AN12339

Antenna design guide for NTAG 5 boost Rev. 1.1 — 30 January 2020

Application note COMPANY PUBLIC

Document information

Info	Content
Keywords	NTAG 5 boost, Antenna Theory, Antenna Design, Measurement Methods, Antenna Design Procedure
Abstract	NTAG 5 boost needs to be connected to an antenna to access NTAG 5 via NFC interface. This application note provides guidance for designing such antenna.



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Revision history

Rev	Date	Description
1.1	20200130	Antenna matching calculation sheet added in the document
1.0	20200116	First release

Contact information

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Antenna design guide for NTAG 5 boost

1. Introduction

NTAG 5 family is ISO/IEC 15693 and NFC Forum Type 5 Tag compliant, with an EEPROM, SRAM and I²C host interface. This Application note helps to easily design and match antennas for NTAG 5 boost with active load modulation.

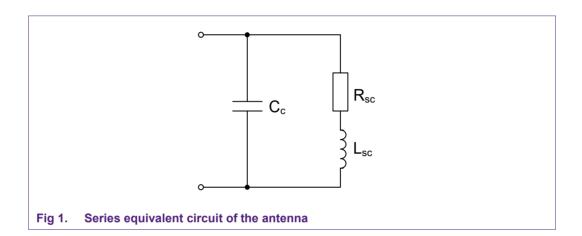
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2. Antenna basics

2.1 Series and parallel equivalent circuits

2.1.1 Series equivalent circuit of the antenna

The antenna can be described by an inductance Lsc in series to a loss resistance Rsc. The antenna capacitance Cc is in parallel to this series circuit. This capacitance consists of the inter-turn capacitance and a possibly designed tag capacitance CIC.

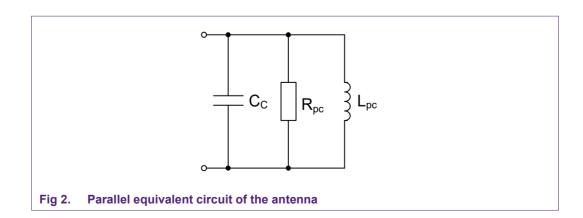


The antenna quality factor is calculated by

$$Q_{sc} = \frac{2 \cdot \pi \cdot f_{op} \cdot L_{sc}}{R_{sc}}$$

with operating frequency f_{op} = 13.56 MHz.

2.1.2 Parallel equivalent circuit of the antenna



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The following applies:

$$L_{pc} = \frac{R_{sc}^2 + (2 \cdot \pi \cdot f_{op} \cdot L_{sc})^2}{(2 \cdot \pi \cdot f_{op})^2 \cdot L_{sc}} = L_{sc} \cdot \frac{1 + Q_{sc}^2}{Q_{sc}^2}$$

$$R_{pc} = \frac{R_{sc}^{2} + (2 \cdot \pi \cdot f_{op} \cdot L_{sc})^{2}}{R_{sc}} = R_{sc} \cdot (1 + Q_{sc}^{2})$$

$$Q_{pc} = \frac{R_{pc}}{2 \cdot \pi \cdot f_{op} \cdot L_{pc}} = Q_{sc}$$

For the further calculations, the parallel equivalent circuit was chosen to simplify the resonance circuit. This makes calculation easier.

2.2 Q factor adjustment

To get a proper shaping in terms off fall a rise time of the pulse the Q-factor needs to be optimized. The Target Q-factor should not be above 14. The Q-factor should also not be too low as this reduces the performance. To check the proper size of the damping resistors, check the answer shaping (see Fig 3). The target hear is to have a proper shaping as shown on the right signal (Fig 3).

