform is as seen a way of representing the function under consideration as an infinite sum of periodic components. When the function is discrete, so will the Fourier transform be, and the integral is replaced with a sum. This gives us the Discrete Fourier Transform (DFT) which transforms the signal into a sum of separate components contributing at different frequencies. The DFT is dependent on the sampling interval, Δ , and we can describe our discrete signal X as a function of N discrete time steps $t_k = k \cdot \Delta$, where $k = 0, 1, \dots, N - 1$:

$$X_k \equiv X(t_k) \quad (4.7)$$

This sample size is supposed to be representative for the entire discrete function, if the function continues beyond the N sampled points. When sampling discretely at interval Δ , there will be a special frequency, the Nyquist critical frequency, defined through the sampling size as:

$$f_{NQ} \equiv \frac{1}{2\Delta}. \quad (4.8)$$

This frequency is of great importance in transformation of discrete signals. If the continuous signal is sampled at an interval Δ is bandwidth limited to frequencies smaller in magnitude than f_{NQ} , $\tilde{X}(f) = 0$ for $|f| \geq f_{NQ}$ - i.e. the transformed function has only non-zero values inside the Nyquist interval, $\tilde{X}(-f_{NQ}), \dots, \tilde{X}(f), \dots, \tilde{X}(f_{NQ})$. This means that the function is completely determined since we have all information about the signal contained in our available frequency space.

On the other hand, which is much more likely, if the continuous signal consists of frequencies both inside and outside the Nyquist interval, then all spectral information outside of this range will be falsely interpreted as being inside this range. Thus a wave inside the interval with a frequency of f_n will have a number of wave siblings outside of the interval, with frequencies of $k \cdot \frac{1}{\Delta} f_n$, k being integers, which will be aliased into the Nyquist interval and give rise to an increased power at the frequency f_n .

When analyzing an already measured discrete signal, this might give rise to some headache. What can be done is to assume that the signal has been sampled competently and then assume that the Fourier transform is zero outside of the Nyquist interval. After the analysis it will then be possible to determine if the signal was indeed competently sampled, as the Fourier series will go to zero at f_{NQ} given a correct assumption, and go to a fixed value, if the sampling was not done competently.

Now with the basics of understanding the limits of frequency transform of a discretely sampled signal, it is possible to estimate the DFT of the signal $X_k \equiv X(t_k)$. Since the Fourier transform is a symmetric transformation it is easiest to assume that N is even.

Since the input information is of size N we should expect only to sample the frequency transform $\tilde{X}(f)$ at only discrete values of f in the range between the upper and lower critical Nyquist frequencies, $-f_{NQ}$ to f_{NQ} :

$$f_n \equiv \frac{n}{N\Delta}, \quad n = -\frac{N}{2}, \dots, \frac{N}{2} \quad (4.9)$$

This will indeed actually give rise to $N + 1$ values, since 0 will be in the interval as well, but the limit frequencies are actually not independent, but all frequencies between are, which reduces it to N samples.

Now the integral from Equation 4.3 needs to be estimated as a sum:

$$\tilde{X}(f_n) = \int_{-\infty}^{\infty} X(\tau) e^{2\pi i f_n \tau} d\tau \approx \sum_{k=0}^{N-1} X_k e^{2\pi i f_n t_k} \Delta = \Delta \sum_{k=0}^{N-1} X_k e^{2\pi i k \frac{n}{N}} \quad (4.10)$$

The Discrete Fourier Transform is thus defined as:

$$\tilde{X}_n \equiv \sum_{k=0}^{N-1} X_k e^{2\pi i k \frac{n}{N}} \quad (4.11)$$

This gives the approximate relation between the DFT estimate and the continuous Fourier transform $\tilde{X}(f)$ when sampling at size Δ as:

$$\tilde{X}(f_n) \approx \Delta \tilde{X}_n \quad (4.12)$$

The inverse DFT is given as:

$$X_n \equiv \frac{1}{N} \sum_{n=0}^{N-1} X \tilde{X}_n e^{-2\pi i k \frac{n}{N}} \quad (4.13)$$

Computation of the DFT can be very slow and tiresome, since it involves complex multiplication between a number of vectors and matrices. If we write Equation 4.11 as $\tilde{X}_n = \sum_{k=0}^{N-1} W^{nk} X_k$, where W is a complex number $W \equiv e^{2\pi i/N}$. This shows that the vector X_k must be multiplied with a complex matrix which (n,k)th component consists of the constant W to the power of nk . This matrix multiplication evidently leads to a process of $O(N^2)$. Fortunately, a number of different algorithms implementing a wide range of different theories from complex number arithmetic and prime-factoring to group and number theory ([3],[6], [2] and others) have been developed for fast and efficient computation of the discrete Fourier transform. One of these is called the Fast Fourier Transform (FFT), which can reduce the computations to just $\mathcal{O}(N \log_2 N)$. In this thesis the FFT used is the one implemented in the `scipy.fft` Python package [19], which is based on the works of [3]. See said article for implementation details. One important thing about this specific algorithm is that for the algorithm to function most efficiently, the number of points computed in the frequency space must be of a power of 2, following the use of base \log_2 .

Nonuniform Discrete Fourier Transform

All FFT algorithms evaluates the DFT definitions from Eqs. 4.11 to 4.13 in fast and efficient ways. But one key assumption for these methods is that the data under examination are equispaced, i.e. uniformly distributed, based on the summation in Eq. 4.11. The computations thus expect uniform data as input and returns uniform data as output. Unfortunately this is not always the case for data collected in physical experiments. In this case the basic

assumptions for the calculations of both DFT and FFT are flawed.

The most general form of a nonuniform transform would be the one that takes non-equispaced data as input and also returns non-equispaced transforms as output. Firstly we wish to create a nonuniform discrete Fourier transform (NUDFT) that transforms a sequence of N complex numbers X_0, \dots, X_{N-1} to a different sequence of M complex numbers, $\tilde{X}_0, \dots, \tilde{X}_{M-1}$. The one-dimensional NUDFT computes the transformed vector $\tilde{\mathbf{X}} = (\tilde{X}_0, \dots, \tilde{X}_{M-1})^T$, with entries computed as the sum

$$\tilde{X}_k = \sum_{n=0}^{N-1} X_n e^{-2\pi i p_n f_k}, \quad 0 \leq k \leq M-1. \quad (4.14)$$

The values X_0, \dots, X_{N-1} are sample values, p_0, \dots, p_{N-1} are sample positions and f_0, \dots, f_{M-1} are frequencies. The NUDFT vector $\tilde{\mathbf{X}}$ is found by computing M sums with each N terms. This meaning that the computational cost will be of order $\mathcal{O}(M \cdot N)$, and if $M = N$ then of $\mathcal{O}(N^2)$. The NUDFT reduces to the DFT if the points are equispaced, $p_n = \frac{n}{N}$, and the frequencies are integers, $f_k = k$, and can be computed at the cost of the FFT, $\mathcal{O}(N \log_2 N)$. In the literature there are many who have presented different ways to develop a fast NUDFT ([16], [13], [15], [11] among others), generally referred to as NUFFT or NFFT. In this work though, the main focus is on the discrete cosine transform, and the NFFT methods will not be described in depth

Discrete Cosine Transform

The Fourier transform in any of its many forms is designed to process complex-valued signals, always producing a complex-valued spectrum, even for signals that were strictly real-valued. The real-valued or complex-valued part of the Fourier spectrum is on their own not enough to represent the full information of the signal, since neither the cosine nor the sine functions (corresponding to the real and the complex parts of the spectrum respectively), constitute a complete set of basis functions. Nonetheless, a purely real-valued signal has a symmetric Fourier spectrum, meaning that it is only necessary to compute half the number of spectral coefficients, without losing any signal information. Since the signals analyzed in this thesis are strictly real, one way to use this knowledge to improve on the works of this project is to consider a different, less expensive, purely real spectral transform. The cosine transform [1] seems to do the trick: it uses only cosine functions as basis functions and operates with only real-valued signal and spectral coefficients, and have properties similar

to the Fourier transform.

