

ME-8930

Convex Optimization Methods for Robust and Optimal Control Design

HW05

Group:

Chinmay Samak

Tanmay Samak

$$m_1 \ddot{q}_1 + k_1 q_1 - k_1 q_2 = f(t) + \omega(t)$$

$$m_2 \ddot{q}_2 + -k_1 q_1 + (k_1 + k_2) q_2 - k_2 q_3 = 0$$

$$m_3 \ddot{q}_3 - k_2 q_2 + k_2 q_3 = 0$$

$$\mathbf{x}_p = \begin{bmatrix} q_1 \\ q_2 \\ q_3 \\ \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \end{bmatrix}$$

$$y = q_3$$

$$\mathbf{x}_p = A_p \mathbf{x}_p + B_p u + D_p w \quad z = \mathbf{x}_p \quad (\text{full state feedback})$$

$$y = C_p \mathbf{x}_p \quad u = G_p \mathbf{x}_p \quad (\text{static state feedback control})$$

$$\begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \ddot{q}_1 \\ \ddot{q}_2 \\ \ddot{q}_3 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ -k_1/m_1 & k_1/m_1 & 0 & 0 & 0 & 0 \\ k_1/m_2 & \frac{(-k_1-k_2)}{m_2} & k_2/m_2 & 0 & 0 & 0 \\ 0 & k_2/m_3 & -k_2/m_3 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \\ q_3 \\ \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1/m_1 \\ 0 \\ 0 \end{bmatrix} f(t) + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} w(t)$$

$$q_3 = [0 \ 0 \ 1 \ 0 \ 0 \ 0] \begin{bmatrix} q_1 \\ q_2 \\ q_3 \\ \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \end{bmatrix}$$

$$A_p = \begin{bmatrix} 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \\ -\frac{k_1}{m_1} & \frac{k_1}{m_1} & 0 & 0 & 0 & 0 \\ \frac{k_1}{m_2} & \frac{(-k_1-k_2)}{m_2} & k_2/m_2 & 0 & 0 & 0 \\ 0 & \frac{k_2}{m_3} & -\frac{k_2}{m_3} & 0 & 0 & 0 \end{bmatrix} \quad B_p = \begin{bmatrix} 0 \\ 0 \\ 0 \\ \frac{1}{m_1} \\ 0 \\ 0 \end{bmatrix} \quad D_p = \begin{bmatrix} 0 \\ 0 \\ 0 \\ \frac{1}{m_1} \\ 0 \\ 0 \end{bmatrix}$$

$$C_p = [0 \ 0 \ 1 \ 0 \ 0 \ 0]$$

General form:

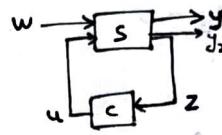
$$\dot{x}_p = A_p x_p + B_p u + D_p w$$

$$y_1 = C_p x_p + B_{y_1} u + D_{y_1} w$$

$$y_2 = C_{y_2} x_p + B_{y_2} u$$

$$z = M_p x_p + D_z w$$

$\rightarrow z = x_p$ (full state feedback)



Comparing with earlier notation $\begin{cases} \dot{x}_p = A_p x_p + B_p u + D_p w \\ y = C_p x_p \end{cases}$

general form \sim earlier notation

$$A_p = A_p$$

$$B_p = B_p$$

$$D_p = D_p$$

$$C_{p_2} = C_p$$

$$B_{y_2} = 0$$

$$D_y = 0$$

we only consider Γ_{ep} from w to y_2 .

to design an optimal H_2 controller so as to minimize Γ_{ep} and ensure CL system

stability by placing the CL poles in LHP

such that $\text{Re}(z) < -1$.

desired region for CL-poles used in "Iming".

Lumped system representation

$$\left. \begin{array}{l} A = A_p \\ B = [D_p \quad B_p] \\ C = \boxed{\cancel{[C_p \quad C_{p_2}]}} \quad [C_p \quad C_{p_2}]^T \\ D = \begin{bmatrix} 0 & B_{y_1} \\ 0 & B_{y_2} \end{bmatrix} \end{array} \right\} S$$

$$\tau = \text{size}(B_{y_2}) = [\text{size}(y_2) \quad \text{size}(u)]$$

$$\text{obj} = [0 \quad 0 \quad 0 \quad 1] \quad \begin{matrix} \uparrow & \uparrow & \uparrow & \uparrow \\ y_1 & y_2 & u & \Gamma_{ep} \end{matrix} \Rightarrow \min \Gamma_{ep} \Rightarrow \text{optimal } H_2 \text{ control design}$$

$$\min (\alpha \Gamma_{ee}^2 + \beta \Gamma_{ep}^2)$$

$$\text{s.t. } \Gamma_{ee} < y_1$$

$$\Gamma_{ep} < y_2$$

$$[\bar{Y}_1, \bar{Y}_2, G_1, S_{cl}, X] = \text{msfsyn}(S, \tau, \text{obj}, \text{region})$$

Γ_{ee} of CL system

Γ_{ep} of CL system

static state feedback control gain ($u = G_1 X$)

CL system representation

Lyapunov parameter matrix

$$A_{cl} = A_p + B_p \cdot G_1$$

$$\dots \begin{cases} u = k \omega \\ \Rightarrow A_{cl} = A + Bk \end{cases}$$

Design validation:

• Performance

$$\rightarrow h_2\text{-norm} = \text{norm2}(S_{\text{OL}})$$

(Γ_{ep})

$$\Gamma_{\text{ep}} = \|CPC^T\|^{1/2} = (\text{tr}(CPC^T))^{1/2}$$

$$\text{where } AP + PA^T + BB^T = 0 \quad (\text{Lyapunov equation})$$

$$P > 0$$

$$\Gamma_{\text{ep}} < \gamma_2^*$$

• Stability

$$\rightarrow \text{CL poles : } \underset{(z)}{\text{Re}}(\lambda_i(A_{\text{CL}})) = \underset{(z)}{\text{Re}}(z) < -1 \leftarrow \text{pole placement (CL) in desired region.}$$

System simulation:

$$w(t) = \begin{cases} 100 & 0 \leq t \leq 2 \\ 0 & t > 2 \end{cases}$$

$$u(t) = 0 \quad \forall t$$

simulate open (S_{OL}) and closed (S_{CL}) loop systems using "lsim" for $t=0$ to $t=10$ seconds with $\Delta t = 0.01$ sec.

Uncertain system:

10% uncertainty in k_2 (nominal $k_2 = 4000$ N/m)

i.e. $3600 \leq k_2 \leq 4400$ N/m

for $k_2 = 3600:1:4400$

$h_2\text{-norm} = \text{norm2}(S_{\text{OL}}) \leftarrow$ using C_1

plot $(k_2, h_2\text{-norm}) \leftarrow \Gamma_{\text{ep}}$ vs. k_2 with C_1

Robust state-feedback controller design:

