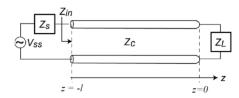
#### HARMONIC SIGNAL



$$\beta = \omega \sqrt{L'C'} = \omega \sqrt{\varepsilon \mu} = \frac{\omega}{v_n} = \frac{2\pi}{\lambda} \left[ \frac{1}{m} \right]$$

$$V^+(z) = V_0^{\phantom{0}} e^{-j\beta z}$$

$$V^-(z) = V_0^- e^{+j\beta z}$$

Reflection coefficient and entrance impedance:

$$\Gamma(0) \equiv \frac{V_0^-}{V_0^+} = \Gamma_L = \frac{Z_L - Z_C}{Z_L + Z_C}$$
  $Z_{in}(z) = Z_C \frac{1 + \Gamma(z)}{1 - \Gamma(z)}$ 

$$\Gamma(z) \equiv \frac{V^{-}(z)}{V^{+}(z)} = \Gamma_{L} \exp(2j\beta z) \qquad \Gamma(z) = \frac{Z_{in}(z) - Z_{C}}{Z_{in}(z) + Z_{C}}$$

$$Z_{in}(z = -L) = Z_C \frac{Z_L + jZ_C \tan(\beta L)}{Z_C + jZ_L \tan(\beta L)}$$

$$Z_{in}\left(z=-\frac{\lambda}{4}\right) = \frac{{Z_C}^2}{Z_L}$$

$$\begin{cases} V(z) = {V_0}^+ e^{-j\beta z} \big[ 1 + \Gamma(z=0) e^{j2\beta z} \big] \\ I(z) = \frac{{V_0}^+}{Z_C} e^{-j\beta z} \big[ 1 - \Gamma(z=0) e^{j2\beta z} \big] \end{cases}$$

## **POWER AND ENERGY CALCULATIONS**

$$P = P_{av} = \langle \mathcal{V}(z, t) \mathcal{I}(z, t) \rangle = \frac{1}{2} \operatorname{Re}[V(z) I^*(z)]$$

$$= \frac{1}{2} |V(z)|^2 \operatorname{Re} \left[ \frac{1}{Z(z)} \right] = \frac{1}{2} |I(z)|^2 \operatorname{Re} [Z(z)]$$

Power of the wave:

$$P^{\pm} = \frac{1}{2} \operatorname{Re} \{ V^{\pm} I^{\pm^*} \} = \pm \frac{1}{2} |V^{\pm}|^2 \operatorname{Re} \left[ \frac{1}{Z_C} \right]$$

$$P = P^+ + P^-$$

Lossless circuit: entrance power equals power on the load

$$P_L = P_{in} = \frac{1}{2} \text{Re}[V_{in}I^*_{in}] = \frac{1}{2} |V_{in}|^2 \text{Re}\left[\frac{1}{Z_{in}}\right]$$

From the Telegraph Eq. we get the wave Eq.:

$$\frac{d^2V}{dz^2} = L'C'\frac{d^2V}{dt^2}$$

$$\frac{d^2I}{dz^2} = L'C'\frac{d^2I}{dt^2}$$

The general solution:

$$\begin{cases} V(z,t) = V^+ \left( t - \frac{z}{v_p} \right) + V^- \left( t + \frac{z}{v_p} \right) \\ I(z,t) = I^+ \left( t - \frac{z}{v_p} \right) + I^- \left( t + \frac{z}{v_p} \right) \end{cases}$$

The propagation velocity:

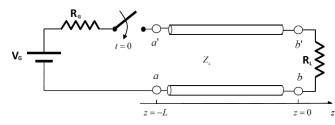
$$v_p = \frac{1}{\sqrt{L'C'}}$$

The characteristic Impedance:

$$Z_c = \sqrt{\frac{L'}{C'}} = \frac{V^+}{I^+} = -\frac{V^-}{I^-}$$

Time Domain solution:

$$\begin{cases} V(z,t) = V_0 + \sum_{n=1}^{\infty} V_n^+ \left( t - \frac{z}{v_p} \right) + \sum_{n=1}^{\infty} V_n^- \left( t + \frac{z}{v_p} \right) \\ I(z,t) = I_0 + \sum_{n=1}^{\infty} I_n^+ \left( t - \frac{z}{v_p} \right) + \sum_{n=1}^{\infty} I_n^- \left( t + \frac{z}{v_p} \right) \end{cases}$$



Reflection coefficient at the load:

$$\Gamma_{\rm L} = \frac{V_n^-(t, z = 0)}{V_n^+(t, z = 0)} = \frac{R_L - Z_c}{R_L + Z_c}$$

Reflection coefficient at the source:

$$\Gamma_{\rm G} = \frac{V_{n+1}^+(t, z = -l)}{V_n^-(t, z = -l)} = \frac{R_G - Z_c}{R_G + Z_c}$$

