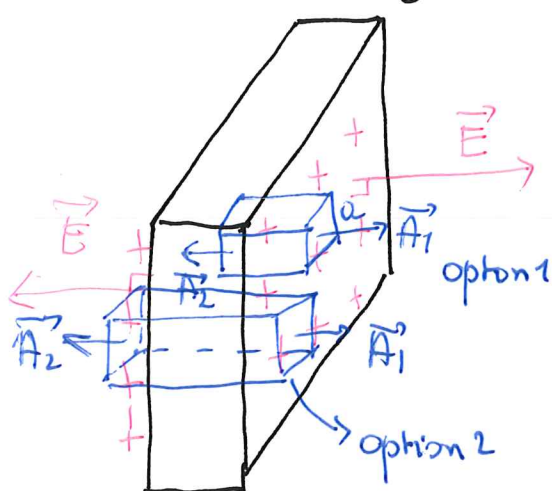


Find E-field due to the conducting plate

Q

$$\sigma = \frac{Q}{2L^2}$$

$$\sigma = \frac{Q}{\text{Area}}$$



Option 1

$$\oint \vec{E} \cdot d\vec{A} = \frac{q_{\text{enc}}}{\epsilon_0}$$

$$\Phi_E = \int_{\text{front face}} \vec{E} \cdot \vec{A}_1 + \int_{\text{back face}} \vec{E} \cdot \vec{A}_2 + \int_{\text{Sides}} \vec{E} \cdot d\vec{A}$$

inside the conductor

$$\Phi_E = E \cdot A_1 = E \cdot a^2$$

$$q_{\text{enc}} = \sigma \cdot a^2$$

$$E \cdot a^2 = \frac{\sigma \cdot a^2}{\epsilon_0}$$

$$E = \frac{\sigma}{\epsilon_0}$$

Option 2

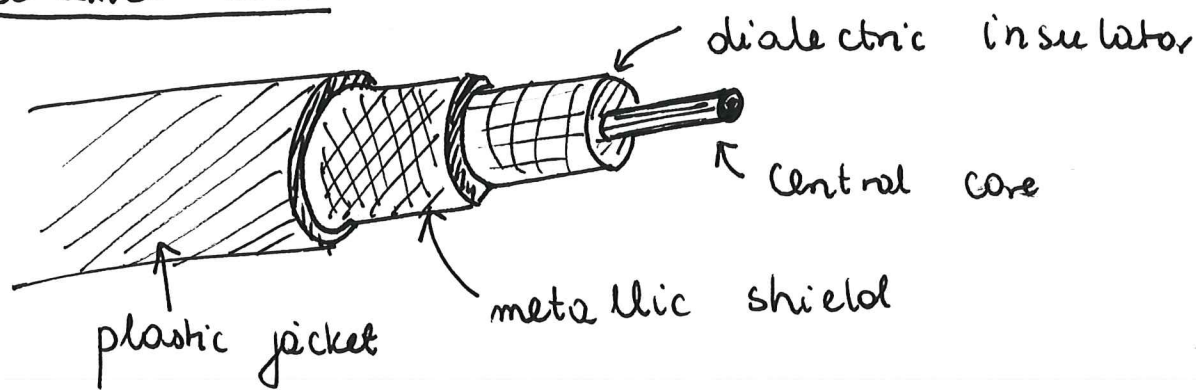
$$\Phi_E = \int_{\text{front}} \vec{E} \cdot \vec{A}_1 + \int_{\text{back}} \vec{E} \cdot \vec{A}_2 = E \cdot a^2 + E \cdot a^2 = 2E \cdot a^2$$