Affine system representation

$$A = A_0 + k_2 A_1$$

$$A_0 = \begin{bmatrix} 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \\ \frac{-k_1}{m_1} & \frac{k_1}{m_1} & 0 & 0 & 0 & 0 \\ \frac{k_1}{m_2} & -\frac{k_1}{m_2} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$A_1 = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & \frac{-1}{m_2} & \frac{1}{m_2} & 0 & 0 & 0 \\ 0 & \frac{1}{m_3} & -\frac{1}{m_3} & 0 & 0 & 0 \end{bmatrix}$$

$$B_0 = B, \quad C_0 = C, \quad D_0 = D$$

$$\left| \begin{array}{l} P = [k_2]; k_2 \in [3600, 4400] \\ = \text{pvec}('box', [3600, 4400]) \end{array} \right.$$

$$S_0 = \text{l4isys}(A_0, B_0, C_0, D_0, 1)$$

$$S_1 = \text{l4isys}(A_1, 0, 0, 0, 0)$$

$$\text{affsys} = \text{psys}(P, [S_0, S_1])$$

$$r = \text{size}(B_{y_2}) = \begin{bmatrix} \text{size}(y_2) & \text{size}(u) \end{bmatrix}$$

$$\text{obj} = [0 \ 0 \ 0 \ 1] \leftarrow \text{optimal H}_2 \text{ control design } (\min \Gamma_{\text{ep}})$$

region = lmi:reg (\leftarrow LHP with $\text{Re}(z) < -1$)

$$[y_i^*, y_i^*, G_2, S_{\text{cl}}, X] = \text{lmsfsyn}(\text{affsys}, r, \text{obj}, \text{region})$$

CL system representation obtained
Robust static state feedback control gain ($u = G_2 u_p$)
 Γ_{ep} of CL system (guaranteed H_2 performance)

$$A_{\text{cl}} = A_p + B_p G_2$$

$$(A_{\text{cl}} = A + BK)$$

for $k_2 = 3600 : 1 : 4400$

$$h_2\text{-norm} = \text{norm2}(S_{\text{cl}}) \leftarrow \text{using } G_2$$

plot (k_2 , $h_2\text{-norm}$) $\leftarrow \Gamma_{\text{ep}}$ vs. k_2 with G_2

(with Jacob + St. Function) \leftarrow no plot available

min k_2 such that $h_2\text{-norm} < 0.001$

min k_2 such that $h_2\text{-norm} < 0.0001$

After a while \leftarrow (constant value)

$$\begin{bmatrix} A_p & B_p \\ C_p & D_p \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

$$\begin{bmatrix} A_{\text{cl}} & B_{\text{cl}} \\ C_{\text{cl}} & D_{\text{cl}} \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

Problem 1

CODE:

```
% PROBLEM 1
```

```
close all
clear
clc

% Define the system parameters
m1 = 20; % kg
m2 = 40; % kg
m3 = 30; % kg
k1 = 2000; % N/m
k2 = 4000; % N/m

% Define the system matrices
Ap = [0 0 0 1 0 0;
       0 0 0 0 1 0;
       0 0 0 0 0 1;
       -k1/m1 k1/m1 0 0 0 0;
       k1/m2 (-k1-k2)/m2 k2/m2 0 0 0;
       0 k2/m3 -k2/m3 0 0 0];
Bp = [0; 0; 0; 1/m1; 0; 0]
Dp = [0; 0; 0; 1/m1; 0; 0]
Cp2 = [0 0 1 0 0 0]
By2 = 0
Dy = 0
```

```
% Lumped system representation
A = Ap;
B = [Dp Bp];
C = [zeros(size(Cp2)); Cp2];
D = [Dy zeros(size(By2)); zeros(size(Dy)) By2];
S = ltisys(A, B, C, D)

% State-feedback controller G1 to minimize the energy-to-peak gain Γep
r = size(By2);
obj = [0 0 0 1]; % Optimal H2 control design objective
region = lmireg; % h (half-plane) --> 1 (LHP, i.e., Re(z) < x0) --> -1 (x0 = -1)
[g1opt, g2opt, G1, Scl, X] = msfsyn(S, r, obj, region)
```

```
% Closed-loop system
Acl = Ap + Bp*G1
h2_norm = norm2(Scl)
% Scl = ss(Acl, [Dp zeros(size(Bp))], C, D)
% h2_norm = norm(Scl, 2)

% Verification
if((h2_norm < g2opt) && all(real(eig(Acl)) < -1.0))
    disp('Verification of H2 norm and pole location constraints successful!')
else
    disp('Verification of H2 norm and pole location constraints failed!')
end
```

```
% Define the lumped (disturbance + control) input
t = 0:0.01:10;
w_amplitude = 100.0;
w_duration = 2;
w_pulse = w_amplitude * (t >= 0 & t <= w_duration);
u = zeros(size(w_pulse));
w = [w_pulse; u];

% Simulate the open-loop system response
Sol = ss(A, B, C, D)
[y_ol, t_out, x_ol] = lsim(Sol, w', t);

% Plot the results
figure;
sgtitle('Open-Loop System Response');
subplot(3, 1, 1);
plot(t, w(1, :), t, w(2, :));
legend('W', 'U');
subplot(3, 1, 2);
plot(t, x_ol(:, 1), ...
      t, x_ol(:, 2), ...
      t, x_ol(:, 3), ...
      t, x_ol(:, 4), ...
      t, x_ol(:, 5), ...
      t, x_ol(:, 6) ...
);
legend('X1', 'X2', 'X3', 'X4', 'X5', 'X6');
subplot(3, 1, 3);
plot(t, y_ol(:, 2));
```

```

legend('Y1');

% Simulate the closed-loop system response
Scl = ss(Acl, [Dp zeros(size(Bp))], C, D)
[y_cl, t_out, x_cl] = lsim(Scl, w', t);

% Plot the results
figure;
sgtitle('Closed-Loop System Response');
subplot(3, 1, 1);
plot(t, w(1, :), t, w(2, :));
legend('W', 'U');
subplot(3, 1, 2);
plot(t, x_cl(:, 1), ...
      t, x_cl(:, 2), ...
      t, x_cl(:, 3), ...
      t, x_cl(:, 4), ...
      t, x_cl(:, 5), ...
      t, x_cl(:, 6) ...
);
legend('X1', 'X2', 'X3', 'X4', 'X5', 'X6');
subplot(3, 1, 3);
plot(t, y_cl(:, 2));
legend('Y1');

```

```

% Define uncertain system parameters
m1 = 20; % kg
m2 = 40; % kg
m3 = 30; % kg
k1 = 2000; % N/m
i = 1;
for k2 = 3600:1:4400 % N/m
    % Define the system matrices
    Ap = [0 0 0 1 0 0;
          0 0 0 0 1 0;
          0 0 0 0 0 1;
          -k1/m1 k1/m1 0 0 0 0;
          k1/m2 (-k1-k2)/m2 k2/m2 0 0 0;
          0 k2/m3 -k2/m3 0 0 0];
    Bp = [0; 0; 0; 1/m1; 0; 0];
    Dp = [0; 0; 0; 1/m1; 0; 0];
    Cp2 = [0 0 1 0 0 0];
    By2 = 0;
    Dy = 0;

```

```

% Lumped system representation
A = Ap;
B = [Dp Bp];
C = [zeros(size(Cp2)); Cp2];
D = [Dy zeros(size(By2)); zeros(size(Dy)) By2];
% Closed-loop system
Acl = Ap + Bp*G1;
Scl = ltisys(Acl, [Dp zeros(size(Bp))], C, D);
h2_norm(i) = norm2(Scl);
% Scl = ss(Acl, [Dp zeros(size(Bp))], C, D);
% h2_norm(i) = norm(Scl, 2);
i = i+1;
end

figure;
sgtitle('Uncertain System with Controller G_1');
plot(3600:1:4400, h2_norm)
xlabel('Spring Constant k_2')
ylabel('Energy to Peak Gain \Gamma_{ep}')

```

```

% Define the system parameters
m1 = 20; % kg
m2 = 40; % kg
m3 = 30; % kg
k1 = 2000; % N/m

% System matrices in affine form
A0 = [0 0 0 1 0 0;
       0 0 0 0 1 0;
       0 0 0 0 0 1;
       -k1/m1 k1/m1 0 0 0 0;
       k1/m2 -k1/m2 0 0 0 0;
       0 0 0 0 0 0];
A1 = [0 0 0 0 0 0;
       0 0 0 0 0 0;
       0 0 0 0 0 0;
       0 0 0 0 0 0;
       0 -1/m2 1/m2 0 0 0;
       0 1/m3 -1/m3 0 0 0];
B0 = B
C0 = C
D0 = D