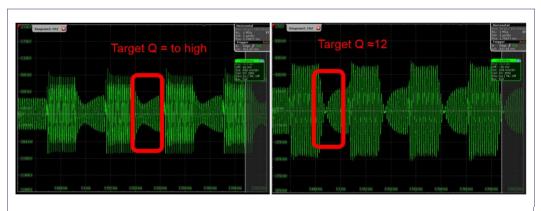
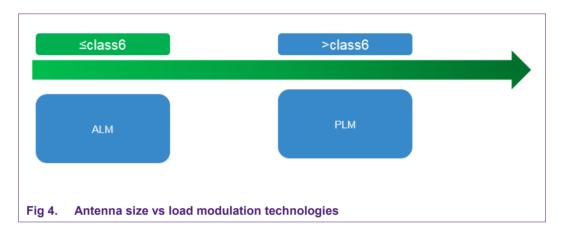


Fig 3. ALM answer shaping

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2.3 Antenna sizes

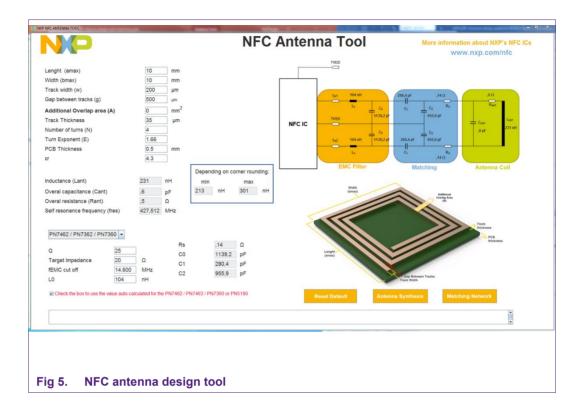
Depending on possible antenna sizes, NTAG 5 link/switch with passive load modulation (PLM) and NTAG 5 boost with active load modulation (ALM) will be used. NTAG 5 boost should be used for antennas smaller or equal class 6. For larger antennas NTAG 5 link/switch should be used (see Fig 4). The active load modulation additionally can be changed from ASK to BPSK mode to increase the response strength even further for smallest antenna sizes.



2.4 Antenna design

After fixing the antenna outline, the number of turns shall be chosen in a way to meet the inductance target value. The antenna inductance can be calculated with the NFC antenna design tool available for download on NXP website.

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The tool calculates the inductance with the given size and shaping a big influence has also the rounding of the edges to the inductance.

In this case an inductance between 213 nH and 301 nH is calculated.

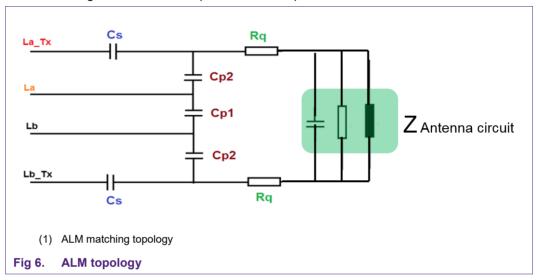
In this case it is within our targeted range so the antenna prototype can be produced, and the measurement and matching can be done on the prototype.

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3. Antenna matching

3.1 Matching topology

The ALM matching topology contains a capacitive voltage divider to guarantee a maximum voltage at the La/Lb Rx pins below 1.4Vp.



3.2 General antenna matching procedure and preparation

For a proper antenna design the antenna impedance must be measured using an impedance analyzer or VNA (vector network analyzer). Such a VNA can be a high-end tool from Agilent or Rohde & Schwarz (like the R&S ZVL), as normally used in this document), but might be a cheap alternative with less accuracy like e.g. the miniVNA Pro (see). In any case the analyzer needs to be able to measure the impedance in magnitude and phase (vector).

Such VNA can be used to measure the antenna coil as well as the antenna impedance including the matching circuit.

The antenna matching is done with the following steps:

- 1. Measure the antenna equivalent circuit parameters
- 2. Calculate the matching components
- 3. Simulate the matching
- 4. Assembly and measurement
- 5. Adaptation of simulation
- 6. Correction and assembly

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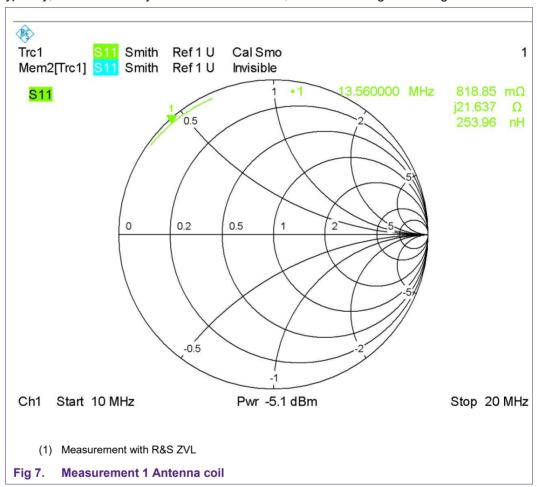
3.2.1 Measure the antenna equivalent circuit parameters

The antenna coil must be designed as described in section 2 be measured. The measurement is required to derive the inductance L, the resistance R_{Coil} and the capacitance C_{pa} as accurate as possible.