$$q_{\text{enc}} = 2 \cdot \sigma \cdot a^2$$

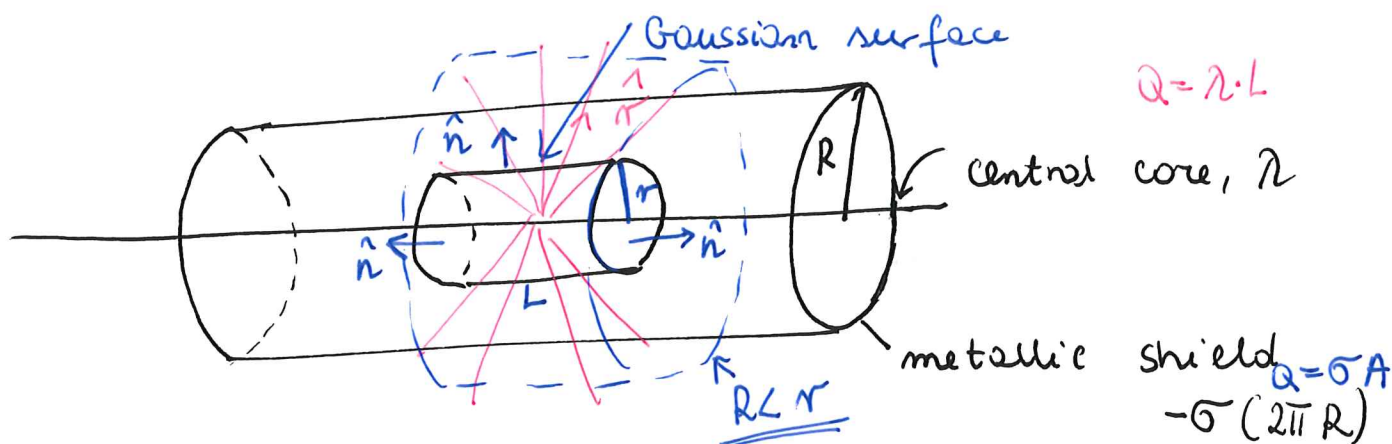
$$2Ea^2 = 2\sigma a^2 / \epsilon_0$$

$$E = \frac{\sigma}{\epsilon_0}$$

# Co-axial cable



Ignore the dielectric insulator and plastic jacket.



In a given length  $L$  of the coaxial cable, the central core carries  $+Q = \lambda L$  and the metallic shield carries  $-Q = -\sigma(2\pi RL)$ .

INSIDE METALLIC SHIELD  $r < R$

Symmetry: the  $E$ -field can only point radially (assuming cable is infinite) and must be constant magnitude at constant radius  $\Rightarrow$  cylindrical Gaussian surface.

$$\oint \vec{E} \cdot d\vec{A} = \int_{\text{cup 1}} \vec{E} \cdot d\vec{A} + \int_{\text{cup 2}} \vec{E} \cdot d\vec{A} + \int_{\text{tube}} \vec{E} \cdot d\vec{A} = E \cdot 2\pi r \cdot L$$

$$q_{\text{enc}} = \lambda \cdot L$$

$$\Rightarrow E \cdot 2\pi r \cdot L = \lambda \cdot L \quad E = \frac{\lambda}{2\pi \epsilon_0 r} \quad \text{for } r < R$$

Inside the cable, the field is that of a line of charge  $\lambda$  from the central core.

## OUTSIDE THE CABLE:

$$\vec{E} = 0$$

- by symmetry  $E$  must still be radial and constant magnitude at constant radius

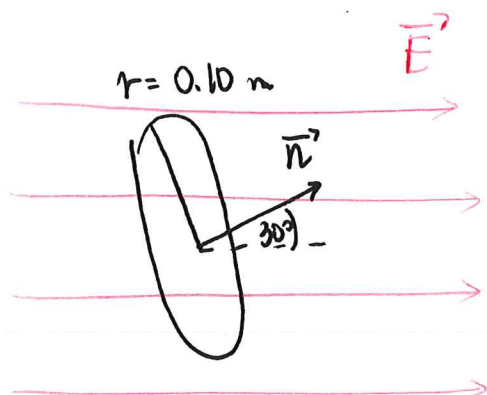
$$\oint \vec{E} \cdot d\vec{A}' = \int_{\text{tube}} E dA = E A_{\text{tube}} = \frac{q_{\text{enc}}}{\epsilon_0}$$

$$\text{but } q_{\text{enc}} = \underset{\substack{\uparrow \\ \text{shield}}}{-Q} + \underset{\substack{\nwarrow \\ \text{core}}}{Q} = 0$$

This is why coaxial cables are used!