```

```
% Uncertain LTI system in affine form
```

```

S0 = ltisys(A0, B0, C0, D0, 1)
S1 = ltisys(A1, zeros(size(B0)), zeros(size(C0)), zeros(size(D0)), 0)

% Parameter vector
P = pvec('box', [3600, 4400]) % k2

% Affine system
affsys = psys(P, [S0, S1])

% State-feedback controller G2 to minimize the energy-to-peak gain Γep
r = size(By2);
obj = [0 0 0 1]; % Optimal H2 control design objective
region = lmireg; % h (half-plane) --> l (LHP, i.e., Re(z) < x0) --> -1 (x0 = -1)
[g1opt, g2opt, G2, Scl, X] = msfsyn(affsys, r, obj, region)

disp('Optimal guaranteed energy-to-peak gain for the uncertain system is:')
disp(g2opt)

```

```

% Define uncertain system parameters
m1 = 20; % kg
m2 = 40; % kg
m3 = 30; % kg
k1 = 2000; % N/m
i = 1;
for k2 = 3600:1:4400 % N/m
    % Define the system matrices
    Ap = [0 0 0 1 0 0;
          0 0 0 0 1 0;
          0 0 0 0 0 1;
          -k1/m1 k1/m1 0 0 0 0;
          k1/m2 (-k1-k2)/m2 k2/m2 0 0 0;
          0 k2/m3 -k2/m3 0 0 0];
    Bp = [0; 0; 0; 1/m1; 0; 0];
    Dp = [0; 0; 0; 1/m1; 0; 0];
    Cp2 = [0 0 1 0 0 0];
    By2 = 0;
    Dy = 0;
    % Lumped system representation
    A = Ap;
    B = [Dp Bp];
    C = [zeros(size(Cp2)); Cp2];
    D = [Dy zeros(size(By2)); zeros(size(Dy)) By2];
    % Closed-loop system

```

```

Acl = Ap + Bp*G2;
Scl = ltisys(Acl, [Dp zeros(size(Bp))], C, D);
h2_norm(i) = norm2(Scl);
% Scl = ss(Acl, [Dp zeros(size(Bp))], C, D);
% h2_norm(i) = norm(Scl, 2);
i = i+1;
end

figure;
sgtitle('Uncertain System with Controller G_2');
plot(3600:1:4400, h2_norm)
xlabel('Spring Constant k_2')
ylabel('Energy to Peak Gain \Gamma_{ep}')

```

OUTPUT:

```

Ap = 6x6
    0         0         0     1.0000         0         0
    0         0         0         0     1.0000         0
    0         0         0         0         0     1.0000
-100.0000  100.0000         0         0         0         0
  50.0000 -150.0000  100.0000         0         0         0
    0   133.3333 -133.3333         0         0         0
Bp = 6x1
    0
    0
    0
  0.0500
    0
    0
Dp = 6x1
    0
    0
    0
  0.0500
    0
    0
Cp2 = 1x6
    0     0     1     0     0     0
By2 = 0
Dy = 0
S = 9x9
    0         0         0     1.0000         0         0         0
  0   6.0000         0         0     1.0000         0         0
    0         0         0         0         0     1.0000         0
    0         0         0         0         0         0     0.0500
-100.0000  100.0000         0         0         0         0     50.0000
  0.0500         0         0   100.0000         0         0         0
    0         0         0         0         0         0         0

```

	0	133.3333	-133.3333	0	0	0	0
0	0			0	0	0	0
	0	0	0	0	0	0	0
0	0	0	1.0000	0	0	0	0
	0	0	0	0	0	0	0
0	-Inf						

Select a region among the following:

- h) Half-plane
- d) Disk
- c) Conic sector
- e) Ellipsoid
- p) Parabola
- s) Horizontal strip
- m) Matrix description of the LMI region
- q) Quit

Select a region among the following:

- h) Half-plane
- d) Disk
- c) Conic sector
- e) Ellipsoid
- p) Parabola
- s) Horizontal strip
- m) Matrix description of the LMI region
- q) Quit

Optimization of $0.000 * G^2 + 1.000 * H^2 :$

Solver for linear objective minimization under LMI constraints

Iterations : Best objective value so far

1	
2	
3	
4	
5	
6	
7	
8	0.123781
9	0.101980
10	0.101980
11	0.028857
12	0.028857
13	0.028857
14	0.012000
15	0.012000
16	0.010372
17	0.010372
18	0.010372
19	6.093835e-03
20	6.093835e-03

```

21      6.093835e-03
22      3.043563e-03
23      3.043563e-03
24      3.043563e-03
25      1.240950e-03
26      1.240950e-03
27      1.231455e-03
28      3.550594e-04
29      2.305720e-04
30      2.305720e-04
31      1.078822e-04
32      1.078822e-04
33      1.078822e-04
34      5.183917e-05
35      5.183917e-05
36      5.183917e-05
37      2.614067e-05
38      2.614067e-05
39      2.614067e-05
40      1.606369e-05
41      1.606369e-05
42      1.596526e-05
43      3.082070e-06
44      3.082070e-06
45      2.599298e-06
46      2.599298e-06
47      2.599298e-06
48      9.165308e-07

```

Result: reached the target for the objective value
 best objective value: 9.165308e-07
 f-radius saturation: 0.520% of R = 1.00e+10

Guaranteed H2 performance: 9.57e-04

```

g1opt =
[]

g2opt = 9.5736e-04
G1 = 1x6
1011 ×
-0.0008 -0.2312 -1.9312 -0.0000 -0.0024 -0.0996
Scl = 9x8
109 ×
0.0000 0 0 0.0000 0 0 0
0 0 0 0 0.0000 0 0
0 0 0 0 0 0.0000 0
0 -0.0038 -1.1562 -9.6558 -0.0000 -0.0120 -0.4980 0.0000
0 0.0000 -0.0000 0.0000 0 0 0
0 0 0.0000 -0.0000 0 0 0
0

