Homework 8.2: Vehicle Dynamics and Stability

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1998 Honda Civic

Most vehicle parameters are found from https://www.eng.auburn.edu/~dmbevly/mech4420/vehicle_params.pdf (see Vehicle No. 452)

Parameter	Value
Mass, m	$m = 1143 \mathrm{kg}$
Length of car, L	$L = 2.621 \mathrm{m}$
Distance to front wheels from CG, a	$a = 1.038 \mathrm{m}$
Yaw moment of inertia, I_{zz}	$I_{zz} = 1785 \mathrm{kg} \cdot \mathrm{m}^2$
Cornering stiffnesses, C_{of} & C_{or}	$C_{\alpha f} = C_{\alpha r} = 50990.278 \frac{N}{\text{rad}}$
Proportioning of front to rear lateral load transfer, \overline{p}	$\overline{p} = 0.5$
Height to center of mass, H	$H = 0.513 \mathrm{m}$
Width of car, T	$T = 1.695 \mathrm{m}$
Roll gain, $\overline{\phi}$	$\frac{1}{\phi} = -4 \frac{\deg}{g}$
Roll Frequency	$freq_R = 1.5 \mathrm{Hz}$
Pitch Frequency	$freq_P = 1 Hz$
Brake limit (from HW6)	<i>BLIMIT</i> = 1787.88N
Braking ratio (from HW6), Q	Q = 2.48
Pitch gain, $\overline{\theta}$	$\frac{1}{\theta} = -0.1 \frac{\text{rad}}{\text{g}}$

Strategy

The strategy of this task was to first and foremost decide on a start location and initial orientation angle.

I choose X(0) = -20m somewhat arbitrarily. The initial orientation angle is found using X(0) and the location of the first target (0m, 3m):

$$\psi(0) = invTan\left(\frac{-3m}{-20m}\right) = 8.531 \text{ deg}$$

Next up I made some assumptions:

- The car drives in a straight path from the starting point to the first target with an initial velocity, u_i .
- At the first target it initiates a step steer, δ_f , that will guide the car all the way to the final target.
- At some point, X_{brake} , between the first target and the final target the car will start braking at some deceleration, decel.

Next up I created a brute-force algorithm that finds the best solution amongst:

- 10 values between 15 and 25 m/s of initial velocity
- 10 values between 0.2 and 0.6 g's of deceleration
- 10 values of step steer values between -1.5 and 2 degrees.
- 10 values between 10 and 40 meters of the location of applying the brakes X_{brake}

Which results in 10000 sets of parameters (which resulted in rather large computation time)

This gave me a solution that took 4.51 seconds to reach the final target with the parameters:

$$u_i = 17.2222 \frac{\text{m}}{\text{s}}, decel = 0.4222g, \delta_f = 1.6667 \text{deg}, X_{brake} = 26.6667 \text{m}$$

I did another run to narrow down the values around the optimized solution:

- 10 values between 16 and 20 m/s of initial velocity
- 10 values between 0.4 and 0.45 g's of deceleration
- 10 values of step steer values between -1.5 and 2 degrees.
- 10 values between 24 and 28 meters of the location of applying the brakes X_{brake}

Which gave me a solution time of 4.39 seconds with the parameters I decided to settle on:

$$u_i = 17.7778 \frac{\text{m}}{\text{s}}$$
, $decel = 0.4444 \text{ g}$, $\delta_f = 1.7222 \text{ deg}$, $X_{brake} = 26.2222 \text{ m}$

Now the way the algorithm determines whether a set of parameters results in a viable solution is by checking the following list of conditions:

- 1. Is the final velocity below 10 m/s?
- 2. Are there no lockups at any point in time on any of the wheels?
- 3. Is the Y position of the front left wheel positive, the Y position of the rear right wheel negative, and the Y position of the center of gravity within the range $[-0.3 \,\mathrm{m}, 0.3 \,\mathrm{m}]$

I found that condition nr. 3 would ensure that the final destination is reached.

If all these conditions where satisfied and the solution time was quicker than the solution time of any of the other sets of parameters, the new set of parameters would be stored as the current fastest solution.