They shield the outside from the fields inside. We will see these again when we talk about magnetic fields.

### Q1 Circular disk



$$E = 2.30 \times 10^5 \text{ N/C}$$

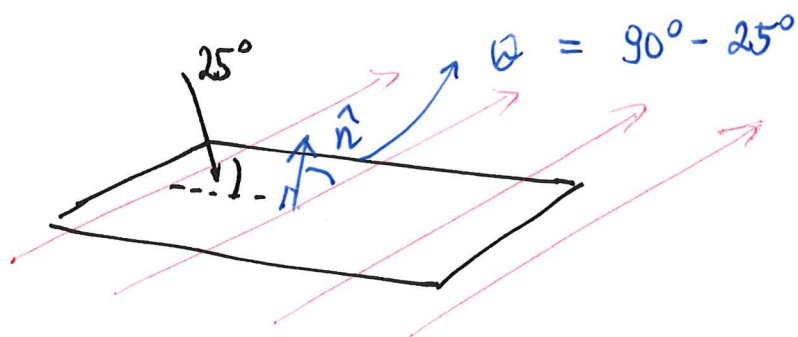
$$\Phi_E = \vec{E} \cdot \vec{A}$$

$$= E \cdot A \cdot \cos \angle (E, A)$$

$$\Phi_E = 2.30 \times 10^5 \text{ N/C} \cdot \pi (0.10 \text{ m})^2 \cdot \cos 30^\circ$$

$$\Phi_E = 6257.6078 \frac{\text{N} \cdot \text{m}^2}{\text{C}} \approx 6.26 \times 10^3 \frac{\text{N} \cdot \text{m}^2}{\text{C}}$$

### Q2 Electric flux (square surface)



$$E = 8.50 \times 10^4 \text{ V/m}$$

$$A = 17.0 \text{ m}^2$$

$$\alpha = 25^\circ$$

(angle b/w the surface  
& E-field vector)

$\theta$  (angle b/w normal  
to the surface  
&  $\vec{E}$ )

$$\theta = 90^\circ - 25^\circ = 65^\circ$$

$$\Phi_E = \vec{E} \cdot \vec{A} = E \cdot A \cos \theta$$

$$= 8.50 \times 10^4 \text{ N/C} \cdot 17.0 \text{ m}^2 \cdot \cos 65^\circ$$

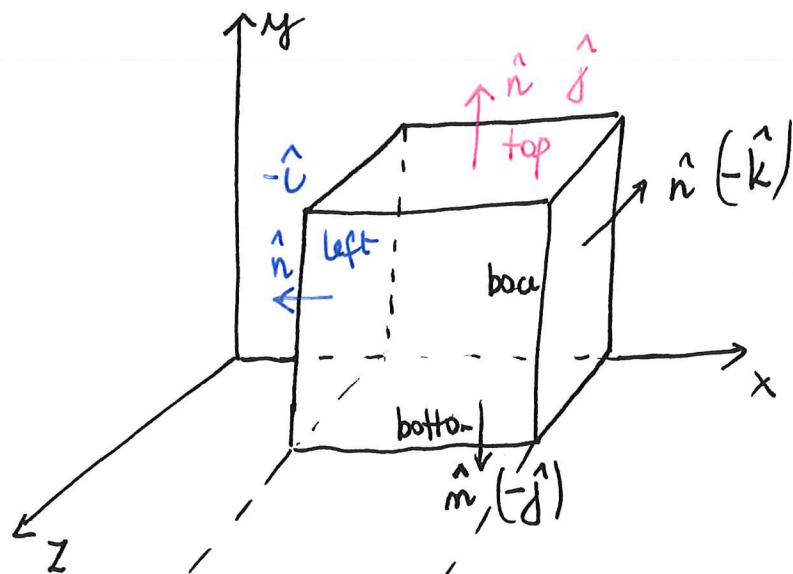
$$= 8.50 \times 10^4 \text{ N/C} \times 17.0 \text{ m}^2 \cdot (0.4226)$$