For the discrete version of the cosine transform, DCT, and its inverse, IDCT, a number of different definitions have been proposed, but for this work, the originally formulations by [1] are used. These are often referred to as "The DCT" and "The IDCT", and other times as DCT-II and DCT-III. The entries of the computed discrete cosine transform vector, $\tilde{X}_0, \dots, \tilde{X}_{M-1}$, of a real-valued signal of N data points, X_0, \dots, X_{N-1} , is computed as

$$\tilde{X}_k = 2 \sum_{n=0}^{N-1} X_n \cos \left(\frac{\pi(2n+1)k}{2N} \right), \quad 0 \leq k < M. \quad (4.15)$$

To orthonormalize the base functions, $\phi_k(n)$, the coefficients are multiplied by a scaling factor f :

$$f = \begin{cases} \frac{1}{\sqrt{2N}}, & \text{if } k = 0 \\ \frac{1}{\sqrt{4N}}, & \text{otherwise} \end{cases} \quad (4.16)$$

so that the base functions, $\phi_k[n] = 2f \cos \left(\frac{\pi(2n+1)k}{2N} \right)$, meet the condition:

$$\sum_{n=0}^{N-1} \phi_k[n] \phi_l[n] = \delta_{lk}. \quad (4.17)$$

The inverse of the DCT, the so called DCT-III, is defined, unnormalized, as:

$$X_k = \tilde{X}_0 + 2 \sum_{n=1}^{N-1} \tilde{X}_n \cos \left(\frac{\pi n(2k+1)}{2N} \right), \quad 0 \leq k < N \quad (4.18)$$

and orthonormalized:

$$X_k = \frac{\tilde{X}_0}{\sqrt{N}} + \sqrt{\frac{2}{N}} \sum_{n=1}^{N-1} \tilde{X}_n \cos \left(\frac{\pi n(2k+1)}{2N} \right), \quad 0 \leq k < N \quad (4.19)$$

Only when the DCT-III is orthonormalized is it exactly the inverse of the orthonormalized DCT-II. If they are both unnormalized, the DCT-III is the inverse of the DCT-II up to a factor $2N$. As with the DFT, the DCT can directly be computed at a cost of $\mathcal{O}(N \cdot M)$, and can also reduced to $\mathcal{O}(N \log N)$. The fast DCT algorithm(FCT) used here is based on [12] as it is implemented in the `scipy.fft.dct` package[19].

Nonuniform Discrete Cosine Transform

Again, as with the FFT, the FCT works under the key assumption that data is equispaced. Though when data is nonuniform, the DCT is described as:

$$\tilde{X}_k = 2 \sum_{n=0}^{N-1} X_n \cos \left(2\pi f_k \left(p_n + \frac{1}{2N} \right) \right), \quad 0 \leq k < M-1 \quad (4.20)$$

with, in the most general case, nonuniformly spaced signal, p_0, \dots, p_{N-1} , data and frequency data, f_0, \dots, f_{M-1} . The inverse of NDCT, the INDCT, is computed as:

$$X_k = \frac{\tilde{X}_0}{\sqrt{N}} + \sqrt{\frac{2}{N}} \sum_{n=1}^{N-1} \tilde{X}_n \cos \left(\left(p_n + \frac{1}{2N} \right) 2\pi f_k \right), \quad 0 \leq k < N-1 \quad (4.21)$$

It is possible to develop algorithms with the computational cost of $\mathcal{O}(N \log N)$ for NDCT and INDCT as it is for the NDFT ([18], [20]) but it has showed to be out of the scope of this project and has not been implemented. This of course slows down the final optimization algorithm, as it requires a number of spectral transformations. In Section ?? it is described how the final algorithm has been designed to minimize the use of NDCT, and thus speeding up the final computations.

Maximum Entropy Method (Burg's Method)

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Write this entire section - maybe not necessary? Maybe use in reconstruction of missing data...

4.1.2 Spectral Filtering

Wiener Filtering

Through spectral analysis it is possible to treat the noise of the signal consistently. The goal is to create spectral filters which enhances the signal while minimizing the effect of the noise, thus increasing the signal-to-noise ratio (SNR).

Theoretically, without any diffusion, the change in isotopic concentration would be described through a step function, going from one constant concentration to another. This step function can be described by the Heaviside function:

$$D(t) = \begin{cases} 0, & t < 0 \\ 1, & t \geq 0 \end{cases} \quad (4.22)$$

In reality, a number of different mixing processes change this step function, and the measured signal will be a smooth curve, $s(t)$, which corresponds to the convolution of $S(t)$ with the mixing response function $M(\tau)$

$$d(t) = \int_{-\infty}^{\infty} D(\tau) \cdot M(t - \tau) d\tau \quad (4.23)$$

4.1.3 Signal Restoration by Optimal Diffusion Length

Kernel Estimation

As is well known, in the spectral domain, convolution is multiplication and the mixing is described as the multiplication between the Fourier transform of S and M :

$$\tilde{d} = \tilde{D} \cdot \tilde{M} \quad (4.24)$$

By differentiation with respect to time, the mixing filter M is unaffected, and differentiation of the measured system response, the Heaviside function, S' is a delta function, which Fourier transformed is unity, leading to:

$$\tilde{d}' = \tilde{D}' \cdot \tilde{M} = \tilde{M} \quad (4.25)$$

The mixing filter can thus be determined by measuring the system response to a step function, differentiating performing Fourier transform of the result d' .

After determination of the mixing filter \tilde{M} , the unmixed signal D can be estimated in theory by inverse Fourier transform of

$$\tilde{D} = \tilde{d} \cdot \tilde{M}^{-1} \quad (4.26)$$

During the mixing, cycles with short wavelengths are heavily washed out, and through the restoration in Eq. 4.26, the amplitudes corresponding to these wavelengths are heavily amplified by the filter. This method though has a drawback, which is that when the measurements contain noise, the restored signal will be dominated by high-frequency noise, greatly amplified by the mixing filter. Thus it is a problem of retaining as much (short wavelength) signal as possible while simultaneously attempting to amplify the high-frequency noise as little as possible. This optimal trade-off can be found by creating an optimum filter for the considered measured isotopic signal:

$$\delta_M(z) = \delta_m(z) + \eta(z) \quad (4.27)$$

This optimal (Wiener) filter \tilde{F} , defined for each wave number $k = 2\pi\omega$, is presented as the ratio between pure signal and pure signal plus noise described in Power Spectral Densities as:

$$\tilde{F}(k) = \frac{|\tilde{\delta}_m(\omega)|^2}{|\tilde{\delta}_m(\omega)|^2 + |\tilde{\eta}(\omega)|^2} \quad (4.28)$$

In this work, the power spectral densities of the signal and the noise, respectively, are determined through analysis of the power spectral density of the combined signal/noise PSD.

The PSD of the noise free measured signal, $|\tilde{\delta}_m(\omega)|^2$, is assumed describe as

$$|\tilde{\delta}_m(\omega)|^2 = P_0 e^{-k^2 \sigma_{\text{tot}}^2} \quad (4.29)$$

where σ_{tot}^2 describes the total estimated diffusion length of the mixing.

The noise is assumed to be red noise, described by an autoregressive process of first order, AR1:

$$|\tilde{\eta}(\omega)|^2 = \frac{\sigma_\eta^2 \Delta z}{|1 + a_1 \exp(-2\pi i \omega \Delta z)|^2} \quad (4.30)$$

where σ_η^2 is the variance of the red noise, a_1 is the AR1 coefficient and Δz is the resolution of the time/depth data. It is then possible to estimate the parameters P_0 , σ_{tot}^2 , σ_η^2 and a_1 by curve fitting, separately, the two expressions in Eq. 4.29 and 4.30 to the data. The estimated parameters are varied to find the optimal guess to use for the filter.

4.2 Enhanced Resolution and Restoration of Signal

4.2.1 Interpolation of Data

For the purpose of this thesis, interpolation of data needs to be fast, efficient and result in a function as smooth as possible. The last criterion is due to the knowledge of the nature of the data. The measurements are not continuous but should indeed in theory be so. Thus a good choice for interpolation of the data examined in this thesis would be the cubic spline interpolation. An instance of a such interpolation can be seen in Figure ??.

Cubic spline interpolation has been used in two instances during this analysis, both times through the Python SciPy package `scipy.interpolate.CubicSpline`. Firstly, to assure equally spaced data points, so as to be able to perform a

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useful frequency analysis through spectral transformation, see Section, ??.

Secondly cubic spline interpolation was used to improve on peak detection in the final back diffused data. The final data have a rather low resolution, leading to an initial guess of peak positioning that might be shifted due to the discretization. Through cubic spline interpolation it is possible to construct a smooth estimate of a signal of higher resolution, leading to a peak positioning estimate that might be less shifted, see Figure ??.

