

遷音速アウトフローモデルによる高赤方偏移 星形成銀河の mass loading factor の推定 (mass loading factor of high-z star-forming galaxies with transonic outflow model)

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(Igarashi, A., Mori, M. & Nitta, S.)

Introduction: Galactic winds in star-forming galaxies

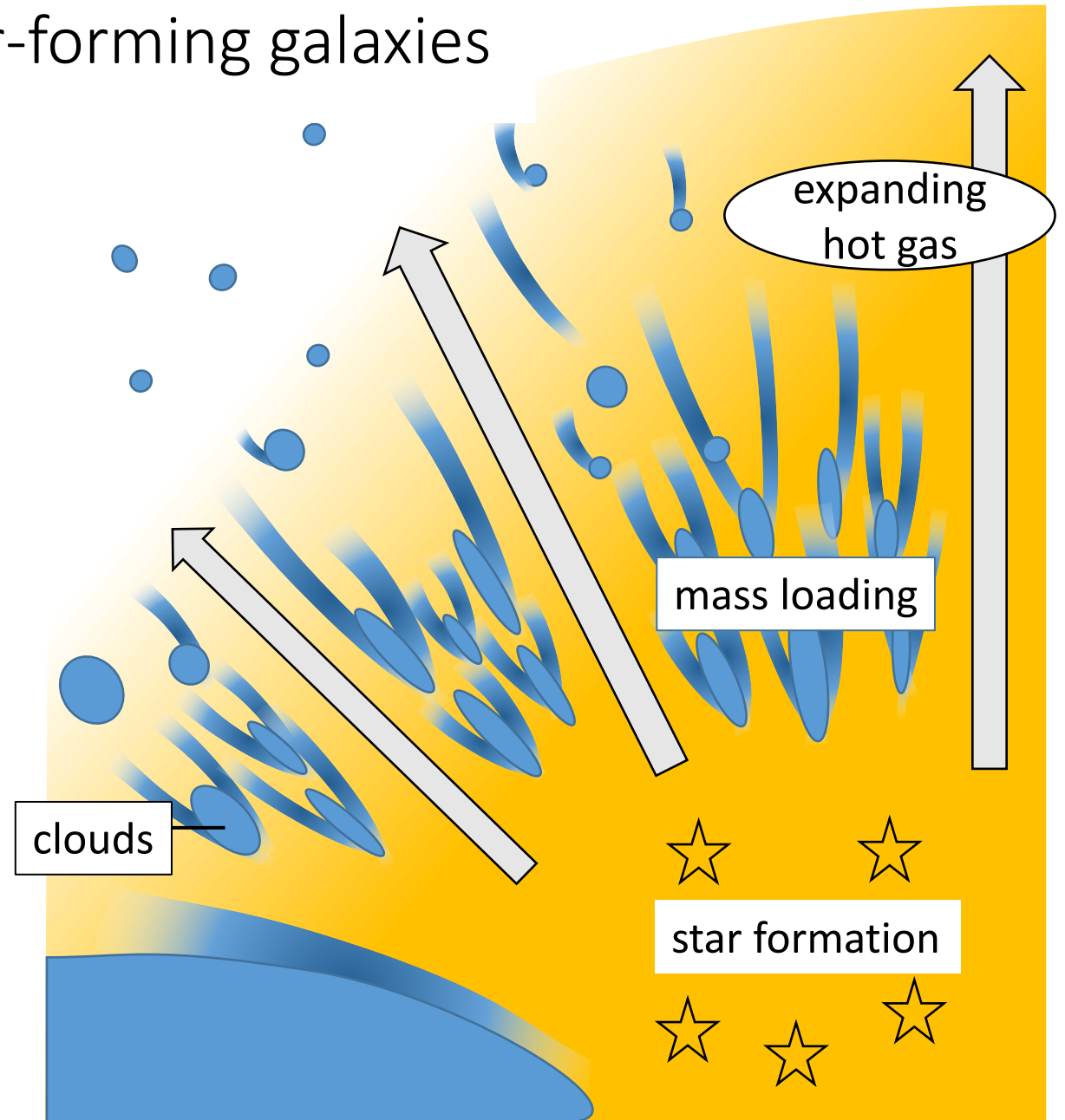
High SFR

→ inject energy to ISM

→ galactic winds

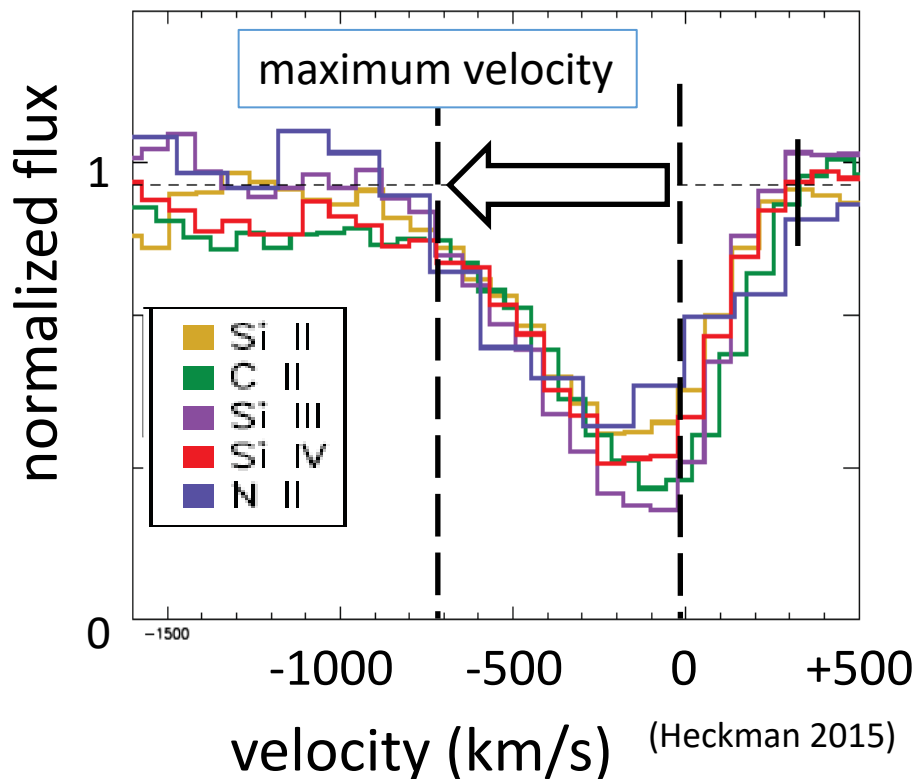


1. suppress star formation
2. metal enrichment in intergalactic space



Introduction: outflow velocity

shifted absorption lines
→ outflow velocity

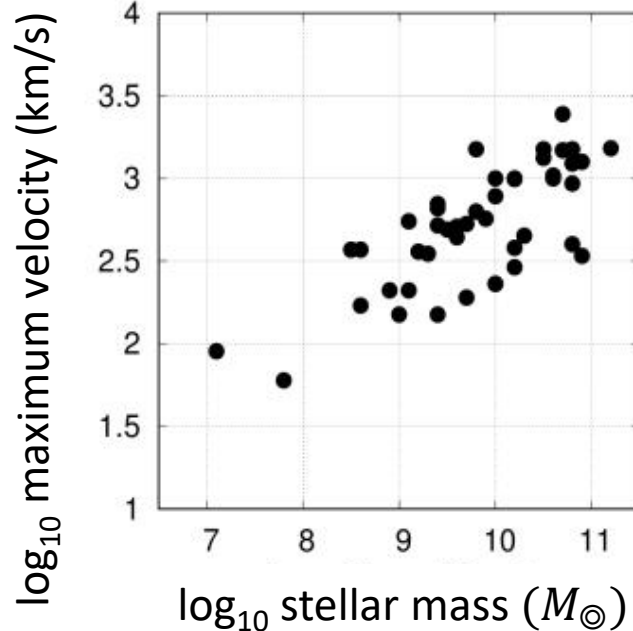


observed maximum velocity

maximum velocity of hot gas (lower limit)

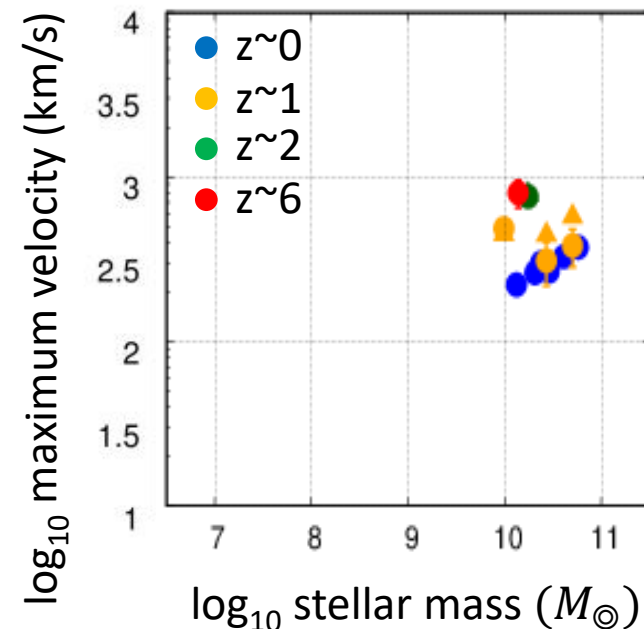
local star-forming galaxies

(Heckman 2015, 2016)



high-z star-forming galaxies

(Sugahara et al. 2017, 2019)



positive correlation to stellar mass (and SFR)

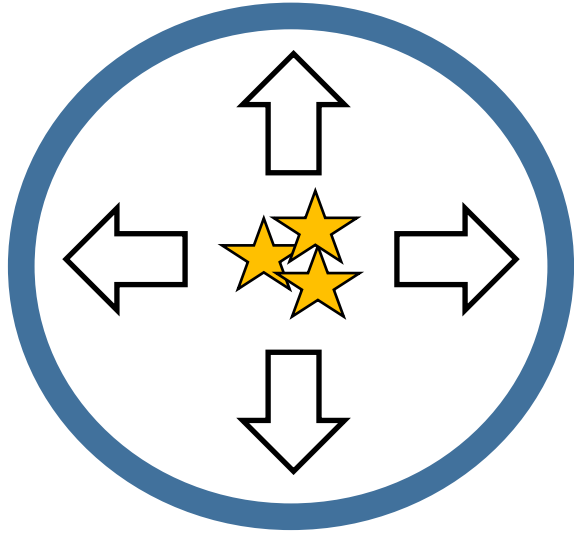
The influence of galactic winds depends on

velocity
massflux

outflow model to estimate massflux

shell model vs transonic outflow model

Introduction: shell outflow model



\dot{M} : massflux
 N_H : column density
 $\langle m \rangle$: average mass
 v_{out} : average velocity
 r_{out} : shell radius

$$\dot{M} \sim 4\pi N_H \langle m \rangle v_{out} r_{out}$$

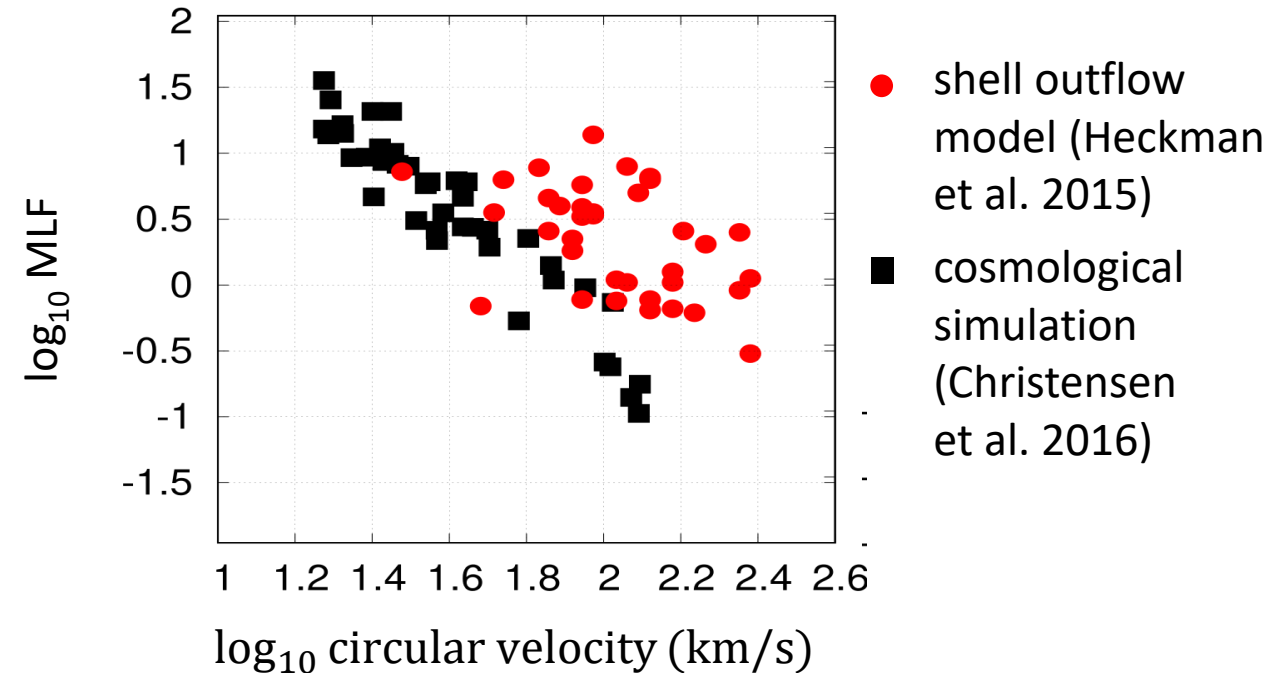
N_H estimated from metal column density

r_{out} assumed to be 2 x effective radius (UV)

N_H and r_{out} have uncertainty

$$\text{mass loading factor (MLF)} = \dot{M} / \text{SFR}$$

MLF \rightarrow efficiency of mass loading



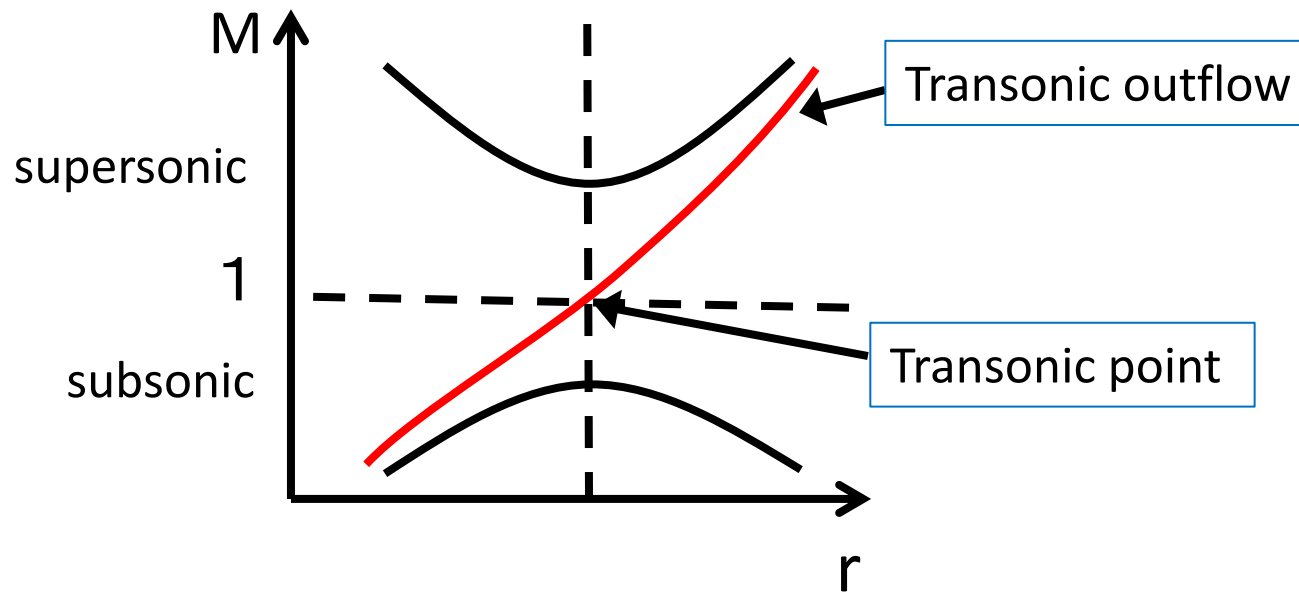
- slightly depends on halo mass
- not agree with theoretical prediction



**re-analyse observed velocity
with new outflow model**

Introduction: transonic outflow model

example: solar model (Parker 1958)



1. Equation of continuity $4\pi\rho v r^2 = \text{const.}$

2. Equation of motion $v \frac{dv}{dr} = -\frac{c_s^2}{\rho} \frac{d\rho}{dr} - \frac{d\Phi}{dr}$



$$\frac{M^2 - 1}{M^2} \frac{dM^2}{dr} = \frac{4}{r} - \frac{2}{c_s^2} \frac{d\Phi}{dr} \quad \left(\Phi(x) \propto -\frac{1}{r} \right)$$