$$= 6.11 \times 10^5 \frac{\text{N} \cdot \text{m}^2}{\text{C}}$$

### Q3 Non-uniform electric field

$$\vec{E} = 6.1 \hat{i} - 9.1(y^2 + 8.5) \hat{j} \quad \text{N/C}$$

$$l = 0.260 \text{ m}$$



top

$$\Phi_{E \text{ top}} = \int \vec{E} \cdot d\vec{A}$$

$$y = 0.260 \text{ m}$$

$$\vec{E} = 6.1 \hat{i} - 9.1((0.260)^2 + 8.5) \hat{j}$$

$$\vec{E} = \underbrace{6.1}_{E_x} \hat{i} - 77.96 \hat{j} = \underbrace{6.1}_{E_x} \hat{i} - \underbrace{78}_{E_y} \hat{j} \quad E_z = 0$$

$$\vec{A}_{\text{top}} = (0.260 \text{ m})^2 \hat{j} = \underbrace{0.0676}_{A_y} \hat{j} \text{ m}^2 \quad A_x = A_z = 0$$

$$\int \vec{E} \cdot \vec{A} = E_x A_x + E_y A_y + E_z A_z$$

$$\int \vec{E} \cdot \vec{A} = 6.1 \times 0 + -78 \times 0.0676 + 0 \times 0 = -5.27 \text{ N}\cdot\text{m}^2/\text{C}$$

bottom

$$y = 0$$

$$\vec{E} = 6.1 \hat{i} - 9.1 \times 8.5 \hat{j} = 6.1 \hat{i} - 77.4 \hat{j}$$

$$\vec{A} = 0.0676 - \hat{j}$$

$$\int \vec{E} \cdot \vec{A} = -77.4 \times 0.0676 \hat{j} = +5.23 \text{ N}\cdot\text{m}^2/\text{C}$$



Left face  $\vec{A}' = 0.0676 - \hat{i}$

$$\int \vec{E}' \cdot \vec{A}' = 6.1 \times (-0.0676) \hat{i} + E_y \times 0 + 0 \times 0 = -0.412 \text{ N}\cdot\text{m}^2/\text{C}$$

Right face  $\vec{E}' = 6.1 \hat{i} - (9.1y^2 + 8.5) \hat{j}$   
 Back face  $\Phi_E = + 0.412 \text{ N}\cdot\text{m}^2/\text{C}$