4.2.2 Detrending and Standardising

4.2.3 Cycle Length Estimation of Detrended Signal

SIGNAL-STANDARD: Think about if this is necessary. Maybe work into recursivity and constraints in Method?

SIGNAL-CYCLE: Think about if this is necessary. Maybe work into recursivity and constraints in Method?

Chapter 5

Computational Methods

5.1 Splines and Interpolation

5.1.1 Interpolation

Interpolation is a tool that can be used - and misused - to extract more information out of a given set of data. Used correctly, interpolation can reveal more information than is initially available and disclose connections not apparent at first, but used incorrectly, it can be manipulated to infer misleading correlations and lead to inaccurate conclusions. Thus it is a tool that must be used with care. Aiming to avoid incorrect deductions and inferences one should at first gain as much knowledge about the data at hand as possible. By understanding how the data have come about and gaining knowledge about the underlying physical theories a somewhat deficient data set can robustly and securely be interpolated to accommodate the needs of the analysis. In the case of this thesis, both knowledge about data gathering and the physics at play have been gained and thus some of the common fallacies may be avoided. The limits of the data available is due to the discrete sampling, leading to a minimum sampling of about 26 samples per meter of ice. When considering that the depth series of 32 years between Tambora and Laki is just above 10 meters, this means that each meter of ice needs to contain at least three years on average. 26 samples per three years might not sound as a bad sampling interval, but if the goal is to show seasonality and give a best estimate of annual layer thickness, interpolation could be put to good use to be able to give better estimates of the exact placement of peaks and valleys.

Existence, Uniqueness and Conditioning

Considering any attempt to create an interpolant to fit a number of data

points, the questions of uniqueness and existence is a matter of matching the data points with the number of parameters in the interpolant. If there are too few parameters, the interpolant does not exist, as it will not pass through all data points. If there are too many, the interpolant will not be unique. Formally this can be described through a system of linear equations.

For any data set consisting of (t_i, y_i) , $i = 1, \dots, m$ points, an interpolant can be chosen from a function space spanned by some suitable set of basis functions, $\phi_1(t), \dots, \phi_n(t)$. The interpolant can then be described as a linear combination of these basis functions:

$$f(t) = \sum_{j=1}^n x_j \phi_j(t) \quad (5.1)$$

The interpolant can then be found by determining the parameters x_j by requiring that the interpolant f must pass through the M data points (t_i, y_i) :

$$f(t_i) = \sum_{j=1}^n x_j \phi_j(t_i) = y_i, \quad i = 1, \dots, m \quad (5.2)$$

This can of course also be written compactly in matrix form as a system of linear equations:

$$\mathbf{A}\mathbf{x} = \mathbf{y} \quad (5.3)$$

In this equation \mathbf{A} is the $m \times n$ basis matrix, which entries consists of the value of the n basis functions evaluated at the m data points, $a_{ij} = \phi_j(t_i)$, the m vector \mathbf{y} consists of the known data values y_i , and the n vector \mathbf{x} consists of the unknown, to be determined, parameters x_j .

From linear algebra we know, that if we choose the number of basis function to be equal to the number of data points, $n = m$, the basis matrix will be square, and thus - given the matrix is nonsingular - the system will be determined, and the data points can be fit exactly. Though in some problems it is beneficial to choose the system to be either overdetermined (less parameters than data points, the data cannot be fit exactly) or underdetermined (more parameters than data points, giving freedom to allow satisfaction of additional properties or conditions).

So the existence and uniqueness of an interpolant is given by the non-singularity of the basis matrix, be it square or not and the conditioning of the matrix points to the parameters' sensitivity to perturbations. An ill-conditioned basis matrix will lead to high sensitivity in the parameters, but this problem can still be approximately solvable through Gaussian elimination with partial pivoting, but this solution will mean that the coefficients may be poorly determined.

Polynomial Interpolation

The most common way to determine an interpolant is through polynomials. Denoting a set of all polynomials of degree at most k , $k \geq 0$ as \mathbb{P}_k , it can be seen that this set forms a vector space of dimension $k+1$. The basis functions that span this vector space can be chosen to be composed of a number of different functions and this choice has a great influence on both the cost of computation and manipulation of the interpolant, and the sensitivity of the parameters, i.e. the conditioning of the basis matrix.

Considering n data points it is obvious to choose $k = n-1$ so that the dimension of the vector space matches the number of data points. The maybe most natural choice of basis for \mathbb{P}_{n-1} is one that consists of the first n monomials¹,

$$\phi_j(t) = t^{j-1}, \quad j = 1, \dots, n. \quad (5.4)$$

Thus any given polynomial $p_{n-1} \in \mathbb{P}_{n-1}$ will be of the form

$$p_{n-1}(t) = x_1 + x_2 t + \dots + x_n t^{n-1}. \quad (5.5)$$

In this basis the system of $n \times n$ linear equations will be of the form

$$\mathbf{A}\mathbf{x} = \begin{bmatrix} 1 & t_1 & \dots & t_1^{n-1} \\ 1 & t_1 & \dots & t_1^{n-1} \\ \vdots & \vdots & \ddots & \vdots \\ 1 & t_1 & \dots & t_1^{n-1} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix} = \begin{bmatrix} y_1 \\ y_2 \\ \vdots \\ y_n \end{bmatrix} = \mathbf{y}. \quad (5.6)$$

This type of matrix with geometric progression, i.e. the columns are successive powers of some independent variable t is called a Vandermonde matrix. When using the monomial basis and using a standard linear equation solver to determine the interpolants coefficients requires $\mathcal{O}(n^3)$ work and often results in ill-conditioned Vandermonde matrices \mathbf{A} , especially for high-degree polynomials. This ill-conditioning is due to the monomials of higher and higher degree being more and more indistinguishable from each other. This makes the columns of \mathbf{A} nearly linearly dependent, resulting in almost singular matrices, and thus highly sensitive coefficients. For high enough n , the Vandermonde matrix becomes efficiently singular, to computational precision at least, though, as mentioned, this can be worked around, but requires some additional computational work.

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Maybe an illustration here? See pp. 314 in Scientific Computing.

¹Roughly speaking, a polynomial with only one term.

Piecewise Polynomial Interpolation and Splines

The amount of work needed to solve the system as well as the conditioning of the system can be improved by using a different basis all together. Some different bases superior to the monomial that are worth mentioning are the Lagrange basis functions, the Newton basis functions and the orthogonal polynomials. But for this thesis we take a step further into the interpolation theory, as the choice of basis functions might not be enough to work around some of the problems connected with fitting a single polynomial to a large number of data points (i.e. oscillatory behaviour in the interpolant, nonconvergence or issues around the boundaries).

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These practical and theoretical issues can be avoided through the use of piecewise polynomial interpolation, with the advantage that a large number of data points can be fitted with low-degree polynomials.

When turning to piecewise polynomial interpolation of the data points (t_i, y_i) , $i = 1, \dots, n$, $t_1 < t_2 < \dots < t_n$, a different polynomial is chosen for each subinterval $[t_i, t_{i+1}]$. Each point t_i , where the interpolant changes is called knots or control points. The simplest piecewise interpolation is piecewise linear interpolation, where each knot is connected with a straight line. If we consider this simple example it appears that by eliminating the problems of nonconvergence and unwanted oscillatory behaviour, the smoothness of the interpolant is sacrificed. This might be true for this simplistic example but since there are a number of degrees of freedom in choosing each piecewise polynomial interpolant, the smoothness can be reintroduced by exploiting a number of these measures. One way of doing this is by demanding knowledge of both the values and the derivatives of the interpolant at each data point. This just adds more equations to the system, and thus to have a well-defined solution, the number of equations must match the number of parameters. This type of interpolation is known as Hermite interpolation. The most common choice for this interpolation, to still maintain simplicity and computational efficiency, is cubic Hermite interpolation. This introduces a piecewise cubic polynomial with n knots, and thus $n - 1$ interpolants each with 4 parameters to fit, leading to $4(n - 1)$ parameters to be determined. Since each of the $n - 1$ cubics must match the data points at each end of the subinterval, it results in $2(n - 1)$ equations, and requiring the derivative to be continuous, i.e. match at the end points, an additional of $n - 2$ equations are taken in. This leads to a system consisting of $2(n - 1) + (n - 2) = 3n - 4$ equations to fit to the $4n - 4$ parameters. This leaves n free parameters, meaning that a cubic Hermite interpolant is not unique and the remaining free parameters can be used to accommodate further or additional constraints that might be around the problem at hand.

