PhD Log

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1	Tasks					
1.	1 TODO Ti3Al report—DFT chapter					
	• Start with the theory of DFT with the HK theorem and KS equation to solve for the density.	ons				
	• Talk a bit about the approximations that are made.					
	• Alloy theory and the structure of Ti3Al					
	• Look at literature to do with all of this. Go through why solutes are incredibly important and why it is necessary do to this research.					
	• How can solutes lead to failure and why is oxygen in particular bad the alloy.	for				
	• Is it wavy or planar slip					
	• Go into the calculations and what I have done for them					
	• Cite the research about the Fe and C vacancy concentration and w the implications are for alloy research	hat				
	• What can I add to the research.					

1.2 TODO Ti/Ti3Al DFT oxygen interstitial/vacancy binding energy

Want to find the vacancy formation energy, and the dissolution energy of oxygen interstitials at different sites in the Ti3Al lattice.

From these measurements we can then do a final calculation on the binding energy of oxygen to a vacancy thus elucidating if it is favourable comapared to just the normal positions.

This will provide insight into the high amount of vacancies with oxygen.

1.2.1 Notes on the calculations

- 1. Setting up relaxation
 - To set up one calculates the self consistent density first by not initiating

relaxation.

 \bullet Using the OPTIONS_{HF} flag one can minimise the energy with respect to the

Harris-Foulkes energy, which is far faster. And it would use the initial electron density for the relaxation, and then only calculate the density using the overlap of atomic densities.

One is then able to minimise the energy accordingly.

2. Basis set optimisators

(a) Notes on the basis set It has been seen that the a smaller sphere radius for the oxygen was giving a much larger overlap (~17%) in the T2 interstitial site than any of the octahedral sites, which have an overlap of ~1.6%.

This would have decreased the accuracy of the results.

So to decrease the radius of the oxygen and to increase the completeness of the basis set one can introduce plane waves between certain energies such that the plane wave basis set is more complete.

This should make the Harris-Foulkes energy smaller by the variational principle.

<2019-05-23 Thu 18:19>

It seems that there is an optimal sphere radius of around 0.8. The best plane wave energy max seems to be at the maximum of around 3 Rydberg, but this is at the edge of the range of search so it seems that the range needs to be extended such that an optimum can be found before the basis set becomes overcomplete. <2019-05-24 Fri 16:05>

There seems to be an optimum. I shall stop putting the plane wave basis set up in energy and now making pwemax = 4.0 ryd. The best sphere radius for the oxygen is 0.78.

<2019-05-24 Fri 18:01>

Asking Dimitar about the plane wave basis set, he said to use the defaulf values that are generated when making a blm file.

- (b) Perfect lattice spec name old rmax new rmax ratio 1 Ti 2.707297 $3.024213\ 1.117060\ 2$ Al $2.638772\ 2.947667\ 1.117060$ Ti RSMH= $1.805\ 1.805\ 1.805\ 1.805\ 1.805\ EH=-0.1\ -0.1\ -0.1\ -0.1\ RSMH2= <math>1.805\ 1.805\ 1.269\ EH2=-0.9\ -0.9\ -0.9\ P=\ 4.699\ 4.466\ 3.875\ 4.155$ $5.089\ Al\ RSMH=\ 1.759\ 1.759\ 1.759\ EH2=\ -0.9\ -0.9\ P=\ 3.837\ 3.75\ 3.392\ 4.13\ 5.089$ gmax = 6.6 Ti RSMH= $1.805\ 1.805\ 1.269\ 1.805\ EH=-0.1\ -0.1\ -0.1\ -0.1\ RSMH2= <math>1.805\ 1.805\ 1.269\ EH2=\ -0.9\ -0.9\ -0.9\ P=\ 4.699\ 4.466\ 3.875\ 4.155$ $5.089\ Al\ RSMH=\ 1.759\ 1.759\ 1.759\ EH=-0.1\ -0.1\ -0.1\ RSMH2= <math>1.759\ 1.759\ EH2=\ -0.9\ -0.9\ P=\ 3.837\ 3.75\ 3.392\ 4.13\ 5.089$
- (c) O2 site (least overlap) spec name old rmax new rmax ratio 1 Ti $2.663548 \ 2.746597 \ 1.031179 \ 2$ Al $2.576718 \ 2.746597 \ 1.065928 \ 3$ O $1.662251 \ 1.714079 \ 1.031179$ Ti RSMH= $1.776 \ 1.776 \ 1.254 \ 1.776 \ 1.254 \ 1.776 \ 1.254 \ EH= -0.1 -0.1 -0.1 -0.1 \ RSMH2= 1.776 \ 1.254 \ EH2= -0.9 -0.9 \ P= 4.686 \ 4.447 \ 3.874 \ 4.155 \ 5.089 \ PZ= 0 \ 13.9381 \ Al \ RSMH= 1.718 \ 1.718 \ 1.718 \ 1.718 \ EH= -0.1 -0.1 \ -0.1 \ RSMH2= 1.718 \ 1.718 \ EH2= -0.9 -0.9 \ P= 3.83 \ 3.74 \ 3.389 \ 4.13 \ 5.089 \ O \ RSMH= 0.845 \ 0.82 \ 1.108 \ 1.108 \ EH=-0.505 \ -0.1 \ -0.1 \ -0.1 \ RSMH2= 0.845 \ 0.82 \ EH2= -1.305 \ -0.9 \ P= 2.886 \ 2.858 \ 3.25 \ 4.11$
- (d) O1 site (next least overlap) spec name old rmax new rmax ratio 1 Ti 2.641151 2.734882 1.035489 2 Al 2.638731 3.547117 1.344251 3 O 1.666646 1.725793 1.035489 gmax = 9.8 Ti RSMH= 1.761 1.761 1.246 1.761 EH= -0.1 -0.1 -0.1 -0.1 RSMH2= 1.761 1.761 1.246 EH2= -0.9 -0.9 -0.9 P= 4.679 4.437 3.873 4.155 5.089 PZ= 0 13.9376 Al RSMH= 1.759 1.759

 $1.759 \ EH= -0.1 \ -0.1 \ -0.1 \ RSMH2 = 1.759 \ 1.759 \ EH2 = -0.9 \ -0.9 \ P=3.837 \ 3.75 \ 3.392 \ 4.13 \ 5.089 \ O \ RSMH= 0.846 \ 0.821 \ 1.111 \ 1.111 \ EH= -0.506 \ -0.1 \ -0.1 \ -0.1 \ RSMH2 = 0.846 \ 0.821 \ EH2 = -1.306 \ -0.9 \ P= 2.886 \ 2.859 \ 3.25 \ 4.11$

(e) T1 site (next most overlap)

spec name old rmax new rmax ratio 1 Ti 2.654621 2.490980 0.938356 2 Al 2.586159 2.447921 0.946547 3 O 1.473639 1.382798 0.938356 gmax = 8.9

Ti RSMH= 1.77 1.77 1.251 1.77 EH= -0.1 -0.1 -0.1 -0.1 RSMH2= 1.77 1.77 1.251 EH2= -0.9 -0.9 -0.9 P= 4.683 4.443 3.874 4.155 5.089 PZ= 0 13.9379 Al RSMH=1.724 1.724 1.724 EH= -0.1 -0.1 -0.1 RSMH2= 1.724 1.724 EH2= -0.9 -0.9 P= 3.831 3.742 3.389 4.13 5.089 O RSMH= 0.831 0.982 0.982 EH= -0.474 -0.1 -0.1 -0.1 RSMH2= 0.831 0.982 EH2= -1.274 -0.9 P= 2.871 2.845 3.25 4.11

(f) T2 site (Most overlap)

1.2.2 Vacancy formation energy definition

\$\$
$$\Delta E_f^{vacancy} = \lim_{N\{a\} \to \infty} E(N\{a\}, 1)$$

• $E(N\{a\} - 1, 0) \setminus \$\$$

Where the first argument of the energy function is the number of lattice sites and the second denotes the number of vacancies. [1]

1.2.3 Dissoluton energy of species definition

The solution enthalpy of particular species is given by

$$E_{textsolution} = E(Ti_N X_1) - E(Ti_N) - E(X)$$

This is the same as a formation energy $\Delta E_{\Omega}^{\rm f}$

1.2.4 Vacancy-solute binding energy

[2] \$\$ - $E_{bind}(X - Vac) = E(Ti_{N-2} X_1 Vac_1)$

• E(Ti_N)

• E(Ti_{N-1} X₁)

where Vac is a vacancy, X is a solute impurity. The binding energy is negative here to keep with the convention that a *positive* binding energy is *favourable*.

I think that there really is a minus sign here

\$\$
$$E_{bind}^{V-X} = + E(Ti_{N-1} X_1)$$

- E(Ti_{N-1} Vac₁)
- E(Ti_{N-2} X₁ Vac₁)
- E(Ti_N) \$\$

1.2.5 Dilute impurity energy and Vacancy formation energy

[2] \$\$
$$E_{text\{impurity\}}(X) = E(Ti_{N-1}X_1)$$

- • N-1 $\overline{_{NE(\mathrm{Ti_N})E(X)\$\$}}$ \$\$ $\mathrm{E_{text\{vacancy\}}}(\mathrm{Vac}) = \mathrm{E}(\ \mathrm{Ti_{N-1}Vac_1}\)$
- N-1 $_{\overline{NE}(\mathrm{Ti}_{\mathrm{N}})$ \$\$

1.2.6 Basis set

1.2.7 Relevant papers

[4]

- [5]
- [6]
- [7]
- [8]

Koizumi states that there is a preference for the interstitial site that is O1 (6 Ti atom coordination). O2 sites (4 Ti & 2 Al atom coordination), is of higher energy.

Site	Neighbouring atoms			
O1	6 Ti			
O2	4 Ti, 2 Al			
T1	3 Ti, 1 Al (on Ti)			
T2	3 Ti, 1 Al (on Al)			

on Ti: the tetrahedral site is located just above a Ti atom in the c-axis direction. on Al: the tetrahedral site is located just above an Al atom in the c-axis direction.

E_{vacancy formation}

Author	Geometry	$ m V_{Ti}$	$ m V_{Al}$
Baulkin (2018)	$2 \times 2 \times 2$	2.209	2.894
Mishin (2000)	Embedded atom?	1.314	1.805

E_{absorption} = - E_{solution} The lower the solution the higher the binding energy the higher the absorption energy, the higher the binding energy.

Author	Geometry	O1	O2	T1	T2
Wei (2011)	Ti3Al/TiAl interface (6 & 6 layers)	6.23	4.75	4.20	3.83
Baulkin (2017)	$2 \times 2 \times 2$	6.16	4.69	4.24	3.78

During relaxation it was found that the tetrahedral sites are unstable and that they actually prefer the hexahedral sites (Baulkin).

The chemical potential/diatomic reference energy for the oxygen molecule decreases with increasing temperature.

Т	(K)	0	500	1000	2000	2500	3000	4000	4500	5000
Ο	(eV)	4.35	4.89	5.5	6.83	7.54	8.27	9.78	10.55	11.34

[9]

Looked at point defects and soluted in an A_mB_n lattice.

It is difficult to determine the concentrations of both vacancies and antisite (substitutional of the other alloying element) defects reliably due to:

• Slow rates of diffusion -> Long equilibriation times.

Point-defect concentrations intimiately linked to chemical potentials of the constituents, and these chemical potentials can be used to discuss relative stability of different grain-boundary structures by comparing excess free energies.

We can say that there exists two sublattices, an A sublattice of m sites and a B sublattice of n sites, with all atoms of a particular type only belonging to that sublattice.

The alloy deviates slightly from stochiometry so we have A_xB_{1-x} where we suppose x to be within a few percent of m/(m+n). Each site of each sublattice can by occupied by its own atom or an atom of the other kind or a vacancy.

 c_{aa} = concentration of A atoms on the A sublattice; c_{bb} = concentration of B atoms on the B sublattice; c_{ab} = concentration of A atoms on the B sublattice; c_{ba} = concentration of B atoms on the A sublattice; c_{va} = concentration of vacancies on the A sublattice; c_{vb} = concentration of vacancies on the B sublattice.

Number of A and B sublattice cites are Nm and Nn. N is the number of fomulae units, which can vary due to the creation/annihilation of vacancies when the temperature or stochiometry varies, while the ratio m/n is constant.

A canonical ensemble is assumed so that the total numbers of A and B atoms are conserved.

There are 7 unknowns in a statistical model of the concentrations, c_i and N and they satisfy the constraints

$$c_{aa} + c_{ba} + c_{va} = 1$$
$$c_{bb} + c_{ab} + c_{vb} = 1$$

There are fixed numbers n_a and n_b of A and B atoms are given by

$$N(mc_{aa} + nc_{ab}) = n_a$$
$$N(mc_{ba} + nc_{bb}) = n_b$$

There are seven unknowns and four equations so there are three independent variables. The conservation of atoms constrains the possible defects which can be generated thermally. The effect of possible defect clustering or ordering is not included.

For a material of a single element, the calculation of, for example, the vacancy formation energy is simple: calculate the total energy of a perfect lattice and subtract it from the energy of a lattice with a defect. This is unique if N is sufficiently large and the same number of atoms is compared with and without the defect.

For an ordered alloy the stochiometry comes into account, so it is not as simple. The physical consequences, of having a working definition, are that we take the equilibrium concentrations of the four point defects and that they must be independent of the definition adopted for the point-defect energies, as long as the formulation is consistent.

If all we want at the end of the calcuation are the equilibrium point-defect concentrations, we do not need single point-defect energies, but rather the energies of three independent stociometry-conserving complex defects. For example it is possible to compare the energy of a block AB containing a pair of vacancies or a triple defect with the energy of the same numbers of A and B atoms in a perfect crystal. However the above uniquely defined complex defect energies can be constructed simple from calculations of individual point-deect energies.

 $e_{\rm mol}$: Cohesive energy / energy per unit mole. We can arbitrarily divide this between atoms of A and B type. This is a natural division in EAM potentials or BOP potentials which allocate energies to each atom.

$$e_{\text{mol}} = me_{aa} + ne_{bb}$$

The energy of a block containing Nm sites of sublattice A and Nn sites of sublattice B is now:

$$[E = Nm (c_{aa} e_{aa} + c_{ba} e_{ba} + c_{va} e_{va})]$$

• Nn (
$$c_{bb}$$
 e_{bb} + c_{ab} e_{ab} + c_{vb} e_{vb}) \]

The assumption has been made that the point defects are assumed to be sufficiently dilute that interactions may be neglected.

We can caw calculate the formation energy e_{vb} of a B vacancy. Construct block of N formula units with Nm sites of A, fully occupies by type A atoms, and Nn-1 sites of type B with a vacancy on the remaining site.

$$e_{vb} = E(N, vb) - Nme_{aa} - (Nn - 1)e_{bb}$$

The energy of an A antisite is:

$$e_{ab} = E(N, ab) - Nme_{aa} - (Nn - 1)e_{bb}$$

One can define stochiometry-conserving complexes (in the case of NiAl)

$$e_{2v} = e_{va} + e_{vb}$$

$$e_{ta} = 2e_{vb} + e_{ba} - e_{bb}$$

$$e_{tb} = 2e_{va} + e_{ab} - e_{aa}$$

This formalism can be generalised to finite temperature if for energy we read free energy and the include both the vibrational entropy and the effect of temperature on the formation energies. (We are not including configurational entropy at this stage). Essentially one can do phonon calculations and then obtain the entropy from standard formulae. The effect is to add $-Ts_i$ to each of the e_i .

To find the enthalpy of the defected crystal, neglecting elastic strains, the total volume can be written as

• Nn (
$$c_{bb} \Omega_{bb} + c_{ab} \Omega_{ab} + c_{vb} \Omega_{vb}$$
) \]

where Ω_i are the partial molar volume and the quantity $m\Omega_{aa} + n\Omega_{bb}$ is uniquely defined as the volume per formula unit, but like the energies this is arbitrarily defined between A and B.