```

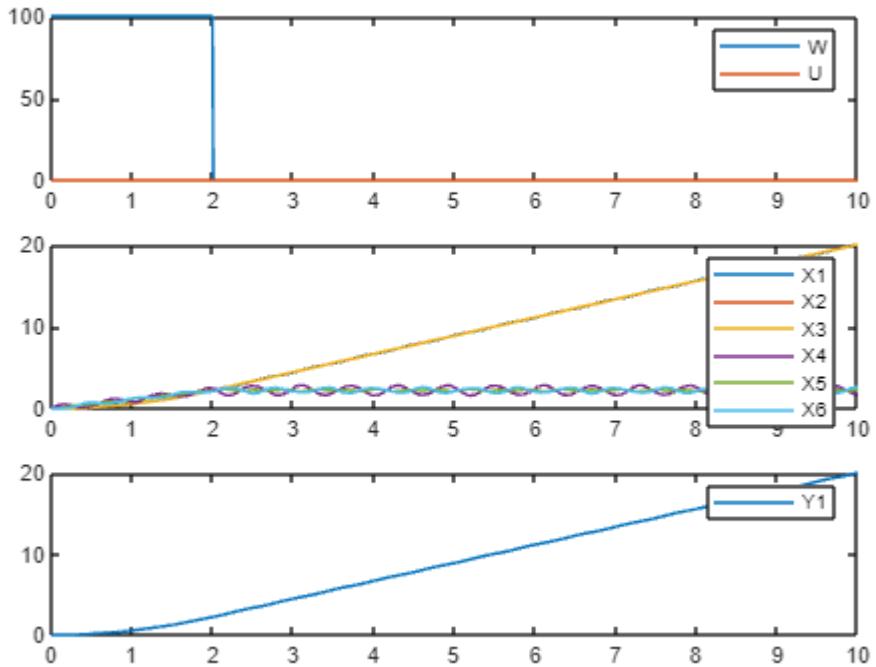
```

0          0          0          0          0          0          0
0          0          0      0.0000          0          0          0
0          0          0          0          0          0          0          -
Inf
X = 6x6
10^6 *
0.0003    0.0000   -0.0000   -0.0080   -0.0002   -0.0000
0.0000    0.0000   0.0000    0.0000   -0.0000   -0.0000
-0.0000    0.0000   0.0000   -0.0000    0.0000   -0.0000
-0.0080    0.0000   -0.0000    1.3121   -0.0003   -0.0000
-0.0002   -0.0000   0.0000   -0.0003    0.0002   0.0000
-0.0000   -0.0000   -0.0000   -0.0000    0.0000   0.0000
Acl = 6x6
10^9 *
0          0          0      0.0000          0          0
0          0          0          0      0.0000          0
0          0          0          0          0      0.0000
-0.0038   -1.1562   -9.6558   -0.0000   -0.0120   -0.4980
0.0000   -0.0000   0.0000    0          0          0
0      0.0000   -0.0000    0          0          0
h2_norm = 1.8822e-11
Verification of H2 norm and pole location constraints successful!
Sol =
A =
      x1      x2      x3      x4      x5      x6
x1      0      0      0      1      0      0
x2      0      0      0      0      1      0
x3      0      0      0      0      0      1
x4     -100     100      0      0      0      0
x5      50    -150     100      0      0      0
x6      0    133.3   -133.3      0      0      0
B =
      u1      u2
x1      0      0
x2      0      0
x3      0      0
x4    0.05    0.05
x5      0      0
x6      0      0
C =
      x1      x2      x3      x4      x5      x6
y1      0      0      0      0      0      0
y2      0      0      1      0      0      0
D =
      u1      u2
y1      0      0
y2      0      0

```

Continuous-time state-space model.

Open-Loop System Response



```
Scl =
```

```
A =
```

$$\begin{array}{ccccccc} & \mathbf{x}_1 & \mathbf{x}_2 & \mathbf{x}_3 & \mathbf{x}_4 & \mathbf{x}_5 & \mathbf{x}_6 \\ \mathbf{x}_1 & 0 & 0 & 0 & 1 & 0 & 0 \\ \mathbf{x}_2 & 0 & 0 & 0 & 0 & 1 & 0 \\ \mathbf{x}_3 & 0 & 0 & 0 & 0 & 0 & 1 \\ \mathbf{x}_4 & -3.805e+06 & -1.156e+09 & -9.656e+09 & -1.15e+04 & -1.205e+07 & -4.98e+08 \\ \mathbf{x}_5 & 50 & -150 & 100 & 0 & 0 & 0 \\ \mathbf{x}_6 & 0 & 133.3 & -133.3 & 0 & 0 & 0 \end{array}$$

```
B =
```

$$\begin{array}{cc} \mathbf{u}_1 & \mathbf{u}_2 \\ \mathbf{x}_1 & 0 \\ \mathbf{x}_2 & 0 \\ \mathbf{x}_3 & 0 \\ \mathbf{x}_4 & 0.05 \\ \mathbf{x}_5 & 0 \\ \mathbf{x}_6 & 0 \end{array}$$

```
C =
```

$$\begin{array}{cccccc} & \mathbf{x}_1 & \mathbf{x}_2 & \mathbf{x}_3 & \mathbf{x}_4 & \mathbf{x}_5 & \mathbf{x}_6 \\ \mathbf{y}_1 & 0 & 0 & 0 & 0 & 0 & 0 \\ \mathbf{y}_2 & 0 & 0 & 1 & 0 & 0 & 0 \end{array}$$

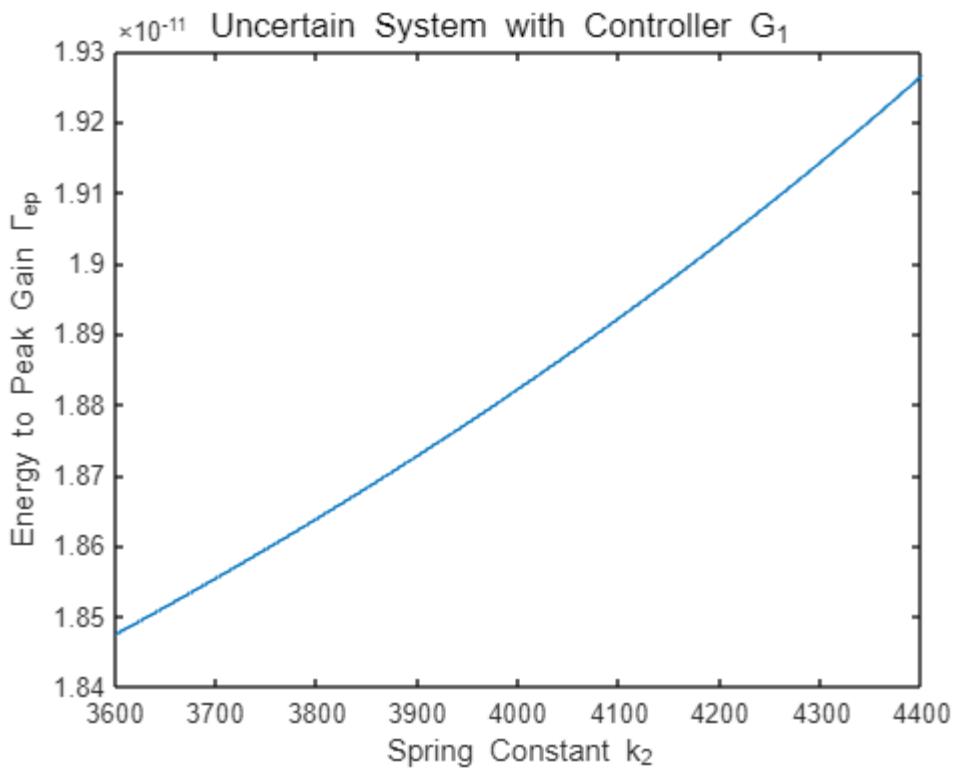
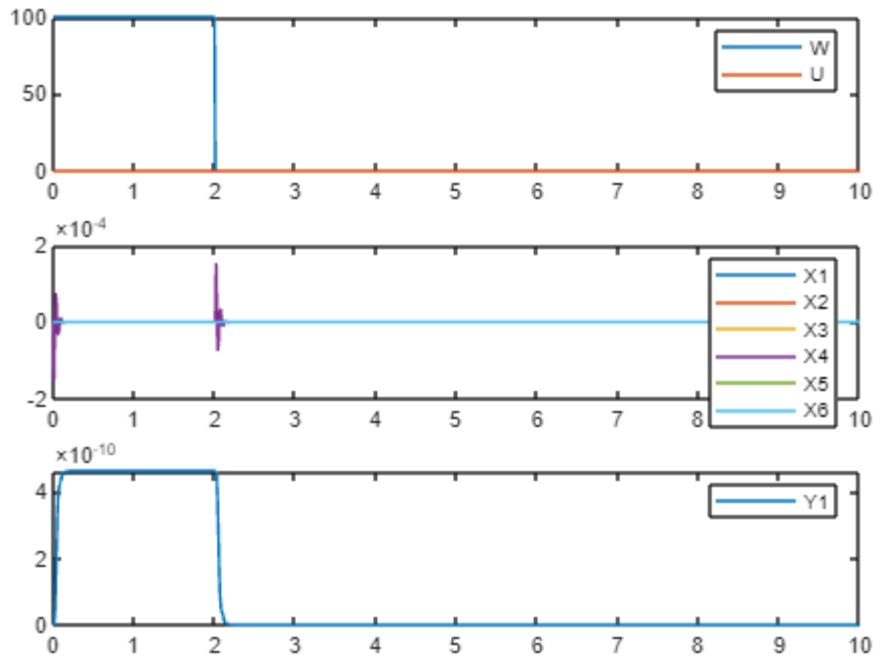
```
D =
```

$$\begin{array}{cc} \mathbf{u}_1 & \mathbf{u}_2 \\ \mathbf{y}_1 & 0 \\ \mathbf{y}_2 & 0 \end{array}$$

Continuous-time state-space model.