Cubic Spline Interpolation

One way of using the remaining free parameters is by introducing *splines*. A cubic spline is, given the spline definition, a piecewise cubic polynomial, a polynomial of degree $k = 3$, and must then be $k - 1 = 2$ times differentiable. Thinking back on the Hermite cubic, we were left with n free parameters. By demanding continuity of also the second derivative, we introduce $n - 2$ new parameters, leaving only 2 final parameters to be free. These 2 remaining parameters can be fixed through a number of different requirements, e.g. by forcing the second derivative at the endpoints to be zero, which leads to the *natural* spline.

The Hermite and spline interpolations are useful for different cases. The Hermite cubic might be more appropriate for preserving monotonicity if it is known that the data are monotonic. On the contrary, the cubic spline may enforce a higher degree of smoothness as it takes the second derivative into account as well.

A spline is a piecewise polynomial of degree k that is continuously differentiable $k - 1$ times.

5.2 Peak Detection

5.3 Parallelization

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Write this entire section

COMP-PARAL: Do
some actual parallelization! And write this entire section

Chapter 6

Estimating σ from Data: Methods and Algorithms

6.1 Estimating σ from Data: First Estimate

This section contains a walk through of the method to back diffuse a given ice core depth series to attempt to restore as much of the original signal as possible. For now, the method has been developed for sections that has been dated to be between the two volcanic eruptions Laki and Tambora, as these are very well dated, and thus it is possible to find the optimal diffusion length to back diffuse with as the actual number of annual layers is exactly known for this data series. The method is easily modified for any other dated depth series, as what is needed is just the number of annual layers in the given data series.

Figure 6.1 shows a flowchart of the method used to estimate the diffusion length of a depth series with a preliminary guess of number of annual layers. In the following sections each of the steps in the method will be discussed more thoroughly and examples will be given, all based on the Greenlandic ice core drilled at Site A near Crete(REFERENCES!!!). The method is built such that it takes two inputs - the isotopic depth series, and the specifications for the particular ice core - and uses these for the first preliminary computations needed to make a first, naïve guess of the diffusion length, σ_0 . This diffusion length is then used to deconvolute the data and give a first estimate of the number of peaks in the data series. If this number is different from the already specified number of annual layers - in this case 32 - then the diffusion length will be updated accordingly: If the counted number is higher(lower) than the actual number, the diffusion length is adjusted downwards(upwards) with $\Delta\sigma_2$

and the deconvolution and peak counting is performed again. On the other hand, if the counted number is equal to the actual number, then the diffusion length is optimized to find the largest diffusion length which still gives the actual number of counted peaks. When this σ_{final} is reached, the algorithm stops and returns the final diffusion length estimate along with the associated back diffused depth series.

6.1.1 Input

To compute the final diffusion length and depth series, two inputs are needed: the measured isotopic depth series and the specifications of the examined core. Through this section all examples have been carried out using the core Site A.

Core	Drilled	Core length	Geographic position		Elevation	Laki	Tambora	Mean accum. rate	Temp. at 10m	Temp at 20m
ID	[Yr]	[m]	Latitude [°N]	Longitude [°E]	[m a.s.l.]	[m]	[m]	[m ice/Yr]	[°C]	[°C]
Crete	1974	404.0	71.12	322.68	3172	74.75	64.70	0.280	-30.40	-30.16
Milcent	1973	398.0	70.30	315.00	2410			0.530	-22.30	-0.00
Camp C	1977	100.1	77.18	298.89	1880	91.50	78.50	0.380	-24.29	-24.35
SiteA	1985	128.6	70.63	324.18	3092	80.85	70.90	0.307	-29.41	-29.41
SiteB	1984	105.6	70.65	322.52	3138	83.70	73.00	0.327	-29.77	-29.48
SiteC	1984	24.9	70.68	321.21	3072			0.340	-29.10	-28.54
SiteD	1984	100.1	70.64	320.38	3018	93.80	81.50	0.365	-28.30	-27.89
SiteE	1985	77.8	71.76	324.15	3087	62.95	53.40	0.225	-30.37	-30.41
SiteF	1985	25.7	71.49	324.12	3092			0.237	-30.42	-30.36
SiteG	1985	70.8	71.15	324.16	3098	69.40	60.50	0.251	-30.10	-30.01
SiteH	1985	26.2	70.87	324.16	3102			0.277	-29.59	-29.53

Table 6.1: Overview of specifications of all examined Greenlandic ice cores.

In Figure 6.2 the depth series between the eruptions Laki and Tambora can be seen along with the entire ice core in the background. This is the diffused, measured raw data from Site A. Dating of the ice cores has been carried out by matching Electrical Conductivity Measurements (ECM, Section ??) with water isotopic - in this case $\delta^{18}\text{O}$ - data measured at the same depths. By doing so it is possible to identify known volcanic horizons in the ECM data and thus getting a sharp marker of when the precipitation of that given depth fell. In Figure 6.3 the matched ECM and $\delta^{18}\text{O}$ profiles can be seen with Tambora marked at depth ---- and Laki at depth ----.

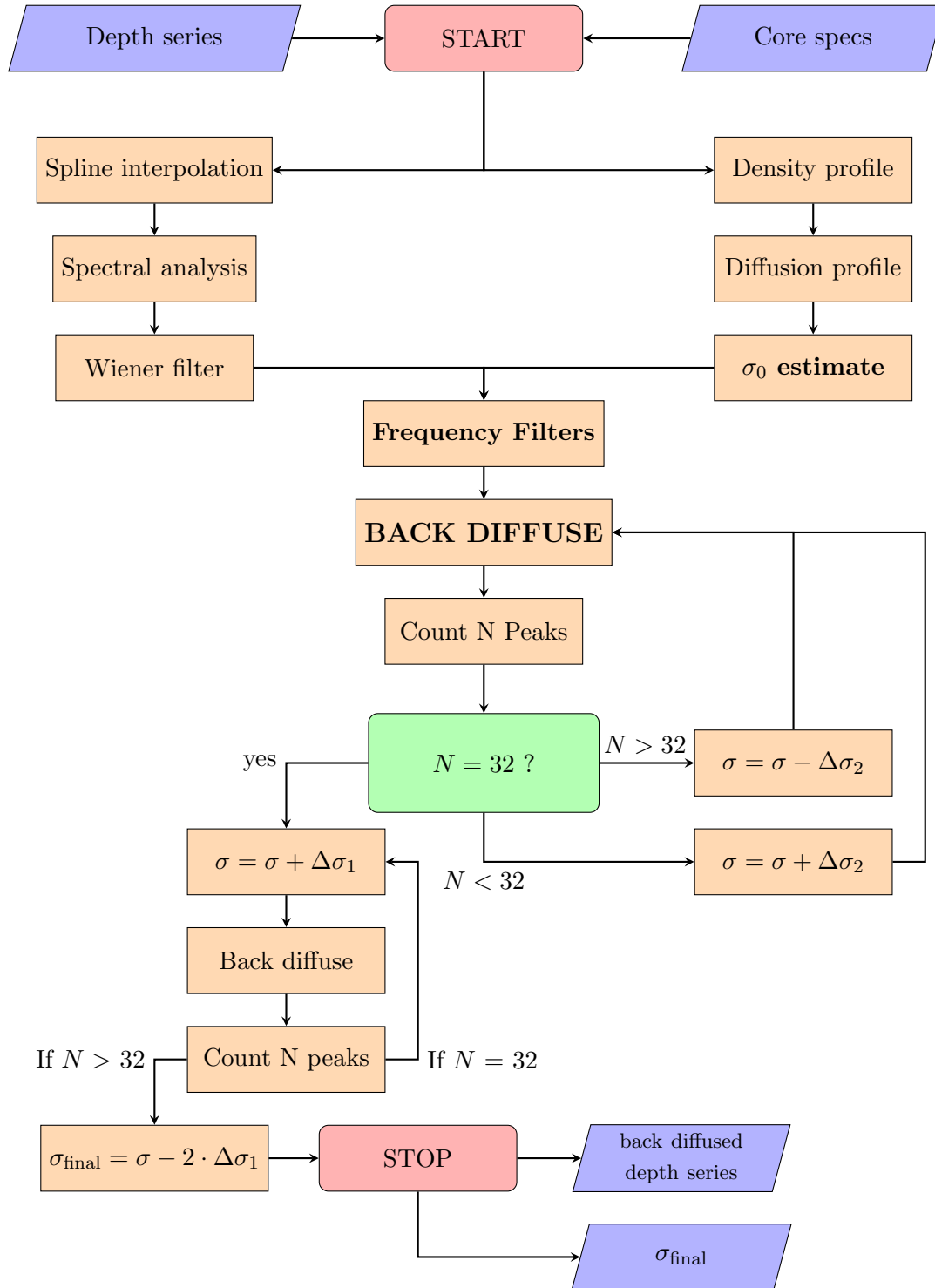


Figure 6.1: Flowchart of method for diffusion length computation.

