

SECTION 1

Quasi-Geostrophic Equations

In this section, I introduce some basic equations in QG theories. Building a foundation for SQG, eSQG and other variations introduced later. The analysis is already in a **stratified ocean**.

SUBSECTION 1.1

Governing Equations

Momentum Equation

$$\frac{D\mathbf{u}}{Dt} + \mathbf{f} \times \mathbf{u} = -\frac{\nabla p}{\rho} \quad (1.1)$$

Mass Conservation

$$\frac{D\rho}{Dt} + \rho \nabla \cdot \mathbf{v} = 0 \quad (1.2)$$

We are in a **stratified ocean**. Breaking the total state variables into a "hydrostatic reference state" (which depends only on z) and a "dynamic perturbation" (which moves the fluid):

$$\rho = \tilde{\rho}(z) + \rho_1(x, y, z, t) \quad (1.3)$$

and

$$p = p_0(z) + p_1(x, y, z, t) \quad (1.4)$$

Then RHS of Eq 1.6 becomes

$$-\frac{1}{\rho} \nabla p_1 \sim -\frac{1}{\rho_0} \nabla p_1$$

Define the **Kinematic Pressure**

$$\phi = \frac{p_1}{\rho_0} \quad (1.5)$$

Momentum Equation becomes

$$\frac{D\mathbf{u}}{Dt} + \mathbf{f} \times \mathbf{u} = -\nabla \phi$$

(1.6)

Hydrostatic balance is a state of equilibrium in a fluid where the upward force of pressure exactly balances the downward force of gravity.

$$-g\tilde{\rho} = \frac{dp_0}{dz} \quad (1.7)$$

In Ocean, we assume the velocity field is divergent free. THen the mass conservation yeilds

$$\frac{\partial \rho_1}{\partial t} + \nabla \cdot ((\tilde{\rho} + \rho_1)\mathbf{v}) = 0 \Rightarrow \boxed{\nabla \cdot (\tilde{\rho}\mathbf{v}) = 0}$$

Remark 1

Here we drop the $\partial_t \rho_1$ term under the **Anelastic assumption**. Essentially by eliminating this partial derivative, we assume the fluid is anelastic, so sound wave is not supported¹ in the system.

¹or less important

Next we define the Buoyancy :

$$b = -g \frac{\rho}{\tilde{\rho}_0} \quad (1.8)$$

Here $\bar{\rho}_0$ is a constant reference density. The the divergent free condition implies

$$\boxed{\frac{Db}{Dt} = 0} \quad (1.9)$$

And thus the Hydrostatic balance equation Eq 1.7 implies

$$\boxed{\frac{\partial \phi}{\partial z} = b} \quad (1.10)$$

All the Boxed Equation together is the **Hydrostatic Anelastic Equations for Stratified Flow**. If we consider the perturbation of Buoyancy

$$b = \tilde{b}(z) + b_1(x, y, z, t)$$

Expand Eq 1.9 can be written as

$$\boxed{\frac{Db_1}{Dt} + w \frac{db}{dz} = 0}^2 \quad (1.11) \quad ^2\text{this is the more familiar buoyancy equation we see in lecture}$$

In a more familiar form we define

$$N^2 = \frac{db}{dz} = -g \frac{\tilde{\rho}_z}{\bar{\rho}_0}$$

Which is the **Brunt Vasala Frequency**.

SUBSECTION 1.2

Scaling Analysis

To simplify our equation, we introduce some scalings.

$$(x, y) \sim L, \quad (u, v) \sim U, \quad t \sim \frac{L}{U}, \quad z \sim H, \quad f \sim f_0$$

Introduce the **Rosby Number**:

$$\text{Ro} = \frac{U}{f_0 L} \quad (1.12)$$

Now let $\phi = \tilde{\phi}(z) + \phi_1(x, y, z, t)$. Then since the gradient in Eq 1.6 is horizontal, we can replace ϕ by ϕ_1 . Now suppose

$$|\mathbf{f} \times \mathbf{u}| \sim |\nabla \phi_1|$$

From Hydrostatic balance we have

$$b \sim \frac{f_0 U L}{H}$$

Then

$$\frac{(\partial b' / \partial z)}{N^2} \sim \text{Ro} \frac{L^2}{L_d^2}$$

Where we have the deformation radius as a function of z .