M : Mach number (= velocity / sound speed)

Transonic process has maximum entropy
→ assume transonic outflow of hot gas

Model: transonic outflow model



spherically symmetric steady model

1. equation
of continuity

2. equation
of motion

3. energy
equation

$$\frac{1}{r^2} \frac{d}{dr} (\rho v r^2) = \dot{\rho}_m$$

$$\rho v \frac{dv}{dr} = -\frac{dP}{dr} + \rho g - \dot{\rho}_m v$$

$$\frac{1}{r^2} \frac{d}{dr} \left\{ v r^2 \left(\frac{1}{2} \rho v^2 + \frac{\Gamma}{\Gamma - 1} P \right) \right\} = \rho v g + \dot{q}$$

$\dot{\rho}_m$: mass injection
(with **mass loading**)

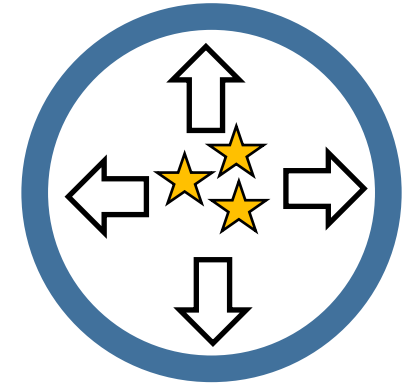
\dot{q} : energy injection

$$\Rightarrow \frac{M^2 - 1}{M^2 \{(\Gamma - 1)M^2 + 2\}} \frac{dM^2}{dr} = \frac{2}{r} - \frac{\Gamma + 1}{2(\Gamma - 1)} \frac{\dot{m}}{\dot{e} - \dot{m}\Phi} \frac{d\Phi}{dr} - \frac{\Gamma M^2 + 1}{2} \frac{\dot{e} - 2\dot{m}\Phi}{\dot{e} - \dot{m}\Phi} \frac{1}{\dot{m}} \frac{d\dot{m}}{dr}$$

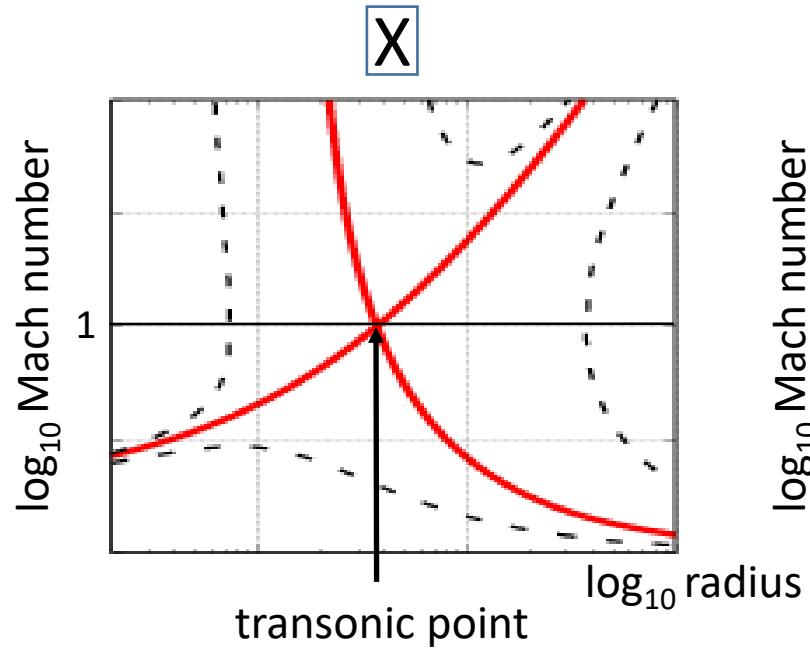
assume energy injection from SNeII

assume dark halo and stellar mass to the gravitational potential

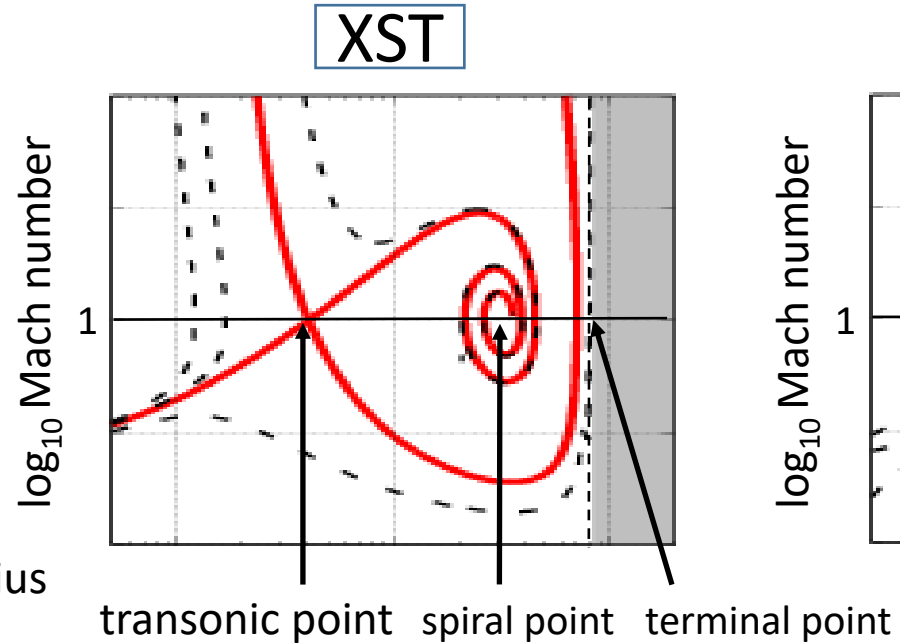
Shell outflow model



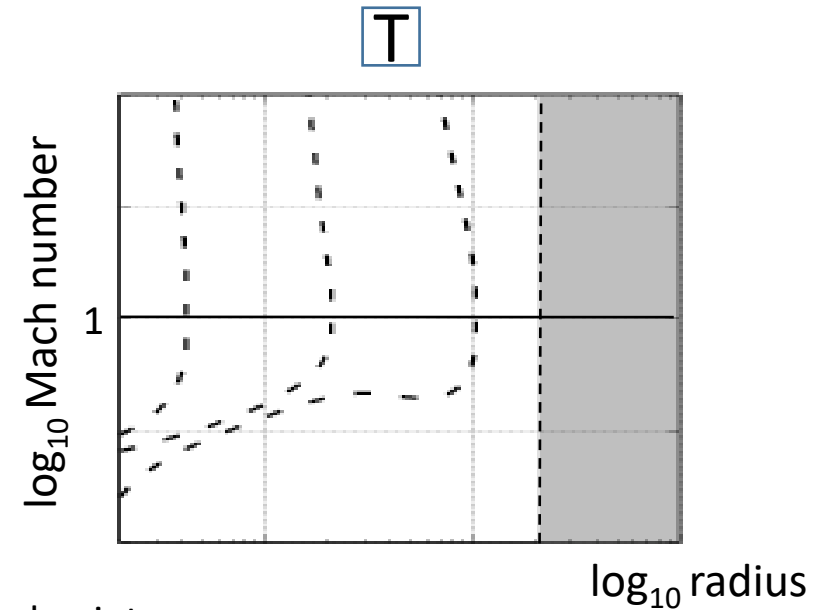
Model: relation of solution type and massflux



Outflows can escape from galaxies



Outflows stop in dark halo



No transonic solution

low

gravity (\propto dark halo mass)

high

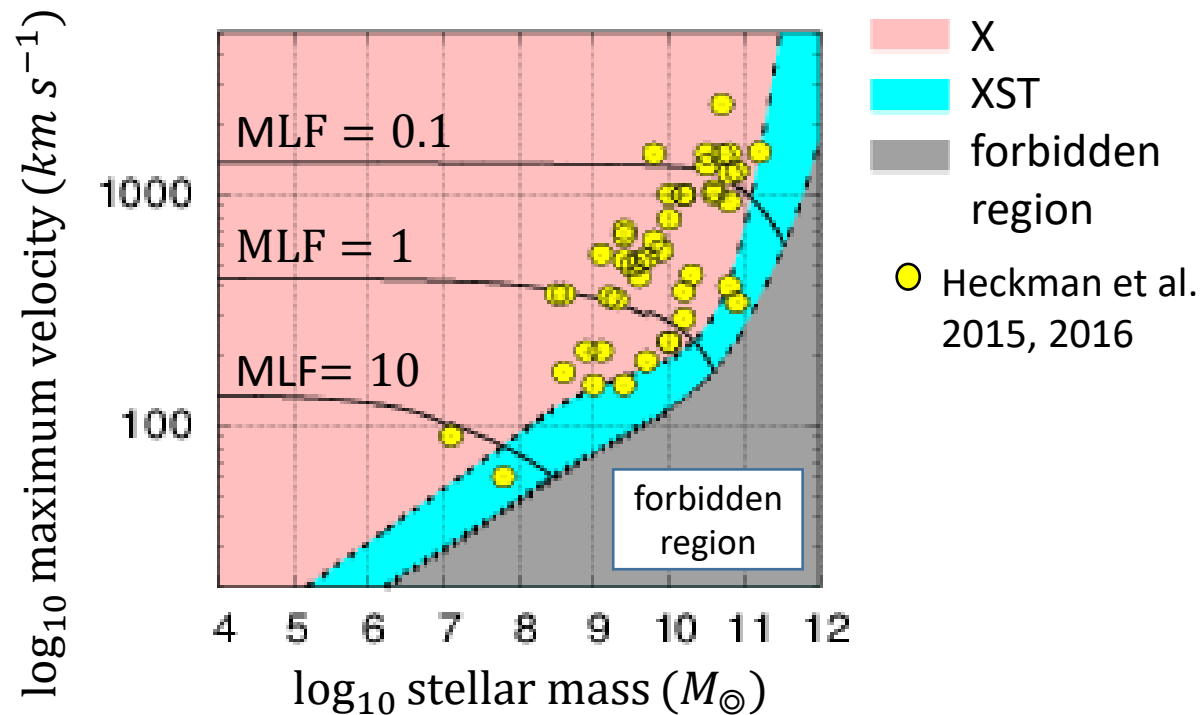
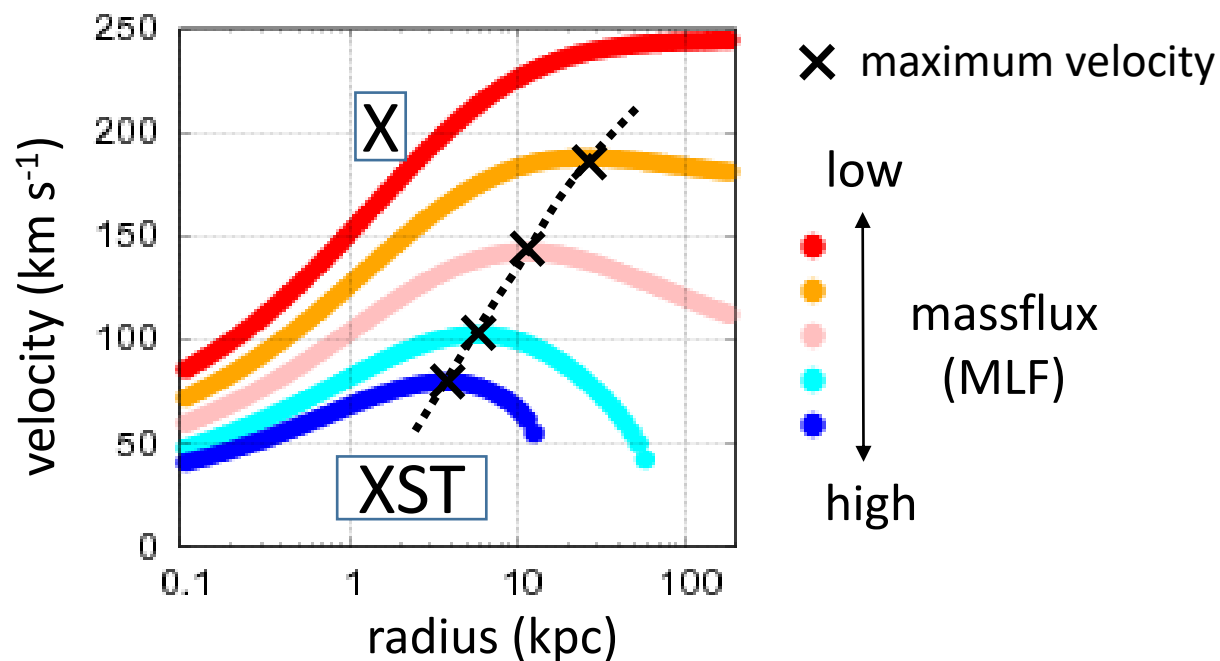
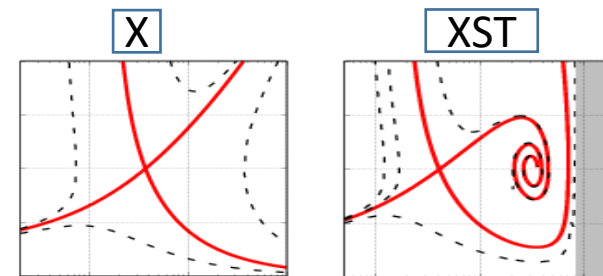
injected energy (\propto SFR)

massflux

Result: velocity profile to mass loading factor (MLF)

example: stellar mass = $10^{8.6} M_{\odot}$
(dark halo mass = $10^{10.96} M_{\odot}$)

$$\text{MLF} = \dot{M} / \text{SFR}$$

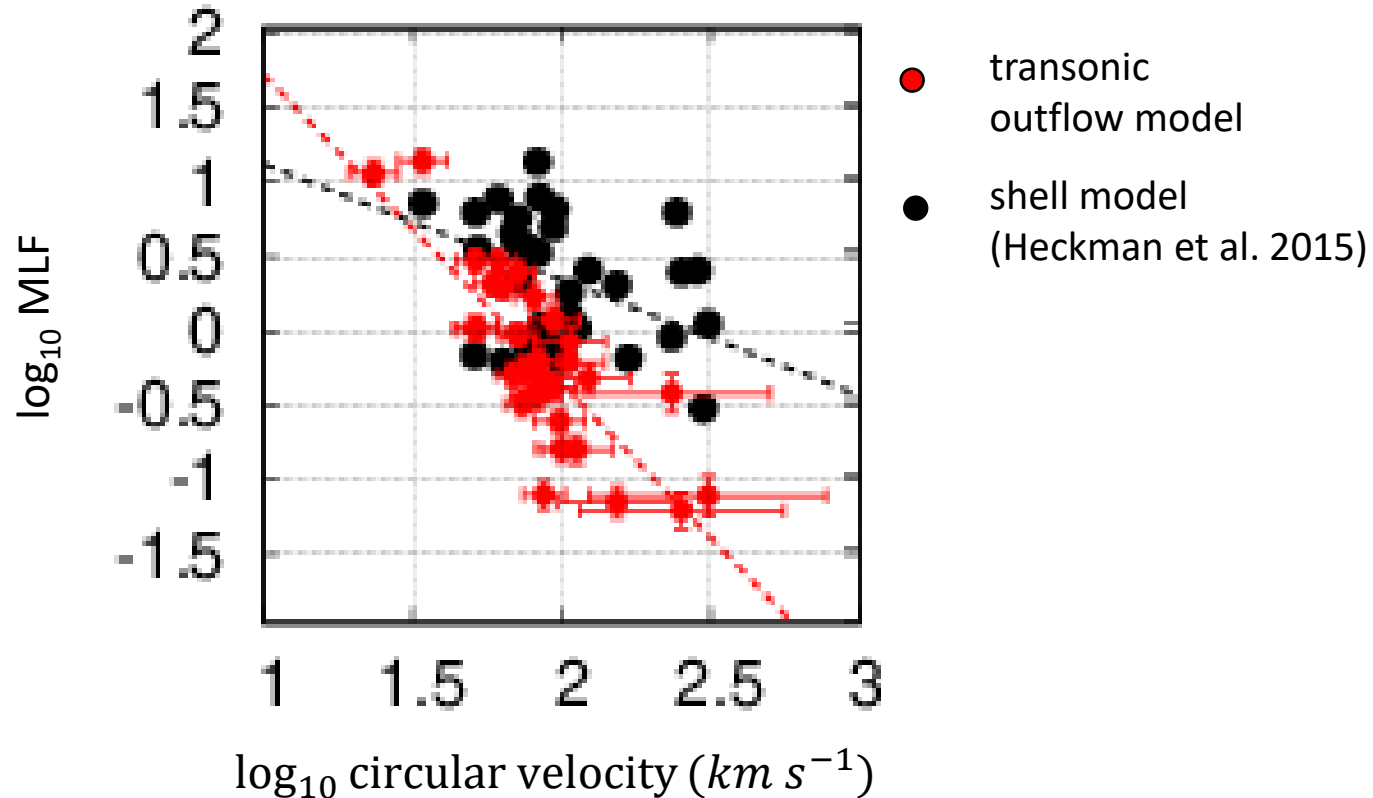


maximum velocity \longleftrightarrow massflux (MLF)