#### GENERAL

$$\eta_0 = \sqrt{\frac{\mu_0}{\varepsilon_0}} = 377\Omega$$

$$\mu_0 = 4\pi \cdot 10^{-7} \frac{\text{Henry}}{\text{m}}, \quad \varepsilon_0 = 8.85 \cdot 10^{-12} \frac{\text{Farad}}{\text{m}}$$

$$c = \frac{1}{\sqrt{\mu_0 \varepsilon_0}} = 2.9979 \cdot 10^8 \frac{\text{m}}{\text{s}}$$

$$S_n \equiv \sum_{k=0}^n r^k = \frac{1 - r^{n+1}}{1 - r}; S_\infty = \sum_{k=0}^\infty r^k = \frac{1}{1 - r}$$

$$sin(jx) = j sinh(x); cos(jx) = cosh(x)$$

$$e^{jx} = \cos(x) + j\sin(x)$$

$$z = x + jy = |z|e^{j\theta}$$
$$|z| = \sqrt{x^2 + y^2} \quad \theta = \arctan\left(\frac{y}{y}\right)$$

#### **PHASORS**

$$V(t) = V_0 \cos(\omega t + \theta) = \text{Re}\{V_0 e^{j\omega t} e^{j\theta}\} = \text{Re}\{\tilde{V} e^{j\omega t}\}$$
$$.\tilde{V} \equiv V_0 e^{j\theta}$$

$$\frac{d}{dt}V(t) \Leftrightarrow j\omega \tilde{V}$$

# DISTRIBUTED LINE IN LC MODEL (WITHOUT LOSSES)

Inductance and Capacitance per unit length

$$L = L'\Delta z$$
  $L'[H/m] \iota C'[F/m]$ 

$$C = C'\Delta z$$

The Telegraph Eq. in the limit of  $\Delta z \rightarrow 0$ 

$$\frac{dV}{dz} = -L'\frac{dI}{dt}$$

$$\frac{dI}{dz} = -C' \frac{dV}{dt}$$

# For this solution we get:

$$\vec{E} \perp \vec{H} \perp \vec{k}$$

$$\frac{\left|\vec{E}\right|}{\left|\vec{H}\right|} = \eta = \sqrt{\frac{\mu}{\varepsilon}} = \sqrt{\frac{\mu_0 \, \mu_r}{\varepsilon_0 \, \varepsilon_r}} = \eta_0 \sqrt{\frac{\mu_r}{\varepsilon_r}} = \frac{\eta_0}{n}$$

$$\vec{H} = \frac{\hat{k} \times \vec{E}}{\eta} = \frac{1}{\eta} (\hat{k} \times \vec{E}_0) e^{-j\vec{k}\cdot\vec{r}}$$

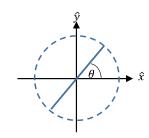
#### **POLARIZATION OF a PLANE WAVE**

In frequency:

$$\vec{E}(z_0) = \hat{x}|E_x| + \hat{y}|E_y|e^{j\phi_y - \phi_x}$$

In time:

$$\vec{E}(z_0, t) = \hat{x} |E_x| \cos(\omega t) + \hat{y} |E_y| \cos(\omega t + \phi_y - \phi_x)$$



#### LINEAR POLARIZATION

$$\phi_{v} - \phi_{x} = m \cdot \pi$$
 ;  $m \in \mathbb{Z}$ 

$$\vec{E}(z_0, t) = \hat{x} |E_x| \cos(\omega t) \pm \hat{y} |E_y| \cos(\omega t)$$

$$\vec{E}(z_0) = |E_x|\hat{x} \pm |E_y|\hat{y}$$

Notating:

$$\theta = \tan^{-1}\left(\pm \frac{|E_y|}{|E_x|}\right); \quad 0 < \theta < \pi$$

$$|E_x| = E_0 \cos(\theta), \quad \pm |E_y| = E_0 \sin(\theta)$$

#### **REFLECTION WITH LOSSES**

$$\Gamma(0) = \frac{Z_L - Z_C}{Z_L + Z_C}, \quad \Gamma(z) = \Gamma(0)e^{+2\gamma z}$$

$$\Gamma(-L) = \Gamma(0)e^{-2\gamma L} = \Gamma(0)e^{-2j\beta L - 2\alpha L}$$

$$Z_{in}(-L) = Z_C \frac{1 + \Gamma(-L)}{1 - \Gamma(-L)} = Z_C \frac{Z_L + Z_C \tanh(j\beta L + \alpha L)}{Z_C + Z_L \tanh(j\beta L + \alpha L)}$$

$$V(z) = V_0^{+} \left[ e^{-\alpha z} e^{-j\beta z} + \Gamma_L e^{+\alpha z} e^{+j\beta z} \right]$$

$$= V_0^{+} e^{-\alpha z} e^{-j\beta z} \left[ 1 + \Gamma_L e^{+2\alpha z} e^{+2j\beta z} \right]$$

$$I(z) = \frac{V_0^+}{Z_0} \left[ e^{-\alpha z} e^{-j\beta z} - \Gamma_L e^{+\alpha z} e^{+j\beta z} \right]$$
$$= \frac{V_0^+}{Z} e^{-\alpha z} e^{-j\beta z} \left[ 1 - \Gamma_L e^{+2\alpha z} e^{+2j\beta z} \right]$$

