



Aktorik und Sensorik mit intelligenten Materialsystemen 4

ASIM 4 Final Exam Assignment: SMA Actuated Wing

Gianluca Rizzello

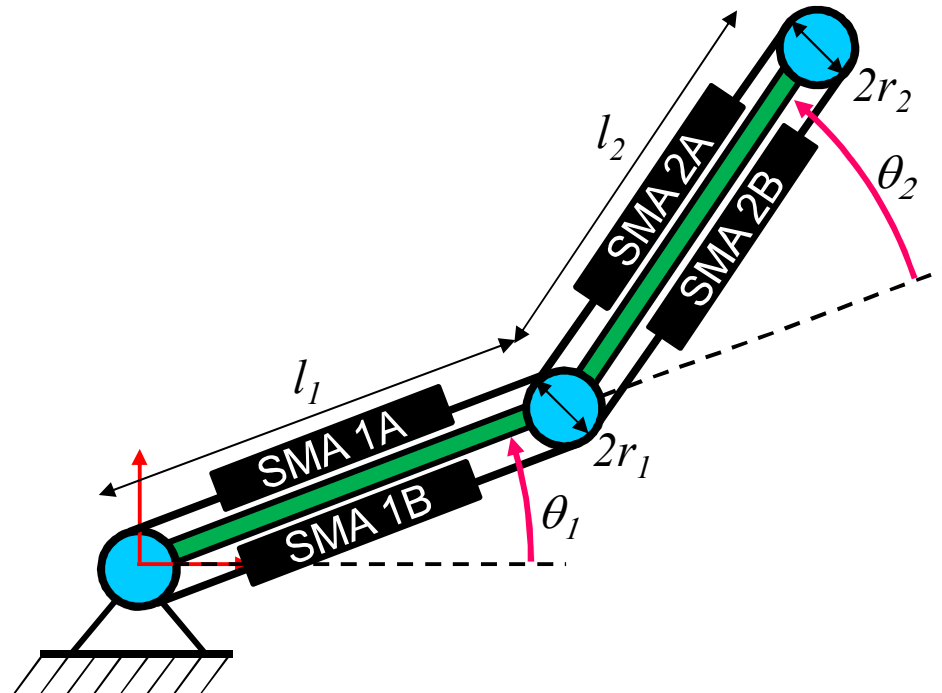
gianluca.rizzello@mmsl.uni-saarland.de

Saarland University



ASIM 4 Final Exam: SMA Wing

- System layout: two **rigid rods** of lengths l_1 and l_2 are connected through two **rotational joints** of radii r_1 and r_2 , and actuate by bundles of **SMA** wire actuators
- By controlling the Joule heating of the SMA wires, rotation angles of both joints θ_1 and θ_2 can be controlled