estimate MLF with transonic outflow model
from observed maximum velocity

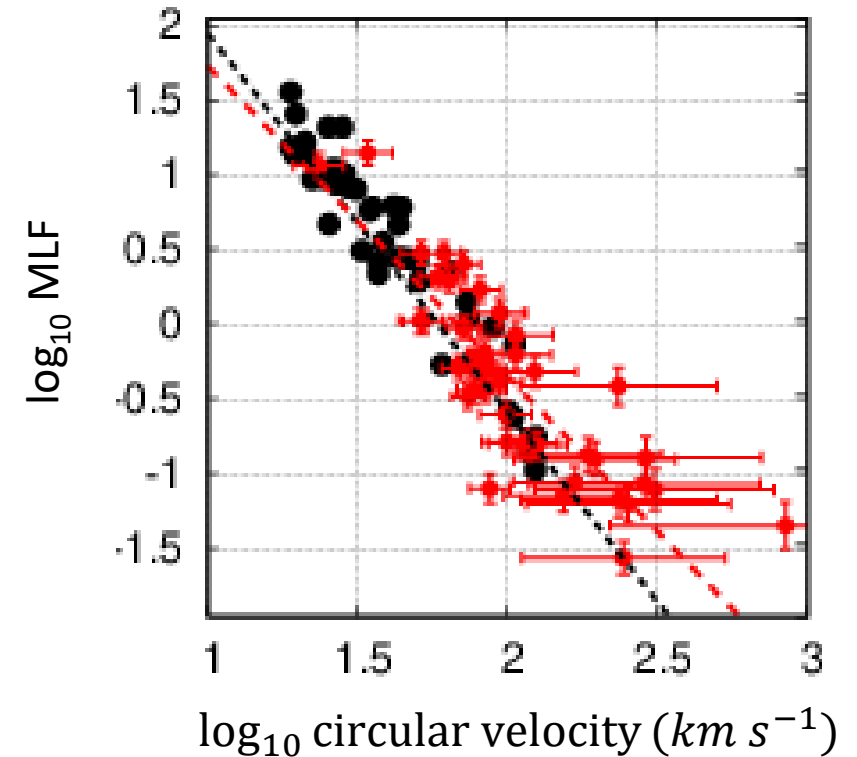
Result: in low-z star-forming galaxies

$$\text{MLF} = \dot{M} / \text{SFR}$$



MLF depends on halo mass ($\text{MLF} \propto V_{\text{circ}}^{-2.5}$)
→ ISM can effectively escape from small galaxies.

- transonic outflow model
- cosmological simulation (Christensen et al. 2016)
(reproduce stellar-halo mass relation, Tully-Fisher relation, mass-metallicity relation)

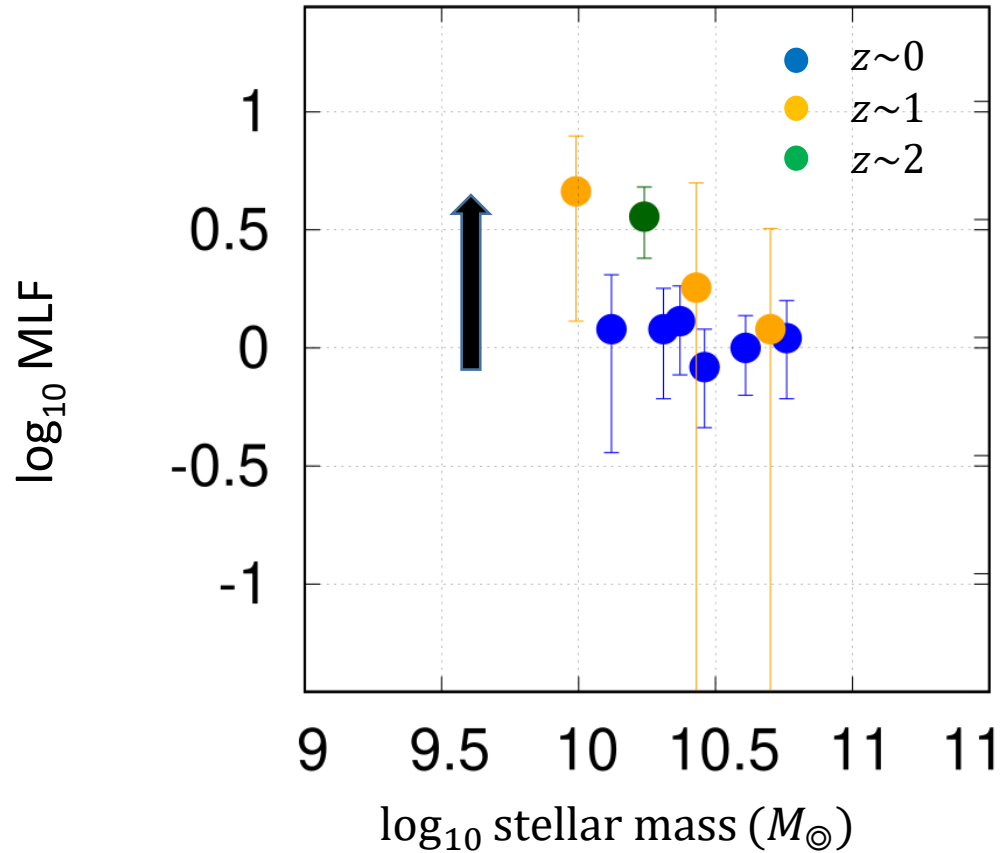


MLF becomes smaller than shell model.
MLF is comparable to theoretical prediction.
→ theoretical studies can reproduce velocity observation.

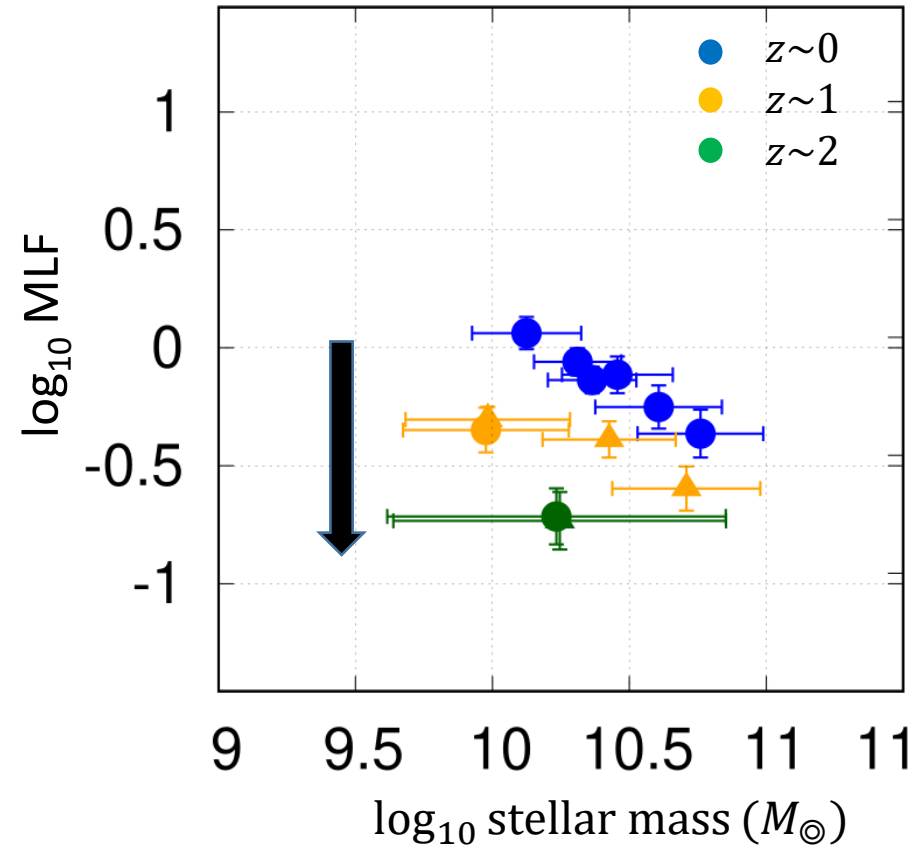
Result: in high-z star-forming galaxies

$$\text{MLF} = \dot{M} / \text{SFR}$$

shell model (Sugahara et al. 2017)



transonic outflow model



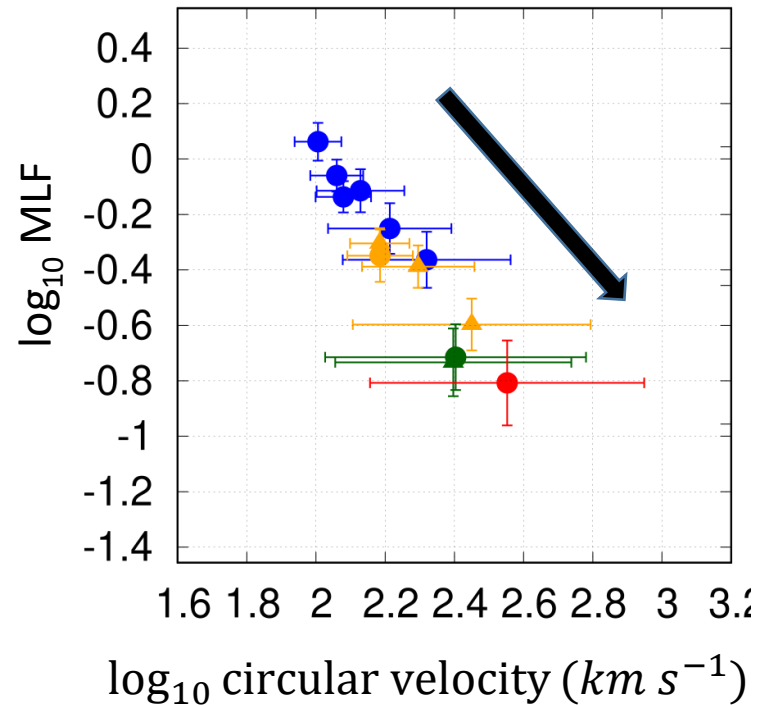
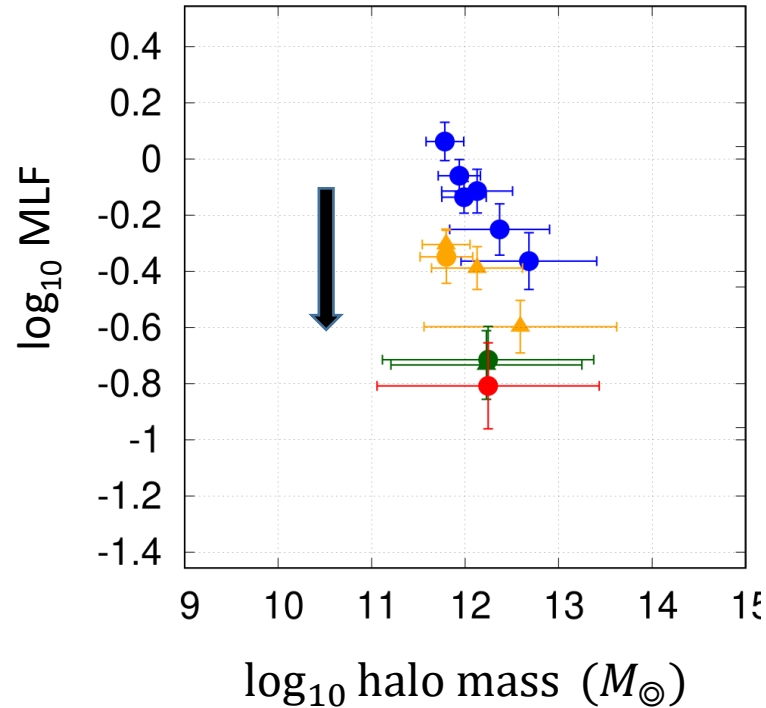
MLF decreases in high-z galaxies
→ opposite trend from shell model

Result: in high-z star-forming galaxies

$$\text{MLF} = \dot{M} / \text{SFR}$$

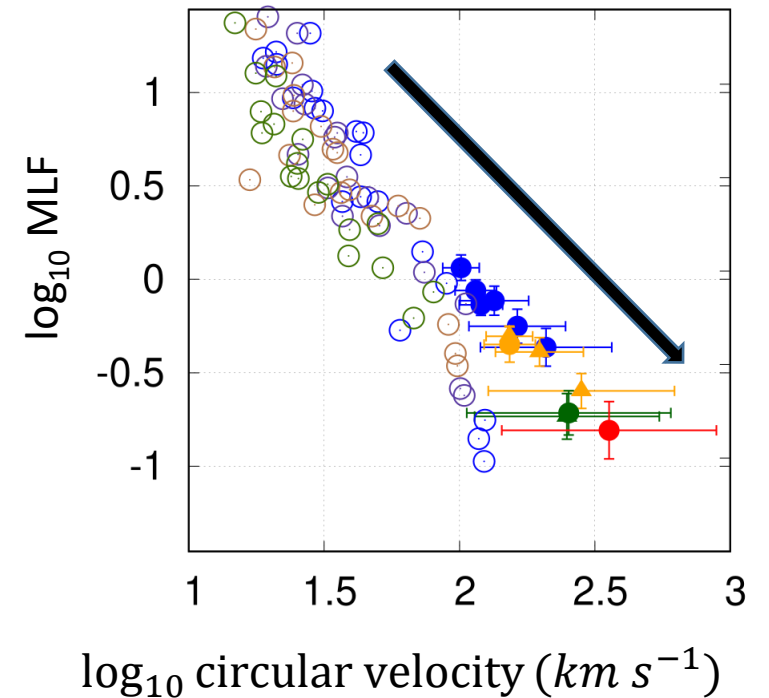
transonic outflow model

- $z \sim 0$
- $z \sim 1$
- $z \sim 2$
- $z \sim 6$



cosmological simulation
(Christensen et al. 2016)

- $z \sim 0$
- $z \sim 1$
- $z \sim 2$



MLFs depend on circular velocities.