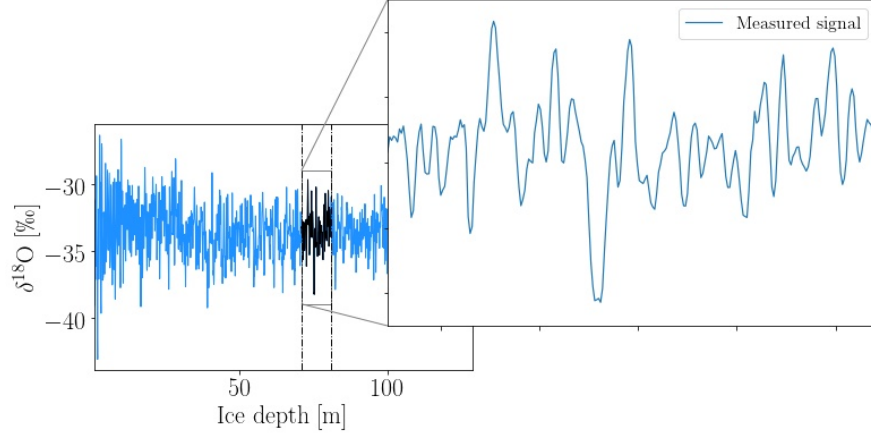


Figure 6.2: The entire ice core isotopic profile from Site A, with a zoom in on the estimated depth series spanning from Tambora to Laki.

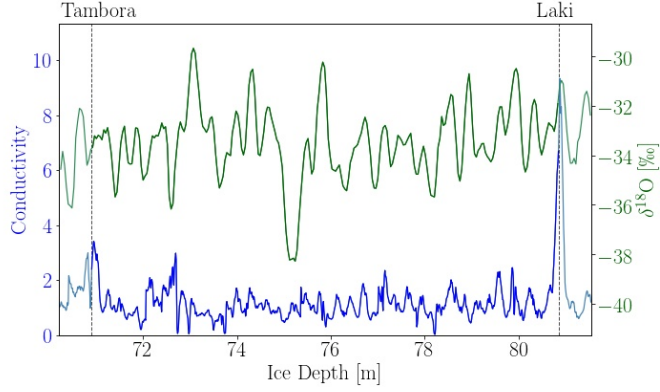


Figure 6.3: Two depth profiles from the core drilled at Site A showing accordingly the measured $\delta^{18}\text{O}$ isotopic values and the conductivity measurements in the depth ranging from the estimated Tambora eruption to the Laki eruption.

6.1.2 Preliminary Computations

From the inputs a number of preliminary computations need to be carried out before the optimization of the diffusion length can be performed. For the depth series this consists of first interpolating the data to make sure that the depth series is evenly sampled, then an analysis of signal and noise in the frequency spectrum needs to be carried out, and from this spectral analysis

a Wiener filter can be constructed to find the optimal high frequency cut off, where as much noise as possible is filtered away while losing as little of the signal as possible. These computations are all based on the depth series data and use only signal analysis theory.

The input of core specifications on the other hand is used to give a more theoretical view of the situation. From these preliminary inputs, containing accumulation rate, borehole temperatures, altitudes and other conditions, it is possible to use ice core and ice flow theory to compute initial estimates of density and diffusion profiles at the given site. From these profiles along with the volcanic horizons indicating the series of interest, an initial estimate of the diffusion length at the depth of Laki to Tambora.

Firstly, the computations associated with the core site specifications are considered and later the ones associated with inputted depth series are described.

Core Specifications: Density Profile

From the input core specifications, specifically the surface temperature, T_0 and accumulation rate, \dot{b}_0 , it is possible to estimate a density/depth profile through the Herron-Langway model described in section ???. This section will contain a brief walk through of the algorithm used to estimate this profile. The Herron-Langway density profile program needs an estimate of surface temperature and annual accumulation rate, but does also take depth-density measurements into the calculations, if they exist and a surface density can also be specified to be taken into account. The adjustable input values and their default values can be seen in Table 6.2. The parameters describe surface temperature, T_0 , annual accumulation rate, \dot{b}_0 , surface density, ρ_0 , density of ice, ρ_{ice} , critical density, ρ_{Cr} , close off density, ρ_{CO} , fit fudge parameters for upper and lower densification zones, f_0 and f_1 , and depth and density measurements, z_{meas} and ρ_{meas} .

The program is built to estimate a semi-analytical estimate of the depth-density profile given certain surface conditions. Furthermore it returns not only the density profile but computes the derivatives $\frac{d\rho}{dz}$ and $\frac{d\rho}{dt}$, and a timescale estimate for the profile. Two calculations repeats themselves, the computation of the values k_0 and k_1 and will just be mentioned this once:

$$k_0 = f_0 \cdot 11 \cdot e^{-\frac{10160}{T_0 \cdot R}} \quad (6.1)$$

$$k_1 = f_1 \cdot 575 \cdot e^{-\frac{21400}{T_0 \cdot R}} \quad (6.2)$$

The program consists of the following different modules:

Variable	Default
T_0	(218.15 K)
\dot{b}_0	(0.027 $\frac{\text{m}}{\text{yr}}$)
ρ_{surf}	(330 $\frac{\text{kg}}{\text{m}^3}$)
ρ_{ice}	917 $\frac{\text{kg}}{\text{m}^3}$
ρ_{Cr}	550 $\frac{\text{kg}}{\text{m}^3}$
ρ_{CO}	804 $\frac{\text{kg}}{\text{m}^3}$
f_0^{init}	1
f_1^{init}	1
z_{meas}	-
ρ_{meas}	-

Table 6.2: Input variables and their default values.

- **calc_dens0**: Calculate surface density. Use default surface value, $\rho_{\text{surf}} = 330 \frac{\text{kg}}{\text{m}^3}$, if no measurements available. Otherwise calculate surface density by using $z_{\text{init}} = z_{\text{meas}}[0]$ and $\rho_{\text{init}} = \rho_{\text{meas}}[0]$ as:

$$\rho_{\text{surf}} = \frac{\rho_{\text{ice}}}{1 + \frac{\rho_{\text{ice}} - \rho_{\text{init}}}{\rho_{\text{init}}} \cdot e^{z_{\text{init}} \cdot \rho_{\text{ice}} \cdot k_0}} \quad (6.3)$$

- **calc_zCr**: Calculate ice depth of critical density (i. e. depth of boundary between first and second stage of densification), $\rho_{\text{Cr}} = 550 \frac{\text{kg}}{\text{m}^3}$:

$$z_{\text{Cr}} = \frac{1}{\rho_{\text{ice}} \cdot k_0} \cdot \left(\ln \left[\frac{\rho_{\text{Cr}}}{\rho_{\text{ice}} - \rho_{\text{Cr}}} \right] - \ln \left[\frac{\rho_{\text{surf}}}{\rho_{\text{ice}} - \rho_{\text{surf}}} \right] \right) \quad (6.4)$$

- **model_0**, **model_1**: Models describing the two first stages of densification. Computed as:

$$\rho_0(z) = \rho_{\text{ice}} \cdot \left(\frac{Z_0(z)}{1 + Z_0(z)} \right), \quad Z_0(z) = e^{\rho_{\text{ice}} \cdot k_0 \cdot z + \ln(\frac{\rho_{\text{surf}}}{\rho_{\text{ice}} - \rho_{\text{surf}}})} \quad (6.5)$$

$$\rho_1(z) = \rho_{\text{ice}} \cdot \left(\frac{Z_1(z)}{1 + Z_1(z)} \right), \quad Z_1(z) = e^{\frac{\rho_{\text{ice}} \cdot k_1 \cdot (z - z_{\text{Cr}})}{\sqrt{b_0}} + \ln(\frac{\rho_{\text{Cr}}}{\rho_{\text{ice}} - \rho_{\text{Cr}}})} \quad (6.6)$$

where $\rho_0(z)$ corresponds to all $z \leq z_{\text{Cr}}$ and $\rho_1(z)$ to all $z > z_{\text{Cr}}$.