Model Properties

Closed-Loop System Response



$A_0 = 6 \times 6$

0	0	0	1	0	0
0	0	0	0	1	0
0	0	0	0	0	1

```

-100    100     0     0     0     0
      50    -50     0     0     0     0
       0     0     0     0     0     0
A1 = 6x6
       0     0     0     0     0     0
       0     0     0     0     0     0
       0     0     0     0     0     0
       0     0     0     0     0     0
       0   -0.0250    0.0250     0     0     0
       0    0.0333   -0.0333     0     0     0
B0 = 6x2
       0     0
       0     0
       0     0
    0.0500    0.0500
       0     0
       0     0
C0 = 2x6
       0     0     0     0     0     0
       0     0     1     0     0     0
D0 = 2x2
       0     0
       0     0
S0 = 9x9
       0     0     0    1.0000     0     0     0
 0    6.0000
       0     0     0     0    1.0000     0     0
 0     0
       0     0     0     0     0    1.0000     0
 0     0
 -100.0000 100.0000     0     0     0     0    0.0500
 0.0500     0
 50.0000 -50.0000     0     0     0     0     0
 0     0
       0     0     0     0     0     0     0
 0     0
       0     0     0     0     0     0     0
 0     0
       0     0    1.0000     0     0     0     0
 0     0
       0     0     0     0     0     0     0
 0     0
       -Inf
S1 = 9x9 complex
 0.0000 - 1.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
 0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
 6.0000 + 0.0000i
 0.0000 + 0.0000i  0.0000 - 1.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
 0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
 0.0000 + 0.0000i
 0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 - 1.0000i  0.0000 + 0.0000i
 0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
 0.0000 + 0.0000i
 0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 - 1.0000i
 0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
 0.0000 + 0.0000i

```



```

0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  -0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 - 0.0010i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i
    0.0100 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i
    0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0010 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i
    0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  -Inf + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
-Inf + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i  0.0000 + 0.0000i
0.0000 + 0.0000i  0.0000 + 0.0000i
Select a region among the following:
```

- h)** Half-plane
- d)** Disk
- c)** Conic sector
- e)** Ellipsoid
- p)** Parabola
- s)** Horizontal strip
- m)** Matrix description of the LMI region
- q)** Quit

Select a region among the following:

- h)** Half-plane
- d)** Disk
- c)** Conic sector
- e)** Ellipsoid
- p)** Parabola
- s)** Horizontal strip
- m)** Matrix description of the LMI region
- q)** Quit

Optimization of 0.000 * G^2 + 1.000 * H^2 :

Solver for linear objective minimization under LMI constraints

Iterations : Best objective value so far

1
2

3
4
5
6
7
8
9
10
11 0.174617
12 0.084142
13 0.084142
14 0.084142
15 0.035606
16 0.035606
17 0.035606
18 0.019613
19 0.019613
20 0.019613
21 0.011597
22 0.011597
23 0.011597
24 7.440620e-03
25 7.440620e-03
26 7.440620e-03
27 4.761071e-03
28 4.761071e-03
29 4.761071e-03
30 3.057379e-03
31 3.057379e-03
32 3.057379e-03
33 2.094639e-03
34 2.094639e-03
35 2.094639e-03
36 1.728979e-03
37 1.728979e-03
38 1.728979e-03
39 1.401557e-03
40 1.401557e-03
41 1.401557e-03
42 7.898234e-04
43 7.898234e-04
44 7.898234e-04
45 3.528895e-04
46 3.528895e-04
47 3.528895e-04
48 1.357855e-04
49 1.357855e-04
50 1.357855e-04
51 5.390543e-05
52 5.390543e-05
53 5.390543e-05
54 2.140225e-05
55 2.140225e-05
56 2.140225e-05
57 1.012459e-05
58 1.012459e-05
59 1.012459e-05

```

60      5.006723e-06
61      5.006723e-06
62      5.006723e-06
63      2.216772e-06
64      2.216772e-06
65      2.216772e-06
66      9.611413e-07

```

Result: reached the target for the objective value
 best objective value: 9.611413e-07
 f-radius saturation: 0.243% of R = 1.00e+10