Relaxation volumes are uniquely defined, like that of a B vacancy:

$$\Omega_{bb} - \Omega_{vb} = N(m\Omega_{aa} + n\Omega_{bb}) - V(N, vb)$$

where V(N, vb) is the volume of a crystal with N formula units with a single vacancy of the B sublattice.

Adding the pV term to construct he enthalpy amounts to replacing e_i by $e_i + p\Omega_i$ everywhere. The total Gibbs free energy without the configurational part is therefore given by replacing each of the e_i in the equations for e_{vb} and e_{ab} with $e_i + p\Omega_i - Ts_i$. These pressure and entropy terms are not included in the following for simplicity but they can be included.

The configurational entropy of the model system is $\ | S = Nmk \ (c_{aa} \log c_{aa} + c_{ba} \log c_{ba} + c_{va} \log c_{va})$

• Nnk ($c_{bb} \log c_{bb} + c_{ab} \log c_{ab} + c_{vb} \log c_{vb}$) \]

1.3 TODO Write up fitting and optimisation

- Used Genetic Algorithm and CMAES.
- Add in quantities to fit to.
- Realised that the prismatic fault was not high enough.

This caused incredibly large dissociation along the prismatic plane for a screw dislocation.

This was unreasonable, and it has been assumed that this can be rectified by a short ranged, very quickly decaying power law added to the pair potential.

Although this means that we need a refitting of the pair potential.

Unfortunately it seems that the accordance with the DFT results of the correct energetic ordering of the phases is lost: omega phase is **not** lower in energy than that of the hcp phase.

Reasonable starting point is:

 $\begin{array}{l} ndt = 2.00000000000 \ cr1 = -6.00000000000 \ cr2 = 3.2217589360 \ r1dd = 6.50000000000 \ rcdd = 10.00000000000 \ cr3 = -1.1418272350 \ rmaxhm = 10.10000000000 \ npar = 18 \\ VARGS - vb2 = 60204900.7590034157 - vm2 = -13.7544131202 - vp2 = 0.00000000000 \ -vfdd = 0.2648249504 - vqdds = 0.5697753882 - vqddp = 0.5648597117 - vqddd = 0.8213593849 \ -vb0 = 49.7557565400 - vp0 = 1.\ 1050685730 - vb1 = -5.0973416100 - vp1 = 0.6991977165 \ -vndt = 2.00000000000 - vcr1 = -6.00000000000 - vcr2 = 3.2217589360 - vr1dd = 6.50000000000 \ -vrcdd = 10.0000000000 - vcr3 = -1.1418272350 - vrma \ xhm = 10.10000000000 \ Quantity \ predicted \ target \ norm_{pred} \ norm_{tar} \ sq \ diff. \ weight \ objective \ * 100^2 \end{array}$

 $a_{hcp}: 5.69823736\ 5.57678969\ 5.69823736\ 5.57678969\ 0.01474954\ 1000.00000000$ $147495.36 \text{ c/a}: 1.57540221\ 1.58731122\ 15.29618259\ 15.41181168\ 0.01337009$ $100.0000000013370.09 \; a_{\rm omega}: \; 9.11713244 \; 8.73254342 \; 1.13964156 \; 1.09156793$ $0.00231107 \ 10.000000000 \ 231.11 \ c_{omega} : 5.50357270 \ 5.32343103 \ 0.68794659$ $0.66542888\ 0.00050705\ 10.000000000\ 50.70\ a_{4h}:\ 5.68949374\ 5.56325146\ 1.02269218$ $1.000000000\,0.00051493\,1.00000000\,5.15\,c_{4h}:\,18.46292975\,17.75908031\,1.03963321$ $1.00000000 \ 0.00157079 \ 1.00000000 \ 15.71 \ a_{6h} : 5.68593900 \ 5.54639384 \ 1.02515962$ $1.000000000\,0.00063301\,1.00000000\,6.33\,c_{6h}:\,27.74967218\,26.77136353\,1.03654310$ $1.00000000 \ 0.00133540 \ 1.00000000 \ 13.35 \ a_{bcc} : 6.20079768 \ 6.17948863 \ 0.88582824$ $0.88278409\ 0.00000927\ 1.00000000\ 0.09\ a_{fcc}:\ 8.03310655\ 7.88677000\ 1.14758665$ 1.12668143 0.00043703 1.00000000 4.37 DE(o,h): 1.19189500 -0.63343333 $0.07945967 - 0.04222889 \ 0.01480810 \ 3000.00000000 \ 444243.14 \ DE(4h,h): \ 1.83337000$ 3.17160000 0.00733348 0.01268640 0.00002865 2000.00000000 573.08 DE(6h,h): $2.75695000\ 3.72005000\ 0.01102780\ 0.01488020\ 0.00001484\ 2000.00000000\ 296.82$ $3.14 \text{ DE}(f,h): 4.17199500 \ 4.51880000 \ 0.04214136 \ 0.04564444 \ 0.00001227$ $2000.00000000\ 245.43\ c_{11}:\ 211.10292175\ 176.10000000\ 0.92212869\ 0.76923077$ $0.02337778\ 100.00000000\ 23377.78\ c_{33}:\ 232.93926611\ 190.50000000\ 0.94059869$ $0.76923077\ 0.02936697\ 100.00000000\ 29366.97\ c_{44}:\ 55.49057353\ 50.80000000$ $0.84025702\ 0.76923077\ 0.00504473\ 100.000000000\ 5044.73\ c_{12}:\ 110.56430372$ $86.90000000 \ 0.97870500 \ 0.76923077 \ 0.04387945 \ 100.00000000 \ 43879.45 \ c_{13}$ $: 73.53441848 \ 68.30000000 \ 0.82818356 \ 0.76923077 \ 0.00347543 \ 10.00000000$ $347.54 \text{ M}_{\text{freq0}}$: 2.86541811 2.85858719 0.20883117 0.20833333 0.00000025 $0.10000000\ 0.00\ M_{freq} \\ 1\colon 2.86541812\ 2.85858719\ 0.20883117\ 0.20833333\ 0.00000025$ $0.10000000\,0.00\,\mathrm{M_{freq}}$: $2.86541812\,2.85858719\,0.20883117\,0.20833333\,0.00000025$ $0.10000000\,0.00\,\mathrm{M_{freg}3}\colon 2.86541813\,2.85858719\,0.20883117\,0.20833333\,0.00000025$ $0.10000000\,0.00\,\mathrm{M_{freq}}4\colon\,6.16074486\,5.66706047\,0.22648223\,0.20833333\,0.00032938$ $0.10000000\,0.33\,\mathrm{M_{freg}5}\colon 6.16074486\,5.66706047\,0.22648223\,0.20833333\,0.00032938$ $0.10000000\ 0.33\ H_{freq0}\colon\ 4.29880135\ 4.80643423\ 0.18633015\ 0.20833333\ 0.00048414$ $0.1000000000.48~H_{freq1}$: 4.29880135~5.58010025~0.16049597~0.20833333~0.00228841

Quantity predicted target $norm_{pred}$ $norm_{tar}$ sq diff. weight objective * 100^2

 $\begin{array}{l} a_{\rm hcp}: 5.68326063\ 5.57678969\ 5.68326063\ 5.57678969\ 0.01133606\ 1000.000000000\\ 113360.60\ c/a: 1.58164523\ 1.58731122\ 15.35679851\ 15.41181168\ 0.00302645\\ 100.00000000\ 3026.45\ a_{\rm omega}: 9.09093887\ 8.73254342\ 1.13636736\ 1.09156793\\ 0.00200699\ 10.00000000\ 200.70\ c_{\rm omega}: 5.49075443\ 5.32343103\ 0.68634430\\ 0.66542888\ 0.00043745\ 10.00000000\ 43.75\ a_{\rm 4h}: 5.67495771\ 5.56325146\ 1.02007931\\ 1.00000000\ 0.00040318\ 1.00000000\ 4.03\ c_{\rm 4h}: 18.41194892\ 17.75908031\ 1.03676252\\ 1.000000000\ 0.00135148\ 1.000000000\ 13.51\ a_{\rm 6h}: 5.67118026\ 5.54639384\ 1.02249866\\ 1.000000000\ 0.00050619\ 1.00000000\ 5.06\ c_{\rm 6h}: 27.67479817\ 26.77136353\ 1.03374631\\ 1.000000000\ 0.00113881\ 1.000000000\ 11.39\ a_{\rm bcc}: 6.20079768\ 6.17948863\ 0.88582824\\ 0.88278409\ 0.00000927\ 1.000000000\ 0.09\ a_{\rm fcc}: 8.01192626\ 7.88677000\ 1.14456089\\ 1.12668143\ 0.00031968\ 1.000000000\ 3.20\ DE(o,h): 1.09675833\ -0.63343333\\ 0.07311722\ -0.04222889\ 0.01330473\ 3000.00000000\ 399141.76\ DE(4h,h): 1.84836500\\ 3.17160000\ 0.00739346\ 0.01268640\ 0.00002802\ 2000.00000000\ 560.30\ DE(6h,h): \end{array}$

```
2.778666667\ 3.72005000\ 0.01111467\ 0.01488020\ 0.00001418\ 2000.00000000\ 283.58
DE(b,h): 8.85897500\ 7.63520000\ 0.08948460\ 0.07712323\ 0.00015280\ 1.00000000
1.53 DE(f,h) : 4.20064500 4.51880000 0.04243076 0.04564444 0.00001033
2000.00000000 \ 206.56 \ c_{11} : 209.98522208 \ 176.10000000 \ 0.91724642 \ 0.76923077
0.02190863\ 100.00000000\ 21908.63\ c_{33}:\ 232.98310764\ 190.50000000\ 0.94077572
0.76923077 \ 0.02942767 \ 100.000000000 \ 29427.67 \ c_{44}: 54.68686450 \ 50.80000000
0.82808699\ 0.76923077\ 0.00346405\ 100.00000000\ 3464.05\ c_{12}:\ 109.06955946
86.90000000 \ 0.96547366 \ 0.76923077 \ 0.03851127 \ 100.00000000 \ 38511.27 \ c_{13}
: 73.74195452 \ 68.30000000 \ 0.83052094 \ 0.76923077 \ 0.00375649 \ 10.00000000
375.65 \text{ M}_{\text{freq0}}: 2.85519402 2.85858719 0.20808604 0.20833333 0.00000006
0.10000000\ 0.00\ M_{freq\,1}\colon 2.85519403\ 2.85858719\ 0.20808604\ 0.20833333\ 0.00000006
0.10000000 \ 0.00 \ M_{freq}: 2.85519403 \ 2.85858719 \ 0.20808604 \ 0.20833333 \ 0.00000006
0.10000000\ 0.00\ M_{\rm freq} \\ \text{3} \colon 2.85519404\ 2.85858719\ 0.20808604\ 0.20833333\ 0.00000006
0.10000000\,0.00\,M_{\rm freq}4\colon\,6.14081288\,5.66706047\,0.22574949\,0.20833333\,0.00030332
0.10000000\,0.30\,\,\mathrm{M_{freg}5}\colon\,6.14081288\,5.66706047\,0.22574949\,0.20833333\,0.00030332
0.10000000\ 0.30\ H_{freq0}\colon\ 4.24870561\ 4.80643423\ 0.18415877\ 0.20833333\ 0.00058441
0.10000000 \ 0.58 \ H_{freq1}: 4.24870561 \ 5.58010025 \ 0.15862565 \ 0.20833333 \ 0.00247085
0.10000000 \ 2.47 \ H_{freq}2: 6.73808691 \ 5.65316738 \ 0.24831533 \ 0.20833333 \ 0.00159856
0.10000000\,1.60\,H_{\rm fred};\,6.73808691\,6.36651842\,0.22049227\,0.20833333\,0.00014784
0.100000000\,0.15\,H_{\mathrm{freq}4}\colon\,8.32193375\,6.40050186\,0.27087504\,0.20833333\,0.00391147
0.100000003.91~H_{freq5}: 8.32193375~7.64082373~0.22690436~0.20833333~0.00034488
0.10000000 0.34 bandw. G: 4.63954304 5.87085872 1.31711085 1.66666667
0.12218927\ 15.00000000\ 18328.39\ \mathrm{bandw}.\ \mathrm{K:}\ 5.74840743\ 4.97424321\ 1.05057689
0.90909091 0.02001828 15.00000000 3002.74 bandw. M: 6.57699445 7.78109872
1.40875444\,1.66666667\,0.06651871\,15.00000000\,9977.81\,\mathrm{bandw}.\,\,\mathrm{L}{:}\,5.31166452
6.34433701\ 1.39538209\ 1.66666667\ 0.07359532\ 15.00000000\ 11039.30\ {\rm bandw}.
H{:}\ 4.44226042\ 9.70902614\ 0.41594476\ 0.90909091\ 0.24319312\ 5.00000000\ 12159.66
0.00\: DOSerr_o\colon\: 98.57124703\: 0.00000000\: 98.57124703\: 0.00000000\: 9716.29074056
0.00000000 \ 0.00 \ E_{prisf}: 119.88060210 220.00000000 119.88060210 220.00000000
10023.89383558 100000.0000000 10023893835581.32
   b2 = 91394018.8920019716 \ m2 = -14.4689417704 \ p2 = 0.00000000000 \ fdd = 0.2648249504
qdds = 0.5697753882 \ qddp = 0.5648597117 \ qddd = 0.8213593849 \ b0 = 49.7557565400
p0=1.1050685730 b1=-5.097 3416100 p1=0.6991977165 ndt=2.00000000000
cr3=-1.1418272350 \text{ rmaxhm}=10.10000000000 \text{ npar}=18 \text{ VARGS -vb2}=91394018.8920019716}
-vm2 = -14.4689417704 - vp2 = 0.00000000000 - vfdd = 0.2648249504 - vqdds = 0.5697753882
-vqddp = 0.5648597117 - vqddd = 0.8213593849 - vb0 = 49.7557565400 - vp0 = 1.
1050685730 \text{ -vb1} = -5.0973416100 \text{ -vp1} = 0.6991977165 \text{ -vndt} = 2.00000000000 \text{ -}
```

-vcr3=-1.1418272350 -vrma xhm=10.1000000000

Quantity predicted target $norm_{pred}$ $norm_{tar}$ sq diff. weight objective * 100^2