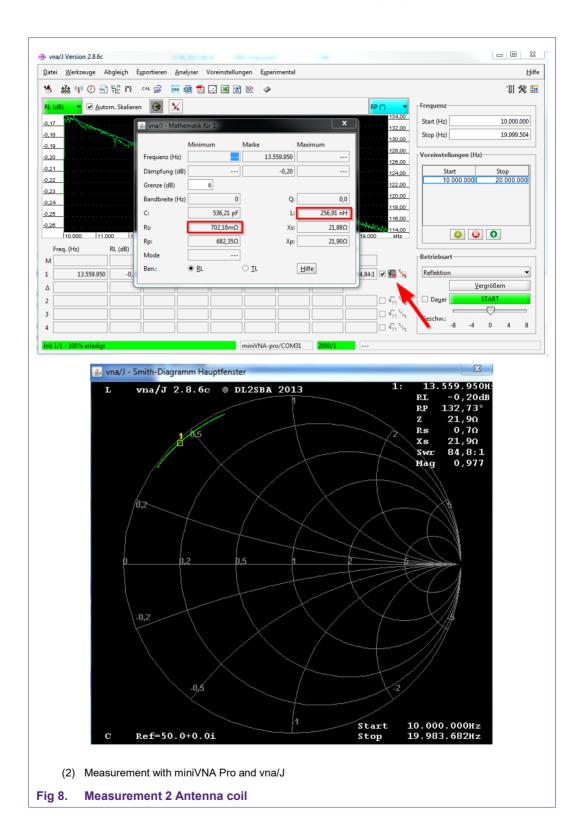
The easiest even though not most accurate way is to use the VNA to measure the impedance \underline{Z} of the antenna coil at 13.56MHz and to calculate L and R out of it:

$$\underline{Z} = R + j\omega L_{Coil} \tag{1}$$

Typically, the VNA directly can show the L and R, as shown in Fig 7 and Fig 8.



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In this example the antenna coil is measured with these values:

L = 253nH

 $R_{Coil} = 0.7 \dots 0.82\Omega$

 C_{pa} = not measured, can be estimated (typical in the range of 1-8pF)

The inductance can be measured quite accurate, but the resistance is not very accurate due to the relationship between R and j ω L. And the capacitance is not measured at all with this simple measurement.

There are several ways to improve the accuracy and even further derive the capacitance, but these simple results are enough to start the tuning procedure. This tuning procedure needs to be done anyway, so there is no real need to spend more effort in measuring the antenna coil parameters more accurate.

3.3 Antenna matching

3.3.1 Matching circuit calculation

The next step is to calculate the values of the matching circuit.

For the ALM the additional capacitive voltage divider needs to be calculated. This divider guarantees that the voltage at the LA / LB pins, during the active pulse, are in the range of max 1.4V.

To generate the matching values the measured antenna values must be inserted in the first part of the calculation sheet (see Fig 11):

1 Measured" values:

La = L = 250nH (measured antenna coil inductance)

 $Ca = C_{pa} = 0.1pF$ (estimated parallel capacitance of the antenna coil)

Ra = R_{Coil} = 1Ω (measured antenna coil resistance)

Enter the values in the first part of the calculation sheet (Fig 11)

Enter the antenna physical parameters in the second part of the excel sheet (Fig 11)

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2. Calculating matching values:

The first step:

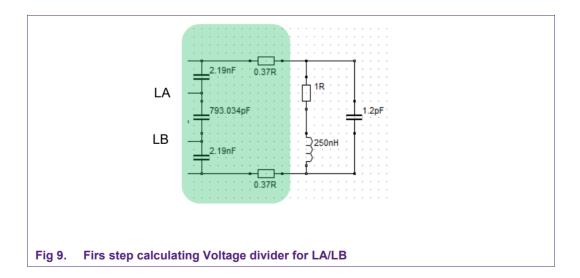
Calculate the Voltage divider based on the assumed max and min field strength (Table 1). This voltage divider is the mayor part for the matching as it limits the Voltage for the Receiver pins to 1,8V. To proper calculate the Voltage divider the Antenna parameters needed to be added in the Excel sheet as it is the base for the Voltage calculation on the Antenna, based on the min and max field strength that should be covered.