Guaranteed H2 performance: 9.80e-04

glopt =

```

[]
g2opt = 9.8038e-04
G2 = 1x6
1011 x
-0.0009 -0.2480 -1.9988 -0.0000 -0.0028 -0.0997
Scl = 9x19
109 x
-Inf 0 0 0 0 0 0 0 0
0 0 0.0000 0 0 0 0 0 0
0 0 0 0.0000 0 0 0 0 0
0 0.0000 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0 0
0.0000 0 0 0 0 0 0 0 0
0.0000 0 0 0 0 0 0 0 0
0.0000 0 0 0 0 0 0 0 0
0 0.0000 0 0 0 0 0 0 0
0.0000 0 -0.0046 -1.2400 -9.9938 -0.0000 -0.0138 -
0.4987 0.0000 0 0 -0.0046 -1.2400 -9.9938 -0.0000
-0.0138 -0.4987 0.0000 0
0.0000 0 0.0000 -0.0000 0.0000 0 0
0 0 0 0.0000 -0.0000 0.0000 0
0 0 0 0 0 0 0
0.0000 0 0 0.0000 -0.0000 0 0
0 0 0 0 0 0 0
0 0 0 0 0 0 0
0 0 0 0 0 0 0
0 0 0 0 0.0000 0 0
0 0 0 0 0 0 0.0000 0
0 0 0 0 0 0 0
0 0 -Inf 0 0 0 0
0 0 0 -Inf 0 0 0 0

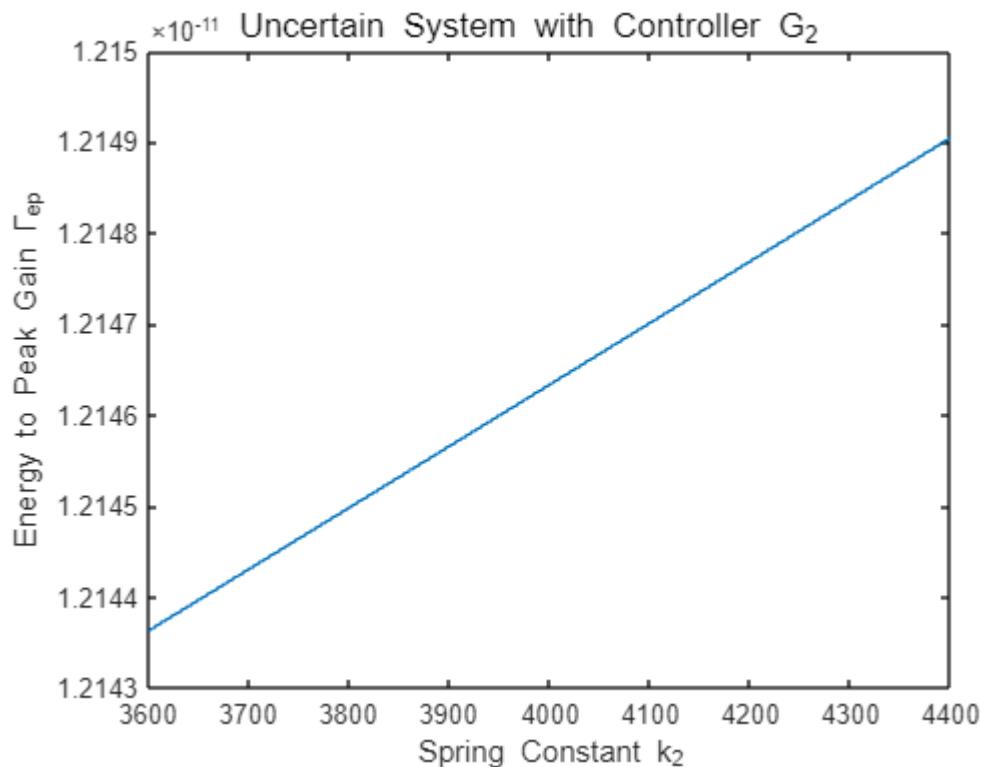
```

```

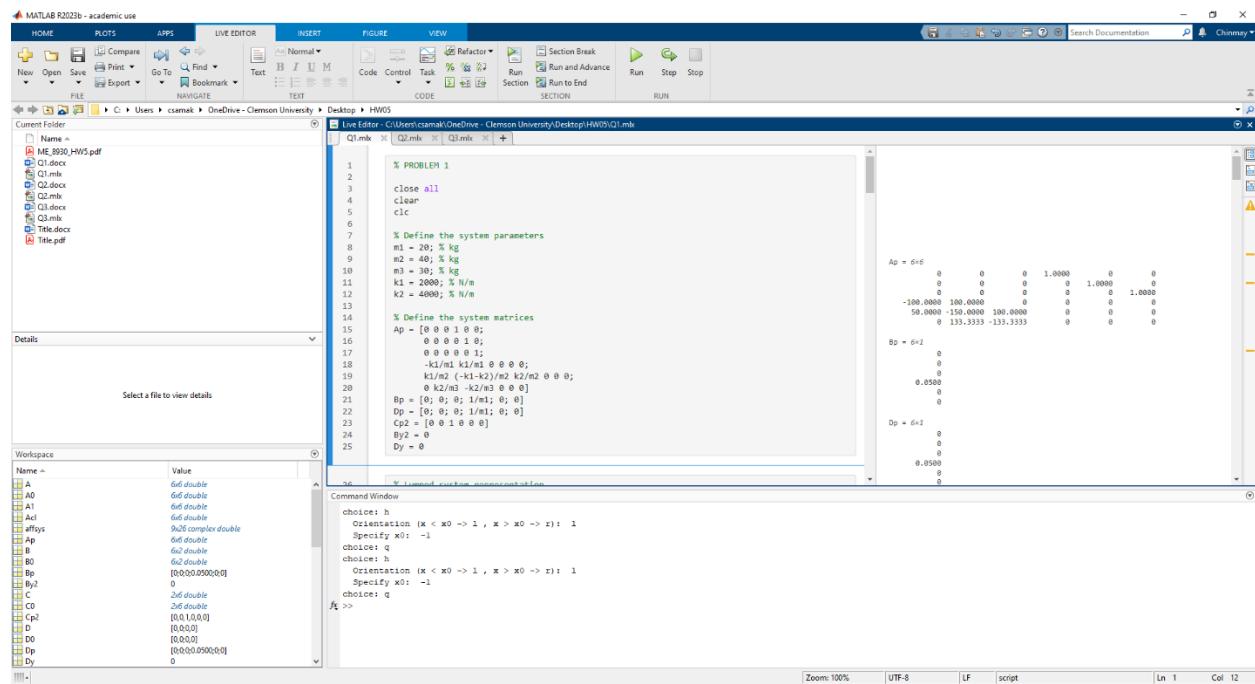
X = 6x6
105 x
0.0013 0.0000 0.0000 -0.0411 -0.0008 -0.0000
0.0000 0.0000 0.0000 0.0000 -0.0000 -0.0000
0.0000 0.0000 0.0000 -0.0000 0.0000 -0.0000
-0.0411 0.0000 -0.0000 5.9055 0.0058 0.0001
-0.0008 -0.0000 0.0000 0.0058 0.0007 0.0000

```

$-0.0000 \quad -0.0000 \quad -0.0000 \quad 0.0001 \quad 0.0000 \quad 0.0000$
 Optimal guaranteed energy-to-peak gain for the uncertain system is:
 $9.8038e-04$



SCREENSHOT:



$$\dot{x}_p = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} x_p + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u + \begin{bmatrix} 0 & 0 \\ 1 & 0 \end{bmatrix} \omega \Rightarrow n_p = 2$$

$$y = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} x_p + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$z = [1 \ 0] x_p + [0 \ 1] \omega$$

Optimal H_∞ controller design ($n_c = 1$)

$\Gamma_{ee} < y \Rightarrow$ reduced order ($n_c < n_p$)

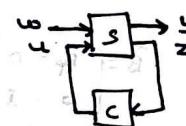
$$\hookrightarrow \gamma = 3, 4, 5$$

General form

$$\text{#} \quad \dot{x}_p = A_p x_p + B_p u + D_p \omega$$

$$y = C_p x_p + B_y u + D_y \omega$$

$$z = M_p x_p + D_z \omega$$



Comparing given system equations with general form

$$A_p = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \quad B_p = \begin{bmatrix} 0 \\ 1 \end{bmatrix} \quad D_p = \begin{bmatrix} 0 & 0 \\ 1 & 0 \end{bmatrix}$$

$$C_p = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \quad B_y = \begin{bmatrix} 0 \\ 1 \end{bmatrix} \quad D_y = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}$$

$$M_p = [1 \ 0] \quad D_z = [0 \ 1]$$

④ Use above system matrices to obtain X and Y

using Standard LMI method and/or Alternating Projection Method (discussed later).

Confirm that $\text{rank}[R] = \text{rank}\begin{bmatrix} X & X^{-1} \\ Y & Y \end{bmatrix} = 3$

↳ This guarantees existence of first order controller

Perform SVD of $\underbrace{Y - \gamma^2 X^{-1}}_{n_p \times n_p}$

$$\text{SVD } (Y - \gamma^2 X^{-1}) = U \Sigma V^T = \underbrace{\begin{bmatrix} U_1 & U_2 \end{bmatrix}}_{n_p \times n_p} \underbrace{\begin{bmatrix} Z_1 & 0 \\ 0 & 0 \end{bmatrix}}_{n_p \times n_p} \underbrace{\begin{bmatrix} V_1^T \\ V_2^T \end{bmatrix}}_{n_c \times n_c}$$

$$\text{Let } \left\{ \begin{array}{l} Y_{11} \in \mathbb{R}^{n \times n} = Y \\ Y_{22} \in \mathbb{R}^{n \times n} = I \\ Y_{12} \in \mathbb{R}^{n \times n} = U_1 \Sigma V_2^T \end{array} \right\} \Rightarrow Y - \gamma^2 X^{-1} = Y_{12} Y_{22}^{-1} Y_{12}^T$$