 $a_{hcp}: 5.62525983 \ 5.57678969 \ 5.62525983 \ 5.57678969 \ 0.00234935 \ 1000.000000000$ $23493.55 \ c/a: 1.60613643 \ 1.58731122 \ 15.59459288 \ 15.41181168 \ 0.03340896$ $100.00000000\,33408.96\;a_{\mathrm{omega}}:\,8.98530887\;8.73254342\;1.12316361\;1.09156793$ $0.00099829\ 10.000000000\ 99.83\ c_{\rm omega}\ :\ 5.44549052\ 5.32343103\ 0.68068632$ $0.66542888 \ 0.00023279 \ 10.000000000 \ 23.28 \ a_{4h}: \ 5.61807095 \ 5.56325146 \ 1.00985386$ $1.00000000 \ 0.00009710 \ 1.00000000 \ 0.97 \ c_{4h} : 18.21768083 \ 17.75908031 \ 1.02582344$ $1.00000000\ 0.00066685\ 1.00000000\ 6.67\ a_{6h}:\ 5.61365761\ 5.54639384\ 1.01212748$ $1.000000000\,0.00014708\,1.00000000\,1.47\,c_{6h}:\,27.38802263\,26.77136353\,1.02303428$ $1.00000000000.000530581.0000000005.31 a_{bcc}: 6.200797686.179488630.88582824$ $0.88278409\ 0.00000927\ 1.000000000\ 0.09\ a_{fcc}:\ 7.93028587\ 7.88677000\ 1.13289798$ $1.12668143 \ 0.00003865 \ 1.00000000 \ 0.39 \ DE(o,h) : 0.56552167 \ -0.63343333$ $0.03770144 - 0.04222889 \ 0.00638886 \ 3000.00000000 \ 191665.75 \ DE(4h,h): \ 1.90610750 \ DE(4h,h)$ $3.17160000\ 0.00762443\ 0.01268640\ 0.00002562\ 2000.00000000\ 512.47\ DE(6h,h)$: $2.86158833\ 3.72005000\ 0.01144635\ 0.01488020\ 0.00001179\ 2000.00000000\ 235.83$ $DE(b,h): 7.52522500 \ 7.63520000 \ 0.07601237 \ 0.07712323 \ 0.00000123 \ 1.000000000$ 0.01 DE(f,h): 4.31089500 4.51880000 0.04354439 0.04564444 0.00000441 $2000.00000000 \, 88.20 \, c_{11} : 199.90553801 \, 176.10000000 \, 0.87321687 \, 0.76923077$ $0.01081311\ 100.00000000\ 10813.11\ c_{33}:\ 226.98933014\ 190.50000000\ 0.91657311$ $0.76923077\ 0.02170976\ 100.00000000\ 21709.76\ c_{44}:\ 52.69685443\ 50.80000000$ $0.79795358 \ 0.76923077 \ 0.00082500 \ 100.00000000 \ 825.00 \ c_{12} : \ 98.48673287$ $86.90000000\ 0.87179546\ 0.76923077\ 0.01051952\ 100.00000000\ 10519.52\ c_{13}$ $: 72.19938307 \ 68.30000000 \ 0.81314769 \ 0.76923077 \ 0.00192870 \ 10.00000000$ 192.87 M_{freq0} : 2.78990046 2.85858719 0.20332746 0.20833333 0.00002506 $0.10000000\,0.03\,\mathrm{M_{freq1}}\colon\,2.78990047\,2.85858719\,0.20332746\,0.20833333\,0.00002506$ $0.10000000\,0.03\,\mathrm{M_{freq}}{}_{2}{}^{:}\,\,2.78990047\,2.85858719\,0.20332746\,0.20833333\,0.00002506$ $0.10000000\,0.03\,\,\mathrm{M_{freg}3:}\,\,2.78990048\,2.85858719\,0.20332746\,0.20833333\,0.00002506$ $0.10000000\,0.03\,\mathrm{M_{freq}}_{4}{:}\,\,6.00974100\,5.66706047\,0.22093101\,0.20833333\,0.00015870$ $0.10000000 \ 0.16 \ H_{freq0}$: $3.99826489 \ 4.80643423 \ 0.17330350 \ 0.20833333 \ 0.00122709$ $0.100000001.23\,H_{freq1}$: $3.99826489\,5.58010025\,0.14927543\,0.20833333\,0.00348784$ $0.10000000\,3.49\,H_{\mathrm{freq}2}\colon\,6.58970446\,\,5.65316738\,\,0.24284706\,\,0.20833333\,\,0.00119120$ $0.100000001.19 H_{freg3}$: 6.58970446 6.36651842 0.21563671 0.20833333 0.00005334 $0.10000000\ 0.05\ H_{freq4}\colon\ 8.23482251\ 6.40050186\ 0.26803961\ 0.20833333\ 0.00356484$ $0.10000000 \ 3.56 \ H_{freq5}$: $8.23482251 \ 7.64082373 \ 0.22452920 \ 0.20833333 \ 0.00026231$ 0.10000000 0.26 bandw. G: 4.85043136 5.87085872 1.37697953 1.66666667 $0.08391864\ 15.000000000\ 12587.80\ \mathrm{bandw}.\ \mathrm{K:}\ 5.99194943\ 4.97424321\ 1.09508653$

 $0.90909091 \ 0.03459437 \ 15.000000000 \ 5189.16 \ bandw. \ M: 6.79332504 \ 7.78109872$ 1.455091221.666666670.0447641715.0000000006714.63 bandw. L: 5.51847114 $6.34433701\ 1.44971049\ 1.66666667\ 0.04706998\ 15.00000000\ 7060.50\ {\rm bandw}.$ $H: 4.61097107\ 9.70902614\ 0.43174174\ 0.90909091\ 0.22786222\ 5.00000000\ 11393.11$ $0.00 \, \mathrm{DOSerr}_0$: $111.68287062 \, 0.000000000 \, 111.68287062 \, 0.00000000 \, 12473.06358905$ $0.00000000 \ 0.00 \ E_{prisf}$: $105.39637060 \ 220.00000000 \ 105.39637060 \ 220.00000000$ $13133.99187172\ 100000.00000000\ 13133991871718.04$

 $fdd = 0.2648249504 \; qdds = 0.5697753882 \; qddp = 0.5648597117 \; qddd = 0.82135938491112 \; qddd = 0.8213593849112 \; qddd = 0.82135938491112 \; qddd = 0.8213591112 \;$ b0=47.9215925588 p0=1.1092837121 b1=-3.99 59790920 p1=0.6574344463rcdd=10.00000000000 cr3=-1.1418272350 rmaxhm=10.1000000000 npar=18 -vfdd = 0.2648249504 - vqdds = 0.5697753882 - vqddp = 0.5648597117 - vqddd = 0.8213593849-vb0 = 47.9215925588 - vp0 = 1.1092837121 - vb1 = -3.9959790920 - vp1 = 0.6574344463-vrcdd=10.0000000000 -vcr3=-1.1418272350 -vrm axhm=10.1000000000 Quantity predicted target norm_{pred} norm_{tar} sq diff. weight objective *

 100^{2}

 $a_{hcp}: 5.58632034 \, 5.57678969 \, 5.58632034 \, 5.57678969 \, 0.00009083 \, 1000.00000000$ $908.33 \text{ c/a}: 1.58324912 \ 1.58731122 \ 15.37237127 \ 15.41181168 \ 0.00155555$ $100.00000000 \ 1555.55 \ a_{\rm omega}: \ 8.94268260 \ 8.73254342 \ 1.11783533 \ 1.09156793$ $0.00068998 \ 10.000000000 \ 69.00 \ c_{\rm omega} : \ 5.41189311 \ 5.32343103 \ 0.67648664$ $0.66542888 \ 0.00012227 \ 10.00000000 \ 12.23 \ a_{4h} : 5.57986672 \ 5.56325146 \ 1.00298661$ $1.00000000\ 0.00000892\ 1.00000000\ 0.09\ c_{4h}:\ 18.08926296\ 17.75908031\ 1.01859233$ $1.00000000 \ 0.00034567 \ 1.00000000 \ 3.46 \ a_{6h} : 5.57525690 \ 5.54639384 \ 1.00520393$ $1.00000000\ 0.00002708\ 1.00000000\ 0.27\ c_{6h}:\ 27.19488908\ 26.77136353\ 1.01582010$ $1.000000000\,0.00025028\,1.00000000\,2.50\,a_{bcc}:6.20079768\,6.17948863\,0.88582824$ $0.88278409\ 0.00000927\ 1.000000000\ 0.09\ a_{fcc}:\ 7.87598731\ 7.88677000\ 1.12514104$ $1.12668143 \ 0.00000237 \ 1.00000000 \ 0.02 \ DE(o,h) : 1.34781000 \ -0.63343333$ $0.08985400 - 0.04222889 \ 0.01744589 \ 3000.00000000 \ 523376.69 \ DE(4h,h): \ 2.01890750$ $3.17160000 \ 0.00807563 \ 0.01268640 \ 0.00002126 \ 2000.00000000 \ 425.18 \ DE(6h,h)$: $3.01372500\ 3.72005000\ 0.01205490\ 0.01488020\ 0.00000798\ 2000.00000000\ 159.65$ $DE(b,h): 7.98701000\ 7.63520000\ 0.08067687\ 0.07712323\ 0.00001263\ 1.00000000$ 0.13 DE(f,h) : 4.52676000 4.51880000 0.04572485 0.04564444 0.00000001 $2000.00000000\ 0.13\ c_{11}:\ 221.16376396\ 176.10000000\ 0.96607594\ 0.76923077$ $0.03874802\ 100.00000000\ 38748.02\ c_{33}:\ 262.04112894\ 190.50000000\ 1.05811076$ $0.76923077\ 0.08345165\ 100.00000000\ 83451.65\ c_{44}:\ 61.54190626\ 50.80000000$

```
0.93188834\ 0.76923077\ 0.02645749\ 100.00000000\ 26457.49\ c_{12}:\ 103.69257328
86.90000000 \ 0.91787708 \ 0.76923077 \ 0.02209572 \ 100.00000000 \ 22095.72 \ c_{13}
:\ 80.66574593\ 68.30000000\ 0.90850035\ 0.76923077\ 0.01939602\ 10.00000000
1939.60 M_{freq0}: 3.01657581 2.85858719 0.21984752 0.20833333 0.00013258
0.10000000\,0.13\,\mathrm{M_{freq}}_{1}\colon 3.01657582\,2.85858719\,0.21984752\,0.20833333\,0.00013258
0.10000000\,0.13\,\mathrm{M}_{\mathrm{freq}2}\colon 3.01657582\,2.85858719\,0.21984752\,0.20833333\,0.00013258
0.10000000\,0.13\,\mathrm{M_{freq}}_{3}\colon\,3.01657583\,2.85858719\,0.21984752\,0.20833333\,0.00013258
0.10000000\,0.13\,\mathrm{M_{freq}}4\colon\,6.55202353\,5.66706047\,0.24086648\,0.20833333\,0.00105841
0.10000000 \ 1.06 \ H_{freq0}: 4.22631935 \ 4.80643423 \ 0.18318844 \ 0.20833333 \ 0.00063227
0.10000000\,0.63\,H_{freq1}\colon\,4.22631935\,\,5.58010025\,\,0.15778985\,\,0.20833333\,\,0.00255464
0.10000000 \ 2.55 \ H_{freq}: 7.21414462 \ 5.65316738 \ 0.26585924 \ 0.20833333 \ 0.00330923
0.100000003.31 H_{freq3}: 7.21414462 6.36651842 0.23607044 0.20833333 0.00076935
0.100000007.10 H_{freq5}: 8.989617367.640823730.245109300.208333330.00135247
0.10000000 1.35 bandw. G: 4.99873347 5.87085872 1.41908073 1.66666667
0.06129880 15.00000000 9194.82 bandw. K: 6.15929951 4.97424321 1.12567138
0.90909091 \ 0.04690710 \ 15.00000000 \ 7036.06 \ bandw. \ M: 6.94162715 \ 7.78109872
1.48685668 1.66666667 0.03233163 15.000000000 4849.74 bandw. L: 5.69262407
6.34433701\ 1.49546072\ 1.66666667\ 0.02931148\ 15.00000000\ 4396.72\ bandw.
H: 4.72525894\ 9.70902614\ 0.44244293\ 0.90909091\ 0.21776034\ 5.00000000\ 10888.02
0.00 \, \mathrm{DOSerr_o}: 93.81903067 \, 0.000000000 \, 93.81903067 \, 0.000000000 \, 8802.01051603
0.00000000\ 0.00\ E_{\rm prisf}{:}\ 121.13361833\ 220.00000000\ 121.13361833\ 220.00000000
9774.56142366 \ 1.000000000 \ 97745614.24
```

 $fdd = 0.2648249504 \; qdds = 0.5697753882 \; qddp = 0.5648597117 \; qddd = 0.8213593849$ b0=47.4028718523 p0=1.1110171622 b1=-4.02 76308878 p1=0.6595005412rcdd=10.0000000000 cr3=-1.1418272350 rmaxhm=10.1000000000 npar=18 -vfdd = 0.2648249504 - vqdds = 0.5697753882 - vqddp = 0.5648597117 - vqddd = 0.8213593849-vb0 = 47.4028718523 - vp0 = 1.1110171622 - vb1 = -4.0276308878 - vp1 = 0.6595005412-vrcdd=10.0000000000 -vcr3=-1.1418272350 -vrm axhm=10.1000000000 Quantity predicted target norm_{pred} norm_{tar} sq diff. weight objective *

 100^{2}

 $a_{hcp}: 5.70613418 \, 5.57678969 \, 5.70613418 \, 5.57678969 \, 0.01673000 \, 1000.000000000$ $167299.96 \text{ c/a}: 1.57212363 \ 1.58731122 \ 15.26434959 \ 15.41181168 \ 0.02174507$