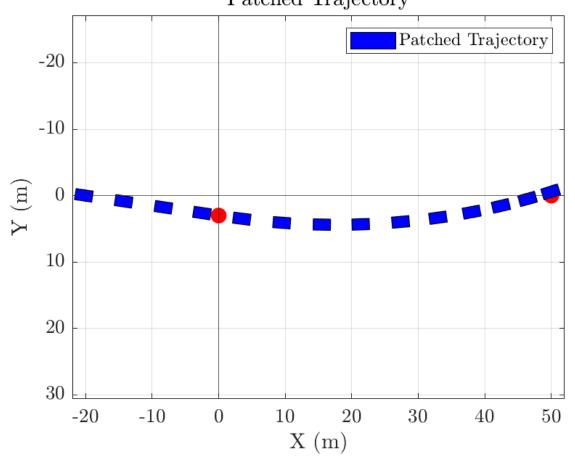
Additionally it is worth noting that the MATLAB function fric_coeff (see all codes in the bottom pages) was also necessary to know the X-position of each wheel in order of determining whether a wheel had crossed into X > 0 which would result in a change of friction coefficient.

Trajectory

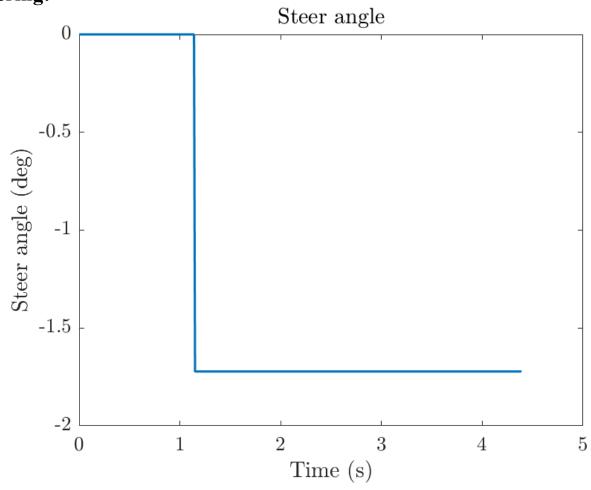
From start $(X_i, Y_i) = (-20 \,\mathrm{m}, 0 \,\mathrm{m})$ to finish $(X_f, Y_f) = (50 \,\mathrm{m}, 0 \,\mathrm{m})$ it takes 4.39 seconds with the optimized solution.

Note that the Y-axis flipped, so that positive values correspond with what looks like a right hand turn.

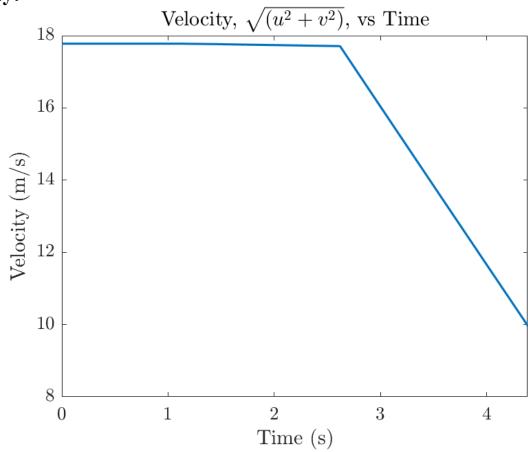
Patched Trajectory

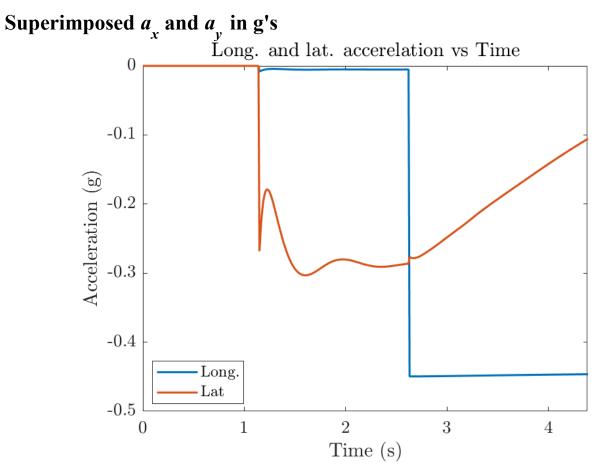


Steering:

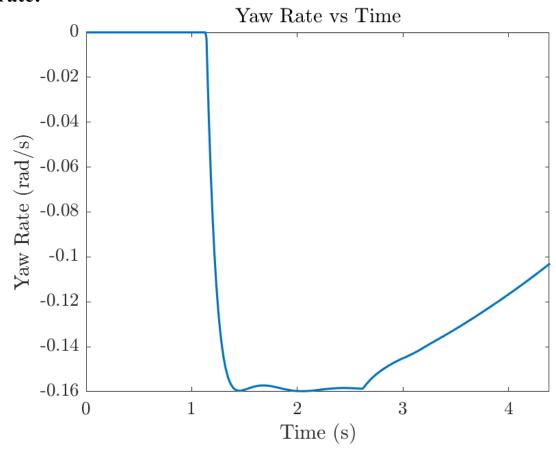


Velocity:

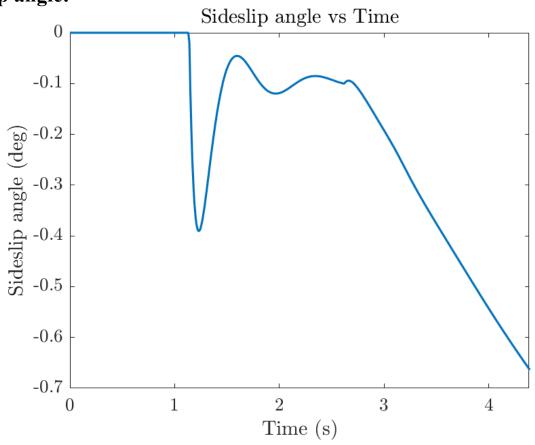


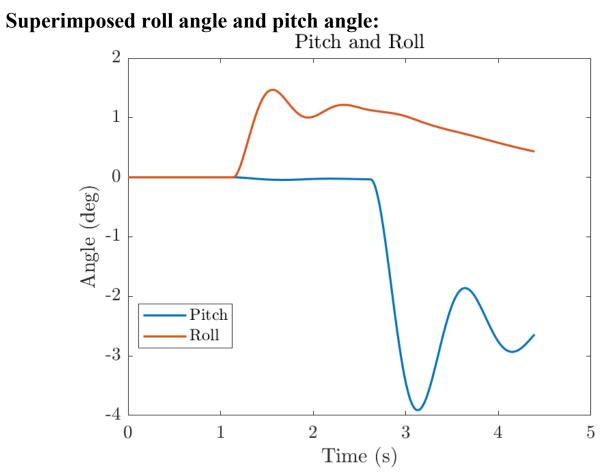


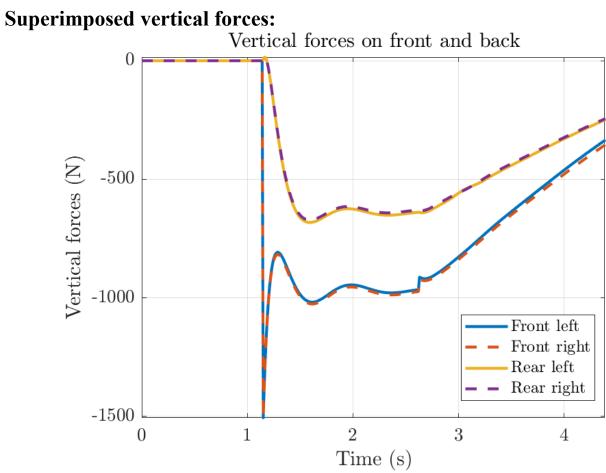
Yaw rate:



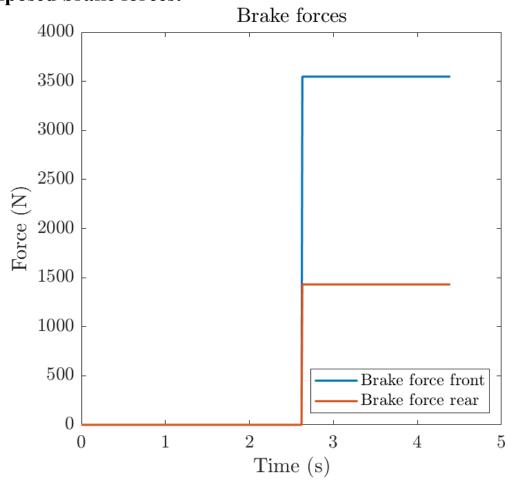
Sideslip angle:



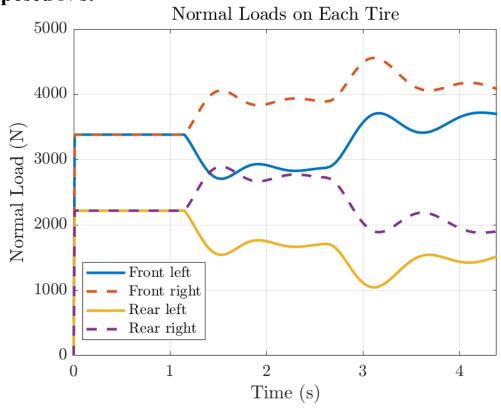




Superimposed brake forces:

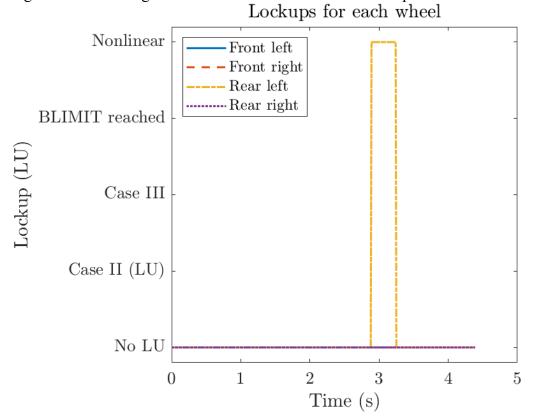


Superimposed N's:



Extra plot:

Plot describing the inner workings of the code. It illustrates that no lockups occur:



Derivative function, car_modelNL, and the functions it calls in order of occurence

```
function [Xdot, a_y, a_x, N_all, Fx_all, BF, delta_f, LU, Fy_all] = car_modelNL(XY
t, car) %n is the iteration number
         tspan = car.tspan; m = car.m; a = car.a; L = car.L; b = car.b; Izz = car.Izz + car.z + car.b; zz = car.z + car
C_f = car.C_f; C_r = car.C_r; g = car.g;
         delta_f = car.delta_f; p_bar = car.p_bar; H2 = car.H2; W = car.W; T = car.T\( \vec{v} \)
phi_bar = car.phi_bar; K = car.K; Ixx = car.Ixx; c_roll = car.c_roll;
         delta_r = car.delta_r;BLIMIT = car.BLIMIT; Q_brak = car.Q_brak; theta_ss = car\(\mathbf{v}\)
theta_ss; Iyy = car.Iyy; K_bar = car.K_bar; H2 = car.H2; c_pitch = car.c_pitch;
         K_dbar = car.K_dbar; X_brake = car.X_brake; decel = car.decel;
         r = X(1);
         v = X(2);
         glob_X = X(3);
         glob_Y = X(4);
         psi = X(5);
         phi = X(6);
         phi_dot = X(7);
                                                               % New variables for longitudinal speed, pitch and pitch
         u = X(8);
rate
         theta = X(9);
         theta_dot = X(10);
         Q = delta_r/phi_bar; % delta_r is 0, so this is 0
         if qlob X < 0
                  delta_f = 0;
                  Q = 0;
                  delta_f = delta_f;
                  Q = Q;
         end
         %Static loads
         N_f = (W * b) / L;
         N_r = (W * a) / L;
         %If we are not braking
         BF_f = 0; BF_r = 0; DeltaN_pitch = 0; %When not braking there is no brake
force, and no pitch.
         st Normal loads - the only difference in normal loads w/o breaking are left-tor
right because of roll
         DeltaN_roll = 2 / T * (-K * phi - c_roll * phi_dot);
         DeltaN_f_roll = p_bar * DeltaN_roll;
         DeltaN_r_roll = (1 - p_bar) * DeltaN_roll;
         %If we are braking:
         if glob_X > X_brake %Break when ~steady state, at t > t_brake
                  decel = 0.39;
                  [~, BF_f, BF_r, ~, ~, ~, ~, ~] = brake_no_trailer(car, decel); %Calculate
forces when braking
                  DeltaN_pitch = K_dbar*theta;
                  %BF_f = 10^6; %To lock up front wheels
```

```
%BF_r = 10^6; %To lock up rear wheels
    end
    BF = [BF_f, BF_r];
    % Brake forces
    SUM_BF = BF_f + BF_r; %[UNUSED]
    %Normal loads
   N_fl = N_f / 2 + DeltaN_f_roll / 2 + DeltaN_pitch / 2;
    N_fr = N_f / 2 - DeltaN_f_roll / 2 + DeltaN_pitch / 2;
   N_rl = N_r / 2 + DeltaN_r_roll / 2 - DeltaN_pitch / 2;
   N_r = N_r / 2 - DeltaN_r_r / 2 - DeltaN_pitch / 2;
   N_all = [N_fl, N_fr, N_rl, N_rr];
    % Slip angles and lateral forces
    alpha_fL = atan2(v + a * r, u + T*r/2) - delta_f;
    alpha_fR = atan2(v + a * r, u - T*r/2) - delta_f;
    alpha_rL = atan2(v - b * r, u + T*r/2) - Q*phi;
    alpha_rR = atan2(v - b * r, u - T*r/2) - Q*phi;
    [mu_fL, mu_fR, mu_rL, mu_rR, ~, ~] = fric_coeff(glob_X, psi, car, glob_Y);
    [Fx_FL_tire, Fy_FL_tire, LU(1)] = NLTire(C_f, alpha_fL, mu_fL, N_fl, BF_f/2)#
%Tiremodel is for 1 wheel, so divide BF with 2
    [Fx FR tire, Fy FR tire, LU(2)] = NLTire(C f, alpha fR, mu fR, N fr, BF f/2);
    [Fx_RL_tire, Fy_RL_tire, LU(3)] = NLTire(C_r, alpha_rL, mu_rL, N_rl, BF_r/2\(\mu\)
BLIMIT);
    [Fx_RR_tire, Fy_RR_tire, LU(4)] = NLTire(C_r, alpha_rR, mu_rR, N_rr, BF_r/2\forall
BLIMIT);
    Fx_FL = Fx_FL_tire*cos(delta_f) - Fy_FL_tire*sin(delta_f);
    Fy_FL = Fx_FL_tire*sin(delta_f) + Fy_FL_tire*cos(delta_f);
    Fx_FR = Fx_FR_tire*cos(delta_f) - Fy_FR_tire*sin(delta_f);
    Fy_FR = Fx_FR_tire*sin(delta_f) + Fy_FR_tire*cos(delta_f);
    Fx_RL = Fx_RL_tire;
    Fy_RL = Fy_RL_tire;
    Fx_RR = Fx_RR_tire;
    Fy_RR = Fy_RR_tire;
    Fx_all = [Fx_FL, Fx_FR, Fx_RL, Fx_RR];
    Fy_all = [Fy_FL, Fy_FR, Fy_RL, Fy_RR];
    % Calculate SUMs
    SUM_Ff_lat = Fy_FL + Fy_FR;
    SUM Fr lat = Fy RL + Fy RR;
    SUM_lat = SUM_Ff_lat + SUM_Fr_lat;
    SUM_Ff_long = Fx_FL + Fx_FR;
    SUM_Fr_long = Fx_RL + Fx_RR;
    SUM_long = SUM_Ff_long + SUM_Fr_long;
    % Calculate dummy variables
    phi_ddot = ((-(SUM_lat)*H2) - ((K - W * H2) * phi) - c_roll * phi_dot) / Ixx;
    theta_ddot = (((SUM_long)*H2) - (K_bar * theta) - c_pitch * theta_dot) / Iyy;
```

```
% Yaw acceleration and lateral acceleration
   / Izz;
   v_{dot} = (SUM_{lat} / m) - (u * r) - H2 * phi_ddot;
   u_dot = (SUM_long / m) + (v * r); % Should I add a phi_ddot term?
   glob_X_dot = u * cos(psi) - v * sin(psi);
   glob_Y_dot = u * sin(psi) + v * cos(psi);
   psi_dot = r;
   % Extracting acceleration
   a_y = SUM_lat / m;
   a_x = SUM_long / m;
   % State derivatives
   Xdot(1, 1) = r_dot;
   Xdot(2, 1) = v_dot;
   Xdot(3, 1) = glob_X_dot;
   Xdot(4, 1) = glob_Y_dot;
   Xdot(5, 1) = psi_dot;
   Xdot(6, 1) = phi_dot;
   Xdot(7, 1) = phi_ddot;
   % Derivatives for new variables
   Xdot(8, 1) = u dot;
   Xdot(9, 1) = theta_dot;
   Xdot(10, 1) = theta_ddot;
end
```

```
function [decel, BF_f, BF_r, N_f, N_r, mu_f, mu_r, eta] = brake_no_trailer(car\mathbf{\xeta})
decel)
m = car.m; a = car.a; L = car.L; b = car.b; g=car.g; H2 = car.H2; W = car.W; BLIMIY
= car.BLIMIT; Q_brak = car.Q_brak; K_dbar = car.K_dbar;
Nf_static = W*b/L;
Nr_static = W*a/L;
% Calculate rear brake force
BF_r = W * decel / (1 + Q_brak);
BF_f = Q_brak*BF_r;
if BF_r > BLIMIT
 BF_r = BLIMIT;
 if Q_brak ~= 0 %Check if we have rear-brakes only-case
   BF_f = W * decel - BF_r;
 end
end
% Calculate normal loads
N_f = Nf_static + W * (decel) * H2 / L;
N_r = Nr_static - W * (decel) * H2 / L;
% Calculate coefficients of friction
mu f = BF f / N f;
mu_r = BF_r / N_r;
% Determine effective coefficient of friction
mu = mu_f;
if mu_r > mu
   mu = mu_r;
end
% Calculate brake efficiency
eta = decel / mu;
end
```

```
function [mu_fL, mu_fR, mu_rL, mu_rR, F_wx, F_wy] = fric_coeff(X, psi, car, Y)
T = car.T; a = car.a; b=car.b;
% Distance between CP and a front wheel
r a=(a^2+(T/2)^2)^0.5;
% Distance between CP and a rear wheel
r_b=(b^2+(T/2)^2)^0.5;
% Angle between the x-axis of the car and the distance vector to the front
% wheel
v_a=atan(T/(2*a));
% Angle between the x-axis of the car and the distance vector to the rear
v b=atan(T/(2*b));
% Orientation equation
FR_wx=X+r_a*(cos(v_a)*cos(psi)-sin(v_a)*sin(psi));
RR_wx=X+r_b*(-cos(v_b)*cos(psi)-sin(v_b)*sin(psi));
RL_wx=X+r_b*(-cos(v_b)*cos(psi)+sin(v_b)*sin(psi));
FL_wx=X+r_a*(cos(v_a)*cos(psi)+sin(v_a)*sin(psi));
FR_wy=Y+r_a*(cos(v_a)*sin(psi)+sin(v_a)*cos(psi));
RR_wy=Y+r_b*(-cos(v_b)*sin(psi)+sin(v_b)*cos(psi));
RL_wy=Y+r_b*(-cos(v_b)*sin(psi)-sin(v_b)*cos(psi));
FL_wy=Y+r_a*(cos(v_a)*sin(psi)-sin(v_a)*cos(psi));
F_wx = [FR_wx, RR_wx, RL_wx, FL_wx];
F_wy = [FR_wy, RR_wy, RL_wy, FL_wy];
% Set friction coefficients based on wheel locations
   (FL_wx < 0) %If the front left positive then i
    mu_fL = 0.3;
else
    mu_fL = 0.9;
end
   (FR_wx < 0)
    mu_fR = 0.3;
else
   mu fR = 0.9;
end
   (RL_wx < 0)
    mu_rL = 0.3;
else
    mu_rL = 0.9;
end
if (RR_wx < 0)
    mu_rR = 0.3;
else
   mu_rR = 0.9;
end
end
```

```
function [Fx_tire, Fy_tire, LU] = NLTire(C_alpha, alpha, mu, N, BF, varargin)
if ~isempty(varargin)
    BLIMIT = varargin{1};
end
LU = 0;
Fx = -BF;
Fy = -C_alpha*alpha;
    if abs(Fy) > (mu*N)/2
       Fy = -mu*N*sign(alpha) * (1 - (mu*N)/(4*C_alpha*abs(tan(alpha))));
       LU = 2;
    end
% Check for lockup
F_check = -mu*N*cos(alpha);
    if abs(F_check) < BF</pre>
        Fy = -mu*N*sin(alpha);
        Fx = F_check;
        LU = 0.5;
    elseif (mu*N)^2 < (BF^2 + Fy^2)
        Fy = -sign(alpha)*sqrt((mu*N)^2 - (BF)^2);
        Fx = -BF;
        LU = 1;
    end
if ~isempty(varargin)
    if BLIMIT == 2*BF
        LU = 1.5;
    end
end
Fy_tire = Fy;
Fx_tire = Fx;
end
```