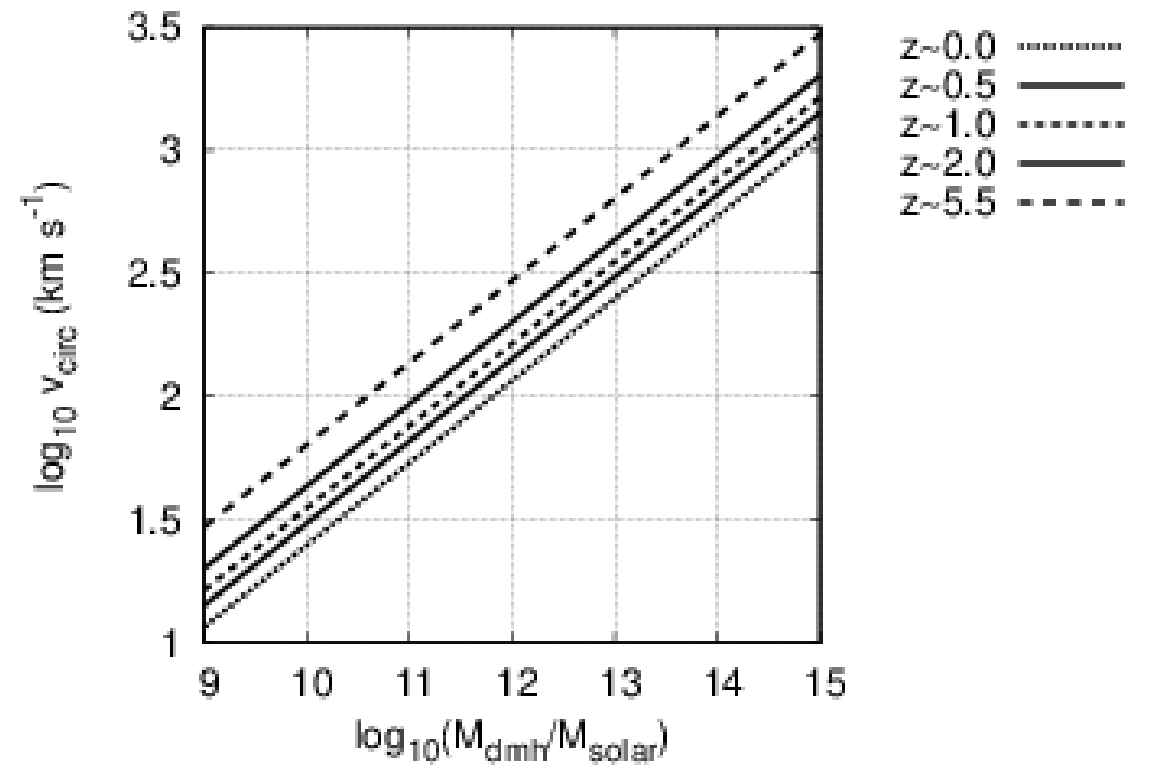
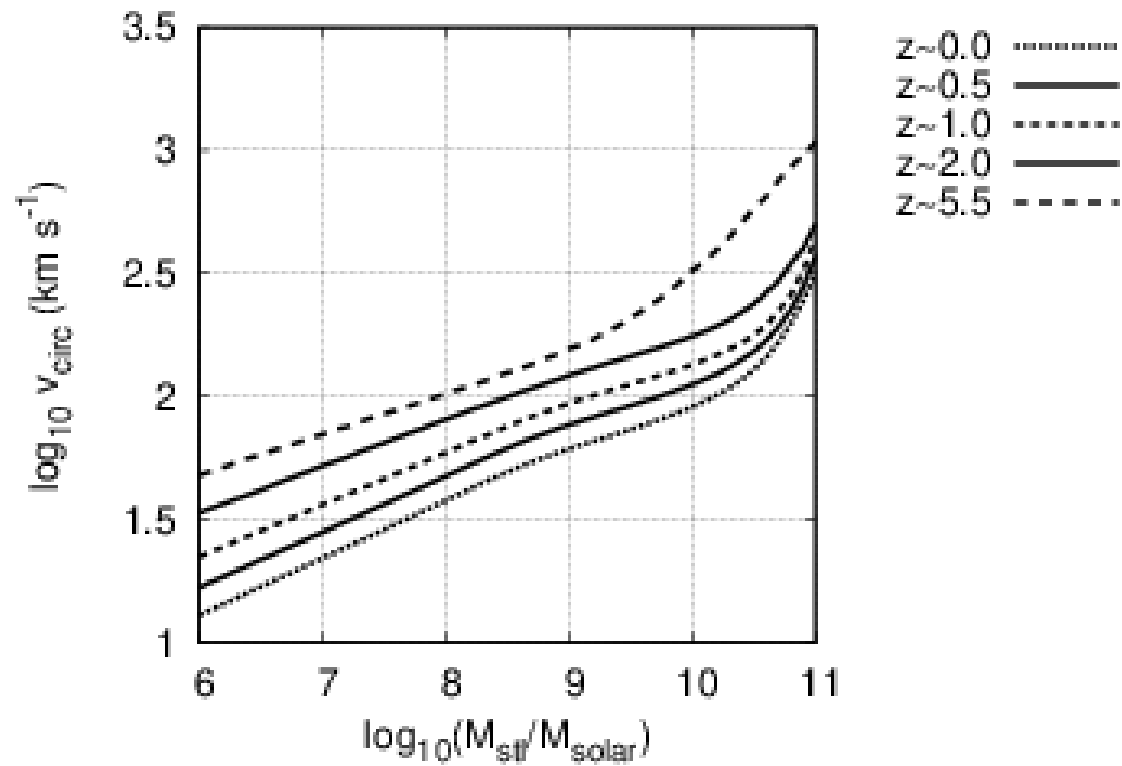
→ structure of gravitational potential determines outflow acceleration

similar trend to
cosmological simulation

Conclusion

- In transonic outflow model, mass loading factor (MLF) depends strongly on gravitational potential of star-forming galaxies.
- We estimate MLF from observed velocities with transonic outflow model.
- The estimated MLFs become smaller than that of shell outflow model.
- Small galaxies can effectively eject interstellar gas with large MLFs.
- The theoretical predictions can reproduce velocity observations.
- In contrast to shell model, the estimated MLFs decrease in high- z star-forming galaxies .
- The MLFs depend on the structure of gravitational potential and change with circular velocities of star-forming galaxies.

Galaxy mass vs circular velocity



Transonic outflow model

adiabatic spherically-symmetric steady model

1.equation of continuity $\frac{1}{r^2} \frac{d}{dr} (\rho v r^2) = \dot{\rho}_m$

2.equation of motion $\rho v \frac{dv}{dr} = -\frac{dP}{dr} + \rho g - \rho \dot{m} v$

3.energy equation $\frac{1}{r^2} \frac{d}{dr} \left\{ v r^2 \left(\frac{1}{2} \rho v^2 + \frac{\Gamma}{\Gamma-1} P \right) \right\} = \rho v g + \dot{q}$

r : radius
 v : velocity
 ρ : density
 c_s : sound speed
 P : pressure
 g : gravity
 M : Mach number
 Γ : specific heat ratio
 $\dot{\rho}_m$: mass injection
 \dot{q} : energy injection

$\Rightarrow \frac{M^2 - 1}{M^2 \{(\Gamma - 1)M^2 + 2\}} \frac{dM^2}{dr} = \frac{2}{r} - \frac{\Gamma + 1}{2(\Gamma - 1)} \frac{\dot{m}}{\dot{e} - \dot{m}\Phi} \frac{d\Phi}{dr} - \frac{\Gamma M^2 + 1}{2} \frac{\dot{e} - 2\dot{m}\Phi}{\dot{e} - \dot{m}\Phi} \frac{1}{\dot{m}} \frac{d\dot{m}}{dr}$

mass flux $\dot{m} \equiv 4\pi\rho v r^2$

energy flux $\dot{e} \equiv \left\{ \frac{1}{2} v^2 + \frac{1}{\Gamma-1} c_s^2 + \Phi \right\} \dot{m}$

assuming mass and energy injected by SNeII

assuming the gravity of dark matter (DM) halo and stellar mass

mass and energy injections

$$\dot{\rho}_m = \lambda_{MLF} (SFR/M_{st}) \rho_{st}$$

$$\dot{q} = e_{SN} (SFR/M_{st}) \rho_{st}$$

e_{SN} : injected energy per stellar mass
 (= $0.1 \times 1.86 \times 10^{-2} \times 10^{51}$ erg)

λ_{MLF} : mass loading factor (=massflux/SFR)

stellar mass distribution (Hernquist 1990)

$$\rho_{st}(r) = \frac{M_{st}}{2\pi} \frac{r_H}{r} \frac{1}{(r + r_H)^3} \quad \left(r_H = \frac{r_{1/2}}{1 + \sqrt{2}} \right)$$

M_{st} : total stellar mass
 r_H : scale radius
 $r_{1/2}$: half light radius

DM halo mass distribution indicated by CDM scenario (Navarro et al. 1996)

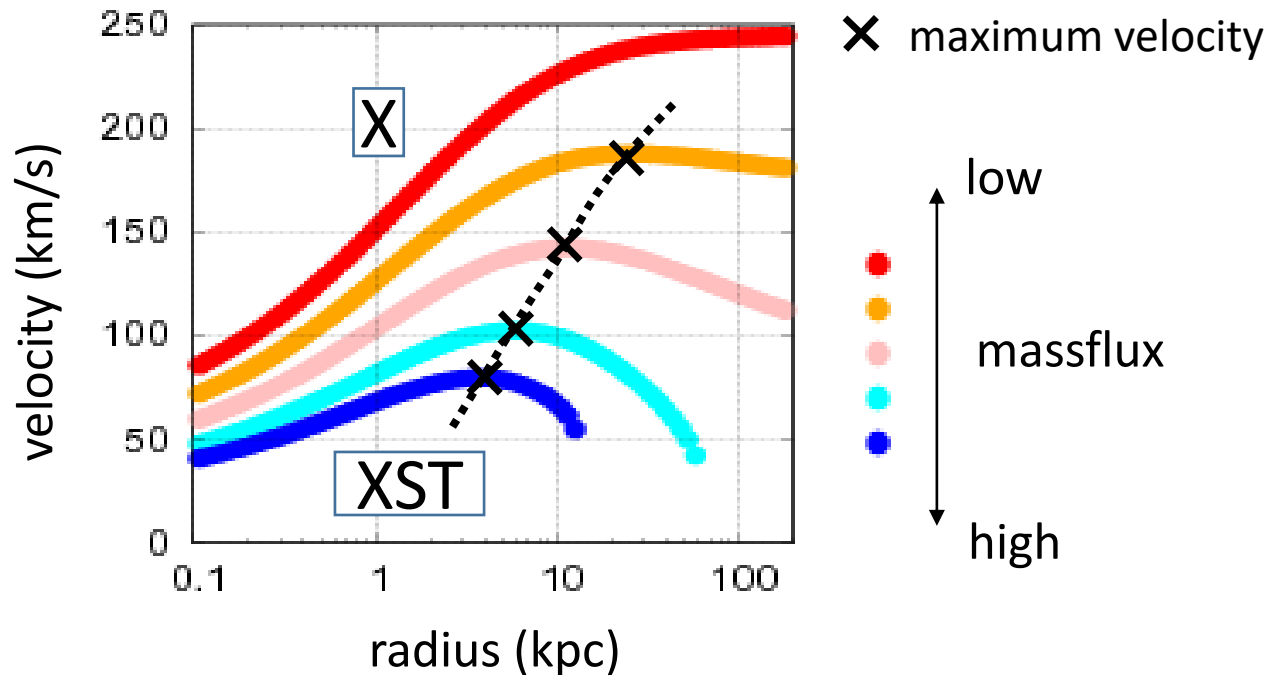
$$\rho_{DMH}(r) = \frac{\rho_{dmh} r_{dmh}^3}{r(r + r_{dmh})^2}$$

r_{dmh} : DM halo scale radius
 ρ_{dmh} : DM halo scale density

Result: velocity profile to mass loading factor (MLF)

$$\text{MLF} = \dot{M} / \text{SFR}$$

example: stellar mass = $10^{8.6} M_{\odot}$
(dark halo mass = $10^{10.96} M_{\odot}$)
SFR = $10 M_{\odot}/\text{yr}$



Massflux corresponds to maximum velocity
(larger than terminal velocity)

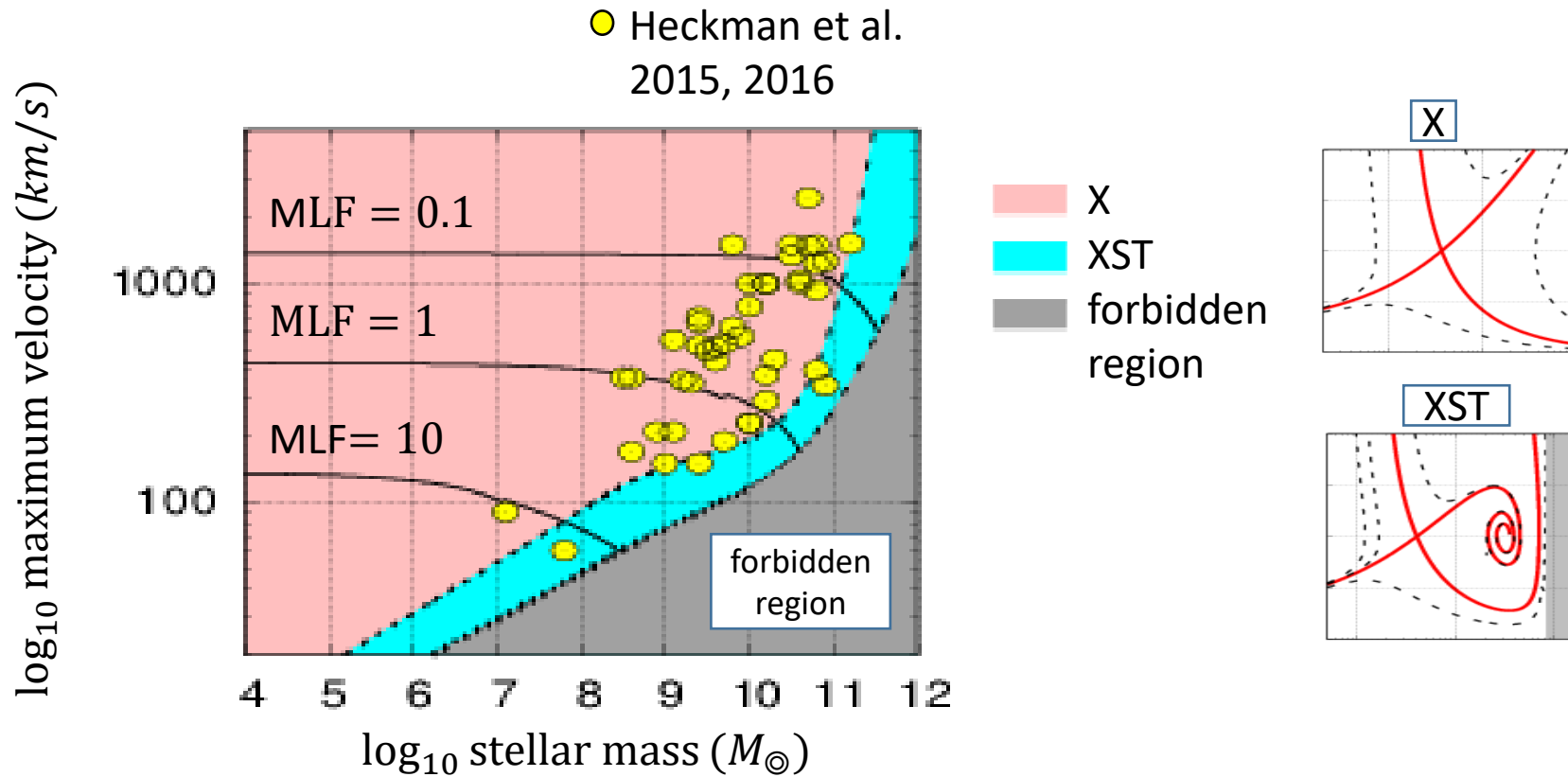


Maximum velocity corresponds to MLF

assume dark halo mass and effective radius from stellar mass
and redshift (Behroozi et al. 2010, 2013; Bullock et al. 2001;
Munoz-Cuartas et al. 2011; Shibuya et al. 2015).

Result: velocity profile to mass loading factor (MLF)

