ELEC 344

Pre-Lab for Experiment: #4	
Section: L1E	
Bench #: 6	
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1 - Winding Resistance Test

Measure:
$$V_{DC}$$
 and I_{DC}
$$R_1 = \frac{V_{DC}}{2I_{DC}}$$

2 - No Load Test

Measure: $V_{l-l,NL}$, I_{NL} and P_{NL}

$$\begin{split} \boldsymbol{P}_{loss} &= \boldsymbol{P}_{NL} - \boldsymbol{R}_{1} (\boldsymbol{I}_{NL})^{2} \\ \boldsymbol{V}_{1} &= \frac{\boldsymbol{V}_{l-l,NL}}{\sqrt{3}} \\ \boldsymbol{Q}_{NL} &= \sqrt{(3\boldsymbol{I}_{NL}\boldsymbol{V}_{1})^{2} - (\boldsymbol{P}_{NL})^{2}} \\ \boldsymbol{X}_{1} + \boldsymbol{X}_{m} &= \boldsymbol{X}_{NL} = \frac{\boldsymbol{Q}_{NL}}{3(\boldsymbol{I}_{NL})^{2}} \end{split}$$

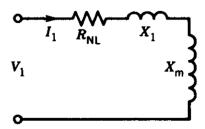


Figure 1. Equivalent circuit diagram for a no load test

3 - Blocked Rotor Test

Measure: $V_{l-l,BR}$, I_{BR} and P_{BR}

$$R_{1} + R_{2}' = R_{BR} = \frac{P_{BR}}{3(I_{BR})^{2}}$$

$$V_{1} = \frac{V_{l-l,BR}}{\sqrt{3}}$$

$$X_{BR} = \sqrt{\left(\frac{V_{1}}{I_{BR}}\right)^{2} - \left(R_{BR}\right)^{2}}$$

$$X_{1} \approx X_{2}' = \frac{X_{BR}}{2}$$
 $X_{m} = X_{NL} - X_{1}$
 $R_{2}' = R_{BR} - R_{1}$

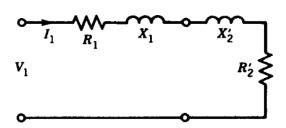


Figure 2. Equivalent circuit diagram for a blocked rotor test

4 - Torque Speed Characteristic

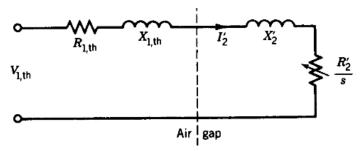


Figure 3. Thevenin equivalent circuit diagram

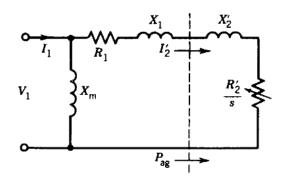


Figure 4. Approximate equivalent circuit diagram

Thevenin :	$\tau_e = \left(\frac{3 \cdot P \cdot (V_{1,th})^2}{2 \cdot \omega_e}\right) \left(\frac{R_2'/S}{(R_{1,th} + R_2'/S)^2 + (X_{1,th} + X_2')^2}\right) where \ \omega_e = 2\pi(60)$
Approximate :	$\tau_e = \left(\frac{3 \cdot P \cdot (V_1)^2}{2 \cdot \omega_e}\right) \left(\frac{R_2' / S}{(R_1 + R_2' / S)^2 + (X_1 + X_2')^2}\right) where \ \omega_e = 2\pi (60)$

5 - Torque Speed Characteristic



Figure 5. Single inductor circuit

$$\begin{split} &V_{1}=L\frac{di}{dt}\\ &V_{1}=\sqrt{2}V_{rms}cos(\omega t)\\ &\sqrt{2}V_{rms}\int cos(\omega t)dt=L\int\frac{di}{dt}dt\\ &\frac{\sqrt{2}V_{rms}}{\omega}sin(\omega t)+C_{1}=Li+C_{2}assume\ C_{1}=C_{2}=0\\ &\frac{\sqrt{2}V_{rms}}{\omega}sin(\omega t)=Li\\ &L=\frac{N\Phi}{i}\\ &\frac{\sqrt{2}V_{rms}}{\omega}sin(\omega t)=i\frac{N\Phi}{i}=N\Phi\\ &\Phi=\frac{\sqrt{2}V_{rms}}{N\omega}sin(\omega t)=\frac{\sqrt{2}V_{rms}}{2\pi Nf}sin(\omega t) \end{split}$$

As can be seen from the derivation above the flux through an inductive element is proportional to the voltage applied to it and inversely proportional to the frequency. As such to maintain a constant flux voltage and frequency should be adjusted together. As such if the voltage is increased, the frequency should also be increased.