#### **POWERS**

$$P(z) = \frac{1}{2} \operatorname{Re}\{VI^*\} =$$

$$= \frac{1}{2} \operatorname{Re}\{|V_0^+|^2 Y_C^* e^{-2\alpha z} (1 - |\Gamma_L|^2 e^{+4\alpha z})\}$$

$$P_{in}(z = -l) = \frac{1}{2} \operatorname{Re}\{|V_0^+|^2 Y_C^* e^{2\alpha l} (1 - |\Gamma_L|^2 e^{-4\alpha l})\}$$

$$P_{load}(z = 0) = \frac{1}{2} \operatorname{Re}\{|V_0^+|^2 Y_C^* (1 - |\Gamma_L|^2)\}$$

## PLANE WAVES

$$\begin{cases} \nabla \times \vec{E} = -j\omega\mu\vec{H} \\ \nabla \times \vec{H} = j\omega\varepsilon\vec{E} \\ \nabla \cdot \vec{E} = 0 \\ \nabla \cdot \vec{H} = 0 \end{cases} \Rightarrow \begin{cases} \nabla^{2}\vec{E} + \omega^{2}\mu\varepsilon\vec{E} = 0 \\ \nabla^{2}\vec{H} + \omega^{2}\mu\varepsilon\vec{H} = 0 \end{cases}$$

The solution is:

$$\vec{E} = \vec{E}_0 e^{-j\vec{k}\cdot\vec{r}}$$

$$\vec{k} \cdot \vec{r} = k_x x + k_y y + k_z z$$

$$k = |\vec{k}| = 2\pi n/\lambda_0 = \omega \sqrt{\mu \varepsilon} = \omega n/c = \sqrt{k_x^2 + k_y^2 + k_z^2}$$

## STANDING WAVE RATIO (SWR)

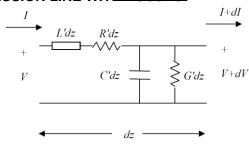
$$S = \frac{|V_{\text{max}}|}{|V_{\text{min}}|} = \frac{1 + |\Gamma|}{1 - |\Gamma|} \ge 1$$

$$|V_{\text{max}}| = |V_0^+|(1+|\Gamma|)$$

$$|V_{\min}| = |V_0^+|(1 - |\Gamma|)$$

$$|\Gamma(z)| = |\Gamma(0)e^{2j\beta z}| = |\Gamma(0)|$$

## TRANSMISSION LINE WITH LOSSES



Conductivity (heat) losses – R'

Dielectric losses – G'

#### WAVE EQUATION WITH LOSSES

$$\begin{cases} \frac{dV}{dz} = -IR' - L' \frac{dI}{dt} \\ \frac{dI}{dz} = -VG' - C' \frac{dV}{dt} \end{cases}$$
$$\frac{d^2V}{dz^2} = L'C' \frac{d^2V}{dt^2} + (C'R' + L'G') \frac{dV}{dt} + R'G'V$$

The solution to the equation:

$$V = \operatorname{Re} \left\{ V_0 e^{-\gamma z} e^{j\omega t} \right\}$$

$$\gamma = \alpha + j\beta = \pm \sqrt{(R' + j\omega L')(G' + j\omega C')}$$
 [1/m]

$$Z_C(\omega) = \frac{V^+}{I^+} = R_0 + jX_0 = \sqrt{\frac{R' + j\omega L'}{G' + j\omega C'}}$$

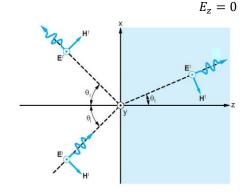
Small losses:  $R' << \omega L', G' << \omega C'$ 

In first order approximation:

$$\beta \approx \omega \sqrt{L'C'}$$
  $\alpha \approx \frac{1}{2} \sqrt{L'C'} \left( \frac{R'}{L'} + \frac{G'}{C'} \right)$ 

Under this approximation, the decay coefficient is not frequency dependent and the propagation coefficient has a linear dependency (no dispersion).