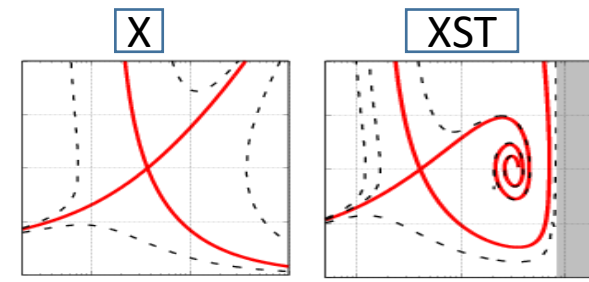
$$\text{MLF} = \dot{M} / \text{SFR}$$



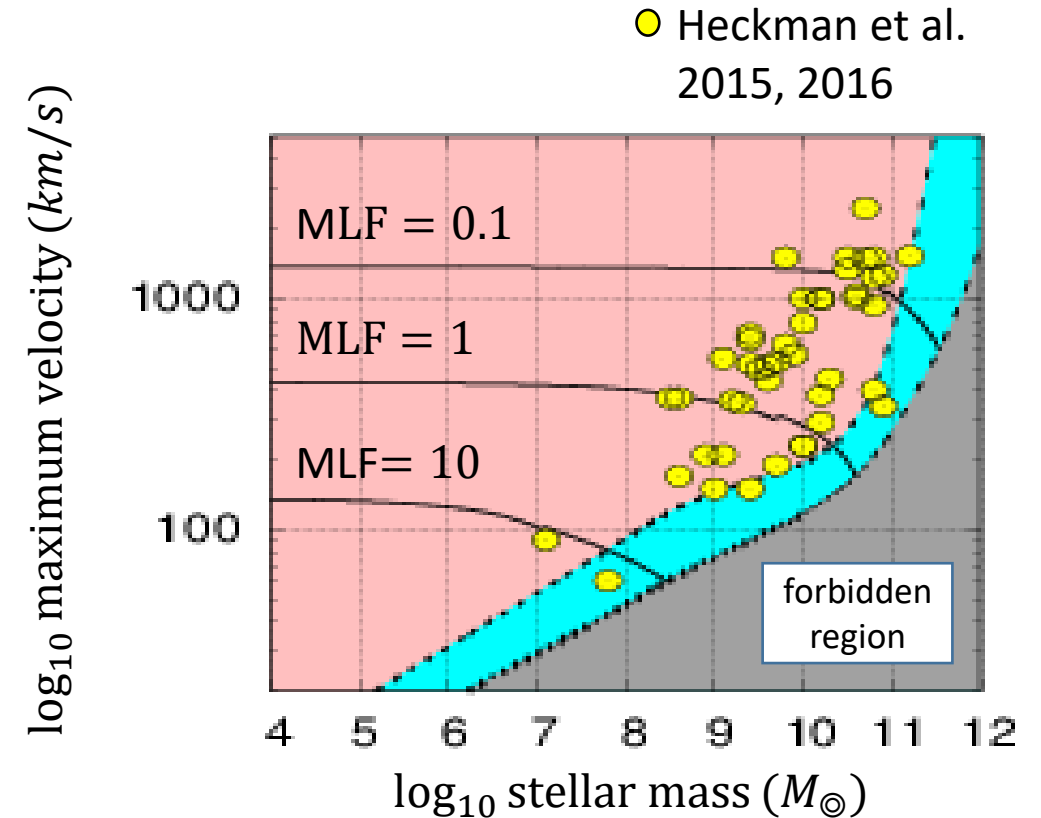
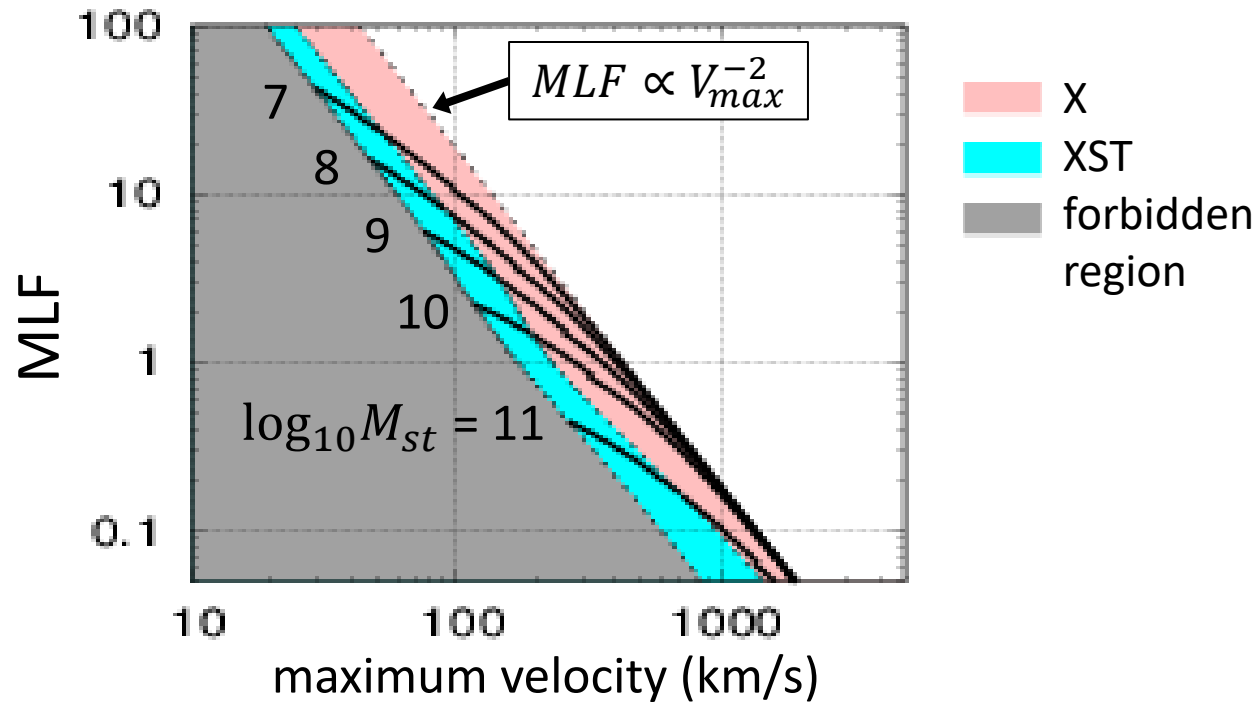
We can estimate massflux with transonic outflow model from observed velocity

Result: velocity profile to mass loading factor (MLF)

$$MLF = \dot{M} / SFR$$



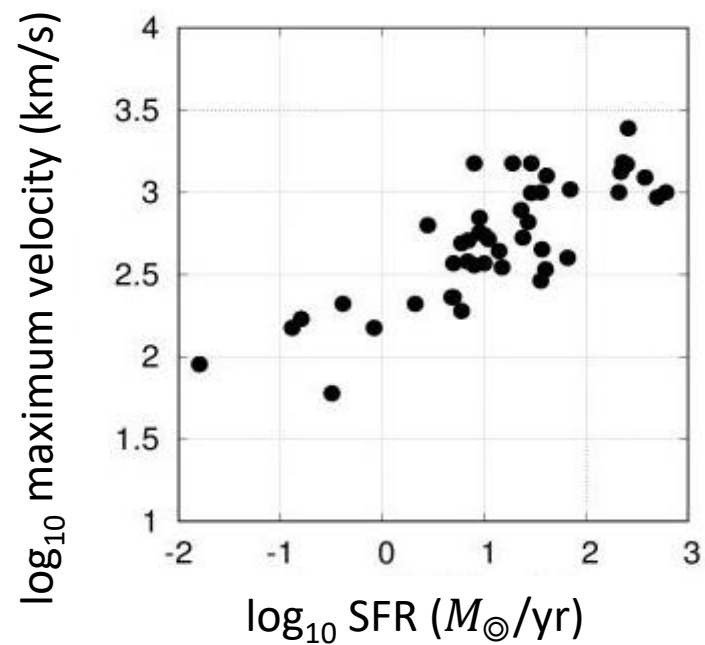
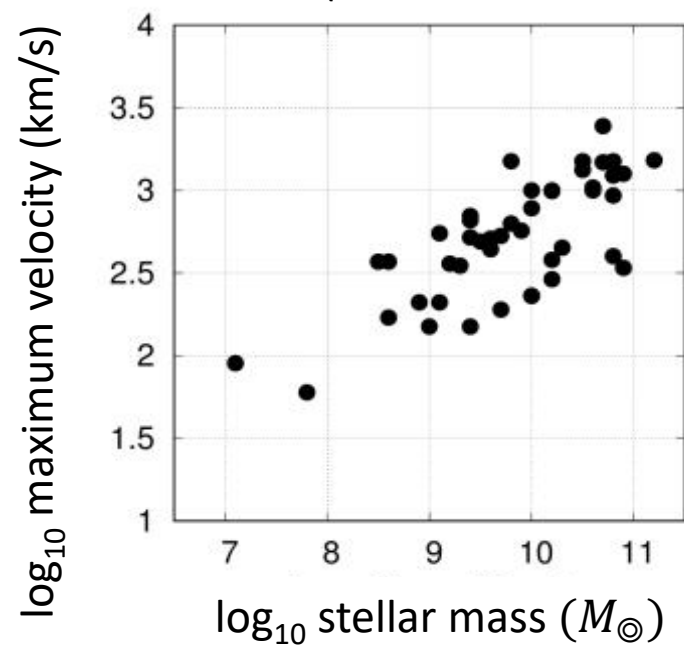
Maximum velocity to MLF (and stellar mass)



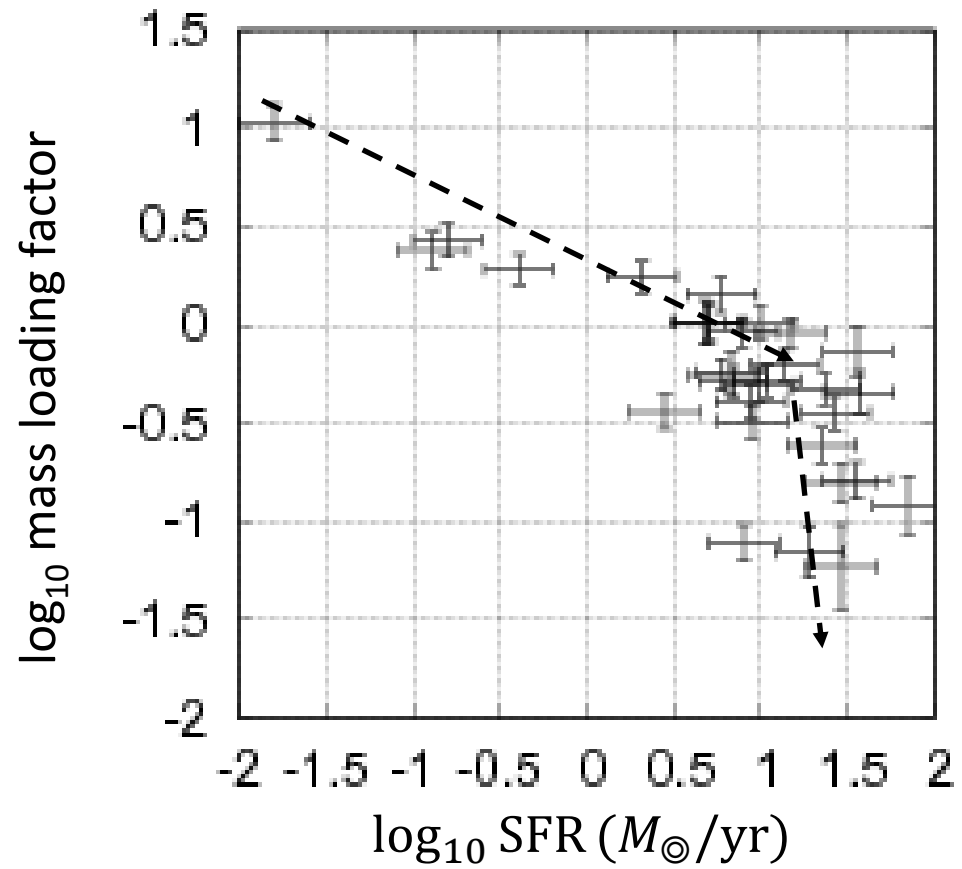
We can estimate massflux with transonic outflow model from observed velocity

outflow velocity

(Heckman 2015, 2016)



discussion

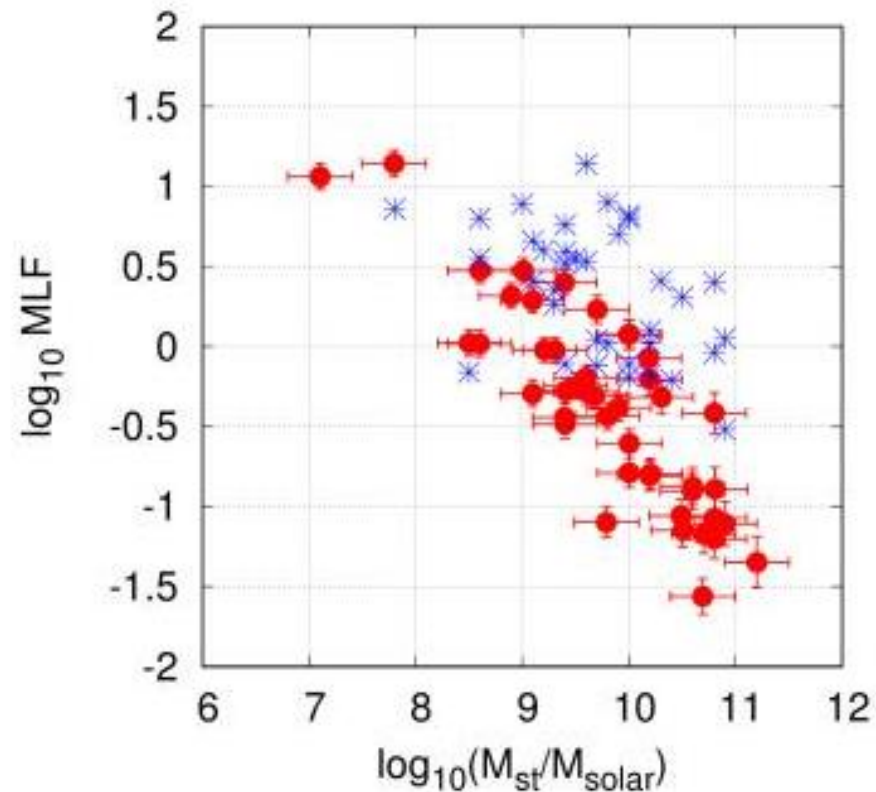
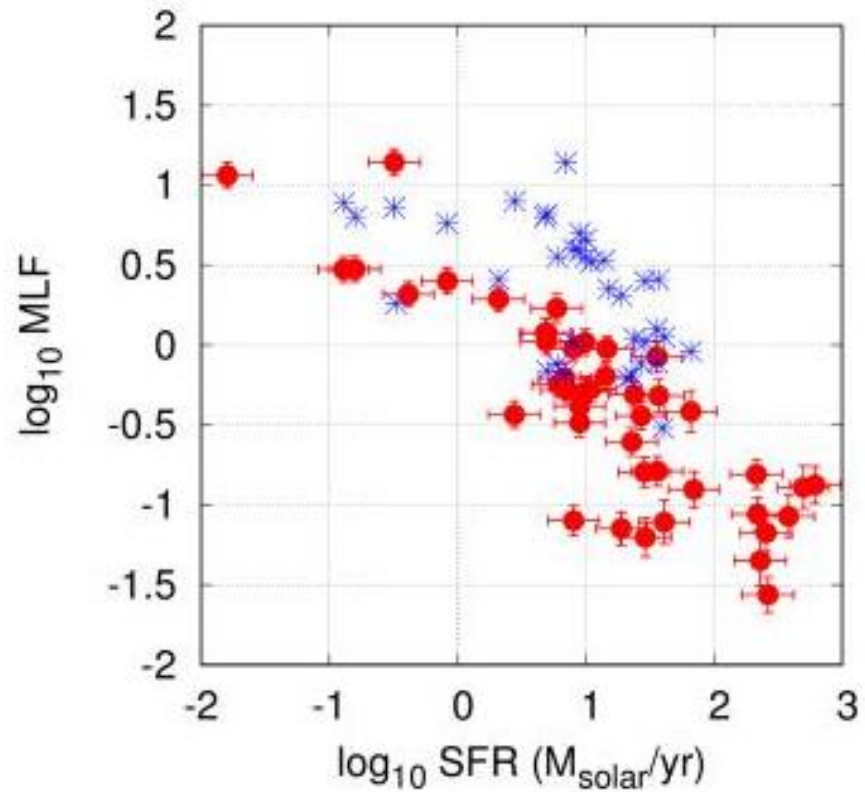


Result: Shell outflow model との比較

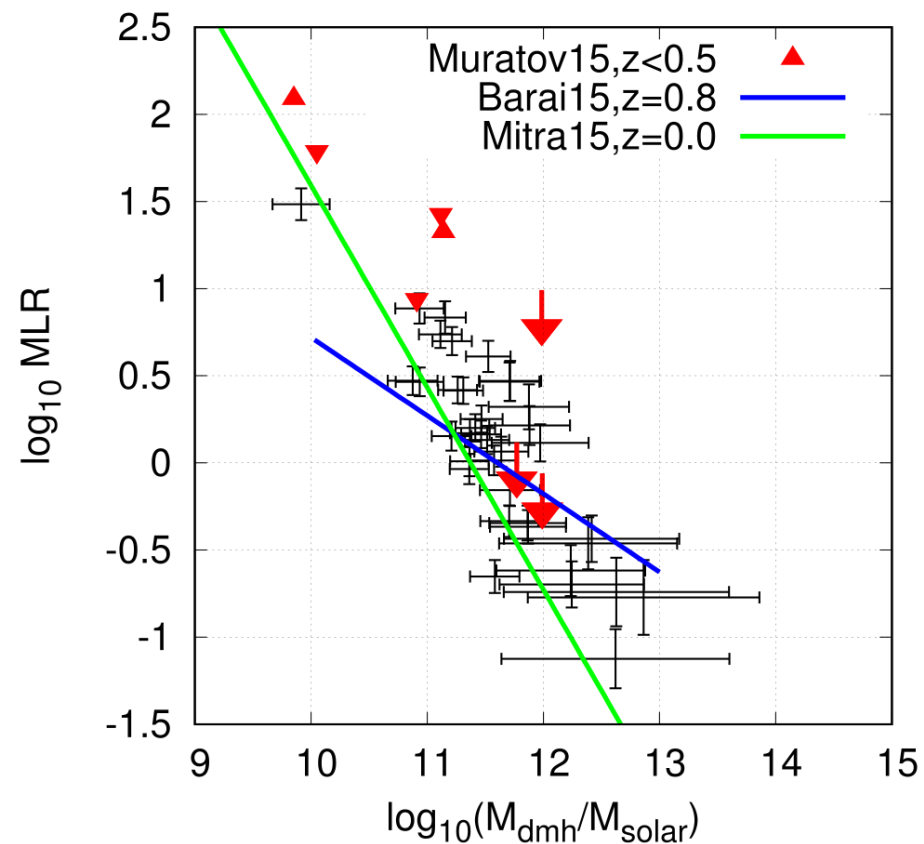
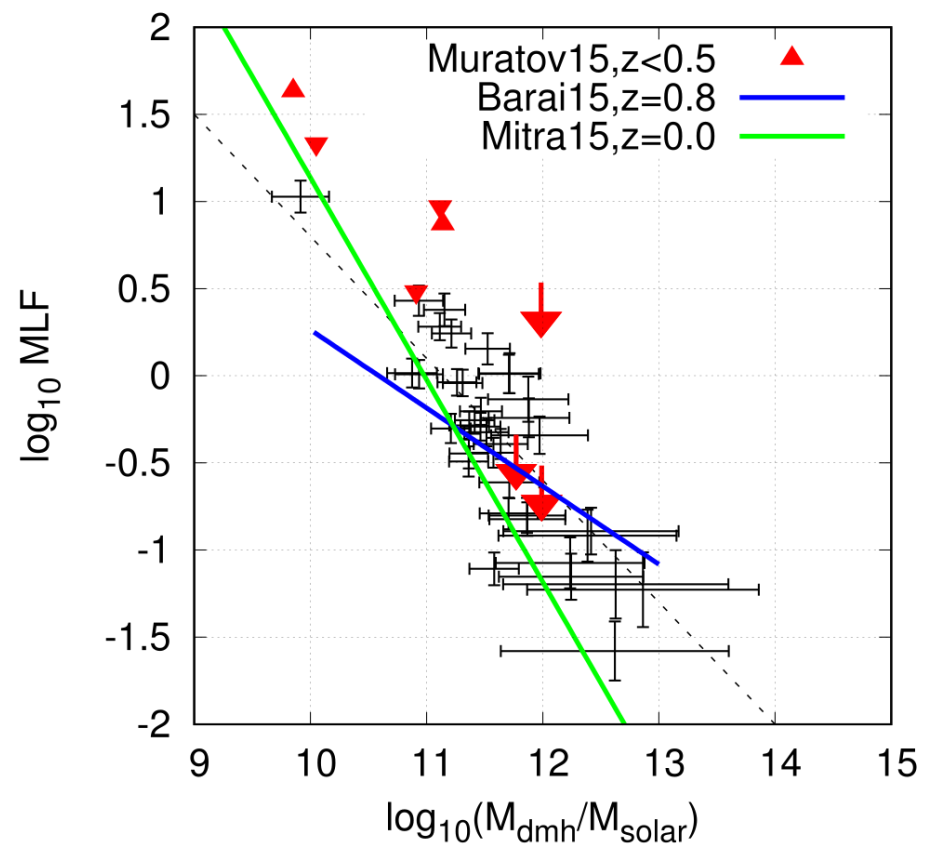
$$\text{MLF} = \dot{M} / \text{SFR}$$