Construct the augmented matrix

$$P = \begin{bmatrix} Y & Y_{12} \\ Y_{12}^T & Y_{22} \end{bmatrix}$$

Find unknown controller parameters by solving the General Matrix Inequality

$$\Gamma G \Lambda + (\Gamma G \Lambda)^T + Q < 0$$

where $\Gamma = \begin{bmatrix} PB \\ 0 \\ H \end{bmatrix}$, $\Lambda = [M \ E \ 0]$, $Q = \begin{bmatrix} PA + A^T P & PD & C^T \\ D^T P & -\gamma^2 I & F^T \\ C & F & -I \end{bmatrix}$

where:

$$A = \begin{bmatrix} A_p & 0 \\ 0 & 0 \end{bmatrix} \quad B = \begin{bmatrix} B_p & 0 \\ 0 & I \end{bmatrix}$$

$$M = \begin{bmatrix} M_p & 0 \\ 0 & I \end{bmatrix} \quad E = \begin{bmatrix} D_p \\ 0 \end{bmatrix}$$

$$H = \begin{bmatrix} B_q & 0 \end{bmatrix} \quad D = \begin{bmatrix} D_p \\ 0 \end{bmatrix}$$

$$C = \begin{bmatrix} C_p & 0 \end{bmatrix} \quad F = D_q$$

$$G = \begin{bmatrix} P_c & C_c \\ B_c & A_c \end{bmatrix}$$

unknown

i.e. Use P and A, B, C, D, E, F, H, M to solve "basiclmi"

$$\Gamma, \Lambda, Q$$

$$G = \text{basiclmi}(Q, \Gamma^T, \Lambda)$$

Use partitioned form of controller matrix G to obtain A_c, B_c, C_c and D_c .

Standard LMI Method:

$$\min \text{trace}(X+Y)$$

X, Y are usually unknown/variable but known in this problem [$Y = 3, 4, 5$]

$$\text{s.t. } \begin{bmatrix} B_p \\ B_y \end{bmatrix}^T \begin{bmatrix} A_p X + X A_p^T + D_p D_p^T & X C_p^T + P_p D_p^T \\ C_p X + D_p D_p^T & D_p D_p^T - Y^2 I \end{bmatrix} \begin{bmatrix} B_p \\ B_y \end{bmatrix} < 0 \quad (C_1)$$

$$\begin{bmatrix} M_p \\ D_2 \end{bmatrix}^T \begin{bmatrix} Y A_p + A_p^T Y + C_p^T C_p & Y D_p + C_p^T D_p \\ D_p^T Y + D_p^T C_p & D_p^T D_p - Y^2 I \end{bmatrix} \begin{bmatrix} M_p \\ D_2 \end{bmatrix} < 0 \quad (C_2)$$

$$\begin{bmatrix} X & Y I \\ Y I & Y \end{bmatrix} \geq 0 \quad (C_3)$$

Alternating Projection Method:

$$\text{rank} \begin{bmatrix} X & Y I \\ Y I & Y \end{bmatrix} \leq n_p + n_c \quad (C_4)$$

Non-convex constraint

Idea: Iteratively projecting on LMIs ($C_1 - C_3$) and the rank constraint (C_4), back & forth until convergence is met.

Approach: 

Solve $(C_1) - (C_3)$ as an LMI problem to obtain X and Y

$$\text{Let } R = \begin{bmatrix} X & Y I \\ Y I & Y \end{bmatrix}$$

for iteration = 1: max_iterations (say 100)

- Enforce the rank constraint (if not satisfied)

$$U \Sigma V^T = \text{svd}(R) ; \Sigma = \begin{bmatrix} \sigma_1 & & 0 \\ & \ddots & \\ 0 & & \sigma_n \end{bmatrix} \text{ with } \sigma_1 > \sigma_2 > \dots > \sigma_{n-1} > \sigma_n$$

If we replace smallest σ_i of R (i.e. σ_n) by zero we get

$$R' = U \begin{bmatrix} \sigma_1 & & 0 \\ & \ddots & \\ 0 & & 0 \end{bmatrix} V^T \text{ whose rank is one less than original } R.$$

Instead of replacing one σ_i with 0, we can replace multiple (m)

so that rank constraint is satisfied.

- Else (if rank constraint is satisfied)

$$R' = R$$

- $\min \|R - R'\|$ ← If $\|R - R'\| < \text{tolerance} \Rightarrow \text{break}$

R' is solution to $(C_1) - (C_3)$

St: $\{ R \text{ is solution to } (C_1) - (C_3) \}$
 $\text{rank}(R') = k-m \quad \dots \text{(using svd)}$

Working space

$\min \|R_1 - R'\|$ \leftarrow If $\|R_1 - R'\| < \text{tolerance} \Rightarrow \text{break}$
 s.t. $R_1 \in \text{LMIs } (C_1) - (C_0)$ $\left\{ \begin{array}{l} R_1 \text{ is the closest approximation} \\ \text{to } R' \text{ used for projection} \end{array} \right.$

Projection onto C_0 space
& working in C_0 space

$$\begin{aligned}
 & \min_{R_1} \|R_1 - R'\| \\
 & \text{s.t. } R_1 \in \text{LMIs } (C_1) - (C_0) \\
 & \quad \Rightarrow \|R_1 - R'\| \leq \hat{\gamma} \begin{bmatrix} I - \hat{\gamma}^2 I & R_1 - R' \\ R_1 - R' & -I \end{bmatrix} \leq 0
 \end{aligned}$$

Get R_1

Set $R = R_1$

Projection onto
(lock) $(C_1) - (C_0)$ space

Continue to go back and forth by
iterating while projecting on $\text{LMIs } (C_1) - (C_0)$
space and rank constraint $\delta(C_0)$ space
until convergence is met (i.e. termination
criteria based on tolerance or max-iterations
is reached).

Problem 2

CODE:

```
% PROBLEM 2

% Clear workspace
close all
clear
clc

% Add parser and solver to path
addpath(genpath('C:\Users\csamak\Downloads\MathWorks\Toolboxes\archives\required\
YALMIP'))
addpath(genpath('C:\Users\csamak\Downloads\MathWorks\Toolboxes\archives\required\
SeDuMi'))

for g = 3:1:5 % Gamma (γ)
    disp('-----')
    if g == 3
        disp('Standard LMI Method | CASE 1: γ = 3')
    elseif g == 4
        disp('Standard LMI Method | CASE 2: γ = 4')
    elseif g == 5
        disp('Standard LMI Method | CASE 3: γ = 5')
    end
    disp('-----')

% Define the system matrices
Ap = [0 1; 0 0];
Bp = [0; 1];
Dp = [0 0; 1 0];
Cp = [0 1; 0 0];
By = [0; 1];
Dy = [0 0; 0 0];
Mp = [1 0];
Dz = [0 1];

% Define the LMI variables
X = sdpvar(2, 2);
Y = sdpvar(2, 2);

% Define the LMI constraints
```

```

C1 = null([Bp; By])' * [(Ap*X + X*Ap' + Dp*Dp') (X*Cp' + Dp*Dy'); (Cp*X +
Dy*Dp') (Dy*Dy' - g^2*eye(size(Dy)))] * null([Bp; By]) <= 0;
C2 = null([Mp'; Dz'])' * [(Y*Ap + Ap'*Y + Cp'*Cp) (Y*Dp + Cp'*Dy); (Dp'*Y +
Dy'*Cp) (Dy'*Dy - g^2*eye(size(Dy)))] * null([Mp'; Dz']) <= 0;
C3 = [X g*eye(size(Dy)); g*eye(size(Dy)) Y] >= 0;

% Set up the objective
Objective = trace(X + Y);

% Define the solver settings (use an LMI solver like YALMIP with a solver of
your choice)
options = sdpsettings('verbose', 1, 'solver', 'sedumi');

% Solve the LMI problem
solution = optimize([C1, C2, C3], Objective, options);

% 1. Obtain X and Y by solving above optimization problem
if solution.problem == 0
    % Extract the optimal solutions
    X = value(X);
    Y = value(Y);
    % Display the results
    disp('X*:');
    disp(X);
    disp('Y*:');
    disp(Y);
else
    fprintf('LMI problem could not be solved.\n');
end

% 2. Confirm that rank([X gamma*I; gamma*I Y]) = 3 and compute terms Y12 and Y22
if rank([X g*eye(size(Dy)); g*eye(size(Dy)) Y]) == 3
    disp('rank([X gamma*I; gamma*I Y]) = 3')
    disp('Solving LMI problem resulted in reduced order controller with nc =
1')
elseif rank([X g*eye(size(Dy)); g*eye(size(Dy)) Y]) == 4
    disp('rank([X gamma*I; gamma*I Y]) = 4')
    disp('Solving LMI problem resulted in full order controller with nc = 2')
else
    disp('rank([X gamma*I; gamma*I Y]) < 3')
    disp('Solving LMI problem resulted in zero order controller with nc = 0')
end
[U, S, V] = svd(Y - g^2*inv(X));
u1 = U(:,1); % Extract u1 so that u1 = np x nc
S1 = S(1,1); % Extract S1 so that S1 = nc x nc
disp('Extracted u1 & S1 so as to obtain reduced order controller with nc =
1')
Y12 = u1*(S1^0.5)

