M.E. 530.646 UR5 Inverse Kinematics

Ryan Keating Johns Hopkins University

Introduction

Figure 1 below illustrates a common assignment of Denavit-Hartenberg convention to the UR5 robot (shown with all joint angles at 0).

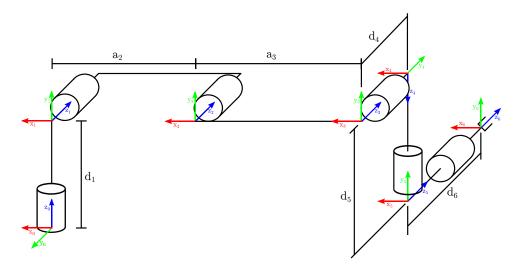


Figure 1: D-H Convention Frame Assignment

Joint	a	α	d	θ
1	0	$\pi/2$	d_1	θ_1
2	$-a_2$	0	0	θ_2
3	$-a_3$	0	0	θ_3
4	0	$\pi/2$	d_4	θ_4
5	0	$-\pi/2$	d_5	θ_5
6	0	0	d_6	θ_6

Table 1: D-H Parameters

As with any 6-DOF robot, the homogeneous transformation from the base frame to the gripper can be defined as follows:

$$T_{6}^{0}(\theta_{1},\theta_{2},\theta_{3},\theta_{4},\theta_{5},\theta_{6}) = T_{1}^{0}(\theta_{1}) T_{2}^{1}(\theta_{2}) T_{3}^{2}(\theta_{3}) T_{4}^{3}(\theta_{4}) T_{5}^{4}(\theta_{5}) T_{6}^{5}(\theta_{6}) = \begin{bmatrix} x_{x} & y_{x} & z_{x} & (P_{6}^{0})_{x} \\ x_{y} & y_{y} & z_{y} & (P_{6}^{0})_{y} \\ x_{z} & y_{z} & z_{z} & (P_{6}^{0})_{z} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$(1)$$

Remember that the columns of the upper-left 3x3 matrix represent the direction of the axes of frame 6 with respect to frame 0 (i.e. that $x = [x_x, x_y, x_z]^T$ is the direction of the x_6 axis in the 0^{th} frame, etc.).[?]

Inverse Kinematics

The first step to solving the inverse kinematics is to find θ_1 . To do so, we must first find the location of the 5^{th} coordinate frame with respect to the base frame, P_5^0 . As illustrated in Figure 2 below, we can do so by translating by d_6 in the negative z direction from the 6^{th} frame.

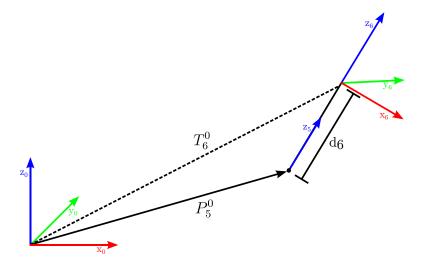


Figure 2: Finding the Origin of the 5^{th} Frame

This is equivalent to the following operation:

$$P_5^0 = T_6^0 \begin{bmatrix} 0 \\ 0 \\ -d_6 \\ 1 \end{bmatrix}$$
 (2)

With the location of the 5^{th} frame, we can draw an overhead view of the robot:

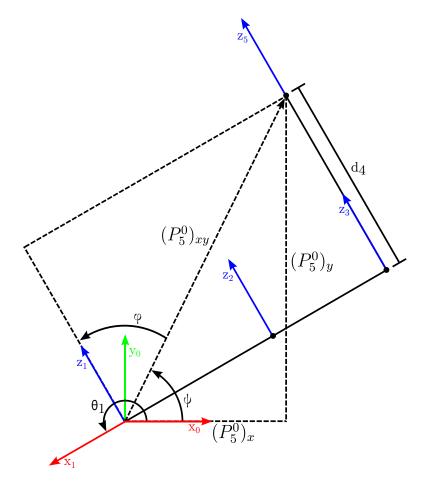


Figure 3: Finding θ_1

From Figure 3, we can see that $\theta_1 = \psi + \phi + \frac{\pi}{2}$ where

$$\psi = \operatorname{atan2}\left((P_5^0)_u, (P_5^0)_x \right) \tag{3}$$

$$\phi = \pm \arccos\left(\frac{d_4}{(P_5^0)_{xy}}\right) = \left(\frac{d_4}{\sqrt{(P_5^0)_x^2 + (P_5^0)_y^2}}\right) \tag{4}$$

The two solutions for θ_1 correspond to the shoulder being either "left" or "right,".