● transonic outflow model

✱ shell outflow model (Heckman et al. 2015)

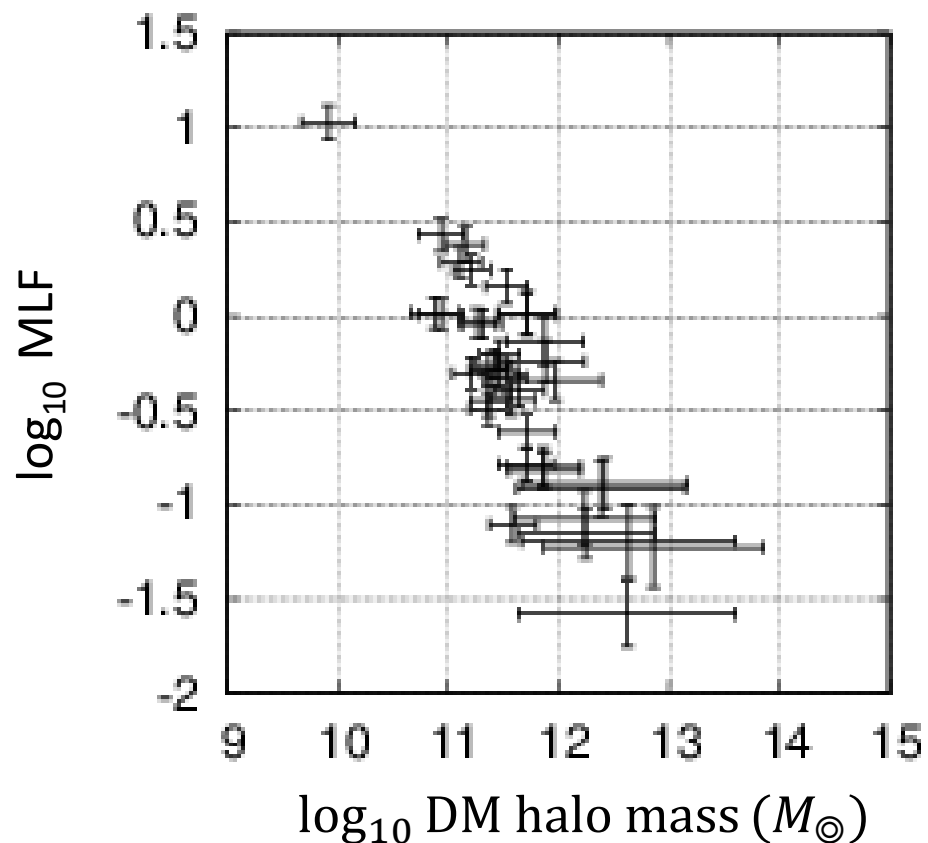


数値実験との比較



Result: ダークマターハロー質量への依存性

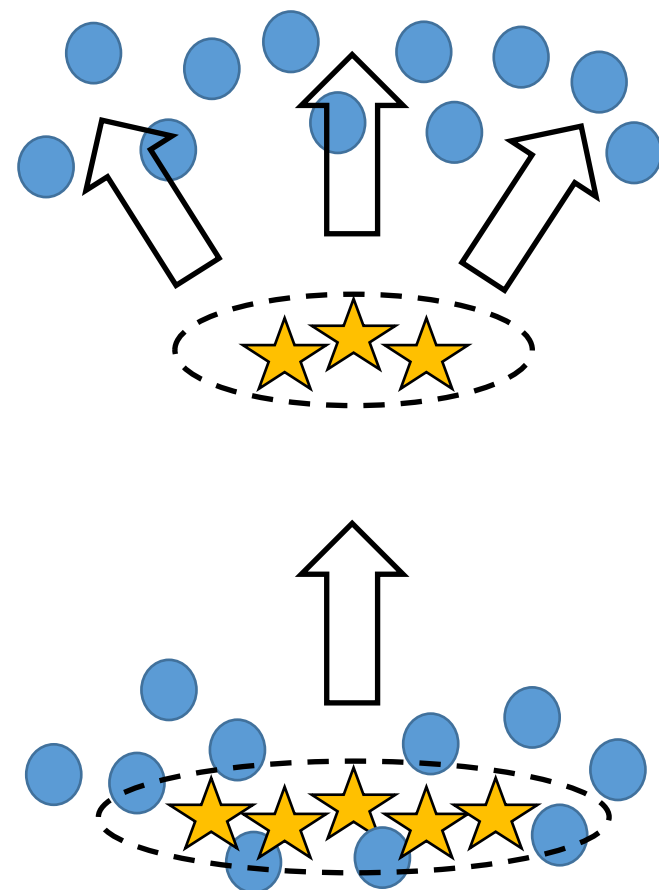
$$\begin{cases} \dot{M}_{SNeII} = 0.35 \text{ SFR} \\ MLF = \dot{M}/\text{SFR} \end{cases} \rightarrow \frac{\dot{M}}{\dot{M}_{SNeII}} = \frac{MLF}{0.35}$$



$M_{DMH} \ll 10^{11.5} M_{\odot}: MLF \gg 0.35$
小質量銀河でガス流出の効率が
高い (星形成が抑制されやすい)

$M_{DMH} \sim 10^{11.5} M_{\odot}: MLF \sim 0.35$
SNeII から放出されたガスが
そのまま出てくる

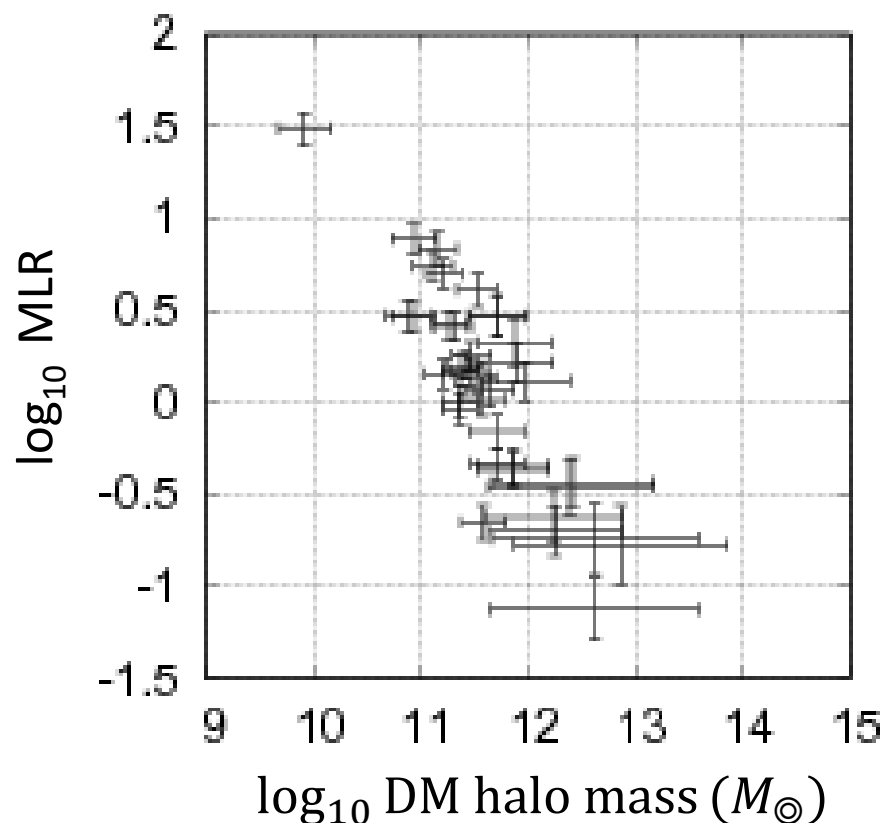
$(M_{DMH} \gg 10^{11.5} M_{\odot}: MLF \ll 0.35)$
(ガス流出の効率が低い)



Result: ダークマターハロー質量への依存性

mass loading rate (MLR): SNeII からの ejected mass と massflux の比
星間ガスの流出効率を示す

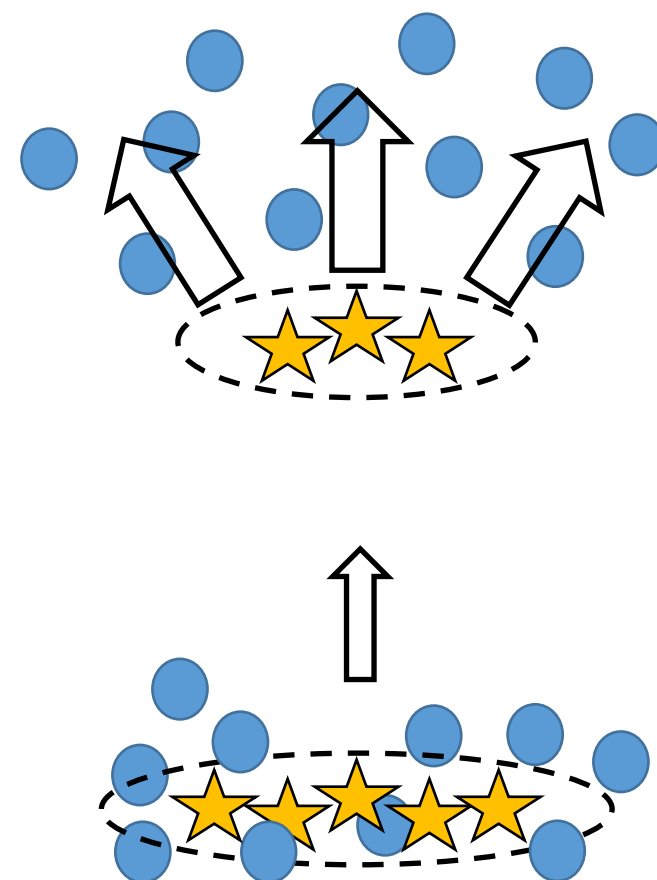
$$\text{MLR} \equiv \dot{M} / \dot{M}_{\text{SNeII}} (\propto \text{MLF}) \quad (\dot{M}_{\text{SNeII}} \propto \text{SFR})$$



$M_{\text{DMH}} \ll 10^{11.5} M_{\odot}$: $\text{MLR} \gg 1$
星間ガスの流出効率が高い
(星形成が抑制されやすい)

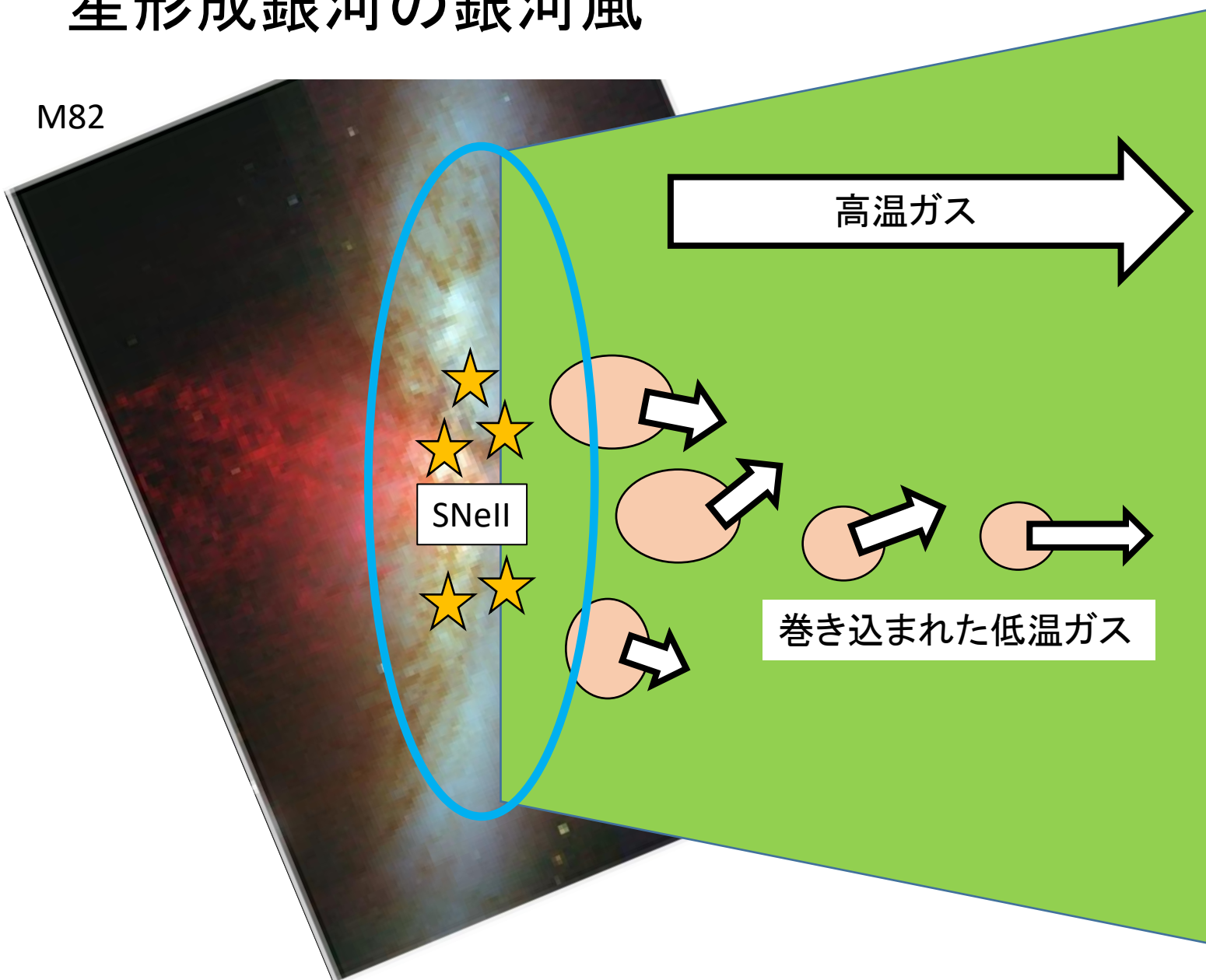
$M_{\text{DMH}} \sim 10^{11.5} M_{\odot}$: $\text{MLR} \sim 1$
SNeII からの ejected mass が
そのまま出てくる