Table 1. Matching target values for voltage divider

Name	Value	
Target Q-factor	12,30	
Target Impedance	50,00	Ω
Receiver Resonance Freq	14,84	MHz
Min. H-Field Support	0,22	A/m (rms)
Max. H-Field Support 10% modulation	6,00	A/m (rms)
RX Division Ratio	0,58	

(defined Q-factor, see chapter 2).

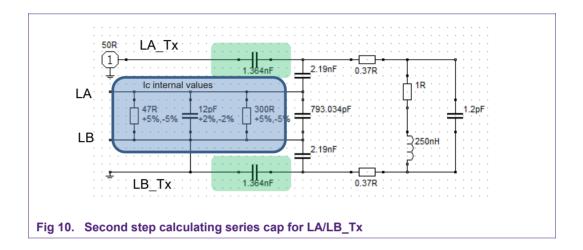
The blue marked values are used to calculate the voltage divider for L A/B. These values should not be touched if there is no change in the max field strength.



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Second Step

Calculate the series Capacitor tor LA/B_Tx based on the values for the Voltage divider. In this case the resulting impedance is limited due to the voltage divider which is the focus of the matching. The series capacitor is calculated in such a way that the impedance is around the real axis at 13.56MHz (Fig 10). To change the impedance the voltage divider needs to be recalculated at first. Due to that reason the target impedance is not incorporated as in standard reader matching.



With these values the matching components can be calculated using the excel sheet.

3 Calculated Values and components using excel sheet:

Components ALM

The matching capacitors are calculated:

Rext = R_Q = 0,37 Ω

Cs = 1,364nF

Cp1 = 793pF

Cp2 = 2,190nF

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Antenna Electrical Parameters				
Inductance	250,00	nH		
Resistance	1,00	Ω		
Parasitic capacitance	0,10	pF		

Antenna Physical parameters			
Antenna Width 10,00 mm			
Antenna Length	10,00	mm	
No. of Turns	4,00		

Matching Target				
Target Q-factor	12,30			
Target Impedance	50,00	Ω		
Receiver Resosnance Freq	14,84	MHz		
Min. H-Field Support	0,22	A/m (rms)		
Max. H-Field Support 10% modulation	6,00	A/m (rms)		
RX Division Ratio	0,58			

Matching Circuit			
Damping Resistance (Rq)	0,37	Ω	
Cp1 Cp2 Cs	793,03	pF	
Cp2	2190,284561	pF	
Cs	1363,95	pF	

(1) ALM calculation sheet

Excel sheet is included in this document as attachment, see section 5.3

Fig 11. Antenna matching calculation ALM

3.3.2 Simulate the matching

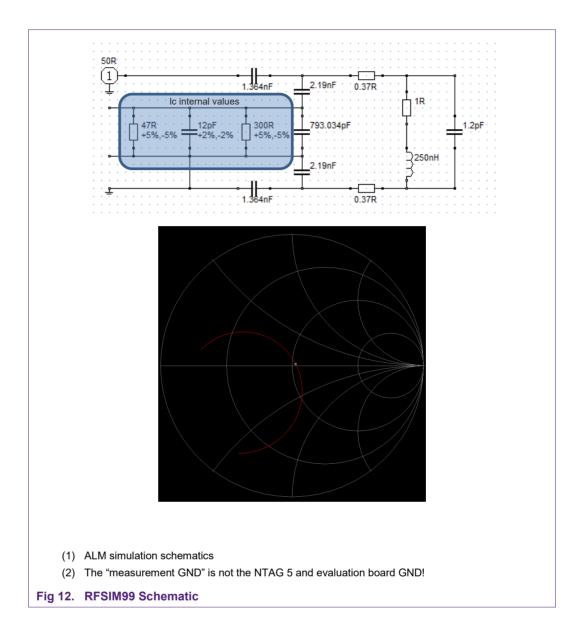
The measurement of the antenna coil itself typically is not very accurate. Therefore a (fine) tuning of the antenna normally is required, which might become easier in combination together with a simulation.

