THE UNIVERSITY OF CALGARY Schulich School of Engineering

ENGG 202 – Engineering Statics Second Midterm Exam March 28, 2017

- 1. The examination is closed textbook
- 2. There are 2 comprehensive questions and 4 multiple-choice questions. Answer all questions directly on the question sheets.
- 3. Only the SSE sanctioned, non-programmable, scientific calculators are permitted.
- 4. **Free body diagrams are required** on all long-answer **equilibrium** questions to obtain full marks. Diagrams must be separate from the given figure.

DO NOT OPEN THE EXAM BOOKLET UNTIL INSTRUCTED TO DO SO

Student's l	Last name:		
Student's l	First name:		
Lecture Se	ction (Circle C	ne):	
L01	TuTh	8:00	Di Martino
L02	MWF	9:00	Epstein
L03	MWF	8:00	Epstein
L04	MWF	15:00	Не

Student ID#:

TRIGONOMETRIC FORMULAE:

Sine Law:
$$\frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$$

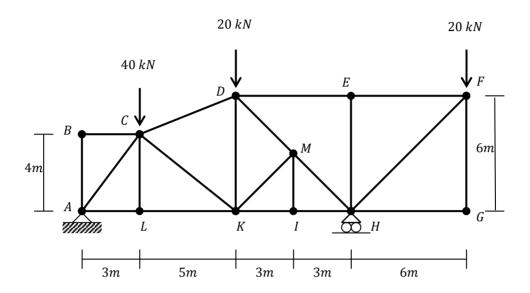
Cosine Law:
$$c^2 = a^2 + b^2 - 2ab\cos C$$

Question	Maximum mark	Mark
Q1	11	
Q2	11	
Q3	8	
Total	30	

Q1.

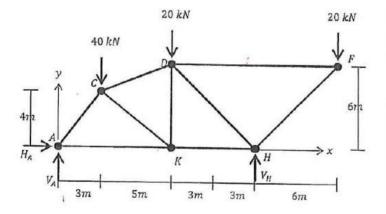
For the truss and loading shown:

- (a) Identify all the zero-force members;
- (b) Using the method of joints, determine the internal forces in all the bars;
- (c) Using the method of sections, verify the results obtained for members CK and HM.



Solution:

- (a) Zero-force members: AB, BC, CL, IM, KM, EH, GH, EF, GF.
- (b) This part should be considered as independent from part (a), whether the student implements or doesn't implement the zero-force members. Below is the FBD of the



Equilibrium equations are:

truss devoid of the zero-force members, but a long solution with all the original nodes is also acceptable.

Find reactions at supports
[Note: in theory, the reactions are not needed for this part, but I don't think there will be a single student that would think they aren't. Moreover, the reactions are indeed needed for part (c)]

$$\Sigma F_{x} = H_{A} = 0$$

$$\Sigma F_{y} = V_{A} + V_{H} - 40 \ kN - 20 \ kN - 20 \ kN = 0$$

$$\Sigma M_{A} = -(40kN)(3m) - (20kN)(8m) - (20kN)(20m) + V_{H}(14m) = 0$$

Solving, we obtain

$$H_A = 0$$
 $V_A = 31.43 \, kN$ (as shown) $V_H = 48.57 \, kN$ (as shown)

FBDs of individual nodes

NODE F

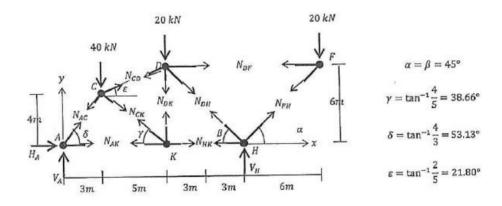
$$\Sigma F_{y} = -20kN - N_{EH} \sin 45^{\circ} = 0 \qquad \therefore \qquad N_{FH} = -28.28 \ kN \ \ (compr.)$$

$$\Sigma F_{x} = -N_{DF} - N_{FH} \cos 45^{\circ} = 0 \qquad \therefore \qquad N_{DF} = 20.00 \ kN \ \ (tension)$$

NODE H

$$\Sigma F_{y} = N_{FH} \sin 45^{\circ} + N_{DH} \sin 45^{\circ} + V_{H} = 0$$
 : $N_{DH} = -40.41 \, kN \, (compr.)$

$$\Sigma F_x = -N_{HK} - N_{DH} \cos 45^\circ + N_{FH} \cos 45^\circ = 0$$
 : $N_{HK} = 8.58 \, kN$ (tension)