## TE SOLUTION (PERPENDICULAR)



$$\vec{k} = k_x \hat{x} + k_z \hat{z} = k(\hat{x} \sin \theta + \hat{z} \cos \theta)$$

$$\hat{e}_{\mathrm{TE}} = \hat{y}$$

$$\hat{h}_{TF} = -\hat{x}\cos\theta + \hat{z}\sin\theta$$

$$\vec{E}_{TF} = E_{TF} \hat{y} e^{-jk \sin \theta x} e^{-jk \cos \theta z}$$

$$E_y = e^{-jk\sin\theta x} \big[ V_0^+ e^{-jk\cos\theta z} + V_0^- e^{jk\cos\theta z} \big], \qquad V_0^+ = E_{\rm TE}$$

#### TL MODEL FOR TE POLARIZATION:

$$E_y^+ \leftrightarrow V^+$$

$$-H_{r}^{+} \leftrightarrow I^{+}$$

$$k_z = k \cos \theta \leftrightarrow \beta$$

$$\frac{\eta}{\cos\theta} \leftrightarrow Z_{C_{TE}}$$

The longitudinal component:

$$H_z = \left[\frac{1}{Z_{CTE}} \tan \theta\right] E_y$$

## FRESNEL EQUATIONS FOR TE:

(For the transverse component Ey):

$$r_{21}^{\mathrm{TE}} = \frac{\frac{\eta_{2}}{\cos\theta_{2}} - \frac{\eta_{1}}{\cos\theta_{1}}}{\frac{\eta_{2}}{\cos\theta_{2}} + \frac{\eta_{1}}{\cos\theta_{1}}} = \frac{n_{1}\cos\theta_{1} - \frac{\mu_{1}}{\mu_{2}}n_{2}\cos\theta_{2}}{n_{1}\cos\theta_{1} + \frac{\mu_{1}}{\mu_{2}}n_{2}\cos\theta_{2}}$$

$$t_{21}^{\text{TE}} = \frac{2\frac{\eta_2}{\cos \theta_2}}{\frac{\eta_2}{\cos \theta_2} + \frac{\eta_1}{\cos \theta_1}} = \frac{2n_1 \cos \theta_1}{n_1 \cos \theta_1 + \frac{\mu_1}{\mu_2} n_2 \cos \theta_2}$$

$$t_{21}^{\mathrm{TE}} = r_{21}^{\mathrm{TE}} + 1$$

Skin depth:

$$\delta_s = \frac{1}{\alpha}$$

In a metal (good conductor):

$$\varepsilon_{\text{eff}} = \varepsilon' - j \left[ \varepsilon'' + \frac{\sigma}{\omega} \right] \xrightarrow{\frac{\sigma}{\omega} > |\varepsilon'|, |\varepsilon''|} - j \frac{\sigma}{\omega}$$

$$k = \omega \sqrt{\mu \varepsilon_{\text{eff}}} = \frac{1 - j}{\sqrt{2}} \sqrt{\omega \mu \sigma}$$

$$\alpha = \beta = \sqrt{\frac{\omega\mu\sigma}{2}}, \qquad \delta_s = \frac{1}{\alpha} = \sqrt{\frac{2}{\omega\mu\sigma}}$$

$$\eta = (1+j)\sqrt{\frac{\omega\mu}{2\sigma}}$$

 $Usually: |Z_{metal}| << Z_{other}$ 

# FRESNEL EQUATIONS FOR PERPENDICULAR INCIDENT:

Refractive index in a dielectric:

$$n = \sqrt{\varepsilon_r}$$

The incident wave is coming from medium 1 to medium 2:

$$n_{1} = \sqrt{\varepsilon_{r1}} \Rightarrow r_{21} = \frac{\eta_{2} - \eta_{1}}{\eta_{2} + \eta_{1}} = \frac{n_{1} - n_{2}}{n_{1} + n_{2}}$$

$$r_{21} = \frac{\eta_{2} - \eta_{1}}{\eta_{2} + \eta_{1}} = \frac{2n_{1}}{n_{1} + n_{2}}$$

$$t_{21} = 1 + r_{21} = \frac{2\eta_{2}}{\eta_{2} + \eta_{1}} = \frac{2n_{1}}{n_{1} + n_{2}}$$

### **ANGLED INCIDENT:**

$$\vec{E}(\vec{r}) = \vec{E}_0 e^{-j\vec{k}\cdot\vec{r}}$$

$$= [E_{\mathrm{TE}}\hat{e}_{\mathrm{TE}} + E_{\mathrm{TM}}\hat{e}_{\mathrm{TM}}]e^{-j\vec{k}\cdot\vec{r}}$$

$$\vec{H}(\vec{r}) = \frac{1}{n} (\hat{k} \times \vec{E}_0) e^{-j\vec{k}\cdot\vec{r}}$$

$$= \left[ \frac{E_{\rm TE}}{n} \, \hat{h}_{\rm TE} + \frac{E_{\rm TM}}{n} \, \hat{h}_{\rm TM} \right] e^{-j\vec{k}\cdot\vec{r}}$$

$$\hat{e}_{\mathrm{TM}} \perp \hat{e}_{\mathrm{TE}} \perp \hat{k}$$

#### CIRCULAR POLARIZATION

$$\phi_y - \phi_x = \pm \frac{\pi}{2} + 2\pi m$$
 ;  $m \in \mathbb{Z}$ 

And the modulus of the amplitudes are equal

$$|E_x| = |E_y| = |E|/\sqrt{2}$$

RIGHT CIRCULAR

$$\phi_{v} - \phi_{x} = -\pi/2$$

$$\{RC\}: \vec{E}(z_0, t) = \frac{|E|}{\sqrt{2}} (\cos(\omega t) \,\hat{x} + \sin(\omega t) \,\hat{y})$$