- **fit_f0**, **fit_f1**: Both modules are only used if any measured data is available. If depth and density data exists then these routines will compute the optimal (least-squares) fudge parameters f_0 and f_1 , see Equations 6.1 and 6.2, by fitting the data with the models for ρ_0 and ρ_1 described above. These updated fudge parameters are then henceforth used in the programs computations.
- **dens_to_depth**: From a given density, calculate the corresponding depth. Same as **calc_zCr**, but for any density, in both stages of densification.

$$z_0(\rho) = \frac{1}{\rho_{\text{ice}} \cdot k_0} \left(\ln \left[\frac{\rho}{\rho_{\text{ice}} - \rho} \right] - \ln \left[\frac{\rho_{\text{surf}}}{\rho_{\text{ice}} - \rho_{\text{surf}}} \right] \right), \quad \rho \leq \rho_{\text{Cr}} \quad (6.7)$$

$$z_1(\rho) = \frac{b_0}{\rho_{\text{ice}} \cdot k_1} \left(\ln \left[\frac{\rho}{\rho_{\text{ice}} - \rho} \right] - \ln \left[\frac{\rho_{\text{Cr}}}{\rho_{\text{ice}} - \rho_{\text{Cr}}} \right] \right) + z_{\text{Cr}}, \quad \rho > \rho_{\text{Cr}} \quad (6.8)$$

- `drho_dz_0`, `drho_dz_1`: Compute the first derivative with respect to z , both stages of densification:

$$\frac{d\rho_0}{dz} = \rho_{\text{ice}}^2 \cdot k_0 \cdot Z_0 \cdot \left[\frac{1 + 2 \cdot Z_0}{(1 + Z_0)^2} \right], \quad \rho_0 \leq \rho_{\text{Cr}} \quad (6.9)$$

$$\frac{d\rho_1}{dz} = \rho_{\text{ice}}^2 \cdot k_1 \cdot Z_1 \cdot \frac{1}{\sqrt{b_0}} \cdot \left[\frac{1 + 2 \cdot Z_1}{(1 + Z_1)^2} \right], \quad \rho_0 > \rho_{\text{Cr}} \quad (6.10)$$

with Z_0 and Z_1 as described in Equations 6.5 and 6.6.

- `drho_dt`: Compute the time evolution of the density profile as the derivative of ρ :

$$\frac{d\rho_0}{dt} = k_0 \cdot \dot{b}_0 \cdot (\rho_{\text{ice}} - \rho_{\text{surf}}), \quad \rho_0 \leq \rho_{\text{Cr}} \quad (6.11)$$

$$\frac{d\rho_1}{dt} = k_1 \sqrt{\dot{b}_0}, \quad \rho_1 > \rho_{\text{Cr}} \quad (6.12)$$

- `time_scale_HL`: From the best optimized Herron-Langway depth-density profile estimate it is possible to compute a age-density profile estimate for the firn column. For the first stage of densification this is computed as:

$$t_0(\rho) = \frac{1}{k_0 \dot{b}_0} \cdot \ln \left[\frac{\rho_{\text{ice}} - \rho_{\text{surf}}}{\rho_{\text{ice}} - \rho} \right], \quad \rho_0 \leq \rho_{\text{Cr}} \quad (6.13)$$

The age of the second stage of densification is computed in the same fashion, and then adding the age at the boundary between the two stages, that is, the critical density, t_{Cr} :

$$t_1(\rho) = \frac{1}{k_1 \sqrt{\dot{b}_0}} \cdot \ln \left[\frac{\rho_{\text{ice}} - \rho_{\text{Cr}}}{\rho_{\text{ice}} - \rho} \right] + t_{\text{Cr}}, \quad \rho_{\text{Cr}} < \rho < \rho_{\text{ice}} \quad (6.14)$$

In Figure 6.4 an example of the semi-analytical depth-density modelling can be seen for the core drilled at Site A. It shows the measured depth and density data (black), the purely analytical model (blue) and the semi-analytical fit-to-data-model (orange). The first and second stages of densification can clearly be seen in both data and model as a kink in a depth just shy of 20 m.

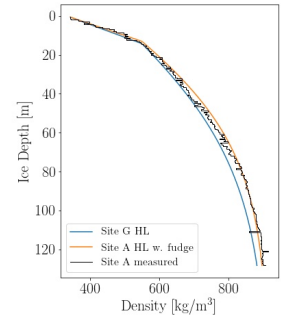


Figure 6.4: Depth density profile at Site A.

Core Specifications: Diffusion Profile

Core Specifications: σ_0 estimate

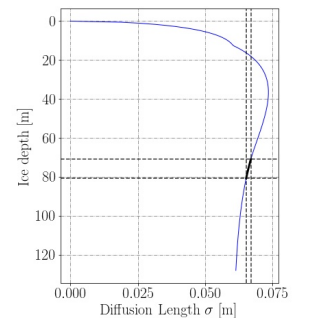


Figure 6.5: Estimated diffusion profile at Site A given a Herron Langway model

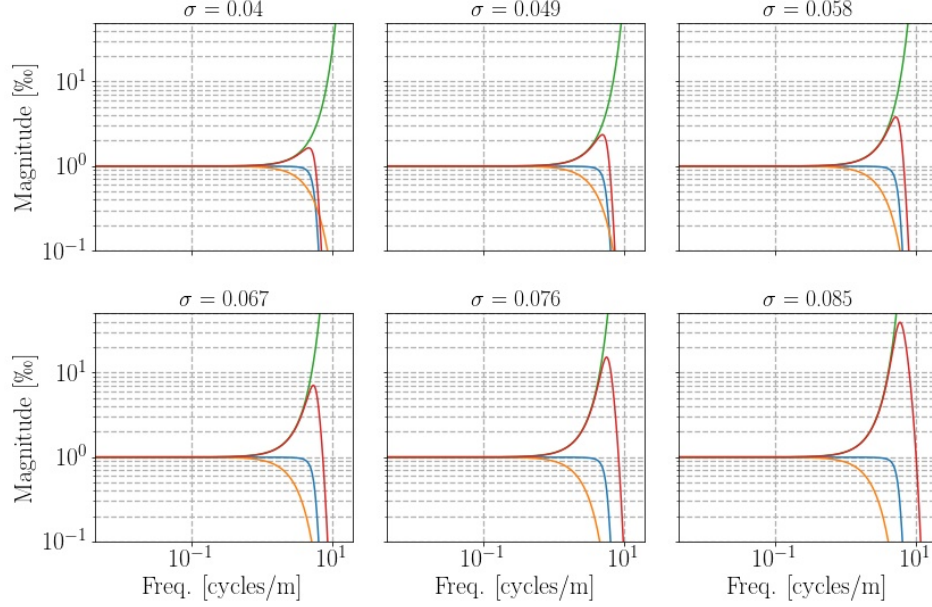


Figure 6.6: Frequency filter examples ranging from diffusion length 0.04 m to 0.085 m.

6.1.3 Back Diffusion/Deconvolution

Depth Series: Spline Interpolation

When working with ice core data, it is not always a certainty that the data you get from the field are as continuous or as evenly sampled as one could have hoped. A lot of factors are at play when drilling, transporting, dividing and cutting an ice core for laboratory studies. Some parts of an ice core contain brittle zones where the ice is likely to break, leaving a section almost impossible to analyze. When transporting the drilled ice cores they are susceptible to both melting and contamination and evaporation of the outermost ice layer of the core. And finally of course there is a number of uncertainties that occur when cutting an ice core into discrete bits to be measured. The quality of data varies rather greatly from site to site, from drill team to drill team and of course from laboratory to laboratory.