NODE A

$$\Sigma F_y = N_{AC} \sin \delta + V_A = 0$$
 : $N_{AC} = -39.29 \, kN \, (compr.)$

$$\Sigma F_x = H_A + N_{AK} + N_{AC} \cos \delta = 0$$
 : $N_{AK} = 23.57 \text{ kN} \text{ (tension)}$

NODE K

$$\Sigma F_{x} = -N_{AK} + N_{HK} - N_{CK} \cos \gamma = 0 \quad \therefore \quad N_{CK} = -19.19 \ kN \ (compr.)$$

$$\Sigma F_{y} = N_{CK} \sin \gamma + N_{DK} = 0 \quad \therefore \quad N_{DK} = 12.00 \ kN \ (tension)$$

NODE D

$$\Sigma F_x = N_{DF} + N_{DH} \cos 45^\circ - N_{CD} \cos \varepsilon = 0$$
 : $N_{CD} = -9.23 \, kN \, (compr.)$

We have now the forces in all bars. Let us verify the satisfaction of the 3 extra equilibrium equations:

At Node D we have

$$\Sigma F_y = -20 kN - N_{DK} - N_{DH} \sin 45^\circ - N_{CD} \sin \varepsilon = 0.002 kN$$

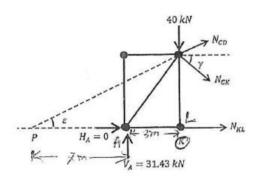
At node C:

$$\Sigma F_x = N_{CD}\cos\varepsilon + N_{CK}\cos\gamma - N_{AC}\cos\delta = 0.019 \ kN$$

$$\Sigma F_y = -40 \ kN - N_{AC}\sin\delta - N_{CK}\sin\gamma + N_{CD}\sin\varepsilon = -0.008 \ kN$$

(c) Method of sections

BAR CK



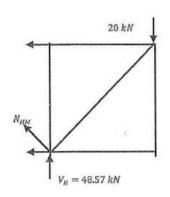
$$PK = \frac{4m}{\tan \varepsilon} = 10.00m$$

$$\Sigma M_P = -(40kN)(10m) + (31.43kN)(7m) - N_{CR}\sin\gamma (10m) - N_{CR}\cos\gamma (4m) = 0$$

Solving, we get

$$N_{CK} = -19.21 \, kN \, (compr.)$$

BAR HM



$$\Sigma F_y = -20kN + 48.57 + N_{HM} \sin 45^\circ = 0$$

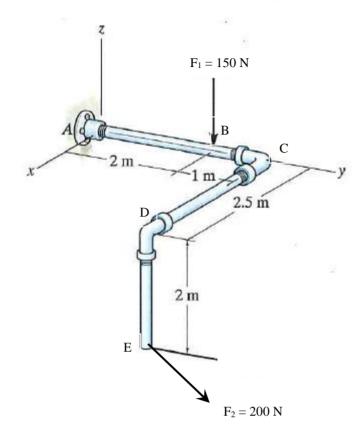
Thus, $N_{HM} = -40.40 \ kN \ (compr.)$

Notice that this force is the same as N_{DH}

Points: /11

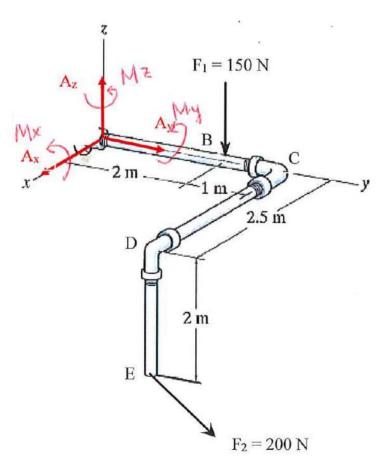
Q2.

Determine the support reactions at the fixed support at point A. The force F_1 of a magnitude of 150 N acting at point B is parallel to the z-axis. The 200 N force, F_2 , acting at point E is in the direction of the unit vector of $0.6 \mathbf{i} + 0.6 \mathbf{j} - 0.53 \mathbf{k}$.