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100.00000000\,21745.07\,a_{\mathrm{omega}}:\,9.16691334\,8.73254342\,1.14586417\,1.09156793
0.00294808\ 10.00000000\ 294.81\ c_{\rm omega}:\ 5.50859785\ 5.32343103\ 0.68857473
0.66542888 \, 0.00053573 \, 10.000000000 \, 53.57 \, a_{4h} : \, 5.69646904 \, 5.56325146 \, 1.02394599
1.000000000\,0.00057341\,1.00000000\,5.73\,c_{4h}:\,18.49515166\,17.75908031\,1.04144761
1.00000000 \ 0.00171790 \ 1.00000000 \ 17.18 \ a_{6h} : 5.69332284 \ 5.54639384 \ 1.02649091
1.00000000\ 0.00070177\ 1.00000000\ 7.02\ c_{6h}:\ 27.79206990\ 26.77136353\ 1.03812680
1.000000000\,0.00145365\,1.000000000\,14.54\,a_{bcc}:\,6.20079768\,6.17948863\,0.88582824
0.88278409\ 0.00000927\ 1.00000000\ 0.09\ a_{fcc}:\ 8.04427434\ 7.88677000\ 1.14918205
1.12668143 0.00050628 1.00000000 5.06 DE(o,h) : 3.32247167 -0.63343333
0.22149811 - 0.04222889 \ 0.06955193 \ 3000.00000000 \ 2086557.92 \ DE(4h,h): \ 1.86745000 \ DE(4h,h): \ DE(4h,h
3.17160000\ 0.00746980\ 0.01268640\ 0.00002721\ 2000.00000000\ 544.26\ DE(6h,h):
2.80055333\ 3.72005000\ 0.01120221\ 0.01488020\ 0.00001353\ 2000.00000000\ 270.55
16.50 DE(f,h): 4.23754500 4.51880000 0.04280348 0.04564444 0.00000807
2000.00000000\,161.42\,c_{11}:\,256.25825401\,176.10000000\,1.11937384\,0.76923077
0.12260017\ 100.00000000\ 122600.17\ c_{33}:\ 285.11928542\ 190.50000000\ 1.15129936
0.76923077\ 0.14597640\ 100.00000000\ 145976.40\ c_{44}:\ 69.13492938\ 50.80000000
1.04686447\ 0.76923077\ 0.07708047\ 100.00000000\ 77080.47\ c_{12}:\ 132.18803667
86.90000000 \ 1.17011628 \ 0.76923077 \ 0.16070920 \ 100.00000000 \ 160709.20 \ c_{13}
:\ 85.78433896\ 68.30000000\ 0.96614865\ 0.76923077\ 0.03877665\ 10.00000000
3877.67 \text{ M}_{\text{freq0}}: 3.29251267 2.85858719 0.23995775 0.20833333 0.00100010
0.10000000\ 1.00\ M_{\rm freq}{}_1{}:\ 3.29251269\ 2.85858719\ 0.23995775\ 0.20833333\ 0.00100010
0.10000000\,1.00\,\mathrm{M_{freq}}{_2}{:}\,\,3.29251269\,2.85858719\,0.23995775\,0.20833333\,0.00100010
0.10000000\ 1.00\ M_{\rm freq} \\ 3:\ 3.29251270\ 2.85858719\ 0.23995775\ 0.20833333\ 0.00100010
0.10000000\,1.00\,\mathrm{M_{freq}}4\colon\,7.05767677\,5.66706047\,0.25945538\,0.20833333\,0.00261346
0.10000000\ 2.61\ M_{freq\,5};\ 7.05767677\ 5.66706047\ 0.25945538\ 0.20833333\ 0.00261346
0.10000000 \ 2.61 \ H_{freq0}: 4.96582422 \ 4.80643423 \ 0.21524204 \ 0.20833333 \ 0.00004773
0.10000000\ 0.05\ H_{freq1}\colon\ 4.96582422\ 5.58010025\ 0.18539931\ 0.20833333\ 0.00052597
0.100000000\,0.53\,\mathrm{H_{freq}}_{2}: 7.78709460\,5.65316738\,0.28697388\,0.20833333\,0.00618434
0.10000000\,6.18\,H_{\mathrm{freq}3}\colon\,7.78709460\,6.36651842\,0.25481924\,0.20833333\,0.00216094
0.10000000 \ 2.16 \ H_{freq4}: 9.46161176 \ 6.40050186 \ 0.30797102 \ 0.20833333 \ 0.00992767
0.100000009.93 H_{freq5}: 9.461611767.640823730.257978610.208333330.00246465
0.10000000 2.46 bandw. G: 4.56062999 5.87085872 1.29470838 1.66666667
0.1383529715.00000000020752.94 bandw. K: 5.654528124.974243211.03341954
0.90909091 \ 0.01545761 \ 15.000000000 \ 2318.64 \ bandw. \ M: 6.49399969 \ 7.78109872
1.39097744 1.66666667 0.07600455 15.00000000 11400.68 bandw. L: 5.23275148
6.34433701\ 1.37465151\ 1.66666667\ 0.08527285\ 15.00000000\ 12790.93\ bandw.
H: 4.37695307\ 9.70902614\ 0.40982980\ 0.90909091\ 0.24926165\ 5.00000000\ 12463.08
0.00 \, \mathrm{DOSerr_o}: 79.18263924 \, 0.00000000 \, 79.18263924 \, 0.00000000 \, 6269.89035742
```

 100^2

 $a_{hcp}: 5.55915799 \ 5.57678969 \ 5.55915799 \ 5.57678969 \ 0.00031088 \ 1000.00000000$ $3108.77 \text{ c/a}: 1.59486281 \ 1.58731122 \ 15.48513296 \ 15.41181168 \ 0.00537601$ $100.000000005376.01 \; a_{\rm omega}: \; 8.89176293 \; 8.73254342 \; 1.11147037 \; 1.09156793$ $0.00039611\ 10.00000000\ 39.61\ c_{omega}:\ 5.39115562\ 5.32343103\ 0.67389445$ $0.66542888 \ 0.00007167 \ 10.000000000 \ 7.17 \ a_{4h} : 5.55256003 \ 5.56325146 \ 0.99807820$ $1.00000000 \ 0.00000369 \ 1.00000000 \ 0.04 \ c_{4b} : 17.99793925 \ 17.75908031 \ 1.01344996$ $1.00000000000.000180901.0000000001.81 a_{6h}: 5.547651955.546393841.00022683$ $1.000000000\,0.00000005\,1.00000000\,0.00\,c_{6h}:27.05991164\,26.77136353\,1.01077824$ $1.000000000\, 0.00011617\, 1.000000000\, 1.16\, a_{bcc}:\, 6.20079768\, 6.17948863\, 0.88582824$ $0.88278409\ 0.00000927\ 1.000000000\ 0.09\ a_{fcc}:\ 7.83651495\ 7.88677000\ 1.11950214$ 1.12668143 0.00005154 1.00000000 0.52 DE(o,h): 1.00654333 -0.63343333 $0.06710289 - 0.04222889 \ 0.01195344 \ 3000.00000000 \ 358603.13 \ DE(4h,h): \ 2.04859250$ $3.17160000\ 0.00819437\ 0.01268640\ 0.00002018\ 2000.00000000\ 403.57\ DE(6h,h)$: $3.05533667\ 3.72005000\ 0.01222135\ 0.01488020\ 0.00000707\ 2000.00000000\ 141.39$ DE(b,h): 8.019550007.635200000.081005560.077123230.000015071.000000000.15 DE(f,h): 4.58537000 4.51880000 0.04631687 0.04564444 0.00000045 $2000.00000000 \ 9.04 \ c_{11} : 214.45221283 \ 176.10000000 \ 0.93675889 \ 0.76923077$ $0.02806567\ 100.00000000\ 28065.67\ c_{33}:\ 256.78024884\ 190.50000000\ 1.03686755$ $0.76923077\ 0.07162945\ 100.00000000\ 71629.45\ c_{44}:\ 59.46475943\ 50.80000000$ $0.90043549 \ 0.76923077 \ 0.01721468 \ 100.000000000 \ 17214.68 \ c_{12} : 97.32695765$ $86.90000000 \ 0.86152923 \ 0.76923077 \ 0.00851901 \ 100.000000000 \ 8519.01 \ c_{13}$ $: 79.57600099 \ 68.30000000 \ 0.89622706 \ 0.76923077 \ 0.01612806 \ 10.00000000$ $1612.81 \text{ M}_{\text{freq0}}$: $2.97174880 \ 2.85858719 \ 0.21658053 \ 0.20833333 \ 0.00006802$ $0.10000000\ 0.07\ M_{\rm freq}{}_1{}^{:}\ 2.97174881\ 2.85858719\ 0.21658053\ 0.20833333\ 0.00006802$ $0.10000000\ 0.07\ \mathrm{M_{freq}}{_{2}}{:}\ 2.97174881\ 2.85858719\ 0.21658053\ 0.20833333\ 0.00006802$

 $0.10000000\,0.07\,\mathrm{M_{freg}}_{3}\colon\,2.97174882\,2.85858719\,0.21658053\,0.20833333\,0.00006802$ $0.10000000\,0.07\,\mathrm{M_{freq}}4\colon 6.47507794\,5.66706047\,0.23803779\,0.20833333\,0.00088235$ $0.10000000\,0.88\,M_{\rm freq}5\colon 6.47507794\,5.66706047\,0.23803779\,0.20833333\,0.00088235$ $0.10000000\,0.88\,H_{\mathrm{freq}0}\!\colon\,4.07088683\,4.80643423\,0.17645127\,0.20833333\,0.00101647$ $0.100000001.02\,H_{\mathrm{freq}1}\colon\,4.07088683\,5.58010025\,0.15198677\,0.20833333\,0.00317494$ $0.10000000\,3.17\,H_{\rm freq2}\colon\,7.12197475\,5.65316738\,0.26246255\,0.20833333\,0.00292997$ $0.10000000\, 2.93\, H_{freq3}\colon\, 7.12197475\, 6.36651842\, 0.23305434\, 0.20833333\, 0.00061113$ $0.10000000 \ 0.61 \ H_{freq4}$: $8.92842683 \ 6.40050186 \ 0.29061611 \ 0.20833333 \ 0.00677045$ $0.10000000\,6.77\,H_{freq5}\colon\,8.92842683\,7.64082373\,0.24344089\,0.20833333\,0.00123254\,1.00000000\,6.79\,H_{freq5}$ 0.10000000 1.23 bandw. G: 5.10621848 5.87085872 1.44959444 1.66666667 0.04712035 15.00000000 7068.05 bandw. K: 6.27902966 4.97424321 1.14755321 $0.90909091\ 0.05686427\ 15.00000000\ 8529.64\ bandw.\ M:\ 7.04639103\ 7.78109872$ 1.50929650 1.66666667 0.02476537 15.00000000 3714.81 bandw. L: 5.79466681 $6.34433701\ 1.52226750\ 1.66666667\ 0.02085112\ 15.000000000\ 3127.67\ {\rm bandw}.$ $H: 4.80961427\ 9.70902614\ 0.45034142\ 0.90909091\ 0.21045109\ 5.00000000\ 10522.55$ $0.00 \, \mathrm{DOSerr_o}$: $98.86547597 \, 0.000000000 \, 98.86547597 \, 0.000000000 \, 9774.38233945$ $0.00000000\ 0.00\ E_{prisf}{:}\ 109.76244599\ 220.00000000\ 109.76244599\ 220.00000000$ $12152.31831491 \ 0.010000000 \ 1215231.83$

fdd=0.2648249504 qdds=0.5697753882 qddp=0.5648597117 qddd=0.8213593849b0=47.7899139676 p0=1.1088003756 b1=-3.93 45715688 p1=0.6568823915 rcdd=10.0000000000 cr3=-1.1418272350 rmaxhm=10.1000000000 npar=18 -vfdd = 0.2648249504 - vqdds = 0.5697753882 - vqddp = 0.5648597117 - vqddd = 0.8213593849-vb0 = 47.7899139676 - vp0 = 1.1088003756 - vb1 = -3.9345715688 - vp1 = 0.6568823915Quantity predicted target norm_{pred} norm_{tar} sq diff. weight objective *

 100^{2}

 $a_{hcp}:\,5.57461126\,\,5.57678969\,\,5.57461126\,\,5.57678969\,\,0.00000475\,\,1000.000000000$ $81.61 \ a_{omega} : 8.91266648 \ 8.73254342 \ 1.11408331 \ 1.09156793 \ 0.00050694$ $10.00000000 \ 50.69 \ c_{\rm omega} \ : \ 5.40535546 \ 5.32343103 \ 0.67566943 \ 0.66542888$ $0.00010487 \ 10.00000000 \ 10.49 \ a_{4h} : 5.56863112 \ 5.56325146 \ 1.00096700 \ 1.00000000$ $0.00000094\ 1.00000000\ 0.01\ c_{4h}:\ 18.04635261\ 17.75908031\ 1.01617608\ 1.00000000$ $0.00026167 \ 1.00000000 \ 2.62 \ a_{6h} : 5.56371838 \ 5.54639384 \ 1.00312357 \ 1.00000000$ $0.00000976\ 1.00000000\ 0.10\ c_{6h}:\ 27.13379120\ 26.77136353\ 1.01353789\ 1.00000000$

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0.00018327\ 1.00000000\ 1.83\ a_{bcc}:\ 6.20079768\ 6.17948863\ 0.88582824\ 0.88278409
0.00000927\ 1.00000000\ 0.09\ a_{fcc}:\ 7.85904307\ 7.88677000\ 1.12272044\ 1.12668143
0.00001569 1.00000000 0.16 DE(o,h): 0.75090833 -0.63343333 0.05006056 -
0.04222889 \ 0.00851734 \ 3000.00000000 \ 255520.25 \ DE(4h,h): 2.02638500 \ 3.17160000
0.00810554\ 0.01268640\ 0.00002098\ 2000.00000000\ 419.69\ DE(6h,h): 3.02486000
3.72005000\ 0.01209944\ 0.01488020\ 0.00000773\ 2000.00000000\ 154.65\ DE(b,h)
: 7.76340500 \ 7.63520000 \ 0.07841823 \ 0.07712323 \ 0.00000168 \ 1.00000000 \ 0.02
DE(f,h): 4.54128500 \ 4.51880000 \ 0.04587157 \ 0.04564444 \ 0.00000005 \ 2000.00000000
1.03 \ c_{11} : 209.20671277 \ 176.100000000 \ 0.91384577 \ 0.76923077 \ 0.02091350
100.00000000 20913.50 c_{33}: 248.51083574 190.50000000 1.00347602 0.76923077
0.05487084\ 100.00000000\ 54870.84\ c_{44}:\ 57.70646584\ 50.80000000\ 0.87381081
0.76923077\ 0.01093698\ 100.00000000\ 10936.98\ c_{12}:\ 96.52645635\ 86.90000000
0.85444327 \ 0.76923077 \ 0.00726117 \ 100.00000000 \ 7261.17 \ c_{13} : 77.57509665
68.30000000\ 0.87369182\ 0.76923077\ 0.01091211\ 10.00000000\ 1091.21\ M_{freq}0:
2.90595602\ \ 2.85858719\ \ 0.21178557\ \ 0.20833333\ \ 0.00001192\ \ 0.10000000\ \ 0.01
M_{freq1}: 2.90595603 2.85858719 0.21178557 0.20833333 0.00001192 0.10000000
0.01~\mathrm{M_{freq2}};~2.90595603~2.85858719~0.21178557~0.20833333~0.00001192~0.100000000
0.01~\mathrm{M_{freg3}};~2.90595604~2.85858719~0.21178557~0.20833333~0.00001192~0.100000000
0.01~\mathrm{M_{freq4}}\colon 6.32257889~5.66706047~0.23243160~0.20833333~0.00058073~0.100000000
0.58\ \mathrm{M_{freq5}}\colon 6.32257889\ 5.66706047\ 0.23243160\ 0.20833333\ 0.00058073\ 0.100000000
0.58 \, H_{\text{freq}0}: 3.99946914 \, 4.80643423 \, 0.17335569 \, 0.20833333 \, 0.00122344 \, 0.10000000
1.22 H_{freq1}: 3.99946914 5.58010025 0.14932039 0.20833333 0.00348253 0.10000000
3.48\,H_{\text{freq}2}: 6.95348945\,5.65316738\,0.25625345\,0.20833333\,0.00229634\,0.10000000
2.30 H_{freg3}: 6.95348945 6.36651842 0.22754095 0.20833333 0.00036893 0.100000000
0.37\ H_{freq4}\colon 8.72200055\ 6.40050186\ 0.28389703\ 0.20833333\ 0.00570987\ 0.10000000
5.71 \, H_{freq5}: 8.72200055 \, 7.64082373 \, 0.23781251 \, 0.20833333 \, 0.00086902 \, 0.10000000
0.87 \ \mathrm{bandw}. \ \ \mathrm{G:} \ 5.04499284 \ 5.87085872 \ 1.43221321 \ 1.66666667 \ 0.05496842
15.00000000 8245.26 bandw. K: 6.21100117 4.97424321 1.13512035 0.90909091
0.05108931\ 15.00000000\ 7663.40\ \mathrm{bandw}.\ \mathrm{M:}\ 6.98652596\ 7.78109872\ 1.49647374
1.66666667 0.02896563 15.00000000 4344.84 bandw. L: 5.73616230 6.34433701
1.50689828\,1.66666667\,0.02552594\,15.00000000\,3828.89\,\mathrm{bandw}.\ \mathrm{H:}\,4.76063375
9.70902614 0.44575520 0.90909091 0.21467998 5.00000000 10734.00 DOSerrh:
DOSerr_0: 106.23490802 0.00000000 106.23490802 0.00000000 11285.85568098
0.00000000 \ 0.00 \ E_{prisf}: 94.24578590 \ 220.00000000 \ 94.24578590 \ 220.00000000
15814.12236427\ 0.01000000\ 1581412.24
```

 $\begin{array}{l} {\rm rcdd=}10.00000000000 \ \, {\rm cr3=-}1.1418272350 \ \, {\rm rmaxhm=}10.10000000000 \ \, {\rm npar=}18 \\ {\rm VARGS-vb2=}997988120.0035278797 \ \, {\rm vm2=-}15.4004196434 \ \, {\rm vp2=}0.00000000000 \\ -{\rm vfdd=}0.2648249504 \ \, {\rm vqdds=}0.5697753882 \ \, {\rm vqddp=}0.5648597117 \ \, {\rm vqddd=}0.8213593849 \\ -{\rm vb0=}53.3178751943 \ \, {\rm vp0=}1 \ \, .1084242896 \ \, {\rm vb1=-}4.8102743429 \ \, {\rm vp1=}0.6630121162 \\ -{\rm vndt=}2.0000000000 \ \, {\rm vcr1=-}6.00000000000 \ \, {\rm vcr2=}3.2217589360 \ \, {\rm vvr1dd=}6.5000000000 \\ -{\rm vrcdd=}10.00000000000 \ \, {\rm vcr3=-}1.1418272350 \ \, {\rm vvrm\ \, axhm=}10.10000000000 \\ -{\rm Quantity\ \, predicted\ \, target\ \, norm_{pred}\ \, norm_{tar}\ \, {\rm sq\ \, diff.\ \, weight\ \, objective\ \, }^* \\ 100^2 \end{array}$