Extra: The brute force optimization algorithm

```
function [t_opt, u_i_opt, decel_opt, X_brake_opt, delta_f_opt] = BF_algorithm
(u_values, decel_values, X_brake_values, delta_f_values, car)
% Generate combinations of values
[comb_u, comb_decel, comb_X_brake, comb_delta_f] = ndgrid(u_values, decel_values
X_brake_values, delta_f_values);
% Reshape the combinations into columns
comb_u = comb_u(:);
comb_decel = comb_decel(:);
comb_X_brake = comb_X_brake(:);
comb_delta_f = comb_delta_f(:);
% Combine all combinations into a single matrix
combinations = [comb_u, comb_decel, comb_X_brake, comb_delta_f];
t_{opt} = 10^9;
for i = 1:length(comb_u)
    ui = comb_u(i);
    decel = comb_decel(i);
    X_brake = comb_X_brake(i);
    delta_f = comb_delta_f(i);
    % Initial conditions
    r0 = 0; v0 = 0; glob_X0 = X_initial; glob_Y0 = 0; psi0 = psi_initial; phi0 = 0\(\varphi\)
phi_dot0 = 0; u0 = ui; theta0 = 0; theta_dot0 = 0; %Velocity at beginning is given
    % Initial conditions with additional state variables
    X0 = [r0; v0; glob_X0; glob_Y0; psi0; phi0; phi_dot0; u0; theta0; theta_dot0];
    [X, a_y, a_x, N_all, Fx_all, BF, ~, LU] = odeRK4(@car_modelNL, X0, tspan, car);
    psi = X(end,5); glob_X = X(end,3); glob_Y = X(end, 4);
    [~,~,~, F_wx, F_wy] = fric_coeff(glob_X, psi, car, glob_Y);
    u_end = X(end, 8);
        if u_end < 10 && all(LU(:) == 0) && -F_wy(end,2) < 0 && -F_wy(end,4) > 0 &&
-0.3 < glob_Y < 0.3
            t = tspan(length(X));
            store_vals = [t, ui, decel, X_brake, delta_f];
            if t < t_opt</pre>
               t_{opt} = t;
               u_i_opt = ui;
               decel_opt = decel;
               X_brake_opt = X_brake;
               delta_f_opt = delta_f;
            end
        end
        if mod(i, 1000) == 0
            fprintf('Iteration number i: %d\n', i);
        end
end
end
```