Solution:

Free body diagram



- Calculation of resultant force
$$\vec{F_1} = -130 \, \text{K} \quad N$$

$$\vec{F_2} = \vec{F_2} \, \vec{n} = 200 \, \left(0.6 \, \hat{i} + 0.6 \, \hat{j} - 0.53 \, \text{K}\right)$$

$$= 120 \, \hat{i} + 120 \, \hat{j} - 106 \, \text{K} \quad N$$

$$\vec{F_A} = Ax \, \hat{i} + Ay \, \hat{j} + Az \, \text{K} \quad N$$

$$\Sigma F_{x} = 0$$
: $|20 + A_{x} = 0| = 7 A_{x} = -120 N$

$$IFy = 0:$$
 $120 + Ay = 0 \Rightarrow Ay = -120N$

$$\overline{Y}_{AE} = (2.5-0)\vec{i} + (3-0)\vec{j} + (-2-0)\vec{k}$$

$$= 2.5\vec{i} + 3\vec{i} - 2\vec{k} \quad m$$

$$\widetilde{M}_{2} = \widetilde{Y}_{AE} \times \widetilde{F}_{2} = (z_{5}i + 3j - z_{K}) \times (|z_{0}i + |z_{0}j - |0_{6}K)$$

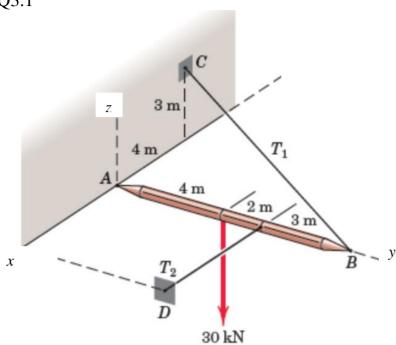
$$= \begin{vmatrix} i & j & k \\ z_{5} & 3 & -z \\ |z_{0}| & |z_{0}| & -|o_{6}| \end{vmatrix}$$

$$= \begin{vmatrix} 3 & -2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} - \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 3 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^{\frac{7}{3}} + \begin{vmatrix} z_{1}5 - 2 \\ |z_{0} - 106 \end{vmatrix}^$$

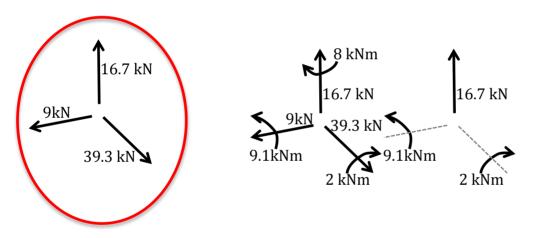
The reaction for cost A $\vec{F}_A = A \times \vec{i} + A y \vec{j} + A \vec{z} \vec{K} = -120 \vec{i} - 120 \vec{j} + 256 \vec{K} N$ $\vec{F}_A = \int (-120)^2 + (-120)^2 + 256^2 = 307.14 N$ The reaction couple at A $\vec{M}_A = M_A \times \vec{i} + M_A y \vec{j} + M_A \times \vec{K} = 378 \vec{i} - 25 \vec{j} + 60 \vec{K} N - M$ $M_A = \int 378^2 + (-25)^2 + 60^2 = 383.55 N - M$

Q3.

Q3.1



For the ball-and-socket support shown at point A in the picture above what are the correct support reactions? (Circle the correct one)

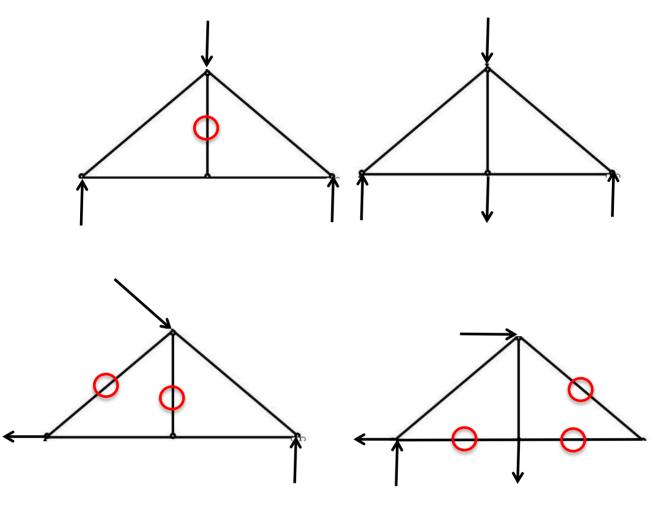


Q3.2

Which statement is true (choose only one):

- a) A two-force member is a member loaded by a force and a couple
- b) A two-force member is subjected to forces and couples at two points
- c) A two-force member is a member with no internal force
- d) None of the above

Q3.3 Identify the zero-force members in the following trusses (circle all zero-force members):



Q3.4

Which statement is true (choose only one):

- (a) A roller in 3D provides two support reactions
- b) A roller in 3D provides one support reaction
 - c) A roller is equivalent to a ball-and-socket joint
 - d) None of the above

Note: In Q3.4, both a) and b) are correct.

Points: /8