 $a_{hcp}: 5.63778583 5.57678969 5.63778583 5.57678969 0.00372053 1000.00000000$ $37205.29 \text{ c/a}: 1.60080459 \ 1.58731122 \ 15.54282399 \ 15.41181168 \ 0.01716423$ $100.0000000017164.23 \, a_{omega} : 9.04280677 \, 8.73254342 \, 1.13035085 \, 1.09156793$ $0.00150411\ 10.00000000\ 150.41\ c_{\rm omega}:\ 5.44646765\ 5.32343103\ 0.68080846$ $0.66542888 \ 0.00023653 \ 10.000000000 \ 23.65 \ a_{4h} : 5.63101774 \ 5.56325146 \ 1.01218106$ $1.00000000\ 0.00014838\ 1.00000000\ 1.48\ c_{4h}:\ 18.26169876\ 17.75908031\ 1.02830205$ $1.00000000 \ 0.00080101 \ 1.00000000 \ 8.01 \ a_{6h}: \ 5.62716702 \ 5.54639384 \ 1.01456319$ $1.000000000000002120910000000002.12c_{6h}: 27.4523248826.771363531.02543618$ $1.00000000\ 0.00064700\ 1.00000000\ 6.47\ a_{bcc}:\ 6.20079768\ 6.17948863\ 0.88582824$ $0.88278409\ 0.00000927\ 1.00000000\ 0.09\ a_{fcc}: 7.94992578\ 7.88677000\ 1.13570368$ 1.12668143 0.00008140 1.00000000 0.81 DE(o,h) : 2.48206667 -0.63343333 $0.16547111 - 0.04222889 \ 0.04313929 \ 3000.00000000 \ 1294178.70 \ DE(4h,h): \ 2.01600500$ $3.17160000\ 0.00806402\ 0.01268640\ 0.00002137\ 2000.00000000\ 427.33\ DE(6h,h)$: $3.00347000\ 3.72005000\ 0.01201388\ 0.01488020\ 0.00000822\ 2000.00000000\ 164.32$ $DE(b,h): 8.86714000\ 7.63520000\ 0.08956707\ 0.07712323\ 0.00015485\ 1.00000000$ 1.55 DE(f,h): 4.51670000 4.51880000 0.04562323 0.04564444 0.000000000 $2000.00000000\ 0.01\ c_{11}: 247.46650824\ 176.10000000\ 1.08097020\ 0.76923077$ $0.09718147\ 100.00000000\ 97181.47\ c_{33}:\ 292.48964963\ 190.50000000\ 1.18106057$ $0.76923077\ 0.16960378\ 100.00000000\ 169603.78\ c_{44}:\ 67.56639226\ 50.80000000$ $1.02311315\ 0.76923077\ 0.06445626\ 100.00000000\ 64456.26\ c_{12}:\ 126.49949516$ $86.90000000 \ 1.11976184 \ 0.76923077 \ 0.12287203 \ 100.00000000 \ 122872.03 \ c_{13}$ $:\ 86.58455848\ 68.30000000\ 0.97516115\ 0.76923077\ 0.04240732\ 10.00000000$ $4240.73 \text{ M}_{\text{freq0}}$: $3.27389129 \ 2.85858719 \ 0.23860062 \ 0.20833333 \ 0.00091611$ $0.10000000\,0.92\,M_{\rm freq}1\colon\,3.27389130\,2.85858719\,0.23860062\,0.20833333\,0.00091611$ $0.10000000\,0.92\,\mathrm{M_{freq}}_{2}\colon\,3.27389130\,2.85858719\,0.23860062\,0.20833333\,0.00091611$ $0.10000000\,0.92\,\mathrm{M_{freg}}_{3}\colon 3.27389132\,2.85858719\,0.23860063\,0.20833333\,0.00091611$ $0.1000000000.92\,\mathrm{M_{freq}}4\colon7.17344228\,5.66706047\,0.26371117\,0.20833333\,0.00306670$ $0.10000000 \ 3.07 \ H_{freq0}$: $4.80388952 \ 4.80643423 \ 0.20822303 \ 0.20833333 \ 0.00000001$ $0.10000000\ 0.00\ H_{freq1}\colon\ 4.80388952\ 5.58010025\ 0.17935347\ 0.20833333\ 0.00083983$ $0.1000000000.84 \, H_{freq}$: $7.98041792\, 5.65316738\, 0.29409833\, 0.20833333\, 0.00735563$

 $b2{=}0.00000000000\ m2{=}0.00000000000\ p2{=}0.00000000000\ fdd{=}0.2648249504$ $qdds{=}0.5697753882\ qddp{=}0.5648597117\ qddd{=}0.8213593849\ b0{=}59.5259478032$ $p0{=}1.1493643262\ b1{=}-4.5351789513\ p\ 1{=}0.6943513856\ ndt{=}2.00000000000$ $cr1{=}-6.0000000000\ cr2{=}3.2217589360\ r1dd{=}6.50000000000\ rcdd{=}10.0000000000$ $cr3{=}-1.1418272350\ rmaxhm{=}10.10000000000\ npar{=}18$

 $a_{hcp}: 5.62308140\; 5.57678969\; 5.62308140\; 5.57678969\; 0.00214292\; 1000.00000000$ $21429.23 \text{ c/a}: 1.60706613 \ 1.58731122 \ 15.60361970 \ 15.41181168 \ 0.03679032$ $100.00000000\,36790.32\,a_{\mathrm{omega}}:\,8.95511122\,8.73254342\,1.11938890\,1.09156793$ $0.00077401 \ 10.000000000 \ 77.40 \ c_{\rm omega} : \ 5.44595238 \ 5.32343103 \ 0.68074405$ $0.66542888 \ 0.00023455 \ 10.000000000 \ 23.46 \ a_{4h} : 5.61681826 \ 5.56325146 \ 1.00962869$ $1.00000000 \ 0.00009271 \ 1.00000000 \ 0.93 \ c_{4h} : 18.20540238 \ 17.75908031 \ 1.02513205$ $1.00000000000.000631621.0000000006.32a_{6h}:5.611974375.546393841.01182399$ $1.00000000\ 0.00013981\ 1.00000000\ 1.40\ c_{6h}:\ 27.37377796\ 26.77136353\ 1.02250219$ $1.00000000 \ 0.00050635 \ 1.00000000 \ 5.06 \ a_{bcc} : 6.20079768 \ 6.17948863 \ 0.88582824$ $0.88278409\ 0.00000927\ 1.000000000\ 0.09\ a_{fcc}:\ 7.92759020\ 7.88677000\ 1.13251289$ $1.12668143\ 0.00003401\ 1.00000000\ 0.34\ DE(o,h): -0.34139500\ -0.63343333$ $0.02275967 - 0.04222889 \ 0.00037905 \ 3000.00000000 \ 11371.52 \ DE(4h,h): \ 1.90152000$ $3.17160000\ 0.00760608\ 0.01268640\ 0.00002581\ 2000.00000000\ 516.19\ DE(6h,h)$: $2.85588500\ 3.72005000\ 0.01142354\ 0.01488020\ 0.00001195\ 2000.00000000\ 238.97$ DE(b,h): 6.940595007.635200000.070107020.077123230.000049231.000000000 $0.49 \text{ DE}(f,h): 4.30125500 \ 4.51880000 \ 0.04344702 \ 0.04564444 \ 0.00000483$ $2000.00000000 96.57 c_{11}: 184.83130888 176.10000000 0.80737041 0.76923077$ $0.00145463\ 100.00000000\ 1454.63\ c_{33}:\ 210.64384444\ 190.50000000\ 0.85057074$ $0.76923077\ 0.00661619\ 100.00000000\ 6616.19\ c_{44}:\ 49.26324195\ 50.80000000$ $0.74596066 \ 0.76923077 \ 0.00054150 \ 100.00000000 \ 541.50 \ c_{12} : 93.83944584$ $86.90000000 \ 0.83065810 \ 0.76923077 \ 0.00377332 \ 100.00000000 \ 3773.32 \ c_{13}$

```
: 67.50316906 \ 68.30000000 \ 0.76025644 \ 0.76923077 \ 0.00008054 \ 10.00000000
8.05~\mathrm{M_{freq0}}:~2.62482946~2.85858719~0.19129711~0.20833333~0.00029023~0.100000000
0.29\,\mathrm{M_{freq1}}\colon\,2.62482947\,\,2.85858719\,\,0.19129711\,\,0.20833333\,\,0.00029023\,\,0.100000000
0.29 \, \mathrm{M_{freq4}}; \, 5.69996224 \, 5.66706047 \, 0.20954287 \, 0.20833333 \, 0.00000146 \, 0.10000000
0.00 H_{freq0}: 3.74539370 4.80643423 0.16234288 0.20833333 0.00211512 0.10000000
2.12\,\mathrm{H_{freq1}}\colon 3.74539370\,5.58010025\,0.13983447\,0.20833333\,0.00469209\,0.10000000
4.69 H_{freq2}: 6.26248075 5.65316738 0.23078805 0.20833333 0.00050421 0.10000000
0.01 \text{ H}_{\text{freq4}}: 7.87194364 \ 6.40050186 \ 0.25622807 \ 0.20833333 \ 0.00229391 \ 0.10000000
0.04 bandw. G: 4.85859478 5.87085872 1.37929702 1.666666667 0.08258131
15.00000000 12387.20 bandw. K: 6.00147342 4.97424321 1.09682713 0.90909091
0.03524489 15.00000000 5286.73 bandw. M: 6.80148846 7.78109872 1.45683977
1.666666670.0440273215.000000006604.10 bandw. L: 5.525273986.34433701
1.45149760 1.66666667 0.04629772 15.00000000 6944.66 bandw. H: 4.61641335
9.70902614 0.43225132 0.90909091 0.22737599 5.00000000 11368.80 DOSerrh:
DOSerr_0: 110.29822598 0.00000000 110.29822598 0.00000000 12165.69865409
0.00000000\ 0.00\ E_{\rm prisf}\text{: }70.80322562\ 220.00000000\ 70.80322562\ 220.00000000
22259.67748515 0.00100000 222596.77
```

 $b2 = 529957467.2048873901 \ m2 = -15.8531159425 \ p2 = 0.000000000000 \ fdd = 0.2648249504 \ qdds = 0.5697753882 \ qddp = 0.5648597117 \ qddd = 0.8213593849 \ b0 = 47.1964963231 \ p0 = 1.0523246525 \ b1 = -4.93 \ 66489527 \ p1 = 0.6329489051 \ ndt = 2.00000000000 \ cr1 = -6.00000000000 \ cr2 = 3.2217589360 \ r1dd = 6.50000000000 \ rcdd = 10.00000000000 \ cr3 = -1.1418272350 \ rmaxhm = 10.100000000000 \ npar = 18$

 $\begin{array}{l} a_{\rm hcp}: 5.57188821\ 5.57678969\ 5.57188821\ 5.57678969\ 0.00002402\ 1000.000000000\\ 240.24\ c/a: 1.58940570\ 1.58731122\ 15.43214786\ 15.41181168\ 0.00041356\\ 100.000000000\ 413.56\ a_{\rm omega}: 8.90037874\ 8.73254342\ 1.11254734\ 1.09156793\\ 0.00044014\ 10.00000000\ 44.01\ c_{\rm omega}: 5.40408192\ 5.32343103\ 0.67551024\\ 0.66542888\ 0.00010163\ 10.00000000\ 10.16\ a_{4h}: 5.57268326\ 5.56325146\ 1.00169538\\ 1.00000000\ 0.00000287\ 1.00000000\ 0.03\ c_{4h}: 18.01242981\ 17.75908031\ 1.01426591\\ 1.00000000\ 0.00002352\ 1.00000000\ 2.04\ a_{6h}: 5.56660954\ 5.54639384\ 1.00364484\\ 1.00000000\ 0.00001328\ 1.00000000\ 0.13\ c_{6h}: 27.10263712\ 26.77136353\ 1.01237418\\ 1.00000000\ 0.00015312\ 1.00000000\ 1.53\ a_{bcc}: 6.20079768\ 6.17948863\ 0.88582824\\ 0.88278409\ 0.00000927\ 1.00000000\ 0.09\ a_{fcc}: 7.86058346\ 7.88677000\ 1.12294049\\ 1.12668143\ 0.00001399\ 1.00000000\ 0.14\ DE(o,h): -0.49262667\ -0.63343333\ -\end{array}$

```
0.03284178 - 0.04222889 \ 0.00008812 \ 3000.00000000 \ 2643.54 \ DE(4h,h): \ 2.28232000
3.17160000 0.00912928 0.01268640 0.00001265 2000.00000000 253.06 DE(6h,h):
3.36564500\ 3.72005000\ 0.01346258\ 0.01488020\ 0.00000201\ 2000.00000000\ 40.19
DE(b,h): 7.56147000\ 7.63520000\ 0.07637848\ 0.07712323\ 0.00000055\ 1.00000000
0.01 \text{ DE}(f,h) : 5.02996000 \ 4.51880000 \ 0.05080768 \ 0.04564444 \ 0.00002666
2000.00000000533.18 c_{11}: 199.75935696176.100000000.872578330.76923077
0.01068072\ 100.00000000\ 10680.72\ c_{33}:\ 257.57041942\ 190.50000000\ 1.04005822
0.76923077\ 0.07334751\ 100.00000000\ 73347.51\ c_{44}:\ 57.74878709\ 50.80000000
0.87445165 \ 0.76923077 \ 0.01107143 \ 100.00000000 \ 11071.43 \ c_{12} : 99.00485786
86.90000000 \ 0.87638185 \ 0.76923077 \ 0.01148135 \ 100.00000000 \ 11481.35 \ c_{13}
: \ 78.58125619 \ 68.30000000 \ 0.88502372 \ 0.76923077 \ 0.01340801 \ 10.00000000
1340.80 \text{ M}_{\text{freq0}}: 2.89853526 \ 2.85858719 \ 0.21124474 \ 0.20833333 \ 0.00000848
0.10000000\ 0.01\ M_{freq} 1\colon 2.89853527\ 2.85858719\ 0.21124474\ 0.20833333\ 0.00000848
0.10000000\ 0.01\ M_{\rm freq} \ 2:\ 2.89853527\ 2.85858719\ 0.21124474\ 0.20833333\ 0.00000848
0.10000000\ 0.01\ M_{freq3}\colon 2.89853528\ 2.85858719\ 0.21124474\ 0.20833333\ 0.00000848
0.10000000\ 0.01\ \mathrm{M_{freq}}_{4}{:}\ 6.67131393\ 5.66706047\ 0.24525185\ 0.20833333\ 0.00136298
0.10000000\,1.36\,M_{\rm freq} 5\colon 6.67131393\,5.66706047\,0.24525185\,0.20833333\,0.00136298
0.10000000\,1.36\,H_{freq0}\colon\,3.83835538\,4.80643423\,0.16637227\,0.20833333\,0.00176073
0.10000000\,1.76\,H_{freq1}\colon\,3.83835538\,5.58010025\,0.14330520\,0.20833333\,0.00422866
0.100000004.23\,H_{\mathrm{fred}2}: 7.48779156\,5.65316738\,0.27594382\,0.20833333\,0.00457118
0.100000004.57 H_{freg3}: 7.48779156 6.36651842 0.24502506 0.20833333 0.00134628
0.10000000\,1.35\,H_{\rm fred}\colon\,9.36361994\,6.40050186\,0.30478144\,0.20833333\,0.00930224
0.100000009.30 H_{freq5}: 9.363619947.640823730.255306790.208333330.00220651
0.10000000 2.21 bandw. G: 5.05587740 5.87085872 1.43530320 1.66666667
0.05352905 15.00000000 8029.36 bandw. K: 6.22324630 4.97424321 1.13735827
0.90909091 0.05210599 15.000000000 7815.90 bandw. M: 6.99741052 7.78109872
1.49880515 1.666666667 0.02817749 15.000000000 4226.62 bandw. L: 5.74704686
6.34433701\ 1.50975767\ 1.66666667\ 0.02462043\ 15.00000000\ 3693.07\ bandw.
H{:}\ 4.77015774\ 9.70902614\ 0.44664696\ 0.90909091\ 0.21385440\ 5.00000000\ 10692.72
0.00\ \mathrm{DOSerr_o:}\ 104.85200112\ 0.000000000\ 104.85200112\ 0.00000000\ 10993.94213887
0.00000000 \ 0.00 \ E_{prisf}: 72.80642405 \ 220.00000000 \ 72.80642405 \ 220.00000000
21665.94880152\ 0.00100000\ 216659.49
```