$$L_d = \frac{NL}{f_0}$$

Introduce dimensionless variables

$$(\hat{u}, \hat{v}) = U^{-1}(u, v) \quad \hat{w} = \frac{L}{UH} w, \quad \hat{f} = f_0^{-1} f, \quad \hat{\phi} = \frac{\phi_1}{f_0 UL}, \quad \hat{b} = \frac{H}{f_0 UL} b_1$$

Remark 2

We then have dimensionless equation of motion for Anelastic Assumption³

$$\text{Momentum Equation : } \text{Ro} \frac{D\hat{\mathbf{u}}}{Dt} + \hat{\mathbf{f}} \times \hat{\mathbf{u}} = -\nabla \hat{\phi} \quad (1.13)$$

$$\text{Buoyancy Equation : } \text{Ro} \frac{D\hat{b}}{Dt} + \left(\frac{L_d}{L} \right)^2 \hat{w} = 0 \quad (1.14)$$

$$\text{Hydrostatic Balance : } \frac{\partial \hat{\phi}}{\partial \hat{z}} = \hat{b} \quad (1.15)$$

$$\text{Continuity : } \hat{\nabla} \cdot \hat{\mathbf{u}} + \frac{1}{\tilde{\rho}} \frac{\partial \tilde{\rho} \hat{w}}{\partial \hat{z}} = 0 \quad (1.16)$$

From now on I will drop the hats.

³often people drop the hat for simplicity. However in the first derivation I keep everything with a hat.

SUBSECTION 1.3

Quasi-Geostrophic Potential Vorticity Equation

We now derive the Quasi-Geostrophic Potential Vorticity Equations. Starting from asymptotic expansions⁴

$$\mathbf{u} = (u, v, w) = \mathbf{u}_g + \text{Ro} \mathbf{u}_1 \quad \phi = \phi_0 + \text{Ro} \phi_1 \quad b = b_0 + \text{Ro} b_1$$

⁴hat is dropped

Here we consider the β effect.

$$\mathbf{f} = f_0 \mathbf{k} + \beta y \mathbf{k}$$

Let $\epsilon = \text{Ro}$. **Momentum Equation :**

The $O(1)$ momentum equation gives the Geostrophic balance

$$f_0 \mathbf{k} \times \mathbf{u}_g = -\nabla \phi_0 \quad (1.17)$$

Immediately this implies

$$\nabla \cdot \mathbf{u}_g = 0$$

And $O(\epsilon)$ is

$$\frac{D_g \mathbf{u}_g}{Dt} + \beta y \mathbf{k} \times \mathbf{u}_g + f_0 \mathbf{k} \times \mathbf{u}_1 = -\nabla \phi_1 \quad (1.18)$$

Here D_g is the geostrophic material derivative

$$D_g = \partial_t + \mathbf{u}_g \cdot \nabla$$

Mass Equation :

Since geostrophic velocity is divergent free then $O(1)$ mass equations is

$$\frac{\partial \tilde{\rho} w_0}{\partial z} = 0$$

and $O(\epsilon)$,

$$\nabla \cdot \mathbf{u}_1 + \frac{1}{\tilde{\rho}} \left(\frac{\partial \tilde{\rho} w_1}{\partial z} \right) = 0 \quad (1.19)$$

Buoyancy Equation :

$O(1)$:

$$\left(\frac{L_d}{L} \right)^2 w_0 = 0$$

and $O(\epsilon)$:

$$\frac{D_g b_0}{Dt} + \left(\frac{L_d}{L} \right)^2 w_1 = 0 \quad (1.20)$$

Now we take the **Curl** of Eq 1.18, note that

$$\nabla \times (\mathbf{k} \times \mathbf{u}_1) = \mathbf{k} \nabla \cdot \mathbf{u}_1 - \underbrace{u_1 \nabla \cdot \mathbf{k}}_{=0} + \underbrace{(\mathbf{u}_1 \cdot \nabla) \mathbf{k}}_{=0} - \underbrace{(\mathbf{k} \cdot \nabla) \mathbf{u}_1}_{=0} = \mathbf{k} \nabla \cdot \mathbf{u}_1$$