{RC}: 
$$\vec{E}(z_0) = \frac{|E|}{\sqrt{2}} \cdot (\hat{x} - j\hat{y})$$

LEFT CIRCULAR

$$\phi_{\nu} - \phi_{x} = +\pi/2$$

{LC}: 
$$\vec{E}(z_0, t) = \frac{|E|}{\sqrt{2}} (\cos(\omega t) \hat{x} - \sin(\omega t) \hat{y})$$

$$\{LC\}: \vec{E}(z_0) = \frac{|E|}{\sqrt{2}} \cdot (\hat{x} + j\hat{y})$$

#### PERPENDICULAR INCIDENT

$$\vec{E}(z) = \vec{E}_0 e^{-j\beta z} = [E_{0x}\hat{x} + E_{0y}\hat{y}]e^{-j\beta z}$$

$$\vec{H}(z) = \frac{1}{\eta} (\hat{z} \times \vec{E}_0) e^{-j\beta z} = \left[ \frac{E_{0x}}{\eta} \hat{y} - \frac{E_{0y}}{\eta} \hat{x} \right] e^{-j\beta z}$$

TL MODEL FOR PERPENDICULAR INCIDENT

$$E_x^+ / E_y^+ \leftrightarrow V^+$$

$$H_{\mathcal{V}}^+ / - H_{\mathcal{X}}^+ \leftrightarrow I^+$$

$$k = \omega \sqrt{\epsilon \mu} \ \leftrightarrow \ \beta$$

$$\eta = \sqrt{\frac{\mu}{\epsilon}} \leftrightarrow Z_C$$

# MEDIUM WITH LOSSES AND CONDUCTIVITY

$$\gamma = jk = j\beta + \alpha$$

Dielectric and magnetic losses:

$$\varepsilon = \varepsilon' - j\varepsilon'', \qquad \mu = \mu' - j\mu''$$

With a finite conductivity:

$$\eta = \sqrt{\frac{\mu}{\varepsilon - j\frac{\sigma}{\omega}}}, \qquad k_2 = \omega \sqrt{\mu \left(\varepsilon - j\frac{\sigma}{\omega}\right)}$$

$$E_T(x;z) = \int_{-\infty}^{\infty} \tilde{E}_T(k_x;z) \cdot e^{-jk_x x} dk_x$$

$$\tilde{E}_T(k_x;z) = \frac{1}{2\pi} \int_{-\infty}^{\infty} E_T(x;z) \cdot e^{jk_x x} dx$$

Spectrum of the field at z=0:

$$E_T(x;0) = \int_{-\infty}^{\infty} \tilde{E}_T(k_x;0) \cdot e^{-jk_x x} dk_x$$

$$\tilde{E}_T(k_x;0) = \frac{1}{2\pi} \int_{-\infty}^{\infty} E_T(x;0) \cdot e^{jk_x x} dx$$

The connection between the spectrum at z and the spectrum at z=0:

$$\tilde{E}(k_x; z) = \tilde{E}(k_x; 0) \cdot e^{-jk_z z} = \tilde{E}_0(k_x) \cdot e^{-j\sqrt{k^2 - k_x^2 \cdot z}}$$

The field in z>0:

$$E(x;z) = \int_{-\infty}^{\infty} \tilde{E}_0(k_x) \cdot e^{-j\sqrt{k^2 - k_x^2} \cdot z} \cdot e^{-jk_x x} dk_x$$

For far field we can neglect the decay waves with

$$E(x;z) = \int_{-k}^{k} \tilde{E}_0(k_x) \cdot e^{-jk_x x} \cdot e^{-j\sqrt{k^2 - k_x^2} \cdot z} dk_x$$

Useful functions:

$$\operatorname{sinc}(x) = \frac{\sin(x)}{x}$$

$$comb\left(\frac{x}{a}\right) = |a| \cdot \sum_{n=0}^{\infty} \delta(x - na)$$

## TEM TRANSMISSION LINES

Structures supporting TEM mode:

$$E_z=H_z=0$$

$$k \leftrightarrow \beta$$

$$\vec{E}(\vec{r}) = \vec{e}(x, y)[V_0^+ e^{-jkz} + V_0^- e^{+jkz}]$$

$$\vec{H}(\vec{r}) = \vec{h}(x, y)[I_0^+ e^{-jkz} + I_0^- e^{+jkz}]$$

$$\vec{h}(x,y) = \frac{Z_C}{\eta} \vec{z} \times \vec{e}(x,y)$$

#### **BRUSTER ANGLE:**

The angle for which there is no reflection for TM only:

$$\theta_B = \tan^{-1}\left(\frac{n_2}{n_1}\right) = \tan^{-1}\left(\sqrt{\frac{\varepsilon_2}{\varepsilon_1}}\right) \Rightarrow r_{21}^{\text{TM}} = 0$$