$M_{\text{DMH}} \gg 10^{11.5} M_{\odot}$: $\text{MLR} \ll 1$
ガス流出の効率が低い



星形成銀河の銀河風

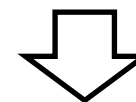
M82



高い星形成率

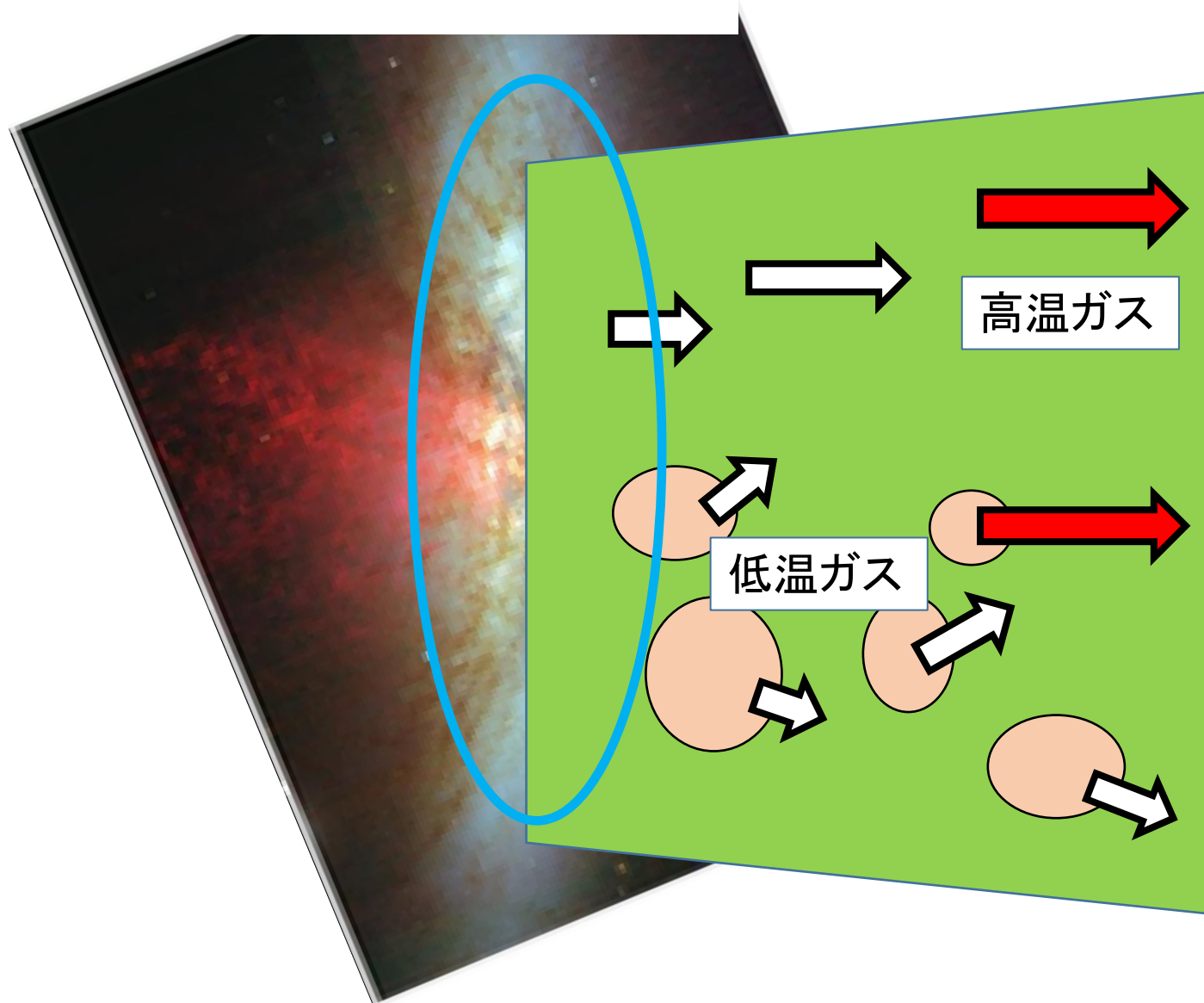
→ 星間ガスにエネルギー注入

→ 銀河風で星間ガスが流出



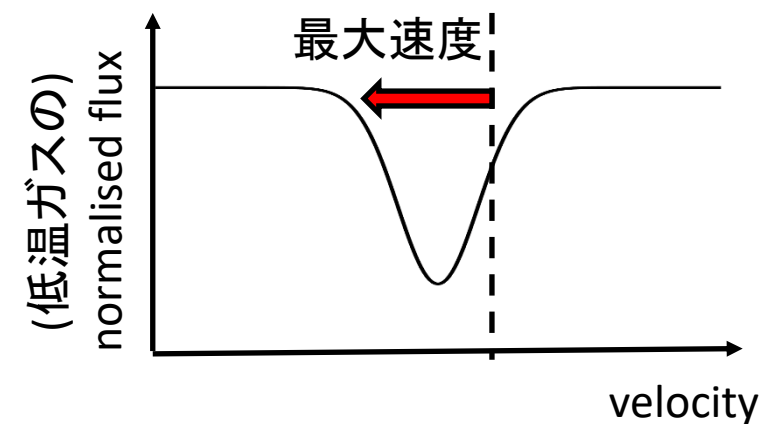
1. 星形成の抑制
2. 銀河間空間の重元素汚染

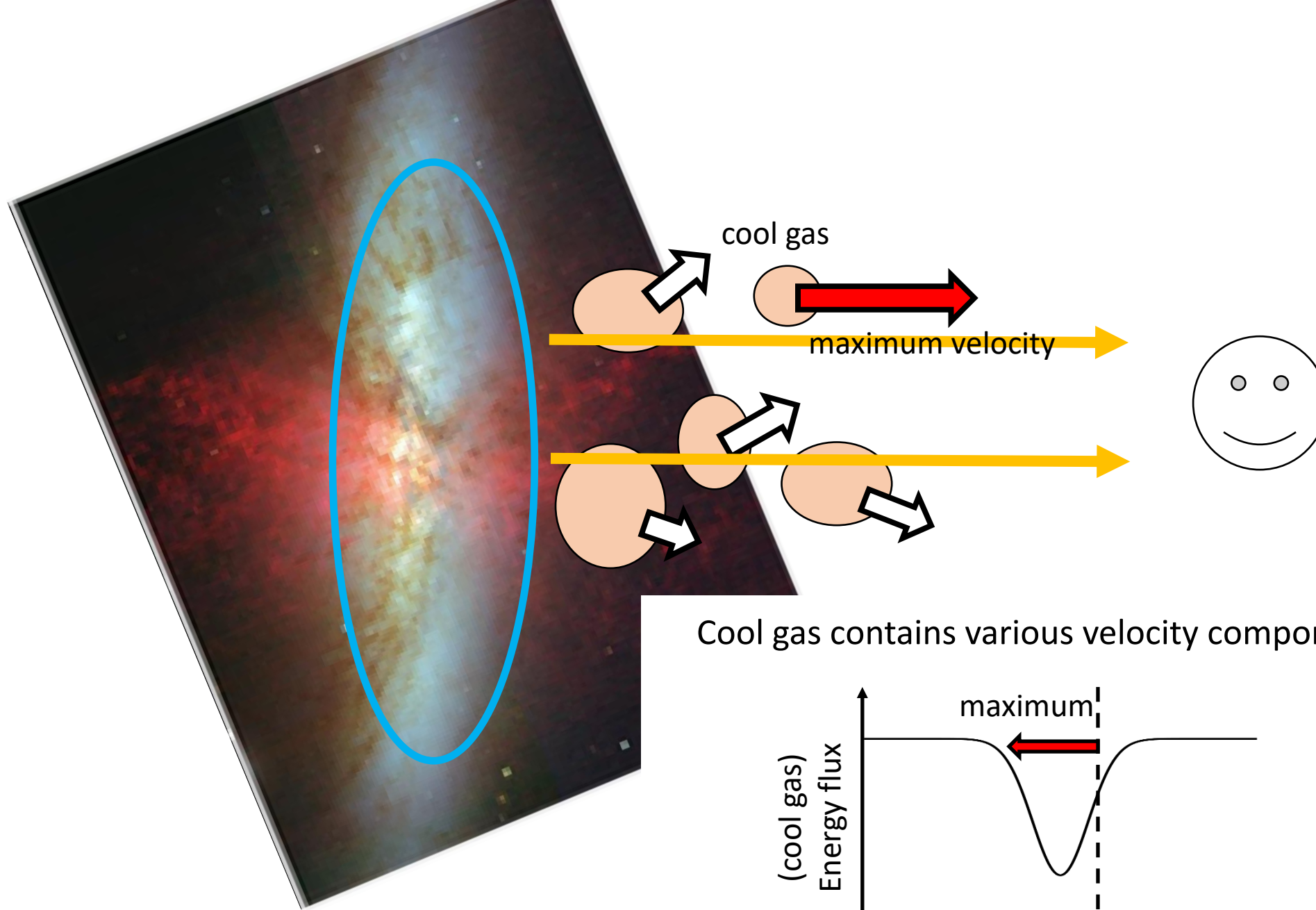
星形成銀河の銀河風速度



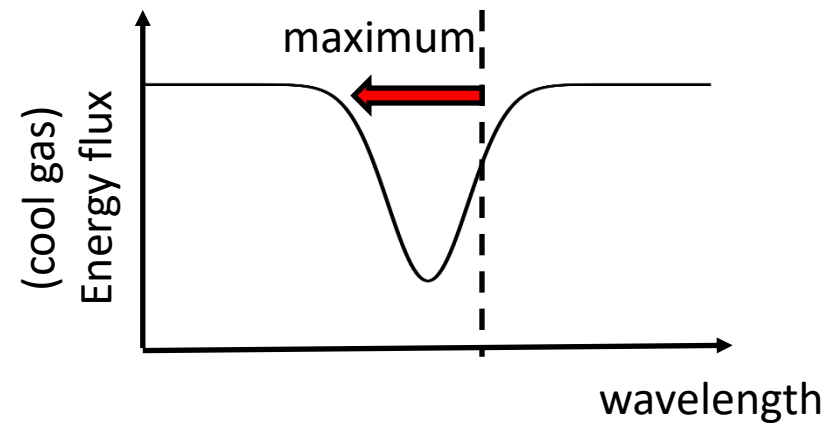
高温ガスの流れによって低温ガスが加速

低温ガスの最大速度
と
高温ガスの最大速度(の下限)





Cool gas contains various velocity components.



Classification of transonic solutions

6 parameters : $(\lambda, SFR, M_{DMH}, M_{st}, r_H, r_d)$

$$\dot{m}_{inj}(\lambda, SFR) \equiv \lambda R_f SFR \quad : \text{total mass flux } (M_o/\text{yr})$$

$$\dot{e}_{inj}(SFR) \equiv \eta \epsilon_{SN} SFR \quad : \text{total injected energy (erg/yr)}$$

$$\dot{e}_{\Phi, dmh}(\lambda, SFR, M_{DMH}, r_d) \equiv \dot{m}_{inj} G \left(\frac{4}{3} \pi \rho_d r_d^3 \right) r_d^{-1} \sim \dot{m}_{inj} \frac{GM_{DMH}}{r_d} \quad : \text{work of DM halo (erg/yr)}$$

$$\dot{e}_{\Phi, H}(\lambda, SFR, M_{st}, r_d) \equiv \dot{m}_{inj} \frac{GM_{st}}{r_d}$$

3 non-dimensional parameters: $\left(\frac{r_H}{r_d}, \frac{\dot{e}_{\Phi, dmh}}{\dot{e}_{inj}}, \frac{\dot{e}_{\Phi, H}}{\dot{e}_{inj}} \right)$

$$\frac{M^2 - 1}{M^2 \{(\Gamma - 1)M^2 + 2\}} \frac{dM^2}{dx} = \frac{2}{x} - \frac{\Gamma + 1}{2(\Gamma - 1)} \frac{\dot{m}_n}{\dot{e}_n - \dot{m}_n \Phi_n} \frac{d\Phi_n}{dx}$$

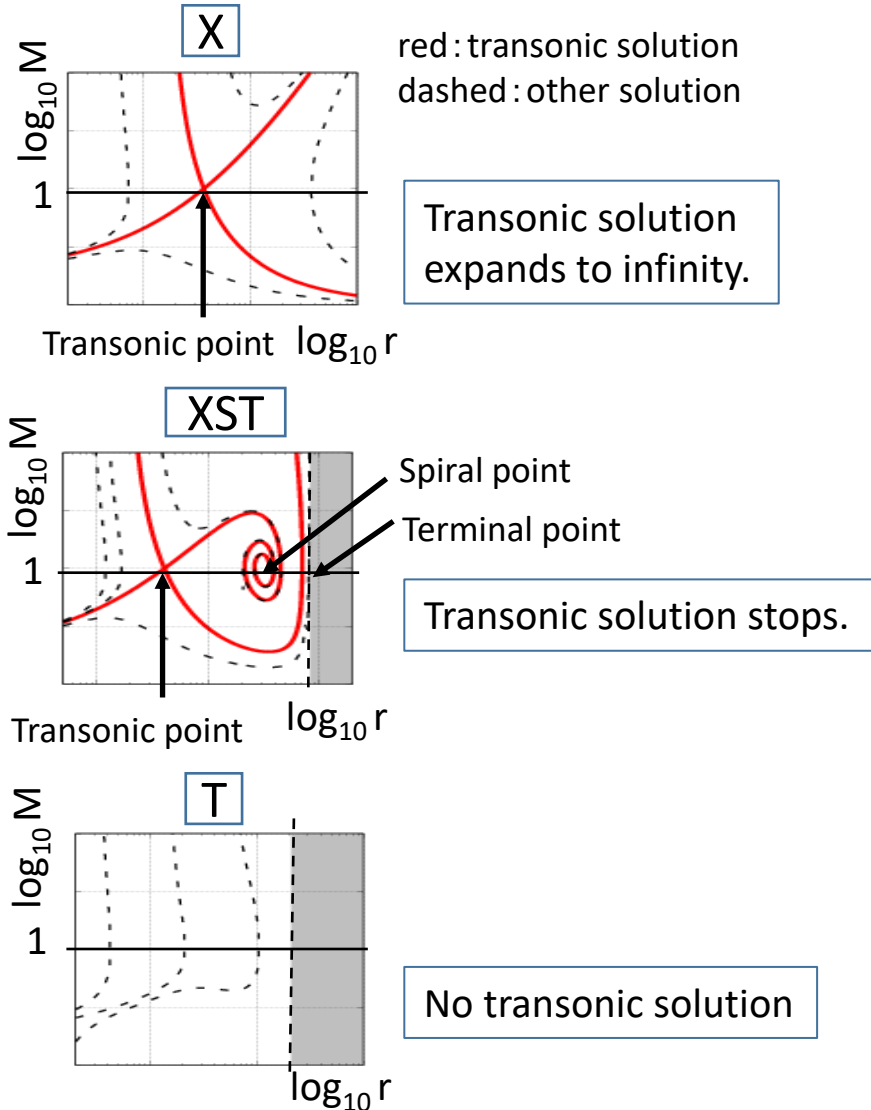
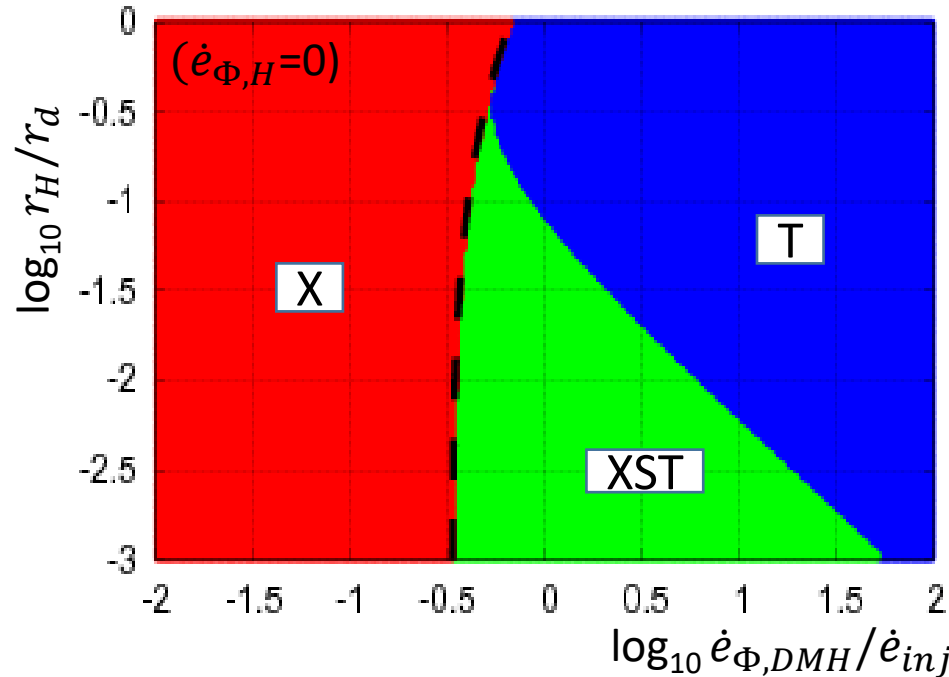
$$- \frac{\Gamma M^2 + 1}{2} \frac{\dot{e}_n - 2\dot{m}_n \Phi_n}{\dot{e}_n - \dot{m}_n \Phi_n} \frac{1}{\dot{m}_n} \frac{d\dot{m}_n}{dx} - \frac{\Gamma M^2 + 1}{2} \frac{1}{\dot{e}_n - \dot{m}_n \Phi_n} \frac{d\dot{e}_n}{dx}$$

$$\Phi_n \equiv \frac{\Phi}{\dot{e}_{inj}/\dot{m}_{inj}} \quad \dot{m}_n \equiv \frac{\dot{m}}{\dot{m}_{inj}} \quad \dot{e}_n \equiv \frac{\dot{e}}{\dot{e}_{inj}}$$