A simple matching simulation tool like e.g. RFSIM99 can be used to support the antenna tuning. The simulation input and the result based on the above given start values for the antenna matching is shown in Fig 12 and Fig 13.

With these values the assembly can be done, even though the result is not yet optimum, as shown in Fig 14. The overall impedance is slightly below 40 Ω and capacitive (-j4 Ω).

Note: The result is not as calculated, since not the exact calculated values of the capacitors are taken for assembly.

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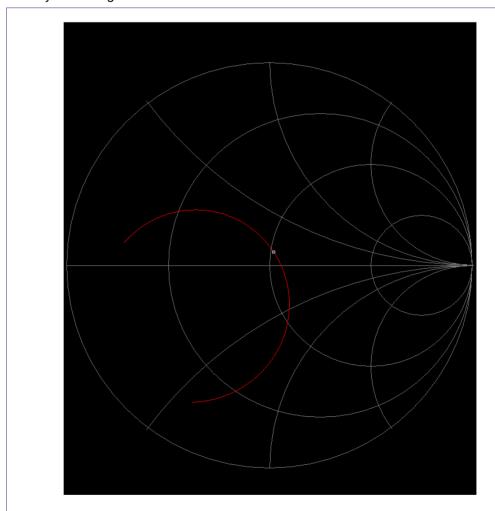
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3.3.3 Assembly and measurement (based on ALM example)

After the first assembly the impedance measurement must be done.

If the measurement result does not meet the requirements, i.e. it needs to be retuned.

The measurement result is typically slightly different than the simulation result, since the accuracy of the original antenna coil measurement is limited.



(3) This matching does not meet the requirements. It must be corrected and retuned.

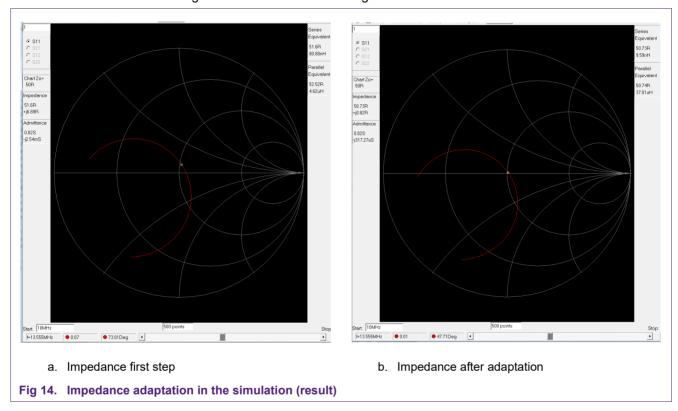
Fig 13. Measurement result of first assembly

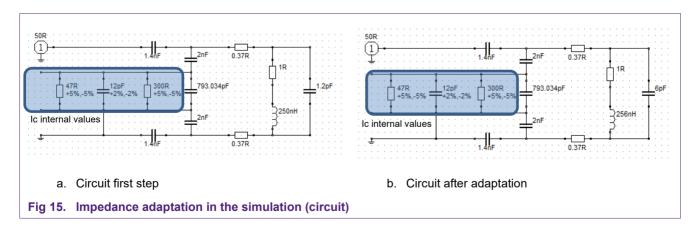
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3.3.4 Impedance fine tuning

The easiest and fastest way to (fine) tune the antenna is to first of all adapt the simulation in such a way that it shows the same result as the reality. The parameters of the antenna coil are the parameters to be changed, since these parameters are not measured (or estimated) correctly.

So with the values of L, C_{pa} , and R_{Coil} the simulation is tuned from Fig 13a to Fig 13b. The changed values can be seen in Fig 14b.





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With these adapted values the antenna coil the last step of the final tuning can be done:

La = L = 256nH

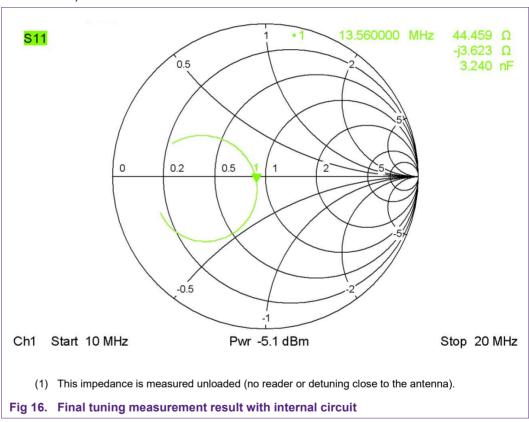
 $Ca = C_{pa} = 6pF$

 $Ra = R_{Coil} = 1\Omega$

The tuning of the impedance is now corrected with the values of Cp1 and Cp2.