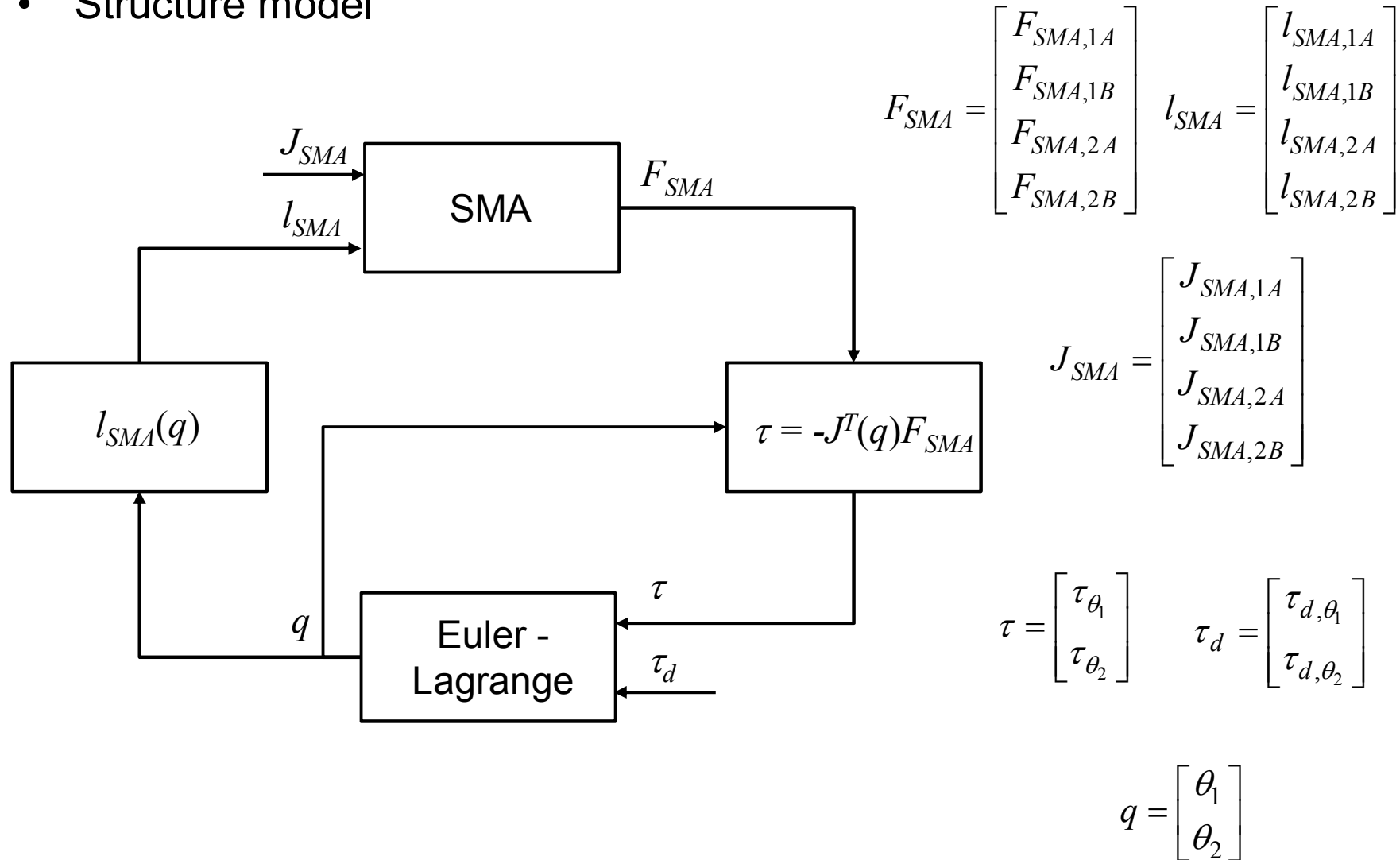




- Project guidelines:
 - Study the effects of control inputs $J_{SMA,1A}$, $J_{SMA,1B}$, $J_{SMA,2A}$, and $J_{SMA,2B}$ on the actuator performance, in terms of θ_1 and θ_2 , with all Joule heating signals limited between 0 and 2 W;
 - Define control inputs u_1 and u_2 , such that
 - if $u_1 \geq 0$ then $J_{SMA,1A} = |u_1|$, $J_{SMA,1B} = 0$
 - if $u_1 < 0$ then $J_{SMA,1A} = 0$, $J_{SMA,1B} = |u_1|$
 - if $u_2 \geq 0$ then $J_{SMA,2A} = |u_2|$, $J_{SMA,2B} = 0$
 - if $u_2 < 0$ then $J_{SMA,2A} = 0$, $J_{SMA,2B} = |u_2|$
 - Find a linear approximation of the responses between u_2 and θ_2 (for $u_1 = 0$),
 - Design and compare linear controllers for position regulation of θ_2
 - Design and compare linear controllers for trajectory tracking of θ_2
 - Compare linear and nonlinear controllers for θ_2
 - Repeat the above identification/control steps for the $u_1 - \theta_1$ response (with $u_2 = 0$)
 - Test the performance of both controllers when they work together to control θ_1 and θ_2 at the same time
 - Compare continuous-time and discrete time controllers obtained with different sampling times and discretization methods, as well as the effects of anti-windup
 - Test the control system response when disturbed τ_d are affecting the actuators
 - Test the control system response when environmental temperature T_E is changing
 - Compare sensor-based and sensorless control based on resistance signals