Extra function - my own Runge Kutta 4th order ode solver

```
function [Y, a_y, a_x, N_all, Fx_all, BF, delta_f, LU, Fy_all] = odeRK4(dYdt, Y0*)
t, car)
% get size of problem
ne = length(Y0); % no. equations
nt = length(t); % timesteps
h = t(2)-t(1); % step size
% initialize output
Y = zeros(nt,ne); %(tom matrix)
Y(1,:) = Y0(:)'; % store results row-wise
% marching forward through time
   for n = 1:nt-1
                       %Take the first row of Y and turn it into a column vector
        Yn = Y(n,:)';
        [-, a_y(n+1,:), a_x(n+1,:), N_all(n+1,:), Fx_all(n+1,:), BF(n+1,:), delta_{\ell}
(n+1,:), LU(n+1,:), Fy_all(n+1,:)] = dYdt(Yn, t(n), car); %Extraction lateral \checkmark
accelerations
        k1 = dYdt(Yn,
                                t(n), car);
        k2 = dYdt(Yn+(h/2)*k1, t(n)+(h/2), car);
        k3 = dYdt(Yn+(h/2)*k2, t(n)+(h/2), car);
        k4 = dYdt(Yn+h*k3,
                             t(n)+h, car);
        Y(n+1,:) = Yn + h/6*k1 + h/3*(k2+k3) + h/6*k4;
        if Y(n,3) >= 50 % If x-position is above 50 meters stop
            Y(n+2:end,:) = [];
            return
        end
    end
end
```