These values are assembled, and the impedance is measured. The result is shown in Fig 16.

Note: For the measurements the internal resistance as well as the capacitance need to be considered (can be added with an additional small board connected during the measurement)



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3.4 ALM LUT

The ALM look up table (LUT) is a dynamic setting of the TX power which is used to change the strength of the answer signal. This is used to stay within the NFC limits and reduce the power in close coupling condition, if needed. The ALM LUT is always used if ALM is enabled and the threshold for each step is fix and cannot be changed.

The LUT contains 16 entries' starting at address 41h up to 44h. each address contains 4 Bytes so 4 entry's per address. (see Fig 17)

Block Address		Purto 0	Puto 1	Puto 2	Puto 3
NFC	I ² C	Byte 0	Byte 1	Byte 2	Byte 3
40h	1040h	ALM_CONF_00	ALM_CONF_01	ALM_CONF_02	ALM_CONF_03
41h	1041h	ALM_LUT_00	ALM_LUT_01	ALM_LUT_02	ALM_LUT_03
42h	1042h	ALM_LUT_04	ALM_LUT_05	ALM_LUT_06	ALM_LUT_07
43h	1043h	ALM_LUT_08	ALM_LUT_09	ALM_LUT_10	ALM_LUT_11
44h	1044h	ALM_LUT_12	ALM_LUT_13	ALM_LUT_14	ALM_LUT_15

Fig 17. LUT address range

The LUT entry is configured depending on the field strength and is switched due to the value at the field digitalization register (first 4 bit of the ALM_STATUS_REG adr. ACh Byte2). Each byte of the ALM LUT contains the option to change the answer strength as well as adjust the bit phase (normally not needed), if necessary. The strength of the answer signal can be adjusted by changing the RON (fine adjustment with small steps) or by changing from BPSK to ASK (substantial change). The RON can be combined with BPSK and ASK mode. (see Fig 18)

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Bit	Name	Value	Description
7 to 5	Dynamic phase adjust	xxxb	adjust phase in 11.25° steps
4	Frakla BDCV	0b	ASK
4	Enable BPSK	1b	BPSK
3 to 0	RON	0000b	1574 Ω
3 10 0	RON	0001b	716 Ω
		0010b	414 Ω
		0011b	248 Ω
		0100b	123 Ω
		0101b	82 Ω
		0110b	62 Ω
		0111b	49 Ω
		1000b	41 Ω
		1001b	35 Ω
		1010b	31 Ω
		1011b	27 Ω
		1100b	25 Ω
		1101b	22 Ω
		1110b	21 Ω
		1111b	17 Ω

Fig 18. ALM LUT value content

The values of the ALM LUT are used according to the field digitization value. That means if the field digitization value is 5 the same ALM LUT value is used. This link is fixed and cannot be changed.

The values of the field digitization are linked to the field strength (Fig 19). The values shown are based on the 10x10mm antenna and corresponding matching, which is part of the development kit. These values vary depending on the matching and antenna size, therefore they can be different depending on the setup. The corresponding measurement is done on the receiver pins and up to 1,15V a Voltage measurement is done and above the current is measured.

Code	Level	Code	Level
0	<0.22V	7	1mA
1	0.22V	8	6mA
2	0.40V	9	7.5mA
3	0.57V	10	10.5mA
4	0.74V	11	13mA
5	0.93V	12	15mA
6	1.15V	13	17mA
		14	18mA

Fig 19. Measured field vs field digitization code

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The default entries of the ALM LUT can be used and only need to be changed if the card answer is to strong, in respect to the field strength during the certification test.