 $b2 = 238992966.9478154778 \ m2 = -15.0156845030 \ p2 = 0.000000000000 \ fdd = 0.2648249504 \ qdds = 0.5697753882 \ qddp = 0.5648597117 \ qddd = 0.8213593849 \ b0 = 47.0500980357 \ p0 = 1.0556839408 \ b1 = -5.13 \ 00359501 \ p1 = 0.6507410387 \ ndt = 2.00000000000 \ cr1 = -6.00000000000 \ cr2 = 3.2217589360 \ r1dd = 6.50000000000 \ rcdd = 10.00000000000 \ cr3 = -1.1418272350 \ rmaxhm = 10.100000000000 \ npar = 18$

 $a_{hcp}: 5.65153719 \ 5.57678969 \ 5.65153719 \ 5.57678969 \ 0.00558719 \ 1000.000000000$

 $55871.89 \text{ c/a}: 1.59497837 \ 1.58731122 \ 15.48625502 \ 15.41181168 \ 0.00554181$ $100.000000005541.81\;a_{\rm omega}:\,9.03327448\;8.73254342\;1.12915931\;1.09156793$ $0.00141311\ 10.000000000\ 141.31\ c_{omega}:\ 5.46261177\ 5.32343103\ 0.68282647$ $0.66542888 \, 0.00030268 \, 10.00000000 \, 30.27 \, a_{4h} : \, 5.65046462 \, 5.56325146 \, 1.01567665$ $1.00000000 \ 0.00024576 \ 1.00000000 \ 2.46 \ c_{4h} : 18.28532568 \ 17.75908031 \ 1.02963247$ $1.00000000\ 0.00087808\ 1.00000000\ 8.78\ a_{6h}:\ 5.64546730\ 5.54639384\ 1.01786268$ $1.00000000 \ 0.00031908 \ 1.00000000 \ 3.19 \ c_{6h} : 27.50655214 \ 26.77136353 \ 1.02746175$ $1.00000000 \ 0.00075415 \ 1.00000000 \ 7.54 \ a_{bcc} : 6.20079768 \ 6.17948863 \ 0.88582824$ $0.88278409\ 0.00000927\ 1.00000000\ 0.09\ a_{fcc}:\ 7.97380174\ 7.88677000\ 1.13911453$ 1.12668143 0.00015458 1.00000000 1.55 DE(o,h): -0.27297000 -0.63343333 - $0.01819800 - 0.04222889 \ 0.00057748 \ 3000.00000000 \ 17324.51 \ DE(4h,h): \ 2.06699250$ $3.17160000\ 0.00826797\ 0.01268640\ 0.00001952\ 2000.00000000\ 390.45\ DE(6h,h)$: $3.06958667\ 3.72005000\ 0.01227835\ 0.01488020\ 0.00000677\ 2000.00000000\ 135.39$ $DE(b,h): 7.84221000\ 7.63520000\ 0.07921424\ 0.07712323\ 0.00000437\ 1.00000000$ $0.04 \text{ DE}(f,h) : 4.60577000 \ 4.51880000 \ 0.04652293 \ 0.04564444 \ 0.00000077$ $2000.0000000015.43\ c_{11}:\ 200.13394216\ 176.10000000\ 0.87421457\ 0.76923077$ $0.01102160\ 100.00000000\ 11021.60\ c_{33}:\ 238.53684776\ 190.50000000\ 0.96320148$ $0.76923077\ 0.03762464\ 100.00000000\ 37624.64\ c_{44}:\ 54.80421660\ 50.80000000$ $0.82986397\ 0.76923077\ 0.00367639\ 100.00000000\ 3676.39\ c_{12}:\ 111.18853892$ $86.90000000\ 0.98423067\ 0.76923077\ 0.04622496\ 100.00000000\ 46224.96\ c_{13}$ $: 72.65583597 \ 68.30000000 \ 0.81828850 \ 0.76923077 \ 0.00240666 \ 10.000000000$ $240.67\ \mathrm{M_{freq}0:}\ 2.84168323\ 2.85858719\ 0.20710138\ 0.20833333\ 0.00000152$ $0.10000000 \ 0.00 \ M_{freq\,1}$: $2.84168324 \ 2.85858719 \ 0.20710138 \ 0.20833333 \ 0.00000152$ $0.10000000\ 0.00\ M_{\rm freq} \\ 2:84168324\ 2.85858719\ 0.20710138\ 0.20833333\ 0.00000152$ $0.10000000\ 0.00\ M_{\rm freq} \\ \text{3} \colon 2.84168325\ 2.85858719\ 0.20710138\ 0.20833333\ 0.00000152$ $0.10000000\,0.00\,M_{\rm freq}4\colon\,6.35692654\,5.66706047\,0.23369429\,0.20833333\,0.00064318$ $0.10000000\,0.64\,\mathrm{M_{freg}}_{5}$: $6.35692654\,5.66706047\,0.23369429\,0.20833333\,0.00064318$ $0.10000000\ 0.64\ H_{freq0}\colon\ 4.05308243\ 4.80643423\ 0.17567954\ 0.20833333\ 0.00106627$ $0.10000000\,1.07\,H_{\rm fred}\colon\,4.05308243\,5.58010025\,0.15132204\,0.20833333\,0.00325029$ $0.10000000\,3.25\,H_{\rm freq2}\colon\,7.14466972\,5.65316738\,0.26329892\,0.20833333\,0.00302122$ $0.10000000 \ 3.02 \ H_{freq3}$: $7.14466972 \ 6.36651842 \ 0.23379699 \ 0.20833333 \ 0.00064840$ $0.10000000\,0.65\,H_{freq4}\colon\,8.81982929\,6.40050186\,0.28708131\,0.20833333\,0.00620124$ $0.100000006.20\,H_{\mathrm{freq}5}\colon\,8.81982929\,7.64082373\,0.24047989\,0.20833333\,0.00103340$ 0.10000000 1.03 bandw. G: 4.75383090 5.87085872 1.34955581 1.666666667 0.10055929 15.00000000 15083.89 bandw. K: 5.88038270 4.97424321 1.07469664 $0.90909091 \ 0.02742526 \ 15.000000000 \ 4113.79 \ bandw. \ M: 6.69400345 \ 7.78109872$ 1.43381710 1.66666667 0.05421892 15.00000000 8132.84 bandw. L: 5.42187068 $6.34433701\ 1.42433340\ 1.666666667\ 0.05872541\ 15.00000000\ 8808.81\ bandw.$ $\text{H:}\ 4.53341860\ 9.70902614\ 0.42448023\ 0.90909091\ 0.23484751\ 5.00000000\ 11742.38$

 $\begin{array}{l} 0.00\ \mathrm{DOSerr_o}\colon 106.26772307\ 0.000000000\ 106.26772307\ 0.000000000\ 11292.82896546\\ 0.00000000\ 0.00\ \mathrm{E_{prisf}}\colon 105.96058776\ 220.00000000\ 105.96058776\ 220.00000000\\ 13004.98754412\ 0.00100000\ 130049.88 \end{array}$

 $b2{=}0.00000000000\ m2{=}0.00000000000\ p2{=}0.00000000000\ fdd{=}0.2648249504$ $qdds{=}0.5697753882\ qddp{=}0.5648597117\ qddd{=}0.8213593849\ b0{=}140.6250881140$ $p0{=}1.5000000000\ b1{=}-0.3349120798\ p1{=}0.5103314042\ ndt{=}2.00000000000\ cr1{=}-6.0000000000\ cr2{=}3.2217589360\ r1dd{=}6.50000000000\ rcdd{=}10.0000000000\ cr3{=}-1.1418272350\ rmaxhm{=}10.10000000000\ npar{=}18$

 $a_{hcp}: 5.56058759 \ 5.57678969 \ 5.56058759 \ 5.57678969 \ 0.00026251 \ 1000.00000000$ $2625.08 \text{ c/a}: 1.59424873 \ 1.58731122 \ 15.47917067 \ 15.41181168 \ 0.00453723$ $100.00000000 4537.23 a_{\text{omega}} : 8.85711014 8.73254342 1.10713877 1.09156793$ $0.00024245 \ 10.000000000 \ 24.25 \ c_{omega} : \ 5.41409627 \ 5.32343103 \ 0.67676203$ $0.66542888 \ 0.00012844 \ 10.0000000012.84 \ a_{4h} : 5.54693871 \ 5.56325146 \ 0.99706777$ $1.00000000\ 0.00000860\ 1.00000000\ 0.09\ c_{4h}:\ 18.02419033\ 17.75908031\ 1.01492814$ $1.00000000\ 0.00022285\ 1.00000000\ 2.23\ a_{6h}:\ 5.54272137\ 5.54639384\ 0.99933786$ $1.000000000\,0.00000044\,1.00000000\,0.00\,c_{6h}$: $27.08087241\,26.77136353\,1.01156119$ $1.00000000\ 0.00013366\ 1.00000000\ 1.34\ a_{bcc}:\ 6.20079768\ 6.17948863\ 0.88582824$ $0.88278409\ 0.00000927\ 1.000000000\ 0.09\ a_{fcc}:\ 7.83131615\ 7.88677000\ 1.11875945$ 1.12668143 0.00006276 1.00000000 0.63 DE(o,h): 1.24301500 -0.63343333 $0.08286767 - 0.04222889 \ 0.01564915 \ 3000.00000000 \ 469474.45 \ DE(4h,h): 1.72554000$ $3.17160000\ 0.00690216\ 0.01268640\ 0.00003346\ 2000.00000000\ 669.15\ DE(6h,h)$: $2.63205667\ 3.72005000\ 0.01052823\ 0.01488020\ 0.00001894\ 2000.00000000\ 378.79$ DE(b,h): 8.050595007.635200000.081319140.077123230.000017611.00000000 $0.18\ DE(f,h)\ :\ 3.97823500\ 4.51880000\ 0.04018419\ 0.04564444\ 0.00002981$ $2000.00000000596.29 c_{11}: 192.43892517 176.10000000 0.84060160 0.76923077$ $0.00509380\ 100.00000000\ 5093.80\ c_{33}:\ 204.85827777\ 190.50000000\ 0.82720887$ $0.76923077 \ 0.00336146 \ 100.00000000 \ 3361.46 \ c_{44} : 50.34135405 \ 50.80000000$ $0.76228580 \ 0.76923077 \ 0.00004823 \ 100.00000000 \ 48.23 \ c_{12} : \ 75.61328960$ $86.90000000 \ 0.66932185 \ 0.76923077 \ 0.00998179 \ 100.00000000 \ 9981.79 \ c_{13}$ $: 68.71389026 \ 68.30000000 \ 0.77389222 \ 0.76923077 \ 0.00002173 \ 10.00000000$ $2.17\,\mathrm{M_{freq0}}\colon\,2.67628898\,\,2.85858719\,\,0.19504747\,\,0.20833333\,\,0.00017651\,\,0.100000000$ $0.18\ \mathrm{M_{freq1}}\colon 2.67628899\ 2.85858719\ 0.19504747\ 0.20833333\ 0.00017651\ 0.10000000$ $0.18\,\mathrm{M_{freq}}$: $2.67628899\,2.85858719\,0.19504747\,0.20833333\,0.00017651\,0.10000000$ $0.18\,\mathrm{M_{freg}}_{3}\colon\,2.67628900\,2.85858719\,0.19504747\,0.20833333\,0.00017651\,0.10000000$ $0.18\,\mathrm{M_{freq}4}\colon 5.25767874\,5.66706047\,0.19328358\,0.20833333\,0.00022650\,0.100000000$ $0.23 H_{freq0}$: 3.63161265 4.80643423 0.15741107 0.20833333 0.00259308 0.10000000 $2.59 \, \mathrm{H_{freq1}}$: $3.63161265 \, 5.58010025 \, 0.13558645 \, 0.20833333 \, 0.00529211 \, 0.10000000$ $5.29 H_{freq2}$: 5.48887273 5.65316738 0.20227867 0.20833333 0.00003666 0.100000000

 $b2 = 0.00000000000 \ m2 = 0.000000000000 \ p2 = 0.00000000000 \ fdd = 0.2648249504$ $qdds = 0.5697753882 \ qddp = 0.5648597117 \ qddd = 0.8213593849 \ b0 = 114.1564941581$ $p0 = 1.3883912590 \ b1 = -1.8695661213 \ p1 = 0.7021069541 \ ndt = 2.000000000000 \ cr1 = -6.00000000000 \ cr2 = 3.2217589360 \ r1dd = 6.50000000000 \ rcdd = 10.00000000000 \ cr3 = -1.1418272350 \ rmaxhm = 10.100000000000 \ npar = 18$