Define the geostrophic vorticity :

$$\xi_g = \nabla \times \mathbf{u}_g$$

Then Eq 1.18 becomes

$$\frac{D_g \xi_g}{Dt} + \beta v_0 = -f_0 \nabla \cdot \mathbf{u}_1^5$$

⁵ this equation is already in \mathbf{k} direction so the unit vector is dropped

Plug in Eq 1.19,

$$= \frac{f_0}{\tilde{\rho}} \frac{\partial \tilde{\rho} w_1}{\partial z}$$

Plug in Eq 1.20 to replace w_1

$$= -\frac{f_0}{\tilde{\rho}} \frac{\partial}{\partial z} \underbrace{\left(\tilde{\rho} \left(\frac{L}{L_d} \right)^2 \frac{D_g b_0}{Dt} \right)}_{\equiv I}$$

Now we examine I , normally in QG theory, we assume L_d is a constant. Thought from its definition, N could actually depends on z . Since $\nabla \tilde{\rho} = 0$, we can put the first two terms into the material derivative.⁶

$$I = \partial_z \left(\tilde{\rho} \left(\frac{L}{L_d} \right)^2 \right) \frac{D_g b_0}{Dt} + \tilde{\rho} \left(\frac{L}{L_d} \right)^2 \partial_z \frac{D_g b_0}{Dt} \equiv I_1 + I_2$$

⁶ Here we use the fact that N is constant

Let's go back to the Hydrostatic balance equation,⁷ For $O(1)$:

$$\frac{\partial \phi_0}{\partial z} = b_0 \quad + \quad f_0 \mathbf{k} \times \mathbf{u}_g = -\nabla \phi_0 \quad \Rightarrow \quad \mathbf{k} \times \frac{\partial \mathbf{u}_g}{\partial z} = -\frac{\nabla b_0}{f_0}$$

⁷ we haven't use it yet.

Then

$$I_2 = \tilde{\rho} \left(\frac{L}{L_d} \right)^2 \partial_z \frac{D_g b_0}{Dt} = \tilde{\rho} \left(\frac{L}{L_d} \right)^2 \left[\frac{D_g \partial_z b_0}{Dt} + \underbrace{\partial_z \mathbf{u}_g \cdot \nabla b_0}_{=0} \right]$$

Therefore

$$I = \partial_z \left(\tilde{\rho} \left(\frac{L}{L_d} \right)^2 \right) \frac{D_g b_0}{Dt} + \tilde{\rho} \left(\frac{L}{L_d} \right)^2 \frac{D_g \partial_z b_0}{Dt} = \frac{D_g}{Dt} \left[\frac{\partial}{\partial z} \left(\tilde{\rho} \left(\frac{L}{L_d} \right)^2 b_0 \right) \right]$$

Then evantly we have

$$\frac{D_g}{Dt} \left[\xi_g + f + \frac{f_0}{\tilde{\rho}} \frac{\partial}{\partial z} \left(\tilde{\rho} \left(\frac{L}{L_d} \right)^2 b_0 \right) \right] = 0 \quad (1.21)$$

We can rewrite this equation using Streamfunction in a more simple form. Recall Eq 1.9, we have

$$b_0 = \frac{\partial \phi_0}{\partial z}$$

From Eq 1.17, the Kinematic Pressure can be expressed in terms of geostrophic streamfunction

$$u_g = -\partial_y \psi_g \quad v_g = \partial_x \psi_g \quad \text{where} \quad \boxed{\phi_0 = f_0 \psi_g} \quad \Rightarrow \quad \xi_g = \nabla^2 \psi_g$$