3.5 LUT Values for 10mmx10mm antenna

The LUT values need to be set according to antenna size and the supply Below are the default values for the 10x10 mm antenna of the evaluation board

Table 2. LUT for 3,3V supply with 10x10mm antenna

Address (I ² C)	Byte 0	Byte 1	Byte 2	Byte 3
1041h	0x1F	0x1F	0x17	0x14
1042h	0x13	0x13	0x12	0x12
1043h	0x10	0x10	0xF0	0xF0
1044h	0xF0	0xF0	0xF0	0xF0

Table 3. LUT for 1.62V supply with 10x10mm antenna

Address (I ² C)	Byte 0	Byte 1	Byte 2	Byte 3
1041h	0x1F	0x1F	0x1F	0x1F
1042h	0x1F	0x1F	0x1F	0x12
1043h	0x10	0x10	0x10	0x10
1044h	0x10	0x10	0x10	0x10

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4.

4. List of abbreviations

This document uses the following list of abbreviations:

Ac Average antenna area
 Active antenna area
 Ai Area of antenna winding i

 a_{avg} , b_{avg} Average dimensions of the antenna a_{max} , b_{max} Maximum dimensions of the antenna a_{o} , b_{o} Overall dimensions of the antenna

C_c Antenna capacitanceC_{br} Bridge capacitance

C_{Con} Capacitance due the connection NTAG 5 IC – antenna

C_{IC} NTAG 5 IC input capacitance

C_{ICT} NTAG 5 IC input capacitance for threshold condition

C_{in} Designed inlet capacitance

 C_{it} Inter turn capacitance of the antenna C_{pl} Parallel equivalent capacitance of the inlet

 C_{plT} Parallel equivalent capacitance of the inlet for threshold condition

d Antenna wire diameter

f Frequency

 f_{op} Operating frequency

f_R Resonance frequency of the inlet

 f_{RT} Threshold resonance frequency of the inlet

g Gap between the tracks H_T Threshold field strength

H_{Tmin} Minimal threshold field strength

 H_{Top} Threshold field strength at operating frequency

I₁ Reader antenna current

*L*_{calc} Inductance calculated out of the geometrical antenna parameters

L_o Objective inductance of the antenna

 L_{pc} Parallel equivalent inductance of the antenna L_{sc} Serial equivalent inductance of the antenna

M Mutual inductance between the inlet antenna and reader antenna

N_c Number of turns of the antenna

p Turn exponent

Q Quality factor of the inlet

 Q_{pc} Quality factor of the antenna for parallel equivalent circuit Q_{sc} Quality factor of the antenna for serial equivalent circuit

Q_⊤ Threshold quality factor of the inlet

R_{Con} Resistance of the connection NTAG 5 IC – antenna

R_{IC} NTAG 5 IC input resistance

R_{ICT} NTAG 5 IC input resistance for threshold condition

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 $R_{
m pc}$ Parallel equivalent resistance of the antenna $R_{
m pl}$ Parallel equivalent resistance of the inlet

R_{plT} Parallel equivalent resistance of the inlet at threshold condition

 $R_{\rm sc}$ Serial equivalent resistance of the antenna

t Track thickness

V_{LA-LB} NTAG 5 IC input voltage

 $V_{\text{LA-LB min}}$ Minimal voltage level for NTAG 5 IC operation

w Track width

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5. Reference documentation

NXP provides several documents to support the development of customized antennas.

5.1 Data sheets

NXP provides the following data sheet:

 NTA5332 - NTAG 5 boost, NFC Forum-compliant I2C bridge for tiny devices, doc.no. 544730

https://www.nxp.com/docs/en/data-sheet/NTA5332.pdf

5.2 Application notes

NXP provides the following application note:

 AN12428 - NTAG 5 design recommendations for FCC and CE certifications https://www.nxp.com/docs/en/application-note/AN12428.pdf

5.3 Included antenna matching calculation excel sheet

As attachment you will find a ZIP file containing the antenna matching calculator.

The Excel file is enclosed in a ZIP file which has the file extension .nxp. To access the Excel file, you can do the following:

- 1. Open the attachment by clicking the paperclip in the left margin.
- 2. You will find a .nxp file added to this PDF as an attachment. Right-click the file and click Save Attachment. Store it at a permanently available (network) storage location.
- 3. Open the location where you saved the attachment.
- 4. Rename the file. Change the extension from .nxp into .zip.
- 5. Now you can open the zip file which contains the Excel file.

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