When looking at the depth series only it might not be an issue to have various spacing between the discrete measurements, but when it comes to spectral analysis, it is of necessity to obtain a depth series signal with an even

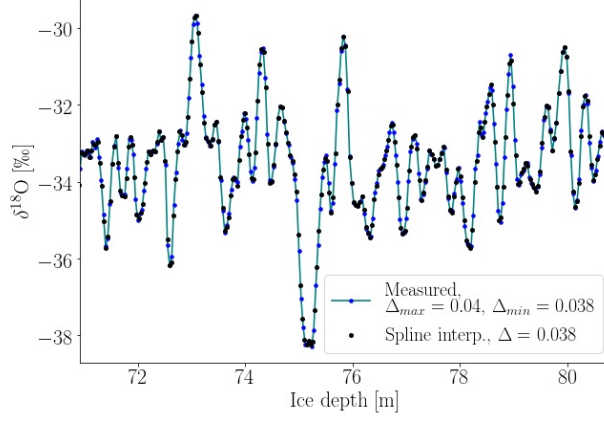


Figure 6.7: The unevenly measured data from Site A in the depth ranging from Tambora to Laki along with the now evenly sampled cubic spline interpolated data. Sampled with an interval of $\Delta = 0.038$.

distribution. To accommodate this need interpolation of the signal can be of use. In the case of the ice core drilled at Site A, it can be seen from Figure 6.7 that the raw measured signal has a minimum sampling size of $\Delta_{\min} = 0.038$ and a maximum sampling size of $\Delta_{\max} = 0.040$. To be able to analyze this signal in the spectral domain the signal can be numerically resampled with an even sampling rate. This is done by choosing the minimum sampling size available, $\Delta_{\min} = 0.038$, and redistributing the depth data points to be evenly spaced with this sampling size. The redistribution is carried out as follows.

Assuming the original depth array \mathbf{d} is distributed as $d_{i-1} < d_i < d_{i+1}$ with $i = 0, \dots, n-1$ has a minimum sampling distance as Δ_{\min} we define the new sampling distance for the new depth array $\hat{\mathbf{d}}$ as $\Delta = \Delta_{\min}$ - again assuming that $\hat{\mathbf{d}}_{j-1} < \hat{\mathbf{d}}_j < \hat{\mathbf{d}}_{j+1}$ with $j = 0, \dots, \hat{n}-1$. This makes it possible to define the first and last value of the new array as

$$\hat{\mathbf{d}}_0 = \Delta \lceil \frac{\mathbf{d}_0}{\Delta} \rceil, \quad (6.15)$$

$$\hat{\mathbf{d}}_{\hat{n}-1} = \Delta \lfloor \frac{\mathbf{d}_{n-1}}{\Delta} \rfloor. \quad (6.16)$$

From this the number of values in the new array, \hat{n} , can be determined as

$$\hat{n} = 1 + \frac{\hat{\mathbf{d}}_{\hat{n}-1} - \hat{\mathbf{d}}_0}{\Delta}, \quad \hat{n} \in \mathbb{Z}. \quad (6.17)$$

Thus our new depth array will be given as

$$\hat{\mathbf{d}} = \hat{\mathbf{d}}_0 + j \cdot \Delta, \quad j = 0, \dots, \hat{n} - 1. \quad (6.18)$$

The original data are then used to define a cubic spline interpolation function to which the redistributed depth data points can be matched. For this part of the data analysis the `SciPy.interpolate` Python (REFERENCE) package with `SciPy.interpolate.CubicSpline` for the cubic spline interpolation. This gives a new distribution of data points as seen in Figure 6.7.

```

1 def interpCores(self, pad = 1):
2
3     # Method in BackDiffuse class
4
5     isoData = self.d180Data
6     d_in = isoData['depth']
7     x_in = isoData['d180']
8
9
10    if self.interpAll:
11        valMin = d_in.min()
12        valmax = d_in.max()
13    else:
14        valMin = self.depthMin - pad
15        valMax = self.depthMax + pad
16
17
18    d = d_in[(d_in >= valMin) & (d_in <= valMax)]
19    x = x_in[(d_in >= valMin) & (d_in <= valMax)]
20
21    diff = np.diff(d)
22    Delta = round(min(diff), 3)
23
24    d_min = Delta * np.ceil(d.values[0]/Delta)
25    d_max = Delta * np.floor(d.values[-1]/Delta)
26
27    n = int(1 + (d_max - d_min)/Delta)
28
29    j_arr = np.linspace(0,n,n)
30    dhat0 = d_min + (j_arr - 1)*Delta
31
32    f = interpolate.CubicSpline(d,x)
33
34    xhat0 = f(dhat0)
35
36    dhat = dhat0[(dhat0 >= self.depthMin) & (dhat0 <= self.
37    depthMax)]
38    xhat = xhat0[(dhat0 >= self.depthMin) & (dhat0 <= self.
39    depthMax)]

```

```

38
39 return dhat, xhat, Delta

```

Listing 6.1: Spline interpolation of $\delta^{18}O$ data.

Implementation of Spectral Transforms

Depth Series: Spectral Analysis

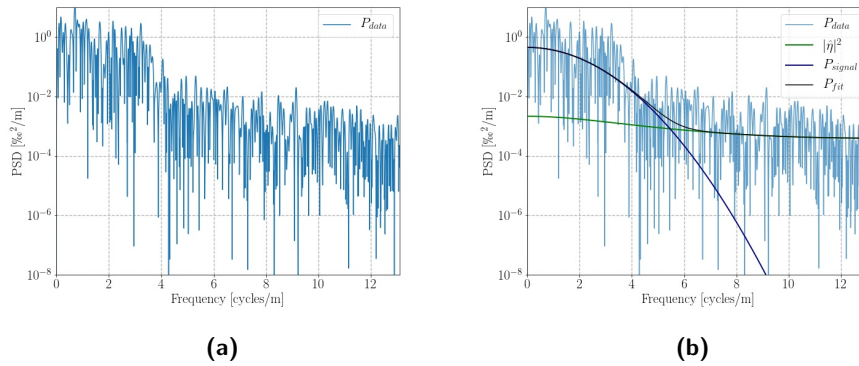
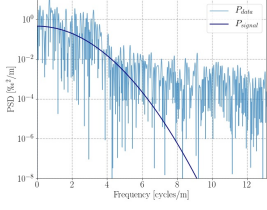


Figure 6.8: Spectral Analysis. **(a)** The power spectral density(PSD) of the interpolated data from Site A shown in Figure 6.7. The PSD was computed through a Discrete Cosine Transform(DCT). **(b)** Spectral estimate of the depth series from Tambora to Laki along with fit to entire spectral data set and the separated estimates of the noise and signal functions, as described in section ??

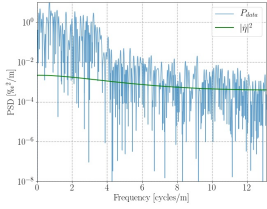
Now with evenly spaced depth series data it is possible to transform the data to the frequency domain and perform spectral analysis on the signal. The basic theory concerning Fast Fourier Transform(FFT), Discrete Cosine Transform(DCT) and Power Spectral Densities(PSD) is discussed in Section ??. In this section the theory is merely put to use. Since the data under examination is completely real with no imaginary parts, pointing towards the sensibility of working only with cosines to enhance computational speed. Furthermore the DCT implies different boundary conditions than the FFT, meaning that some of the odd spectral behaviour, like aliasing can be avoided by using a different transform.

For the depth series between Laki and Tambora at Site A, the PSD computed through the DCT as $PSD = |DCT|^2$ can be seen in Figure 6.8a. This spectrum shows a higher intensity in the low frequency area and a lower intensity at

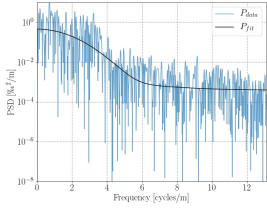
METH-SPECT:
Make a comment
on Nyquist frequency.



(a)



(b)



(c)

Figure 6.9: (a) Signal estimate given through fitting to all data (noise and signal). (b) Noise estimate given through fitting to all data (noise and signal). (c) Complete spectral fit to all data (blue), both noise and signal.

high frequencies indicating a low frequency signal and some high frequency noise.

Since the signal is that of a real physical phenomena, and even one that we do have some acquaintance with, it is relevant to use some knowledge of the theory to describe the apparent spectrum, which has also been done in section ???. Recalling the definitions of the noise and the signal as they are assumed to be based on the physical theory, it is possible to carry out a fitting routine to determine the parameters of the noise, signal and combined model function. This routine is performed in the following steps:

- Define the noise, signal and model functions to fit:

$$|\eta(\omega)|^2 = \frac{\sigma_\eta^2 \Delta z}{|1 + a_1 \exp(-2\pi i \omega \Delta z)|^2} \quad (6.19)$$

$$P_{\text{signal}}(k) = P_0 \cdot e^{-k^2 \sigma_{\text{tot}}^2} \quad (6.20)$$

$$P_{\text{model}} = |\eta(\omega)|^2 + P_{\text{signal}}(\omega) \quad (6.21)$$

- Define two methods to calculate residuals between the measured data, \mathbf{y} , and the modelled estimate \mathbf{m} . The listings of these methods can be seen in Listings 6.2 and 6.3.

```

1 def calc_res(params, x, y, dt, weights):
2     # Set parameters as input parameters
3     P0, s_eta2, s_tot2, a1 = params
4
5     # Define signal and noise function based on given params
6     Noise = self.func_Noise(x, s_eta2, a1, dt)
7     Signal = self.func_Signal(x, P0, s_tot2)
8
9     # Define model as sum of noise and signal
10    Pmod = Noise + Signal
11    # Calculate (weighted) log residual
12    res = weights*(np.log10(y) - np.log10(np.copy(Pmod)))
13
14    return res

```

Listing 6.2: Residual calculations for spectral fit.

```

1 def sum2_res(params, x, y, dt, weights):
2
3     # Calculate sum of the squared residuals.
4     return np.sum(calc_res(params, x, y, dt, weights)**2)

```

Listing 6.3: Calculation of the sum of squared residuals.