 $a_{hcp}: 5.62641713 \ 5.57678969 \ 5.62641713 \ 5.57678969 \ 0.00246288 \ 1000.00000000$ $24628.83 \text{ c/a}: 1.60564282 \ 1.58731122 \ 15.58980022 \ 15.41181168 \ 0.03167992$ $100.00000000\,31679.92\;a_{\rm omega}:\,8.96538123\;8.73254342\;1.12067265\;1.09156793$ $0.00084709\ 10.000000000\ 84.71\ c_{\rm omega}:\ 5.45575817\ 5.32343103\ 0.68196977$ $0.66542888 \ 0.00027360 \ 10.000000000 \ 27.36 \ a_{4h}: \ 5.61278398 \ 5.56325146 \ 1.00890352$ $1.00000000 \ 0.00007927 \ 1.00000000 \ 0.79 \ c_{4h} : 18.24121329 \ 17.75908031 \ 1.02714853$ $1.00000000000000737041.0000000007.37 a_{6h}: 5.609121525.546393841.01130963$ $1.00000000\ 0.00012791\ 1.00000000\ 1.28\ c_{6h}:\ 27.40562165\ 26.77136353\ 1.02369166$ $1.00000000 \ 0.00056129 \ 1.00000000 \ 5.61 \ a_{bcc} : 6.20079768 \ 6.17948863 \ 0.88582824$ $0.88278409\ 0.00000927\ 1.000000000\ 0.09\ a_{fcc}:\ 7.92527962\ 7.88677000\ 1.13218280$ 1.12668143 0.00003027 1.00000000 0.30 DE(o,h): 1.26412500 -0.63343333 $0.08427500 - 0.04222889 \ 0.01600323 \ 3000.00000000 \ 480097.02 \ DE(4h,h): \ 1.69892000$ $3.17160000 \ 0.00679568 \ 0.01268640 \ 0.00003470 \ 2000.00000000 \ 694.01 \ DE(6h,h)$: $2.59242333\ 3.72005000\ 0.01036969\ 0.01488020\ 0.00002034\ 2000.00000000\ 406.89$ $DE(b,h): 7.56535500 \ 7.63520000 \ 0.07641773 \ 0.07712323 \ 0.00000050 \ 1.00000000$ 0.00 DE(f,h) : 3.93098500 4.51880000 0.03970692 0.04564444 0.00003525 $2000.00000000705.08 c_{11}: 195.05516670176.1000000000.852029730.76923077$ $0.00685567\,100.00000000\,6855.67\,c_{33}:\,206.27436836\,190.50000000\,0.83292699$ $0.76923077\ 0.00405721\ 100.00000000\ 4057.21\ c_{44}:\ 49.63461769\ 50.80000000$ $0.75158416 \ 0.76923077 \ 0.00031140 \ 100.00000000 \ 311.40 \ c_{12} : 86.92490619$ $86.90000000\, 0.76945124\, 0.76923077\, 0.00000005\, 100.00000000\, 0.05\, c_{13}:\, 68.73179082\, c_{14}$ $68.30000000\,0.77409383\,0.76923077\,0.00002365\,10.000000000\,2.36\,M_{freq0}\colon\,2.68061683$ $2.85858719\ 0.19536289\ 0.20833333\ 0.00016823\ 0.10000000\ 0.17\ M_{freq}$: 2.68061684 $2.85858719\ 0.19536289\ 0.20833333\ 0.00016823\ 0.10000000\ 0.17\ M_{freq3}{:}\ 2.68061685$ $2.85858719\ 0.19536289\ 0.20833333\ 0.00016823\ 0.10000000\ 0.17\ M_{freq}4\colon 5.45403129$ $5.66706047\ 0.20050192\ 0.20833333\ 0.00006133\ 0.10000000\ 0.06\ M_{freq}5\colon 5.45403129$ $5.66706047\ 0.20050192\ 0.20833333\ 0.00006133\ 0.10000000\ 0.06\ H_{freq}$: 3.89335853 $4.80643423\ 0.16875636\ 0.20833333\ 0.00156634\ 0.10000000\ 1.57\ H_{freq1}\colon\ 3.89335853$ $5.58010025\ 0.14535874\ 0.20833333\ 0.00396580\ 0.10000000\ 3.97\ H_{freq}{}_{:}\ 5.77373518$ $5.65316738\ 0.21277656\ 0.20833333\ 0.00001974\ 0.10000000\ 0.02\ H_{freq3}$: 5.77373518 $6.36651842\ 0.18893552\ 0.20833333\ 0.00037627\ 0.10000000\ 0.38\ H_{freq}\text{4}\text{: }7.33883803$ $6.40050186\,0.23887574\,0.20833333\,0.00093284\,0.10000000\,0.93\,H_{frea}$; $7.33883803\,0.00093284\,0.10000000\,0.93\,H_{frea}$; $7.64082373 \ 0.20009945 \ 0.20833333 \ 0.00006780 \ 0.10000000 \ 0.07 \ bandw.$ G: $4.84634965\ 5.87085872\ 1.37582078\ 1.666666667\ 0.08459133\ 15.000000000\ 12688.70$ bandw. K: 5.98650715 4.97424321 1.09409190 0.90909091 0.03422537 15.00000000 5133.81 bandw. M: 6.78924333 7.78109872 1.45421694 1.666666667 0.04513489 15.00000000 6770.23 bandw. L: 5.51302886 6.34433701 1.44828079 1.66666667 $0.04769239\ 15.000000000\ 7153.86\ \mathrm{bandw}.\ \mathrm{H:}\ 4.60552880\ 9.70902614\ 0.43123216$ 0.90909091 0.22834898 5.000000000 11417.45 DOSerrh: 0.00000000 0.00000000 $0.00000000 \ 106.36466941 \ 0.00000000 \ 11313.44289798 \ 0.00000000 \ 0.00 \ E_{prisf}$ $92.22065278\ 220.000000000\ 92.22065278\ 220.000000000\ 16327.56157472\ 0.00100000$ 163275.62

 $\begin{array}{l} a_{\rm hcp}: 5.56276602\ 5.57678969\ 5.56276602\ 5.57678969\ 0.00019666\ 1000.000000000\\ 1966.63\ c/a: 1.59331360\ 1.58731122\ 15.47009117\ 15.41181168\ 0.00339650\\ 100.000000000\ 3396.50\ a_{\rm omega}: 8.86570413\ 8.73254342\ 1.10821302\ 1.09156793\\ 0.00027706\ 10.00000000\ 27.71\ c_{\rm omega}: 5.39008159\ 5.32343103\ 0.67376020\\ 0.66542888\ 0.00006941\ 10.00000000\ 6.94\ a_{4h}: 5.55263546\ 5.56325146\ 0.99809176\\ 1.00000000\ 0.00000364\ 1.00000000\ 0.04\ c_{4h}: 18.02391102\ 17.75908031\ 1.01491241\\ 1.00000000\ 0.00002238\ 1.00000000\ 2.22\ a_{6h}: 5.54842769\ 5.54639384\ 1.00036670\\ 1.00000000\ 0.00000013\ 1.00000000\ 0.00\ c_{6h}: 27.08910587\ 26.77136353\ 1.01186874\\ 1.00000000\ 0.00014087\ 1.00000000\ 0.09\ a_{fcc}: 7.83901807\ 7.88677000\ 1.11985972\\ 1.12668143\ 0.00004654\ 1.00000000\ 0.47\ DE(o,h): 0.70288333\ -0.63343333\\ \end{array}$

 $0.04685889 - 0.04222889 \ 0.00793663 \ 3000.00000000 \ 238098.96 \ DE(4h,h): \ 1.86685500$ $3.17160000\ 0.00746742\ 0.01268640\ 0.00002724\ 2000.00000000\ 544.76\ DE(6h,h)$: $2.81596667\ 3.72005000\ 0.01126387\ 0.01488020\ 0.00001308\ 2000.00000000\ 261.56$ $DE(b,h): 7.38194000\ 7.63520000\ 0.07456505\ 0.07712323\ 0.00000654\ 1.00000000$ 0.07 DE(f,h): $4.24119000 \ 4.51880000 \ 0.04284030 \ 0.04564444 \ 0.00000786$ $2000.00000000157.26 c_{11} : 208.93562758176.1000000000.912661630.76923077$ $0.02057241\ 100.00000000\ 20572.41\ c_{33}:\ 237.98543138\ 190.50000000\ 0.96097489$ $0.76923077\ 0.03676581\ 100.000000000\ 36765.81\ c_{44}:\ 54.28185458\ 50.80000000$ $0.82195419\ 0.76923077\ 0.00277976\ 100.00000000\ 2779.76\ c_{12}:\ 97.64679227$ $86.90000000 \ 0.86436038 \ 0.76923077 \ 0.00904964 \ 100.00000000 \ 9049.64 \ c_{13}$ $: 74.24437438 \ 68.30000000 \ 0.83617946 \ 0.76923077 \ 0.00448213 \ 10.00000000$ $448.21 \text{ M}_{\text{freq0}}$: 2.82856685 2.85858719 0.20614546 0.20833333 0.00000479 $0.10000000\ 0.00\ M_{freq} 1\colon 2.82856686\ 2.85858719\ 0.20614546\ 0.20833333\ 0.00000479$ $0.10000000\ 0.00\ M_{\rm freq} \\ 2\colon 2.82856686\ 2.85858719\ 0.20614546\ 0.20833333\ 0.00000479$ $0.10000000\ 0.00\ M_{freq3}\colon 2.82856687\ 2.85858719\ 0.20614546\ 0.20833333\ 0.00000479$ $0.10000000\ 0.00\ M_{\rm freq\,4};\ 6.02957369\ 5.66706047\ 0.22166010\ 0.20833333\ 0.00017760$ $0.10000000\,0.18\,\mathrm{M_{freq}}_{5}\colon 6.02957369\,5.66706047\,0.22166010\,0.20833333\,0.00017760$ $0.10000000\,0.18\,H_{freq0}\colon\,4.01647120\,4.80643423\,0.17409264\,0.20833333\,0.00117242$ $0.10000000\,1.17\,H_{freq1}\colon\,4.01647120\,5.58010025\,0.14995516\,0.20833333\,0.00340801$ $0.100000003.41 \; H_{fred}$: $6.59737209 \; 5.65316738 \; 0.24312963 \; 0.20833333 \; 0.00121078$ $0.100000001.21~H_{freg3}$: 6.59737209~6.36651842~0.21588762~0.20833333~0.00005707 $0.10000000\ 3.73\ H_{\rm freq5}\colon\ 8.27795011\ 7.64082373\ 0.22570511\ 0.20833333\ 0.00030178$ 0.10000000 0.30 bandw. G: 5.09125222 5.87085872 1.44534569 1.66666667 0.04898297 15.00000000 7347.45 bandw. K: 6.26406339 4.97424321 1.14481798 0.90909091 0.05556725 15.000000000 8335.09 bandw. M: 7.03142476 7.78109872 $1.50609081 \ 1.66666667 \ 0.02578461 \ 15.000000000 \ 3867.69 \ bandw. \ L: 5.78242168$ $6.34433701\ 1.51905068\ 1.66666667\ 0.02179048\ 15.00000000\ 3268.57\ bandw.$ $H{:}\ 4.79736914\ 9.70902614\ 0.44919486\ 0.90909091\ 0.21150437\ 5.00000000\ 10575.22$ $0.00\:\mathrm{DOSerr_o}\colon\:105.23589358\:0.000000000\:105.23589358\:0.00000000\:11074.59329851$ $0.00000000 \ 0.00 \ E_{prisf}$: $94.86005764 \ 220.00000000 \ 94.86005764 \ 220.00000000$ $15660.00517479\ 0.00100000\ 156600.05$

 $\begin{array}{l} PARAMETERS\ b2=1000000.0000000000\ m2=-12.00000000000\ p2=0.00000000000\ fdd=0.2648249504\ qdds=0.5697753882\ qddp=0.5648597117\ qddd=0.8213593849\ b0=55.0000000000\ p0=1.0500000000\ b1=-6.9791\ 271873\ p1=0.6629981150\ ndt=2.00000000000\ cr1=-6.0000000000\ cr2=3.2217589360\ r1dd=6.50000000000\ rcdd=10.0000000000\ cr3=-1.1418272350\ rmaxhm=10.1000000000\ npar=18\ VARGS\ -vb2=1000000.0000000000\ -vm2=-12.00000000000\ -vp2=0.0000000000\ -vfdd=0.2648249504\ -vqdds=0.5697753882\ -vqddp=0.5648597117\ -vqddd=0.8213593849 \end{array}$

```
-vb0 = 55.0000000000 - vp0 = 1.0500000000 - vb1 = -6.9791271873 - vp1 = 0.6629981150
a_{hcp}: 5.58686494 \ 5.57678969 \ 5.58686494 \ 5.57678969 \ 0.00010151 \ 1000.00000000
1015.11\ \mathrm{c/a}:\ 1.58301742\ 1.58731122\ 15.37012160\ 15.41181168\ 0.00173806
100.000000001738.06 \ a_{\rm omega}: 8.91730311\ 8.73254342\ 1.11466289\ 1.09156793
0.00053338 10.00000000 53.34 c_{omega} : 5.40664954 5.32343103 0.67583119
0.66542888 \ 0.00010821 \ 10.00000000 \ 10.82 \ a_{4h} : 5.58766385 \ 5.56325146 \ 1.00438815
1.00000000\ 0.00001926\ 1.00000000\ 0.19\ c_{4h}:\ 18.06717880\ 17.75908031\ 1.01734879
1.000000000 \ 0.00030098 \ 1.000000000 \ 3.01 \ a_{6h} : 5.58217511 \ 5.54639384 \ 1.00645127
1.00000000 \ 0.00004162 \ 1.00000000 \ 0.42 \ c_{6h} : 27.18237891 \ 26.77136353 \ 1.01535280
1.00000000\ 0.00023571\ 1.00000000\ 2.36\ a_{bcc}:\ 6.20079768\ 6.17948863\ 0.88582824
0.88278409\ 0.00000927\ 1.00000000\ 0.09\ a_{fcc}: 7.88330413\ 7.88677000\ 1.12618630
1.12668143 0.00000025 1.00000000 0.00 DE(o,h): -0.60419667 -0.63343333 -
0.04027978 - 0.04222889 \ 0.00000380 \ 3000.00000000 \ 113.97 \ DE(4h,h): \ 2.29304250
3.17160000\ 0.00917217\ 0.01268640\ 0.00001235\ 2000.00000000\ 247.00\ DE(6h,h):
3.37653833\ 3.72005000\ 0.01350615\ 0.01488020\ 0.00000189\ 2000.00000000\ 37.76
DE(b,h): 7.21744000 \ 7.63520000 \ 0.07290343 \ 0.07712323 \ 0.00001781 \ 1.00000000
0.18 DE(f,h) : 5.04380000 4.51880000 0.05094747 0.04564444 0.00002812
2000.00000000\, 562.44\, c_{11}:\, 210.19151749\, 176.10000000\, 0.91814755\, 0.76923077
0.02217621\ 100.00000000\ 22176.21\ c_{33}:\ 273.40612781\ 190.50000000\ 1.10400213
0.76923077\ 0.11207186\ 100.00000000\ 112071.86\ c_{44}:\ 60.02683608\ 50.80000000
0.90894664\ 0.76923077\ 0.01952052\ 100.00000000\ 19520.52\ c_{12}:\ 115.11424042
86.90000000 \ 1.01898062 \ 0.76923077 \ 0.06237499 \ 100.00000000 \ 62374.99 \ c_{13}
: \ 81.44035229 \ 68.30000000 \ 0.91722438 \ 0.76923077 \ 0.02190211 \ 10.00000000
2190.21 \text{ M}_{\text{freq0}}: 2.97521129 \ 2.85858719 \ 0.21683288 \ 0.20833333 \ 0.00007224
0.10000000\,0.07\,\mathrm{M_{freq}}_{1}\colon\,2.97521130\,2.85858719\,0.21683288\,0.20833333\,0.00007224
0.10000000\,0.07\,\mathrm{M_{freq}}{_2}{:}\,\,2.97521130\,2.85858719\,0.21683288\,0.20833333\,0.00007224
0.10000000\,0.07\,\mathrm{M_{freg}3}\colon\,2.97521131\,2.85858719\,0.21683288\,0.20833333\,0.00007224
0.10000000\,0.07\,\mathrm{M_{freq}4:}\,\,6.93944416\,5.66706047\,0.25510889\,0.20833333\,0.00218795
0.10000000\ 2.19\ M_{freq}5\colon 6.93944416\ 5.66706047\ 0.25510889\ 0.20833333\ 0.00218795
0.10000000 \ 2.19 \ H_{freq0}: 4.09232153 \ 4.80643423 \ 0.17738035 \ 0.20833333 \ 0.00095809
0.10000000\,0.96\,H_{freq1}\colon\,4.09232153\,5.58010025\,0.15278704\,0.20833333\,0.00308539
0.10000000 \ 3.09 \ H_{freq2}: 7.87058136 \ 5.65316738 \ 0.29005058 \ 0.20833333 \ 0.00667771
0.10000000\,6.68\,H_{\mathrm{freg}3}\colon\,7.87058136\,6.36651842\,0.25755120\,0.20833333\,0.00242240
0.10000000 \ 2.42 \ H_{freq4}: 9.73498160 \ 6.40050186 \ 0.31686908 \ 0.20833333 \ 0.01178001
0.10000000\ 11.78\ H_{freq5}\colon 9.73498160\ 7.64082373\ 0.26543227\ 0.20833333\ 0.00326029
0.10000000 3.26 bandw. G: 4.99737290 5.87085872 1.41869448 1.66666667
0.06149021 15.00000000 9223.53 bandw. K: 6.15657837 4.97424321 1.12517406
0.90909091 \ 0.04669193 \ 15.00000000 \ 7003.79 \ bandw. M: 6.93890601 \ 7.78109872
```

1.4 TODO Gamma Surfaces for New Model

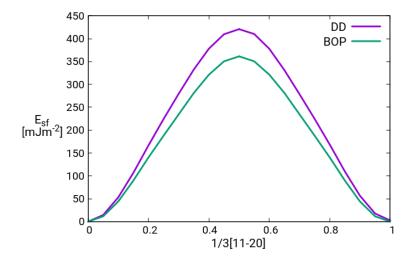
1.4.1 BOP

This was determined using non-periodicity along the z direction.