$$\vec{A}' = 0.0676 - \hat{k}$$

$\vec{E}'$  has no z component  $\Phi_E = 0$

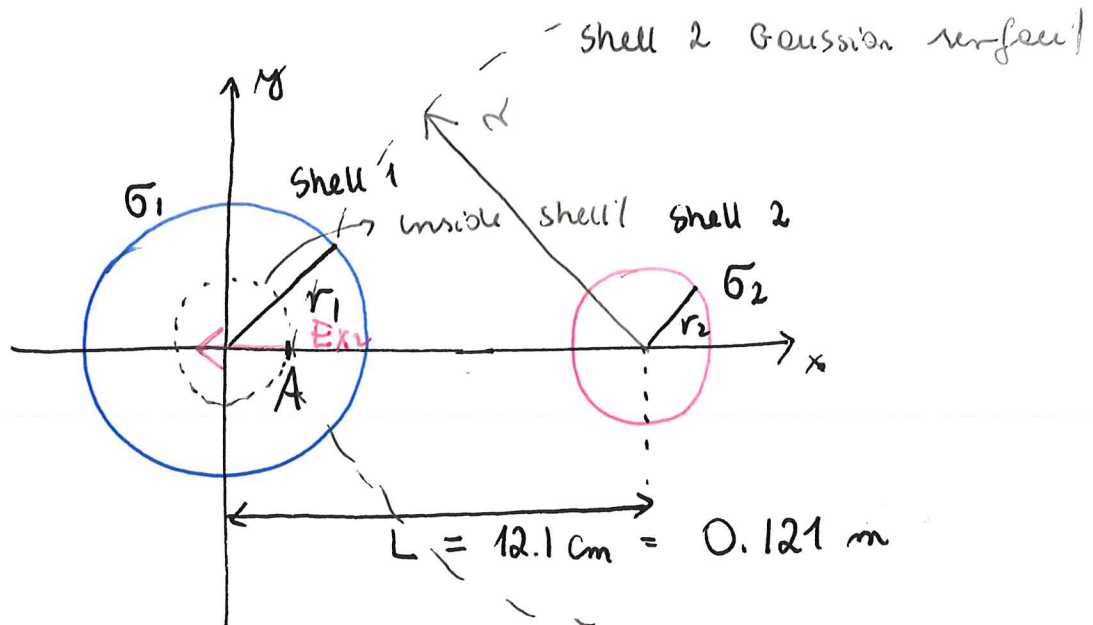
The same is true for the front face.  $\Phi_E = 0$

Total (net) flux

$$\Phi_{E, \text{net}} = \Phi_{\text{top}} + \Phi_{\text{bottom}} + \Phi_{\text{left}} + \Phi_{\text{right}} + \Phi_{\text{back}} + \Phi_{\text{front}}$$

$$\Phi_{E, \text{net}} = \Phi_{\text{top}} + \Phi_{\text{bottom}} + \underbrace{\Phi_{\text{left}} - \Phi_{\text{left}}}_{=0}$$

$$\begin{aligned} \Phi_{E, \text{net}} &= -5.27 \text{ N}\cdot\text{m}^2/\text{C} + 5.23 \text{ N}\cdot\text{m}^2/\text{C} \\ &= -0.04 \text{ N}\cdot\text{m}^2/\text{C} \end{aligned}$$



$$\begin{aligned} \sigma_1 &= +5.2 \mu\text{C}/\text{m}^2 = 5.2 \times 10^{-6} \text{ C}/\text{m}^2 & \sigma_2 &= +3.3 \mu\text{C}/\text{m}^2 = 3.3 \times 10^{-6} \text{ C}/\text{m}^2 \\ r_1 &= 4.2 \text{ cm} = 0.042 \text{ m} & r_2 &= 2.2 \text{ cm} = 0.022 \text{ m} \end{aligned}$$

$$E_x = ? \quad \underline{A}: x = 2.0 \text{ cm} = 0.02 \text{ m}$$

Use superposition:

$$E_x = E_{x1} + E_{x2}$$

//  
0  
inside shell 1

$$E_{x2} \Rightarrow \oint \vec{E} \cdot d\vec{A} = E \cdot 4\pi r^2$$

$$q_{\text{enc}} = \sigma_2 \cdot 4\pi r_2^2$$

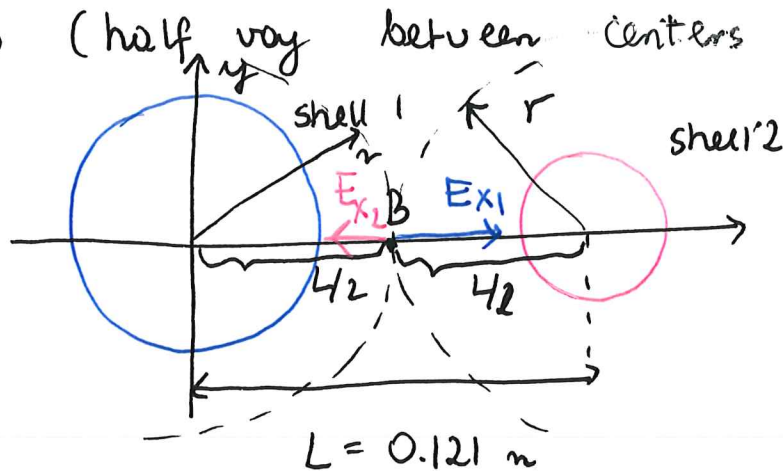
E - constant, spherical symmetry

$$E = \cancel{4\pi} r^2 = \frac{\sigma_2 \cancel{4\pi} r_2^2}{\epsilon_0} \Rightarrow$$

$$E = \frac{\sigma_2 r_2^2}{\epsilon_0 r^2} = \frac{\sigma_2 r_2^2}{\epsilon_0 (L-x)^2} = \frac{3.3 \times 10^{-6} \text{ C}/\text{m}^2 \cdot (0.022 \text{ m})^2}{(8.85 \times 10^{-12} \text{ C}^2/\text{N}\cdot\text{m}^2) (0.121 - 0.02)^2}$$

$$= 17700 \text{ N/C} \quad (2)$$

At point B (half way between centers of shell 1 and 2)



$$E_x = E_{x1} + E_{x2}$$

Spherical symmetry, E constant at given r.

$$\oint \vec{E} \cdot d\vec{A} = E \cdot 4\pi r^2 \quad r = \frac{L}{2}$$

shell 1

$$Q_{enc} = \sigma_1 \cdot 4\pi r_1^2$$

$$E_{x1} \cdot 4\pi \left(\frac{L}{2}\right)^2 = \frac{\sigma_1 \cdot 4\pi r_1^2}{\epsilon_0}$$

$$E_{x1} = \frac{\sigma_1 r_1^2}{\epsilon_0 \left(\frac{L}{2}\right)^2} (\hat{x})$$

shell 2

$$Q_{enc} = \sigma_2 \cdot 4\pi r_2^2$$

$$E_{x2} \cdot 4\pi \left(\frac{L}{2}\right)^2 = \frac{\sigma_2 \cdot 4\pi r_2^2}{\epsilon_0}$$

$$E_{x2} = \frac{\sigma_2 r_2^2}{\epsilon_0 \left(\frac{L}{2}\right)^2} (-\hat{x})$$

$$\text{at B: } \Rightarrow E_x = \frac{1}{\epsilon_0 \left(\frac{L}{2}\right)^2} (\sigma_1 r_1^2 - \sigma_2 r_2^2)$$

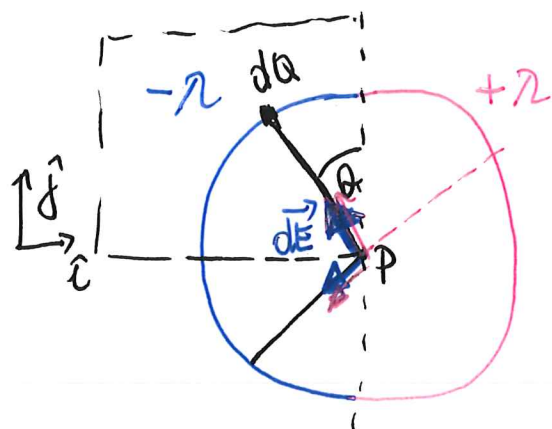
$$E_x = \frac{1}{8.85 \times 10^{-12} \text{ C}^2/\text{N}\cdot\text{m}^2} \left( \frac{5.2 \times 10^{-6} \text{ C/m}^2 \cdot (0.042 \text{ m})^2}{\left(\frac{0.121}{2}\right)^2} - \frac{3.3 \times 10^{-6} \text{ C/m}^2 \cdot (0.022 \text{ m})^2}{\left(\frac{0.121}{2}\right)^2} \right)$$

$$E_x = \frac{9.17 \times 10^{-9} - 1.53 \times 10^{-9}}{8.85 \times 10^{-12} \cdot \left(\frac{0.121}{2}\right)^2} \text{ N/C}$$

$$E_x = \frac{7.58 \times 10^{-9}}{8.85 \times 10^{-12} \cdot 3.6 \times 10^{-3}} = 0.238 \times 10^6 \text{ N/C} = 238 \text{ kN/C} (\hat{x})$$

(2)





Find  $\vec{E}$  at P.

