ENGG 201 – Kinetic Theory Flux Examples

Chapter 5 – Example #1 - Mass

A cubical container (1 m wide, 2 m deep, 3 m high) is filled with nitrogen gas at 300K and 1 atm. One wall of the container (2 m by 3 m) is made of a thin semi-permeable plastic sheet, which allows oxygen to pass through. The concentration of oxygen just inside the plastic is 0.01 kmol/m³, and the diffusivity of oxygen in nitrogen is 1.521x10⁻⁵m²/s.

- (a) Use this information to estimate the collision diameter of oxygen ().
- (b) Calculate the diffusivity of oxygen in nitrogen at 400K and 2 atm (m²/s).
- (c) Calculate the diffusion flux of oxygen through the container (i.e. from the plastic wall to the opposite wall) at 300K and 1 atm (kmol/m²s).
- (d) Determine the amount of oxygen that would be transported in 2 h through the plastic at 300K and 1 atm (kg), assuming that the flux remains the same as calculated in c).

Ans. (a) 3.67

(b) $1.17x10^{-5}m^2/s$ (c) $1.52x10^{-7}kmol/m^2s$

(d) 0.210kg

$$D_{AA} = \frac{RT}{PN_A \pi \sigma^2} \sqrt{\frac{RT}{\pi M}}$$

Chapter 5 –Example #2 – Heat

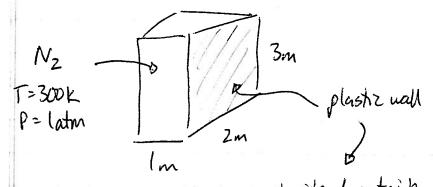
Two infinite slabs are separated by a distance of 10 cm and argon gas (M=39.95 kg/kmol) at low pressure is held between them. One slab is maintained at a constant temperature of 350 K while the other slab is held at 330K. The molecular diameter of the Argon molecule is 3.5 angstroms. Calculate:

- (a) The constant volume heat capacity of Argon (in J/mole K).
- (b) The thermal conductivity of the Argon (in W/m K) at an average temperature of 340K.
- (c) The heat flux (Q/A) occurring between the two slabs using Fourier's Law and an average thermal conductivity as calculated in part (b) above. Report the heat flux in W/m².

Ans.

(a) 12.47 J/mol. K (b) $8x10^{-3} \text{ W/m.} K$ (c) 1.6 W/m^2 .

Chapter 5 - Example #1 - Mass Flux



Doyler = 1.50x 10-5 mg/s

$$C_{02} = 0.01 \frac{\text{kmod}}{\text{m}^3}$$

a)
$$D = \frac{RT}{PNA \pi \sigma^2} \sqrt{\frac{RT}{\pi M}}$$

b)
$$D \propto \frac{T^{3/2}}{P}$$
 $D_{i} \propto \frac{T_{i}^{3/2}}{P_{i}}$

$$D_{i} \propto \frac{T_{i}^{3/2}}{P_{i}}$$

$$\frac{D_2}{D_1} = \frac{T_2^{3/2} P_1}{T_1^{3/2} P_2} = \frac{(400 \, \text{k})^{3/2}}{(300 \, \text{k})^{3/2}} \frac{(01.3254 \text{kg})}{202.65 \, \text{kg}} = 0.7698$$

$$D_2 = 1.521 \times 10^{-5} \frac{m^2}{5} \times 0.7698 = \boxed{1.17 \times 10^{-5} \frac{m^2}{5}}$$

Flux
$$\frac{1}{3m}$$
 $\frac{1}{2m}$ $\frac{1}$

d)
$$j_{02} = \frac{\Lambda}{A \pm}$$
 $- \delta$ $\Lambda = j_{02} A \pm$

$$\Lambda = (1.521 \times 10^{-7} \frac{land}{m^2 s})(6 m^2)(2 h \times 3600 \frac{s}{h})$$
Flux area = $2 \times 3 m$ $\Lambda = 6.57 \times 10^{-3} \frac{land}{m^2 s}$

$$M = 1 M$$

 $M = 6.57 \times 10^{-3} \text{ kmd} \times 32 \frac{\text{lcs}}{\text{kmd}}$
 $M = 0.210 \text{ kg}$

Chapter 5 - Example #2 - Heat Flux

$$T = 350K$$
 $T = 330K$
 $T =$

a)
$$C_V = \frac{3}{2}R$$
 for ideal gas
$$C_V = \frac{3}{2}8.314 \, kJ / land \, k = [12.471 \, kJ / land \, k]$$

c)
$$\frac{Q}{A} = -k \frac{dT}{dx} = -8.07 \times 10^{-3} \frac{W}{MK} \frac{330 K - 350 K}{10 \times 10^{-2} m}$$