Initally the number of layers was not enough. This meant that the atoms which were at the interface of the stacking fault actually obtained the information of it's local atomic environment from some the atoms at the free surface, hence why the stacking fault energy was high as the energy from the free surfaces was contributing.

The number of layers was increased to 64 for both the basal and the prismatic stacking fault.

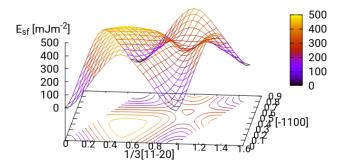
1. Basal gamma line

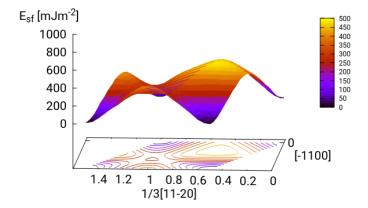


We can see that the gamma line from the bop model is consistently lower than that of the one from the direct-diagonalisation plot. This may be due to the fact that the number of layers in the BOP simulation was much higher (64 compared to 30), so that the actual interaction between the tight-binding fault surfaces under homogeneous shear boundary conditions had more of an effect on the stacking fault energy than the free surfaces in the BOP simulation.

2. Basal Gamma Surfaces

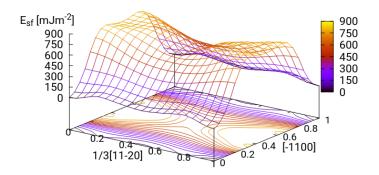
(a) the

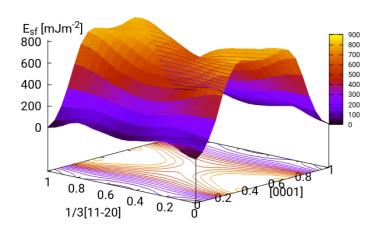




3. Prismatic Gamma Surfaces

(a) the





1.5 Final Model

 $\begin{array}{l} {\rm fdd}{=}0.2648249504\ {\rm qdds}{=}0.5697753882\ {\rm qddp}{=}0.5648597117\ {\rm qddd}{=}0.8213593849\\ {\rm b0}{=}49.75575654\ {\rm p0}{=}1.105068573\ {\rm b1}{=}{-}5.09734161\ {\rm p1}{=}0.6991977165\ {\rm cr2}{=}3.221758936\\ {\rm cr3}{=}{-}1.141827235\ {\rm cr1}{=}{-}6.0\ {\rm ndt}{=}2.0\ {\rm r1dd}{=}6.3741123381\ {\rm rcdd}{=}9.8768388324 \end{array}$

```
rmaxhm=9.9756072207 VARGS -vfdd=0.2648249504 -vqdds=0.5697753882
-vqddp = 0.5648597117 - vqddd = 0.8213593849 - vb0 = 49.75575654 - vp0 = 1.105068573
-vb1 = -5.09734161 - vp1 = 0.6991977165 - vcr2 = 3.221758936 - vcr3 = -1.141827235
-\text{vcr1}=-6.0 - \text{vndt}=2.0 - \text{vr1dd}=6.3741123381 - \text{vrcdd}=9.8768388324 - \text{vrmaxhm}=9.9756072207
    a_{hcp}: 5.55908396 5.57678969 5.55908396 5.57678969 0.00031349 1500.00000000
4702.39 \text{ c/a}: 1.61268131 \ 1.58731122 \ 15.65813964 \ 15.41181168 \ 0.06067746
100.00000000\,60677.46\,\,a_{\mathrm{omega}}:\,8.84739387\,\,8.73254342\,\,1.10592423\,\,1.09156793
0.00020610\ 10.00000000\ 20.61\ c_{\rm omega}\ :\ 5.38456249\ 5.32343103\ 0.67307031
0.66542888 \ 0.00005839 \ 10.000000000 \ 5.84 \ a_{4h} : 5.55471471 \ 5.56325146 \ 0.99846551
1.00000000 \ 0.00000235 \ 1.00000000 \ 0.02 \ c_{4h} : 17.98986999 \ 17.75908031 \ 1.01299559
1.00000000\ 0.00016889\ 1.00000000\ 1.69\ a_{6h}:\ 5.54952123\ 5.54639384\ 1.00056386
1.00000000 \ 0.00000032 \ 1.00000000 \ 0.00 \ c_{6h} : 27.05646584 \ 26.77136353 \ 1.01064953
1.0000000000000113411.0000000001.13 a_{bcc}: 6.276652506.179488630.89666464
0.88278409\ 0.00019267\ 1.000000000\ 1.93\ a_{fcc}:\ 7.83824788\ 7.88677000\ 1.11974970
1.12668143 0.00004805 1.00000000 0.48 DE(o,h): -1.09765167 -0.63343333 -
0.07317678 - 0.04222889 \ 0.00095777 \ 3000.00000000 \ 28733.15 \ DE(4h,h): \ 1.97809750
3.17160000\ 0.00791239\ 0.01268640\ 0.00002279\ 2000.00000000\ 455.82\ DE(6h,h):
2.97676333\ 3.72005000\ 0.01190705\ 0.01488020\ 0.00000884\ 2000.00000000\ 176.79
DE(b,h): 9.826625007.635200000.099258840.077123230.00048999200.000000000
979.97 DE(f,h): 4.48794500 4.51880000 0.04533278 0.04564444 0.00000010
2000.00000000 \ 1.94 \ c_{11} : 180.67966452 \ 176.10000000 \ 0.78923542 \ 0.76923077
0.00040019\ 100.00000000\ 400.19\ c_{33}:\ 206.14770273\ 190.50000000\ 0.83241552
0.76923077 \ 0.00399231 \ 100.00000000 \ 3992.31 \ c_{44} : 48.30576681 \ 50.80000000
0.73146225 \ 0.76923077 \ 0.00142646 \ 100.00000000 \ 1426.46 \ c_{12} : \ 95.22633084
86.90000000\ 0.84293468\ 0.76923077\ 0.00543227\ 100.00000000\ 5432.27\ c_{13}
: 66.46772326 \ 68.30000000 \ 0.74859470 \ 0.76923077 \ 0.00042585 \ 50.000000000
212.92 \ \mathrm{M_{freq0}}; \ \ 2.52855122 \ \ 2.85858719 \ \ 0.18428037 \ \ 0.20833333 \ \ 0.00057855
0.10000000\,0.58\,M_{\rm freq1}\colon\,2.52855123\,\,2.85858719\,\,0.18428037\,\,0.20833333\,\,0.00057855
0.10000000\,0.58\,\mathrm{M_{freq}}{}_{2}{}^{:}\,\,2.52855123\,2.85858719\,0.18428037\,0.20833333\,0.00057855
0.10000000\,0.58\,\mathrm{M_{freg}3}\colon\,2.52855124\,2.85858719\,0.18428037\,0.20833333\,0.00057854
0.10000000\,0.58\,\mathrm{M_{freq}}_{4}\colon\,5.59220819\,5.66706047\,0.20558160\,0.20833333\,0.00000757
0.10000000\ 0.01\ \mathrm{M_{freq5}}\colon 5.59220819\ 5.66706047\ 0.20558160\ 0.20833333\ 0.00000757
0.10000000 \ 0.01 \ H_{freq0}: 3.57525560 \ 4.80643423 \ 0.15496829 \ 0.20833333 \ 0.00284783
0.10000000\ 2.85\ H_{freq1}\colon\ 3.57525560\ 5.58010025\ 0.13348235\ 0.20833333\ 0.00560267
0.10000000 \, 5.60 \, H_{freq} \, 2: 6.11165910 \, 5.65316738 \, 0.22522990 \, 0.20833333 \, 0.00028549
0.1000000000.29 H_{freg3}: 6.111659106.366518420.199993500.208333330.00006955
0.10000000\,0.07\,H_{\rm freq4}\colon\,7.75488320\,6.40050186\,0.25241781\,0.20833333\,0.00194344
0.100000001.94 H_{frea5}: 7.754883207.640823730.211443260.208333330.00000967
0.10000000 0.01 bandw. G: 5.03138714 5.87085872 1.42835071 1.66666667
0.05679449 1.00000000 567.94 bandw. K: 6.21236174 4.97424321 1.13536901
```

- 1.6 TODO Write first section of Literature review
- 1.6.1 TODO Summarise Stacking Faults and write review
- 1.6.2 TODO Write up the tight binding fitting of oxygen and an explanation for paramagnetism.
- 1.6.3 TODO Summarise dislocations and Oxygen interactions (review)
- 1.7 TODO See how the PDOS changes with addition of oxygen and how the tetrahedral/octahedral sites change this.
- 1.8 TODO Calculate solution enthalpy of oxygen in titanium.
 - The solution enthalpy $E_{\rm sol}$ and excess volume ΔV is

$$E_{\text{sol}=E(\text{Ti}_n\text{O})-E(\text{Ti}_n)-E(O)}$$

$$\Delta V = V(\mathrm{Ti}_n\mathrm{O}) - V(\mathrm{Ti}_n)$$

- $E(\text{Ti}_n\text{O})$ is the excess energ of the bulk supercell with n Ti atoms and one impurity atom. $E(\text{Ti}_n)$ is the energy of the pure cells.
- Influence of cell sizes and solution enthalpy needs to be considered.
- 1.9 TODO Has anyone investigated the stacking faults of Omega phase?
 - Maybe as Omega phase doesn't occur that often, perhaps it has not been studied in detail.
 - I should look further into thsi

1.10 TODO Finish doing the gamma surfaces for all planes for pure titanium.

1.10.1 Checking the convergence criteria

- Now checking the convergence criteria.
- 1. How the lattice parameters change with the fineness of the k mesh
 - Maybe with a less fine k mesh the lattice parameters become worse.
 - SOLUTION: The lattice parameters do not change that much under

differences with the k mesh. File with change of the lattice parameters with k mesh. a vs nk c_{vsnk} e_{vsnk}

- (a) What if rmaxh is smaller or larger?
 - If rmaxh is is smaller (say rmaxh = 6.7 bohr) then we get the same results.

Variation of total energy of hcp at minimum lattice parameters with nk

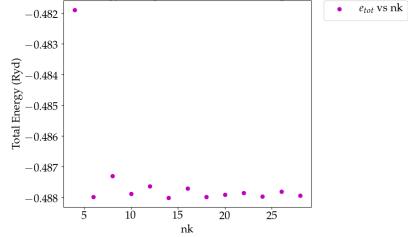


Figure 1: Variation of energy with k mesh.

]]

 $\bullet\,$ Data: a_{hcp} small rmaxh, c_{hcp} small rmaxh, e_{hcp} small rmaxh.

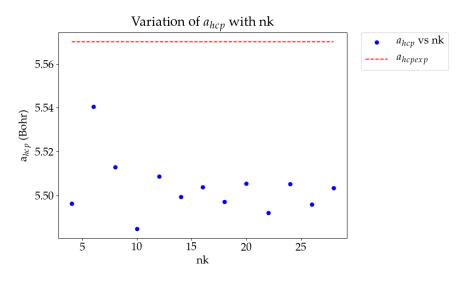


Figure 2: Variation of a hcp with k mesh.

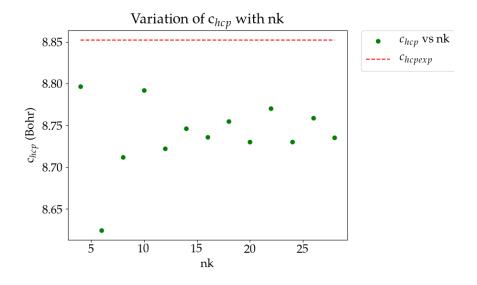


Figure 3: Variation of c hcp with k mesh.

• If rmaxh is larger (rmaxh = 20 bohr), all possible interactions must be included then. And so we get the same results.

of total energy of hcp at minimum lattice parameters.

-0.488

-0.490

-0.492

-0.494

5 10 15 20 25

Figure 4: Variation of energy with k mesh.

- \bullet Data: a_{hcp} large rmaxh, c_{hcp} large rmaxh, e_{hcp} large rmaxh
- 2. How does rmaxh change the lattice parameters?
 - (a) How does rmaxh change the energy of a supercell
 - How does the number of neighbours change and what is the relation between rmaxh and larger cell sizes.

1.10.2 Notes on the model.

It seems that there is a lot of charge moving around when doing the relaxations. I think that this may be due to the fact that there is no Hubbard U interactions, a parameter for the coulomb interaction, which stops the charges from moving freely.

• TBE control file is currently set to this:

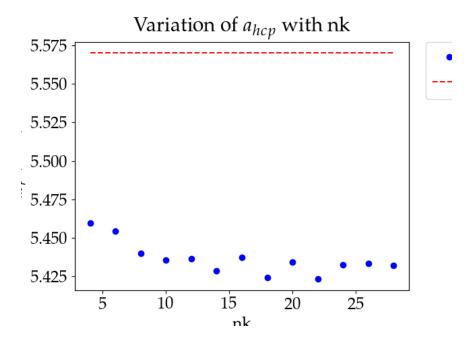


Figure 5: Variation of a hcp with k mesh.

1.10.3 DONE Implement Homogenous Shear boundary conditions for gamma surface calculation.

2 Notes

2.1 Dislocation dipole simulation

<2019-03-29 Fri> It seems that actually, for the Clouet method, the x component for the accommodation of strain is *positive*. These additions to the tilt vectors make the dislocations in a stable position in the quadrupolar array.

There is no asymmetry in relaxations now between the dislocations of different sign. This now works as expected.

2.2 Embedded atom method

This is a semi empirical method that does not take into account directional bonding. It does not treat covalency or charge transfer. Neither does it incorporate Fermi surface effects.

The main physical property incorporated in the EAM is the moderation

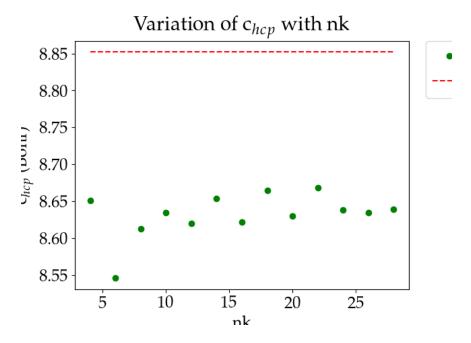


Figure 6: Variation of c hcp with k mesh.

of bond strength by other bonds (coordination-dependent bond strength).

3 Completed Tasks

ARCHIVE

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 morphologies and mechanisms. International Journal of Materials
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5 Current Papers

5.1 Omega phase transformation – morphologies and mechanisms.

Banerjee, S., Tewari, R., & Dey, G. K. (2006). International Journal of Materials Research, 97(7), 963–977. doi:10.3139/146.101327 [10]

Omega is found in both trigonal and perfect (hexagonal) forms.

Positions are: A: 0. 0. 0. B: 2/3 1/3 (1/2-z); 1/3 2/3 (1/2+z)

Where z = 1/6 is cubic symmetry.

The two atomic sites in the omega unit cell are not equivalent. B-type atomic sites are more closely packed as compare to the A-type atomic site.