Knowing θ_1 , we can now solve for θ_5 . Once again we draw an overhead view of the robot, but this time we consider location of the 6^{th} frame with respect to the 1^{st} .

We can see that $(P_6^1)_z = d_6 \cos(\theta_5) + d_4$, where $(P_6^1)_z = (P_6^0)_x \sin(\theta_1) - (P_6^0)_y \cos(\theta_1)$. Solving for θ_5 ,

$$\theta_5 = \pm \arccos\left(\frac{(P_6^1)_z - d_4}{d_6}\right) \tag{5}$$

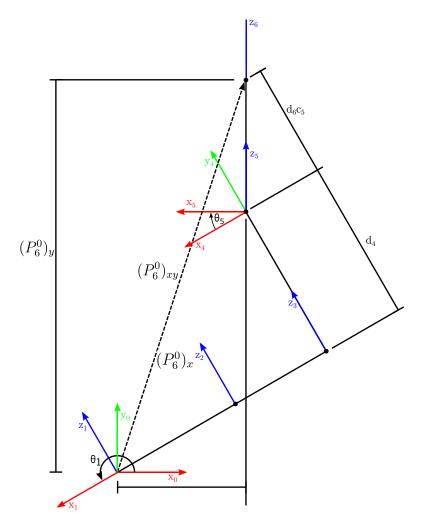


Figure 4: Finding θ_5

Once again, there are two solutions. These solutions correspond to the wrist being "down" and "up." Equation 5 also indicates that θ_5 is only well-defined when $\frac{(P_6^1)_z - d_4}{d_6} \leq 1$.

Figure 5 illustrates that, ignoring translations between frames, z_1 can be represented with respect to frame 6 as a unit vector defined with spherical coordinates. We can find the x and y components of of this vector by projecting it onto the x-y plane and then onto the x or y axes.

Next we find transformation from frame 6 to frame 1,

$$T_1^6 = ((T_1^0)^{-1} T_6^0)^{-1} (6)$$

Remembering the relation between the of the first three columns of the homogenous transformation T_1^6 to the frames themselves, we can form the collowing equalities:

$$-\sin(\theta_6)\sin(\theta_5) = z_y \tag{7}$$

$$\cos(\theta_6)\sin(\theta_5) = z_x \tag{8}$$

Solving for θ_6 ,

$$\theta_6 = \operatorname{atan2}\left(\frac{-z_y}{\sin(\theta_5)}, \frac{z_x}{\sin(\theta_5)}\right) \tag{9}$$

Equation 9 shows that θ_6 is not well-defined when $\sin(\theta_5) = 0$ or when $z_x, z_y = 0$. We can see from Figure 5 that these conditions are actually the same. In this configuration joints 2, 3, 4, and 6 are parallel. As a result, there four degrees of freedom to determine the position and rotation of the end-effector in the plane, resulting in an infinite number of solutions. In this case, a desired value for q_6 can be chosen to reduce the number of degrees of freedom to three.

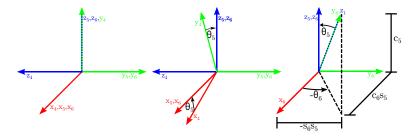


Figure 5: Finding θ_6

We can now consider the three remaining joints as forming a planar 2R manipulator. First we will find the location of frame 3 with respect to frame 1. This is done as follows:

$$T_4^1 = T_6^1 \ T_4^6 = T_6^1 \ (T_5^4 \ T_6^5)^{-1} \tag{10}$$

$$P_3^1 = T_4^1 \begin{bmatrix} 0 \\ -d_4 \\ 0 \\ 1 \end{bmatrix} \tag{11}$$

Now we can draw the plane containing frames 1-3, as shown in Figure 6. We can see that

$$\cos(\xi) = \frac{||P_3^1||^2 - a_2^2 - a_3^2}{2a_2 a_3}$$
(12)

with use of the law of cosines.