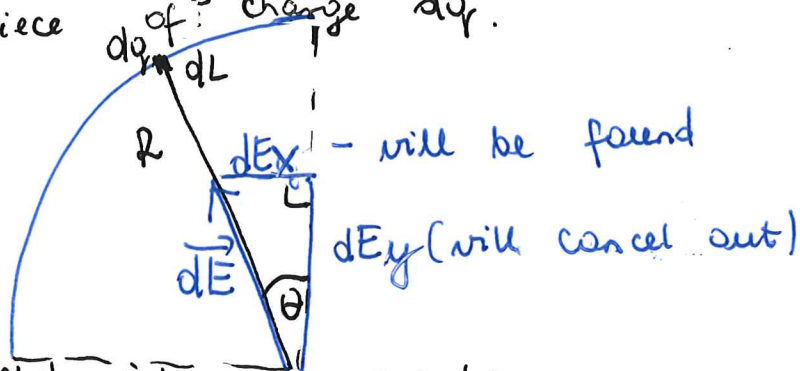
Radius, R

1. Cut the distribution into a bunch of tiny pieces each with charge  $dQ$

2. Look for a symmetry  $\rightarrow$  can use  $1/4$  circle (arc)

Find  $\vec{E}$  and multiply it by 4.

3. Calculate the magnitude of E-field due to ARBITRARY piece of charge  $dq$ .



4. Decompose field into components

$$\frac{dE_x}{dE} = \sin \theta$$

$$\frac{dE_y}{dE} = \cos \theta$$

$$dE_x = dE \sin \theta$$

$$= \frac{1}{4\pi\epsilon_0} \frac{dq}{R^2} \sin \theta$$

$$dE_y = \frac{1}{4\pi\epsilon_0} \frac{dq}{R^2} \cos \theta$$

$\Rightarrow$  not needed

due to symmetry

5. For each non-zero component, sum up all pieces  $dQ$  by integrating over the whole charge distribution

$$\int dE_x = \frac{1}{4\pi\epsilon_0} \int \frac{dq}{R^2} \sin \theta$$

6. Express  $dQ$  in terms of a variable to be integrated over using linear/surface/volume density

$$\int dE_x = \frac{1}{4\pi\epsilon_0} \int \frac{\lambda dL}{R^2} \cdot \sin\theta = \frac{1}{4\pi\epsilon_0} \int \frac{\lambda \cdot R \sin\theta d\theta}{R^2}$$

$$E_x = \frac{\lambda}{4\pi\epsilon_0 R} \int_0^{\pi/2} \sin\theta d\theta$$

$dL = R d\theta$   
 $\pi/2$  - quarter of the circle

$$\int \sin x dx = -\cos x$$

$$E_x = \frac{\lambda}{4\pi\epsilon_0 R} [-\cos\theta]_0^{\pi/2} = \frac{\lambda}{4\pi\epsilon_0 R} [-\cos(\frac{\pi}{2}) - (-\cos 0^\circ)]$$

$$= \frac{\lambda}{4\pi\epsilon_0 R}$$

Total electric field

$$E_{\text{net}} = 4E_x = \frac{4\lambda}{4\pi\epsilon_0 R} = \frac{\lambda}{\pi\epsilon_0 R}$$

$$\vec{E}_{\text{net}} = \frac{\lambda}{4\pi\epsilon_0 R} (-\hat{x})$$