- Define boundaries for the parameters examined: $P_0, \sigma_\eta, \sigma_{tot}, a_1$.
- Make initial parameter guess :
- Optimization routine to minimize residuals. This routine is carried out by using the Python package `sp.optimize.fmin_l_bfgs_b`, an optimization through the limited-memory BFGS bound constraint algorithm .

The signal, noise and combined fit can be seen separately in Figure 6.9a, 6.9b and 6.9c, respectively, and plotted together in Figure 6.8.

Depth Series: Wiener Filter

When the optimal fit to the spectral data has been found, it is possible to construct an optimal filter to cut off as much high frequency noise as possible while still maintaining the most signal. This is commonly called a Wiener filter . Recalling from Section ?? this filter is described as the ratio between the signal alone and the signal plus noise model:

$$\tilde{F}(k) = \frac{P_{\text{signal}}(k)}{P_{\text{signal}}(k) + |\tilde{\eta}(k)|^2}. \quad (6.22)$$

This yields a filter that annihilates high frequencies above a certain cut but at the same time leaves room around this cut for both dampening low frequencies and not completely killing high frequencies in that area. This logistic curve can be seen plotted on a linear and a double logarithmic scale in Figures 6.10a and 6.10b respectively.

Now, the one branch of the preliminary work considering the raw depth series, has been dealt with and the remaining work before back diffusion can be carried out consisting of using the specifications of the core at the given drill site to give a qualified first guess on diffusion length.

6.1.4 Peak Counting

Spline Interpolation for Optimal Peak Detection

6.2 Estimating σ from Data: Optimal Diffusion Length

6.2.1 Decision Algorithm

6.2.2 Output

METH-SPECTFIT:

Write boundaries

METH-SPECTFIT:

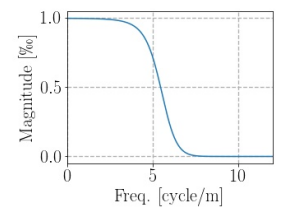
Write initial guesses

METH-SPECTFIT:

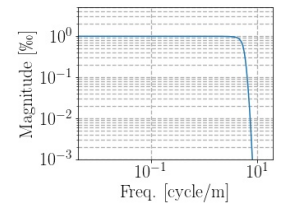
REFERENCE!!!

Maybe write more?

No...



(a)



(b)

Figure 6.10: (a) Wiener filter on linear scale. (b) Wiener filter on double logarithmic scale.

METH-WIENER:

REFERENCE!!!

METH-OUT: Re-

member: write

about sampling

sigma

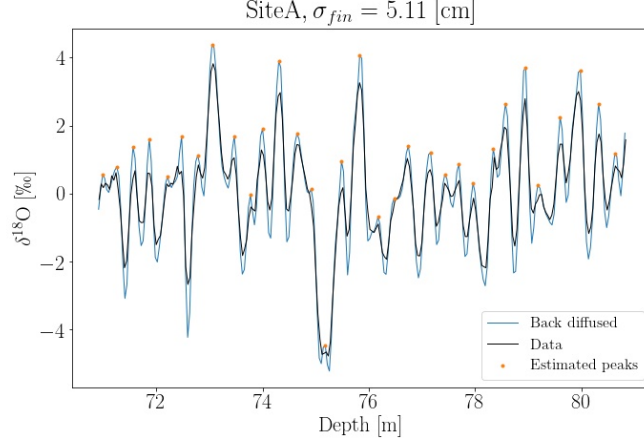


Figure 6.11: Best estimate of deconvoluted depth series given an annual count of 32 years - marked as orange dots. The best estimate is taken as the largest diffusion length that still yields 32 years in the depth span from Tambora to Laki.

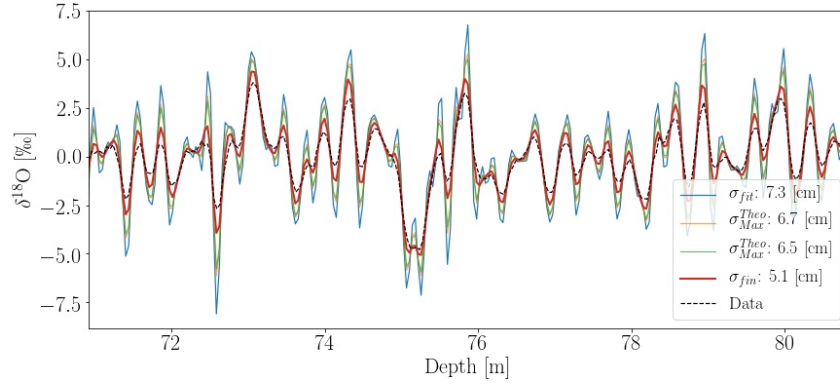


Figure 6.12: Estimated back diffused data series with different diffusion length estimates: diffusion length estimate from spectral fit (σ_{fit}), maximum (σ_{Max}^{Theo}) and minimum (σ_{Min}^{Theo}) theoretically estimated diffusion lengths and final estimated diffusion length.

6.3 Method Testing and Stability

6.3.1 Diffusion Length Estimate Versus Number of Counted Peaks

METH-TESTS:
Write entire section.

6.3.2 Interpolation of Data Before Deconvolution

METH-TESTMAX:
Write entire section.

6.3.3 Interpolation of Data After Deconvolution

METH-TESTINT1:
Write entire section.

METH-TESTINT2:
Write entire section.

6.4 Upgrading the Algorithms

6.4.1 Peak Detection through Machine Learning

METH-UPGRADE:
Write entire section.

6.4.2 Linear Timescale

METH-UPGRADEPEAK:
Do the ML Peak Detection, then Write entire section.

6.4.3 Standardization and Detrending

METH-UPGRADETIME:
Incorporate Linear Timescale in Recursivity - then Write entire section.

6.4.4 Recursivity and New Constraints

METH-UPGRADESTAND:
Maybe not necessary? Write entire section.

6.5 Reconstruction of Missing Data

METH-UPGRADERECURS:
Develop recursive algorithm with new constraints for peak finding - then write entire section.

METH-MISSDATA:

6.5.1 Interpolation Method

METH-
MISSDATAINTERP:
Write entire section.
Show baddddd
figures.

6.5.2 Maximum Entropy Method

METH-
MISSDATAMEM:
Write entire sec-
tion. Refer to Bo
Vinther's MEM re-
construction method.

Chapter 7

Diffusion Length Estimate Results

	Crete		Site A		Site B		Site D		Site E		Site G	
	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}
FFT												
DCT	6.08	6.02	5.97	5.85	5.71	5.83	4.55	4.41	6.37	6.24	8.81	8.72
NDCT	5.98	5.93	6.27	6.16	6.25	6.36	4.57	4.43	6.55	6.43	8.84	8.75

	Crete		Site A		Site B		Site D		Site E		Site G	
	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}
σ_{constant}												
$\sigma(z)$												

	Crete		Site A		Site B		Site D		Site E		Site G	
	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}	σ_{opt}	σ_{firn}
No constraints												
Constraints												

Chapter 8

Temperature Reconstruction

8.1 Temperature Estimate from Optimal Estimated σ

8.1.1 Steady State Solution

Accumulation Distributions

8.1.2 Further Possibilities of the Iso-CFM

TEMP-DATAEST:
Write entire section.

TEMP-
DATAESTSTST:
Write entire section.

TEMP-
DATAESTACCUM:
Write entire section.

TEMP-
DATAESTCFM:
Write entire section.

Chapter 9

Layer Counting and Annual Layer Thickness Estimation

Clevercleverclever

Chapter 10

Conclusion

This is great. I did a great thesis. High-five to me!

CONC: Write a better conclusion. Please..

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