$$cos(\xi) = -\cos(\pi - \xi)
= -\cos(-\theta_3)
= \cos(\theta_3)$$
(13)

Combining 12 and 13

$$\theta_3 = \pm \arccos\left(\frac{||P_3^1||^2 - a_2^2 - a_3^2}{2a_2a_3}\right) \tag{14}$$

Figure 6 also shows that

$$\theta_2 = -(\delta - \epsilon) \tag{15}$$

where $\delta = \operatorname{atan2}((P_3^1)_y, -(P_3^1)_x)$ and ϵ can be found via law of sines:

$$\frac{\sin(\xi)}{||P_3^1||} = \frac{\sin(\epsilon)}{a_3} \tag{16}$$

Combining 15 and 16

$$\theta_2 = -\operatorname{atan2}((P_3^1)_y, -(P_3^1)_x) + \arcsin\left(\frac{a_3\sin(\theta_3)}{||P_3^1||}\right)$$
(17)

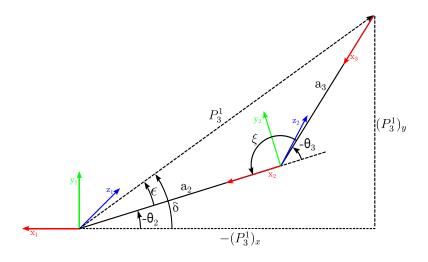


Figure 6: Finding θ_2 and θ_3

Notice that there are two solutions for θ_2 and θ_3 . These solutions are known as "elbow up" and "elbow down."

The final step to solving the inverse kinematics is to solve for θ_4 . First we want to find T_4^3 :

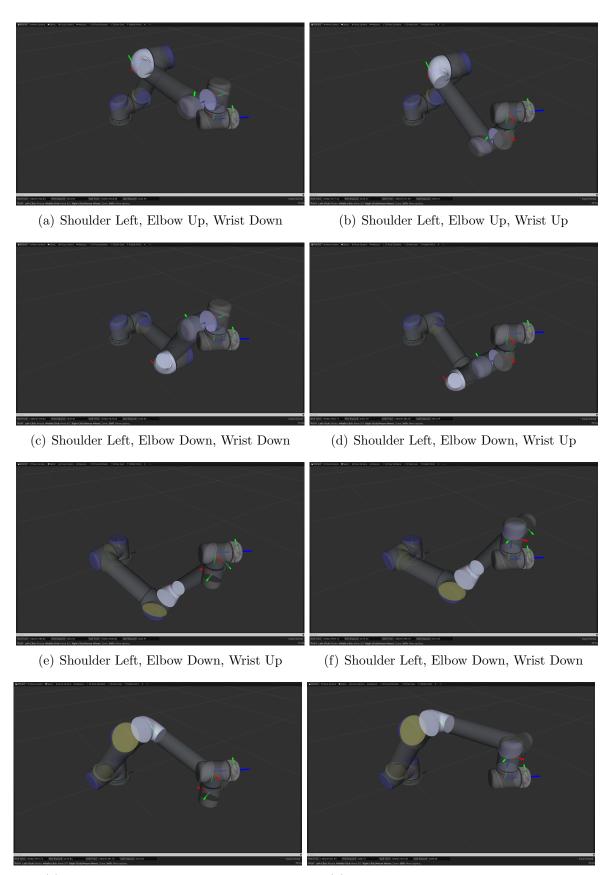
$$T_4^3 = T_1^3 T_4^1 = (T_2^1 T_3^2)^{-1} T_4^1$$
(18)

Using the first column of T_4^3 ,

$$\theta_4 = \operatorname{atan2}(x_y, x_x) \tag{19}$$

Below are figures which show the eight solutions for one end-effector position/orientation.

This solution was adapted from an existing solution written by Kelsey P. Hawkins



(g) Shoulder Left, Elbow Up, Wrist Up

(h) Shoulder Left, Elbow Up, Wrist Down