In general:

$$\theta_B = \sin^{-1} \left[ \sqrt{\frac{\mu_2 \varepsilon_2 (\eta_2^2 - \eta_1^2)}{\eta_2^2 \mu_1 \varepsilon_1 - \eta_1^2 \mu_2 \varepsilon_2}} \right]$$

#### SNELL'S LAW:

$$\frac{\sin \theta_1}{\sin \theta_2} = \frac{\sqrt{\mu_{r2}\varepsilon_{r2}}}{\sqrt{\mu_{r1}\varepsilon_{r1}}} = \frac{n_2}{n_1}$$

$$n_1 > n_2$$

The critic angle:

$$\sin \theta_{cr} = \frac{n_2}{n_1}$$

For incident angle greater than the critic:  $\theta_i > \theta_{cr}$ :

$$|\Gamma_{\text{TE}}| = |\Gamma_{\text{TM}}| = 1 = e^{j\phi}$$

$$\cos \theta_2 = -j \sqrt{\frac{\sin^2 \theta_1}{\sin^2 \theta_{cr}} - 1}$$

Plugging in:  $\vec{E}_2(z) = \vec{E}_{0z} e^{-jk_2(x\sin\theta_t + z\cos\theta_t)}$ 

leads to propagation in x and decay in z:

$$\vec{E}_2(z) = \vec{E}_{0_2} \mathrm{e}^{-jk_2 x} \frac{\sin\theta_1}{\sin\theta_{cr}} e^{-k_2 z} \sqrt{\frac{\sin^2\theta_1}{\sin^2\theta_{cr}} - 1}$$

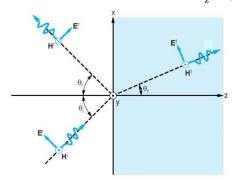
In a full reflection:

$$\Gamma_{\text{TM}} = e^{j\phi_{\text{TM}}} \quad \phi_{\text{TM}} = 2 \tan^{-1} \left( -\frac{\sqrt{\sin^2 \theta_1 - \sin^2 \theta_{cr}}}{\cos \theta_1 \sin^2 \theta_{cr}} \right)$$

$$\Gamma_{\rm TE} = e^{j\phi_{\rm TE}} \quad \phi_{\rm TE} = 2 \tan^{-1} \left( \frac{\sqrt{\sin^2 \theta_1 - \sin^2 \theta_{cr}}}{\cos \theta_1} \right)$$

## TM SOLUTION (PARALLEL)

 $H_z = 0$ 



$$\vec{k} = k_x \hat{x} + k_z \hat{z} = k(\hat{x} \sin \theta + \hat{z} \cos \theta)$$

$$\hat{e}_{\text{TM}} = \hat{x} \cos \theta - \hat{z} \sin \theta$$

$$\hat{h}_{\mathrm{TM}} = \hat{1}$$

$$\vec{E}_{\text{TM}} = E_{\text{TM}} \left( \hat{x} \cos \theta - \hat{z} \sin \theta \right) e^{-jk \sin \theta x} e^{-jk \cos \theta z} =$$

$$E_x = e^{-jk\sin\theta x} [V_0^+ e^{-jk\cos\theta z} + V_0^- e^{jk\cos\theta z}],$$

$$V_0^+ = E_{\rm TM} \cos \theta$$

## TL MODEL FOR TM POLARIZATION:

$$E_x^+ \leftrightarrow V^+$$

$$H_y^+ \leftrightarrow I^+$$

$$k_z = k \cos \theta \leftrightarrow \beta$$

$$\eta \cos \theta \leftrightarrow Z_{C_{TM}}$$

The longitudinal component:

$$E_z = \left[ -Z_{C_{TM}} \tan \theta \right] H_v$$

## FRESNEL EQUATIONS FOR TM POLARIZATION:

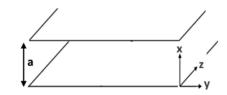
(For the transverse component Ex):

$$r_{21}^{\text{TM}} = \frac{\eta_2 \cos \theta_2 - \eta_1 \cos \theta_1}{\eta_2 \cos \theta_2 + \eta_1 \cos \theta_1} = \frac{n_1 \cos \theta_2 - \frac{\mu_1}{\mu_2} n_2 \cos \theta_1}{n_1 \cos \theta_2 + \frac{\mu_1}{\mu_2} n_2 \cos \theta_1}$$

$$t_{21}^{\text{TM}} = \frac{2\eta_2 \cos \theta_2}{\eta_2 \cos \theta_2 + \eta_1 \cos \theta_1} = \frac{2n_1 \cos \theta_2}{n_1 \cos \theta_2 + \frac{\mu_1}{\mu_2} n_2 \cos \theta_1}$$