Classification of transonic solutions

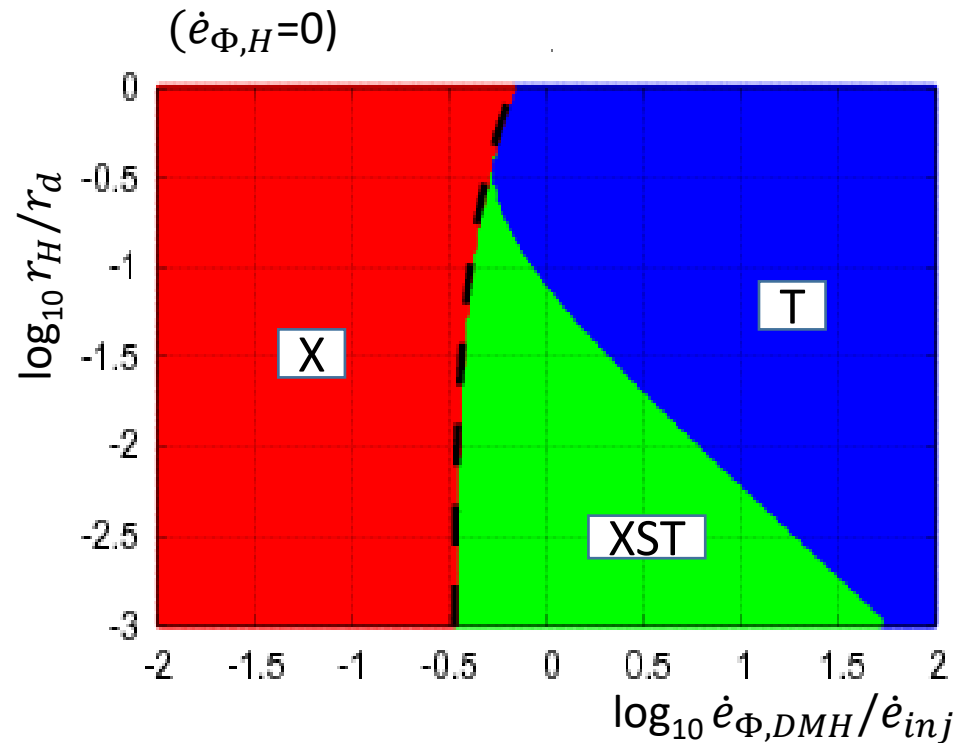
$$\frac{r_H}{r_d} = \frac{\text{Stellar scale length}}{\text{DM halo scale length}} \quad \frac{\dot{e}_{\Phi,dmh}}{\dot{e}_{inj}} \sim \frac{\text{Work of DM halo gravity}}{\text{Injected energy}}$$

There are 3 patterns of transonic solutions.



Classification of transonic solutions

$$\frac{r_H}{r_d} = \frac{\text{Stellar scale length}}{\text{DM halo scale length}} \quad \frac{\dot{e}_{\Phi,dmh}}{\dot{e}_{inj}} \sim \frac{\text{Work of DM halo gravity}}{\text{Injected energy}}$$



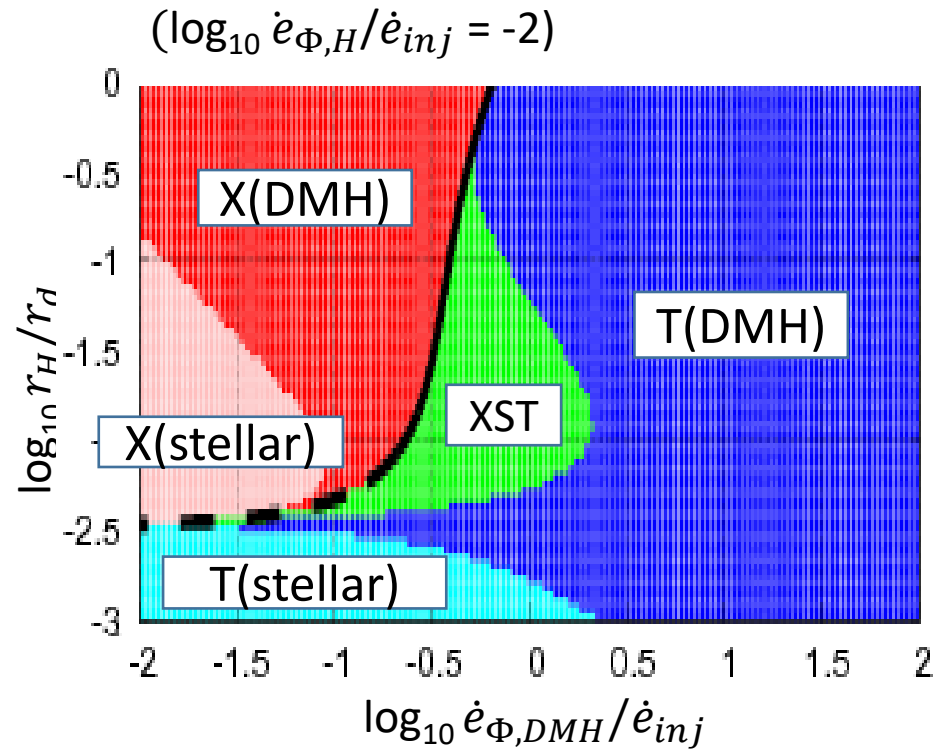
Dashed line shows the case that the total energy becomes 0 in $x \rightarrow \infty$,

$$\dot{e} - \dot{m}\Phi = 0$$

$$\frac{\dot{e}_{\Phi,dmh}}{\dot{e}_{inj}} = \frac{(1 - r_H/r_{dmh})^2}{3r_H/r_{dmh}} \times \left(\log(r_H/r_{dmh}) + \frac{1-r_H/r_{dmh}}{r_H/r_{dmh}} \right)^{-1}.$$

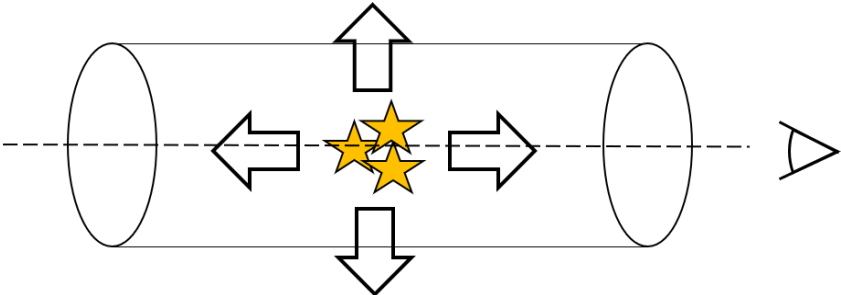
Classification of transonic solutions

$$\frac{r_H}{r_d} = \frac{\text{Stellar scale length}}{\text{DM halo scale length}} \quad \frac{\dot{e}_{\Phi,dmh}}{\dot{e}_{inj}} \sim \frac{\text{Work of DM halo gravity}}{\text{Injected energy}}$$

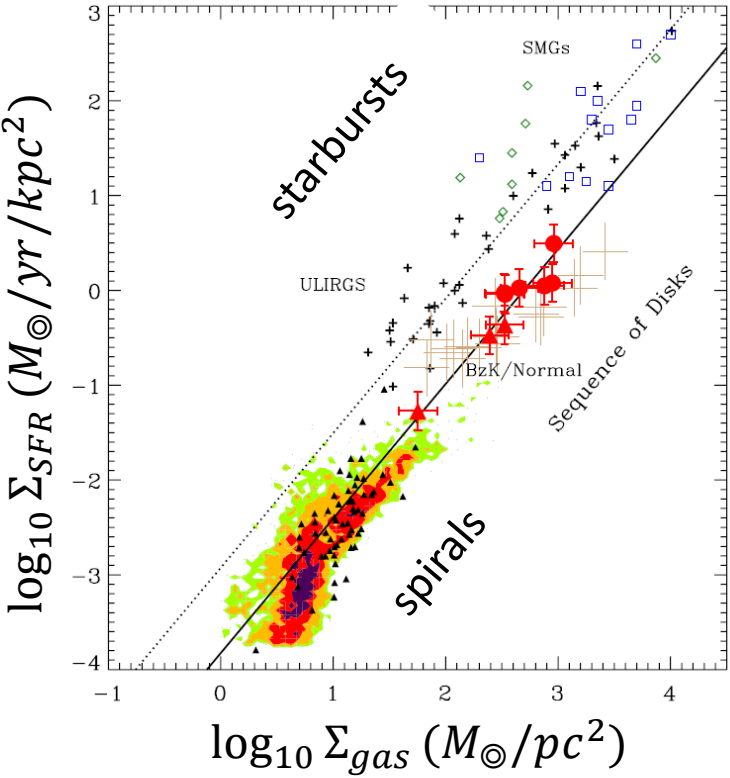
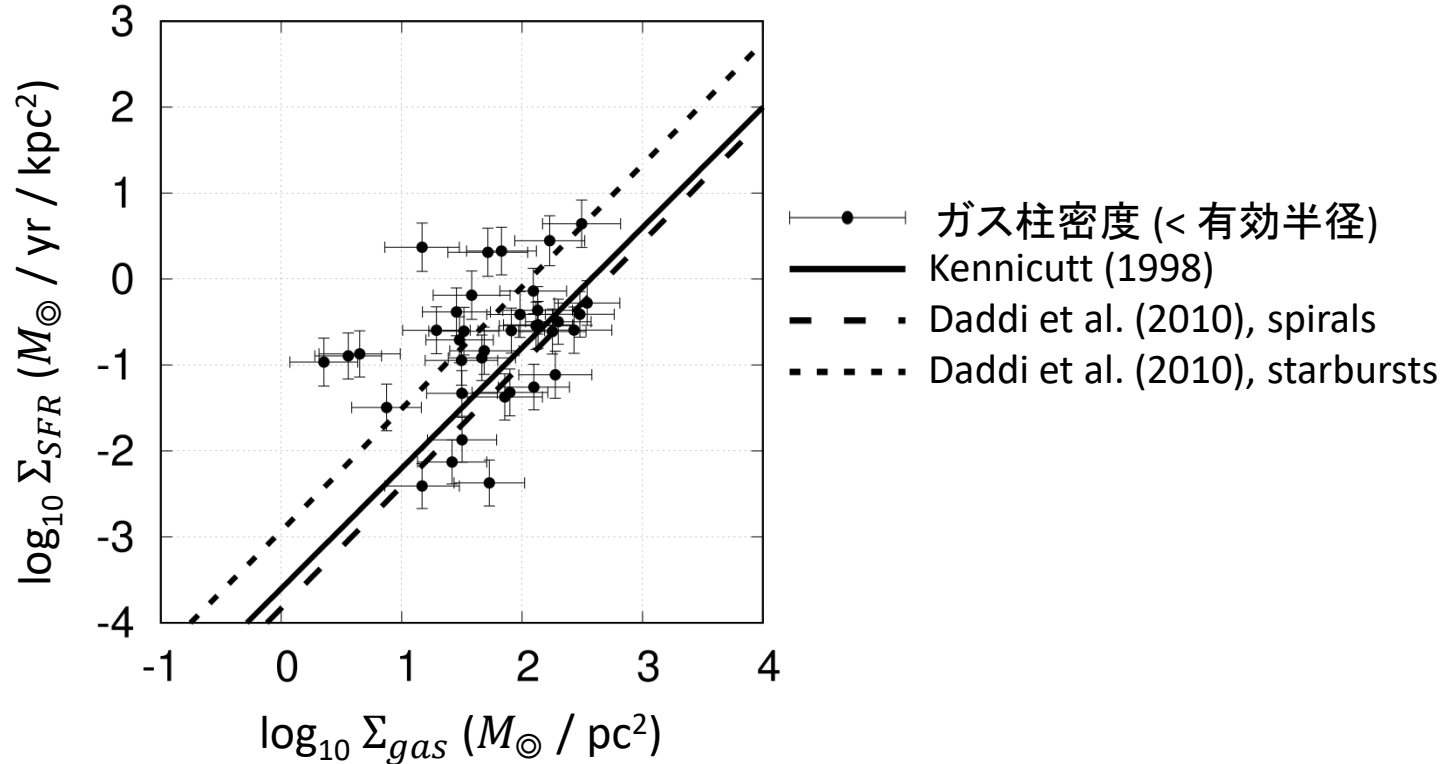


discussion: ガス柱密度

質量流束からガス柱密度が予想できる
Kennicutt-Schmidt law と比較



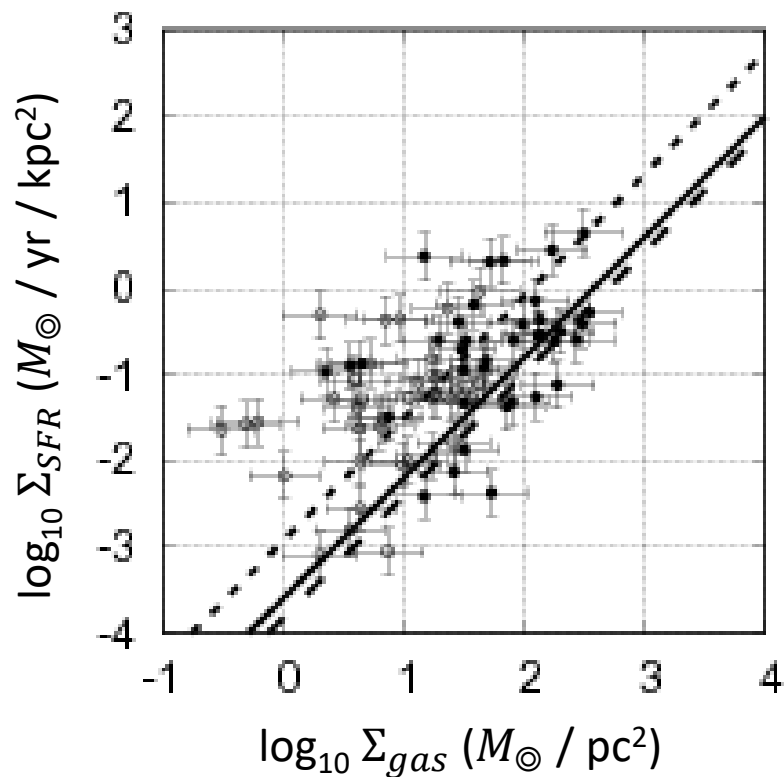
Kennicutt-Schmidt law for
spirals and starbursts
(Daddi et al. 2010)



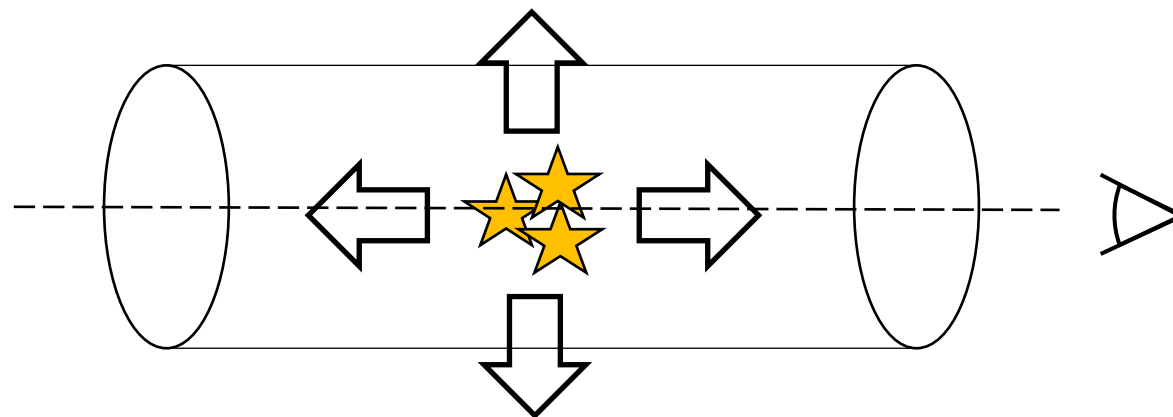
遷音速モデルで予想されたガス柱密度は (starburst galaxies の) Kennicutt-Schmidt law と矛盾しない

discussion: ガス柱密度

質量流束からガス柱密度が予想できる
Kennicutt-Schmidt law と比較



- ガス柱密度 (< 有効半径)
- ガス柱密度 (< 2.68 x 有効半径)
- Kennicutt (1998)
- - - Daddi et al. (2010), spirals
- ... Daddi et al. (2010), starbursts



遷音速モデルで予想されたガス柱密度は (starburst galaxies の) Kennicutt-Schmidt law と矛盾しない

discussion: ガス柱密度

質量流束からガス柱密度を評価
Kennicutt-Schmidt law と比較