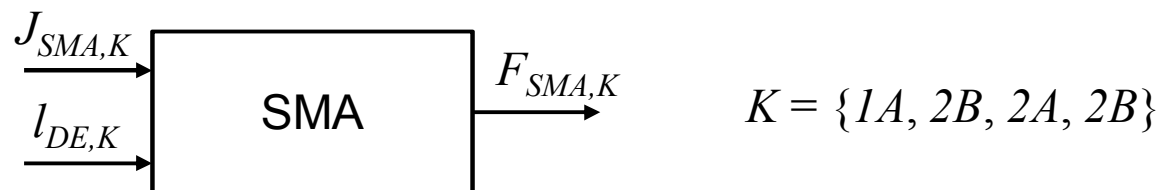
- Structure model





- SMA bundle model

$$\left\{ \begin{array}{l} \dot{T}_{SMA,K} = -\frac{\lambda A_s}{m C_v} (T - T_E) + \frac{1}{m C_v N} J_{SMA,K} + \frac{VH_+}{m C_v} (-x_{+,SMA,K} p^{+A} + (1 - x_{+,SMA,K}) p^{A+}) \\ \dot{x}_{+,SMA,K} = -x_{+,SMA,K} p^{+A} + (1 - x_{+,SMA,K}) p^{A+} \\ F_{SMA,K} = N \pi r_0^2 \frac{\frac{l_{SMA,K} - l_0}{l_0} - \varepsilon_T x_{+,SMA,K}}{\frac{x_{+,SMA,K}}{E_M} + \frac{1 - x_{+,SMA,K}}{E_A}} \end{array} \right.$$





- Kinematic model

$$l_{SMA}(q) = \begin{bmatrix} l_{SMA,1A}(q) \\ l_{SMA,1B}(q) \\ l_{SMA,2A}(q) \\ l_{SMA,2B}(q) \end{bmatrix} = \begin{bmatrix} l_0 + \Delta - r_1 \theta_1 \\ l_0 + \Delta + r_1 \theta_1 \\ l_0 + \Delta - r_2 \theta_2 \\ l_0 + \Delta + r_2 \theta_2 \end{bmatrix}$$

- Jacobian matrix

$$J(q) = \frac{\partial l_{SMA}(q)}{\partial q} = \begin{bmatrix} \frac{\partial l_{SMA,1A}}{\partial \theta_1} & \frac{\partial l_{SMA,1A}}{\partial \theta_2} \\ \frac{\partial l_{SMA,1B}}{\partial \theta_1} & \frac{\partial l_{SMA,1B}}{\partial \theta_2} \\ \frac{\partial l_{SMA,2A}}{\partial \theta_1} & \frac{\partial l_{SMA,2A}}{\partial \theta_2} \\ \frac{\partial l_{SMA,2B}}{\partial \theta_1} & \frac{\partial l_{SMA,2B}}{\partial \theta_2} \end{bmatrix} = \begin{bmatrix} -r_1 & 0 \\ r_1 & 0 \\ 0 & -r_2 \\ 0 & r_2 \end{bmatrix}$$



- Kinetic energy

$$\begin{aligned} \mathcal{T}(q, \dot{q}) &= \frac{1}{2} m_1 \left[\left(-\frac{l_1}{2} \dot{\theta}_1 \sin(\theta_1) \right)^2 + \left(\frac{l_1}{2} \dot{\theta}_1 \cos(\theta_1) \right)^2 \right] + \frac{1}{2} I_1 \dot{\theta}_1^2 \\ &\quad + \frac{1}{2} m_2 \left[\left(-l_1 \dot{\theta}_1 \sin(\theta_1) - \frac{l_2}{2} (\dot{\theta}_1 + \dot{\theta}_2) \sin(\theta_1 + \theta_2) \right)^2 + \left(l_1 \dot{\theta}_1 \cos(\theta_1) + \frac{l_2}{2} (\dot{\theta}_1 + \dot{\theta}_2) \cos(\theta_1 + \theta_2) \right)^2 \right] + \frac{1}{2} I_2 \dot{\theta}_2^2 \\ &= \frac{1}{2} m_1 \frac{l_1^2}{4} \dot{\theta}_1^2 + \frac{1}{2} I_1 \dot{\theta}_1^2 + \frac{1}{2} m_2 \left(l_1^2 \dot{\theta}_1^2 + \frac{l_2^2}{4} (\dot{\theta}_1 + \dot{\theta}_2)^2 + l_1 l_2 (\dot{\theta}_1^2 + \dot{\theta}_1 \dot{\theta}_2) \cos(\theta_2) \right) + \frac{1}{2} I_2 \dot{\theta}_2^2 \end{aligned}$$