$$t_{21}^{\text{TM}} = r_{21}^{\text{TM}} + 1$$

## PLATES WAVEGUIDE:



Wave vector:

$$\beta_{m} = \sqrt{k^{2} - k_{c,m}^{2}} = \omega \sqrt{\mu \varepsilon \left[1 - \left(\frac{f_{c,m}}{f}\right)^{2}\right]}$$

$$k_{c,m} = \left(\frac{m\pi}{a}\right)$$

Cut-off frequency:

$$f_{c,m} = \frac{1}{2\sqrt{\mu\varepsilon}} \left(\frac{m}{a}\right)$$

#### TEM MODE:

$$E_x = Ae^{-jkz}$$

$$H_y = \frac{E_x}{\eta} e^{-jkz}$$

#### TE MODES:

$$E_{y} = C_{m} \sin\left(\frac{m\pi}{a}x\right) e^{-j\beta_{m}z}$$

$$H_x = -\frac{\beta_m}{\omega\mu} C_m \sin\left(\frac{m\pi}{a}x\right) e^{-j\beta_m z}$$

$$H_z = j \frac{m\pi}{\omega \mu a} C_m \cos\left(\frac{m\pi}{a}x\right) e^{-j\beta_m z}$$

$$Z_m^{\rm TE} = \frac{\omega \mu}{\beta_m} = \frac{k\eta}{\beta_m}$$

#### TM MODES:

$$H_y = C_m \cos\left(\frac{m\pi}{a}x\right) e^{-j\beta_m z}$$

$$E_x = \frac{\beta_m}{\omega \varepsilon} C_m \cos\left(\frac{m\pi}{a}x\right) e^{-j\beta_m z}$$

$$E_z = \frac{jm\pi}{\omega \varepsilon a} C_m \sin\left(\frac{m\pi}{a}x\right) e^{-j\beta_m z}$$

$$Z_m^{\text{TM}} = \frac{\beta_m}{\omega \varepsilon} = \frac{\beta_m \eta}{k}$$

# Wavelength:

$$\lambda_{nm} = \frac{2\pi}{\beta_{nm}}$$

# TE MODES:

$$H_z = A_{nm} \cos\left(\frac{n\pi x}{a}\right) \cos\left(\frac{m\pi y}{b}\right) e^{-j\beta_{nm}z}$$

$$E_x = \frac{j\omega\mu}{k^2 - \beta_{nm}^2} \frac{m\pi}{b} A_{nm} \cos\left(\frac{n\pi x}{a}\right) \sin\left(\frac{m\pi y}{b}\right) e^{-j\beta_{nm}z}$$

$$E_{y} = -\frac{j\omega\mu}{k^{2} - \beta_{nm}^{2}} \frac{n\pi}{a} A_{nm} \sin\left(\frac{n\pi x}{a}\right) \cos\left(\frac{m\pi y}{b}\right) e^{-j\beta_{nm}z}$$

$$H_x = \frac{j\beta_{nm}}{k^2 - \beta_{nm}^2} \frac{n\pi}{a} A_{nm} \sin\left(\frac{n\pi x}{a}\right) \cos\left(\frac{m\pi y}{b}\right) e^{-j\beta_{nm}z}$$

$$H_{y} = \frac{j\beta_{nm}}{k^{2} - \beta_{nm}^{2}} \frac{m\pi}{b} A_{nm} \cos\left(\frac{n\pi x}{a}\right) \sin\left(\frac{m\pi y}{b}\right) e^{-j\beta_{nm}z}$$

$$Z_{nm}^{\mathrm{TE}} = -\frac{E_{y}}{H_{x}} = \frac{E_{x}}{H_{y}} = \frac{k\eta}{\beta_{nm}} = \frac{\eta}{\sqrt{1 - \left(\frac{f_{c,nm}}{f}\right)^{2}}}$$

### TM MODES:

$$E_z = B_{nm} \sin\left(\frac{n\pi x}{a}\right) \sin\left(\frac{m\pi y}{b}\right) e^{-j\beta_{nm}z}$$

$$H_x = \frac{j\omega\varepsilon}{k^2 - \beta_{nm}^2} \frac{m\pi}{b} B_{nm} \sin\left(\frac{n\pi x}{a}\right) \cos\left(\frac{m\pi y}{b}\right) e^{-j\beta_{nm}z}$$