Then Eq 1.21 becomes

$$\frac{Dg}{Dt} \left[\nabla^2 \psi_g + f + \frac{f_0^2}{\tilde{\rho}} \frac{\partial}{\partial z} \left(\tilde{\rho} \left(\frac{L}{L_d} \right)^2 \frac{\partial \psi_g}{\partial z} \right) \right] = 0 \quad (1.22)$$

Restore the dimensions

$$\frac{Dg}{Dt} \left[\nabla^2 \psi_g + f + \frac{f_0^2}{\tilde{\rho}} \frac{\partial}{\partial z} \left(\frac{\tilde{\rho}}{N^2} \frac{\partial \psi}{\partial z} \right) \right] = 0 \quad (1.23)$$

SECTION 2

Surface Quasi-Geostrophic Equations

The surface Quasi-Geostrophic Equation takes the problem to the next step, how could we retrieve the interior motion from surface measurements such as SSH and SST. Recall the Buoyancy Equation

$$\frac{Db_1}{Dt} + w N^2 = 0 \quad (2.1)$$

At the surface, $z = \eta$, the boundary condition yeilds that $w = 0$. We denote the surface buoyancy as b_s and surface velocity \mathbf{u}_s . Then

$$\frac{\partial b_s}{\partial t} + \mathbf{u}_s \cdot \nabla b_s = 0$$

and

$$b_s = f_0 \frac{\partial \psi}{\partial z} \Big|_{z=0}$$

Explanation 1 The critical principle of SQG is to view surface buoyancy as a PV sheet. Since

$$\int_0^\epsilon f + \nabla^2 \psi_g + \frac{f_0^2}{\tilde{\rho}} \frac{\partial}{\partial z} \left(\frac{\tilde{\rho}}{N^2} \frac{\partial \psi}{\partial z} \right) dz = 0$$

Then we impose a boundary condition

$$\frac{\partial \psi}{\partial z} \Big|_{z=\epsilon} = \frac{b_s}{f_0} \quad \Rightarrow \quad \int_0^\epsilon \frac{b_s}{f_0} = \frac{\partial \psi}{\partial z} \Big|_0^\epsilon$$

Compare the latter with the integral, by defining

$$q_{\text{SQG}} = \nabla^2 \psi_g + f + \frac{f_0^2}{\tilde{\rho}} \frac{\partial}{\partial z} \left(\frac{\tilde{\rho}}{N^2} \frac{\partial \psi}{\partial z} \right) + \frac{b_s}{f_0} \delta(z)$$

We have

$$\frac{Dq}{Dt} = 0 \quad \frac{\partial \psi}{\partial z} = 0$$

Then the surface buoyancy appears in the QGPV equation naturally, it is as if adding an additional PV sheet at the surface. This inspires us to seperate the surface induced dynamics and

| interior dynamics.

Interior Dynamics

$$\begin{cases} q &= \nabla^2\psi + f + \frac{f_0^2}{\tilde{\rho}} \frac{\partial}{\partial_z} \left(\frac{\tilde{\rho}}{N^2} \frac{\partial\psi}{\partial z} \right) \\ f_0 \frac{\partial\psi}{\partial z} \Big|_{z=0} &= 0 \\ \frac{Dq}{Dt} &= 0 \end{cases}$$

SUBSECTION 2.1

Surface Buoyancy Induced Dynamics

Surface Dynamics, this is the Surface Quasi-Geostrophic Dynamics:

$$\begin{cases} q &= \nabla^2\psi + f + \frac{f_0^2}{\tilde{\rho}} \frac{\partial}{\partial_z} \left(\frac{\tilde{\rho}}{N^2} \frac{\partial\psi}{\partial z} \right) = 0^8 \\ f_0 \frac{\partial\psi}{\partial z} \Big|_{z=0} &= b_s \\ \frac{Db_s}{Dt} &= 0 \end{cases}$$

⁸no interior Potential vorticity

The key assumption for SQG theories is that all the Potential vorticity is injected into the system by surface buoyancy.⁹

SECTION 3

⁹surface buoyancy is actually first order, so it is also called surface buoyancy anomaly in some context.

QG⁺¹ Model