- Potential energy

$$\mathcal{V}(q) = 0$$

- Lagrangian

$$\mathcal{L}(q, \dot{q}) = \mathcal{T}(q, \dot{q}) - \mathcal{V}(q) = \frac{1}{2} m_1 \frac{l_1^2}{4} \dot{\theta}_1^2 + \frac{1}{2} I_1 \dot{\theta}_1^2 + \frac{1}{2} m_2 \left(l_1^2 \dot{\theta}_1^2 + \frac{l_2^2}{4} (\dot{\theta}_1 + \dot{\theta}_2)^2 + l_1 l_2 \dot{\theta}_1 (\dot{\theta}_1 + \dot{\theta}_2) \cos(\theta_2) \right) + \frac{1}{2} I_2 \dot{\theta}_2^2$$



- Euler-Lagrange model

$$M(q)\ddot{q} + C(q, \dot{q}) = \tau - B\dot{q} + \tau_d$$

- Definition of above quantities

$$M(q) = \begin{bmatrix} m_1 \frac{l_1^2}{4} + I_1 + m_2 l_1^2 + m_2 \frac{l_2^2}{4} + m_2 l_1 l_2 \cos(\theta_2) & m_2 \frac{l_2^2}{4} + \frac{1}{2} m_2 l_1 l_2 \cos(\theta_2) \\ m_2 \frac{l_2^2}{4} + \frac{1}{2} m_2 l_1 l_2 \cos(\theta_2) & m_2 \frac{l_2^2}{4} + I_2 \end{bmatrix}$$

$$C(q, \dot{q}) = \begin{bmatrix} -m_2 l_1 l_2 \left(\dot{\theta}_1 \dot{\theta}_2 + \frac{\dot{\theta}_2^2}{2} \right) \sin(\theta_2) \\ \frac{1}{2} m_2 l_1 l_2 \dot{\theta}_1^2 \sin(\theta_2) \end{bmatrix}$$
$$B = \begin{bmatrix} b_1 & 0 \\ 0 & b_2 \end{bmatrix}$$



- Complete model in compact form

$$\begin{cases} \dot{T}_{SMA,K} = -\frac{\lambda A_s}{mC_v} (T - T_E) + \frac{1}{mC_v N} J_{SMA,K} + \frac{VH_+}{mC_v} \left(-x_{+,SMA,K} p^{+A} + (1 - x_{+,SMA,K}) p^{A+} \right), & K \in \{1A, 1B, 2A, 2B\} \\ \dot{x}_{+,SMA,K} = -x_{+,SMA,K} p^{+A} + (1 - x_{+,SMA,K}) p^{A+}, & K \in \{1A, 1B, 2A, 2B\} \\ \dot{q} = v \\ \dot{v} = M^{-1}(q) \left(-G(q, v) - J^T(q) F_{SMA}(l_{SMA,K}(q), x_{+,SMA,K}) - Bv + \tau_d \right) \end{cases}$$

- Inverse of inertia matrix

$$M^{-1}(q) = \frac{1}{\det(M(q))} \begin{bmatrix} m_2 \frac{l_2^2}{4} + I_2 & -m_2 \frac{l_2^2}{4} - \frac{1}{2} m_2 l_1 l_2 \cos(\theta_2) \\ -m_2 \frac{l_2^2}{4} - \frac{1}{2} m_2 l_1 l_2 \cos(\theta_2) & m_1 \frac{l_1^2}{4} + I_1 + m_2 l_1^2 + m_2 \frac{l_2^2}{4} + m_2 l_1 l_2 \cos(\theta_2) \end{bmatrix}$$

$$\det(M(q)) = m_1 m_2 \frac{l_1^2 l_2^2}{16} + m_2^2 \frac{l_1^2 l_2^2}{4} (1 - \cos^2(\theta_2)) + I_1 m_2 \frac{l_2^2}{4} + m_1 I_2 \frac{l_1^2}{4} + I_1 I_2 + m_2 I_2 l_1^2 + m_2 I_2 \frac{l_2^2}{4} + m_2 I_2 l_1 l_2 \cos(\theta_2)$$