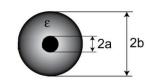
$$H_{y} = -\frac{j\omega\varepsilon}{k^{2} - \beta_{nm}^{2}} \frac{n\pi}{a} B_{nm} \cos\left(\frac{n\pi x}{a}\right) \sin\left(\frac{m\pi y}{b}\right) e^{-j\beta_{nm}z}$$

$$E_x = -\frac{j\beta_{nm}}{k^2 - \beta_{nm}^2} \frac{n\pi}{a} B_{nm} \cos\left(\frac{n\pi x}{a}\right) \sin\left(\frac{m\pi y}{b}\right) e^{-j\beta_{nm}z}$$

$$E_{y} = -\frac{j\beta_{nm}}{k^{2} - \beta_{nm}^{2}} \frac{m\pi}{b} B_{nm} \sin\left(\frac{n\pi x}{a}\right) \cos\left(\frac{m\pi y}{b}\right) e^{-j\beta_{nm}z}$$

$$Z_{nm}^{\mathrm{TM}} = -\frac{E_y}{H_x} = \frac{E_x}{H_y} = \frac{\beta_{nm}\eta}{k} = \eta \sqrt{1 - \left(\frac{f_{c,nm}}{f}\right)^2}$$

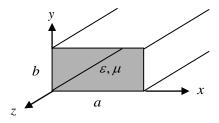
#### **COAXIAL LINE:**



$$\vec{e}(r,\phi) = \hat{r} \frac{1}{\ln(b/a)} \frac{1}{r}, \qquad \vec{h}(r,\phi) = \hat{\phi} \frac{1}{2\pi r}$$

$$Z_C = \eta \frac{\ln(b/a)}{2\pi}$$

#### **RECTANGULAR WAVEGUIDE:**



Wave vector:

$$\beta_{nm} = \sqrt{k^2 - k^2_{c,nm}}, \qquad k = \omega \sqrt{\mu \varepsilon}$$

$$k_{c,nm} = \sqrt{\left(\frac{n\pi}{a}\right)^2 + \left(\frac{m\pi}{b}\right)^2}$$

Cut-off frequency:

$$f_{c,nm} = \frac{1}{2\sqrt{\mu\varepsilon}} \sqrt{\left(\frac{n}{a}\right)^2 + \left(\frac{m}{b}\right)^2}$$

Phase velocity:

$$v_p = \frac{\omega}{\beta_{nm}} = \frac{\frac{1}{\sqrt{\mu \varepsilon}}}{\sqrt{1 - \left(\frac{f_{c,nm}}{f}\right)^2}} \underset{f > f_{c,nm}}{\overset{}{\underset{\text{propagating}}{\sum}}} \frac{1}{\sqrt{\mu \varepsilon}}$$

Group velocity:

$$v_g = \frac{\beta_{nm}}{k} \frac{1}{\sqrt{\mu \varepsilon}} \le \frac{1}{\sqrt{\mu \varepsilon}}$$

$$\underline{E} \simeq \underline{\hat{\theta}} j \omega \mu g(r) I_0 d \sin \theta \ e^{jk\underline{\hat{r}} \cdot \underline{r}'}, \underline{H} \simeq \underline{\hat{\phi}} \eta^{-1} E_{\theta}$$

Radiation Pattern:

$$F(\theta, \phi) = \frac{|E(\theta, \phi)|}{|E|_{max}}$$

## **POINTING VECTOR:**

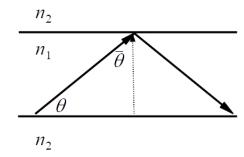
$$\underline{S} = \frac{1}{2}\underline{E} \times \underline{H}^* = \hat{\underline{r}} \frac{|E|^2}{2\eta}$$

## **DISPERSION:**

$$v_p = \frac{\omega}{\beta(\omega)}$$

$$v_g = \frac{1}{\partial \beta(\omega)/\partial \omega}$$

#### **DIELECTRIC WAVEGUIDE:**



$$\bar{\theta}_c = \cos^{-1}\left(\frac{n_2}{n_1}\right)$$

Solutions for TE modes:

$$\tan\left(\frac{\pi d}{\lambda}n_1\sin\theta - m\frac{\pi}{2}\right) = \sqrt{\frac{\sin^2\bar{\theta}_c}{\sin^2\theta} - 1}$$

## **RADIATION:**

$$J = \underline{\hat{z}} I_0 d\delta(\underline{r} - \underline{r}') e^{j\omega t}$$

The dipole location:

$$\underline{r}' = x'\underline{\hat{x}} + y'\underline{\hat{y}} + z'\underline{\hat{z}}$$

The observation point:

$$\underline{r} = x\underline{\hat{x}} + y\underline{\hat{y}} + z\underline{\hat{z}}$$

$$= r(\sin\theta\cos\phi\,\hat{\underline{x}} + \sin\theta\sin\phi\,\hat{y} + \cos\theta\,\hat{\underline{z}})$$

The magnetic vector potential of the dipole:

$$\underline{A} = \underline{\hat{z}}\mu I_0 d \frac{e^{-jkR}}{4\pi R}, R = \left|\underline{r} - \underline{r}'\right|$$

Far field approximation:

$$R = r - \underline{\hat{r}} \cdot \underline{r}'$$

$$\underline{A} = \underline{\hat{z}}\mu g(r)I_0 de^{jk\underline{\hat{r}}\cdot\underline{r}'}, g(r) = \frac{e^{-jkr}}{4\pi r}$$