```

```

Y22 = eye(size(Y12', 1), size(Y12, 2))

% 3. Define augmented matrix P & find controller by solving general matrix
inequality
P = [Y Y12; Y12' Y22]
A = [Ap [0; 0]; [0 0] 0];
B = [Bp [0; 0]; 0 1];
C = [Cp [0; 0]];
D = [Dp; [0 0]];
E = [Dz; [0 0]];
F = Dy;
H = [By [0; 0]];
M = [Mp 0; [0 0] 1];
Gamma = [P*B; [0 0]; [0 0]; H] % Γ
Lambda = [M E [0; 0] [0; 0]] % Λ
Q = [P*A+A'*P P*D C'; D'*P -g^2*eye(2) F'; C F -eye(2)] % Q
G = basiclmi(Q, Gamma', Lambda); % Solve general matrix inequality
if size(G) ~= 0
    disp('Controller matrix (G):')
    disp(G)
    fprintf('Ac = %f', value(G(2,2)))
    fprintf('Bc = %f', value(G(2,1)))
    fprintf('Cc = %f', value(G(1,2)))
    fprintf('Dc = %f', value(G(1,1)))
end
end

```

```

% Clear workspace
close all
clear
clc

% Add parser and solver to path
addpath(genpath('C:\Users\csamak\Downloads\MathWorks\Toolboxes\archives\required\
YALMIP'))
addpath(genpath('C:\Users\csamak\Downloads\MathWorks\Toolboxes\archives\required\
SeDuMi'))

for g = 3:1:5 % Gamma (γ)
    disp('-----')
    if g == 3
        disp('Alternating Projection Method | CASE 1: γ = 3')
    elseif g == 4
        disp('Alternating Projection Method | CASE 2: γ = 4')
    end
end

```

```

elseif g == 5
    disp('Alternating Projection Method | CASE 3: γ = 5')
end
disp('-----')

% Define the system matrices
Ap = [0 1; 0 0];
Bp = [0; 1];
Dp = [0 0; 1 0];
Cp = [0 1; 0 0];
By = [0; 1];
Dy = [0 0; 0 0];
Mp = [1 0];
Dz = [0 1];

% Define the LMI variables
X = sdpvar(2, 2);
Y = sdpvar(2, 2);

% Define the LMI constraints
C1 = null([Bp; By]')' * [(Ap*X + X*Ap' + Dp*Dp') (X*Cp' + Dp*Dy'); (Cp*X + Dy*Dp') (Dy*Dy' - g^2*eye(size(Dy)))] * null([Bp; By]') <= 0;
C2 = null([Mp'; Dz']')' * [(Y*Ap + Ap'*Y + Cp'*Cp) (Y*Dp + Cp'*Dy); (Dp'*Y + Dy'*Cp) (Dy'*Dy - g^2*eye(size(Dy)))] * null([Mp'; Dz']') <= 0;
C3 = [X g*eye(size(Dy)); g*eye(size(Dy)) Y] >= 0;

% Set up the objective
Objective = trace(X + Y);

% Define the solver settings (use an LMI solver like YALMIP with a solver of
your choice)
options = sdpsettings('verbose', 1, 'solver', 'sedumi');

% Alternating projection method
max_iterations = 100;
tolerance = 1e-22;

% Working in C1-C3 space
solution = optimize([C1, C2, C3], Objective, options);
if solution.problem == 0
    X = value(X);
    Y = value(Y);
end
R = [X, g*eye(size(Dy)); g*eye(size(Dy)), Y];

for iteration = 1:max_iterations
    [U, S, V] = svd(R);

```

```

if not(rank(R) == 3)
    S(size(S,1), size(S,2)) = 0;
    R_prime = U*S*V';
else
    R_prime = R;
end
% Check for convergence between R and R_prime
if norm(R - R_prime) < tolerance
    disp(['Converged at iteration ', num2str(iteration)]);
    break;
end
% Projection onto C4 space & working in C4 space
R1 = sdpvar(size(R,1), size(R,2)); % Define the LMI variable
g_sqr = sdpvar(1, 1); % Define the LMI variable
LMI_R1 = [-g_sqr*eye(size(R)) R1-R_prime; R1-R_prime -eye(size(R))] <= 0;
% Define the LMI constraint
Objective_R1 = g_sqr; % Set up the objective
solution_R1 = optimize(LMI_R1, Objective_R1, options); % Solve the LMI
problem
if solution_R1.problem == 0
    R1 = value(R1); % Extract the optimal solution
end
% Check for convergence between R1 and R_prime
if norm(R1 - R_prime) < tolerance
    disp(['Converged at iteration ', num2str(iteration)]);
    break;
end
% Projection onto C1-C3 space
R = R1;
end

% Display the results
disp('X*:');
disp(X);
disp('Y*:');
disp(Y);

% Display rank information
if rank(R_prime) == 3
    disp('Solving LMI problem resulted in a reduced-order controller with nc = 1');
else
    disp('Rank constraint not satisfied.');
    return; % Exit if the rank constraint is not satisfied
end

% Extract u1 & Σ1 to obtain reduced order controller with nc = 1
[U, S, V] = svd(Y - g^2*inv(X));

```

```

u1 = U(:, 1);
S1 = S(1, 1);
Y12 = u1 * (S1^0.5);
Y22 = eye(size(Y12', 1), size(Y12, 2));

% Define augmented matrix P for the controller
P = [Y, Y12; Y12'; Y22];

% Obtain the controller matrix G
A = [Ap, [0; 0]; [0 0], 0];
B = [Bp, [0; 0]; 0, 1];
C = [Cp, [0; 0]];
D = [Dp; [0 0]];
E = [Dz; [0 0]];
F = Dy;
H = [By, [0; 0]];
M = [Mp, 0; [0 0], 1];
Gamma = [P * B; [0 0]; [0 0]; H]; % Γ
Lambda = [M, E, [0; 0], [0; 0]]; % Λ
Q = [P * A + A' * P, P * D, C'; D' * P, -g^2 * eye(2), F'; C, F, -eye(2)]; %

Q
G = basiclmi(Q, Gamma', Lambda); % Solve general matrix inequality
if size(G) ~= 0
    disp('Controller matrix (G):')
    disp(G)
    fprintf('Ac = %f', value(G(2,2)))
    fprintf('Bc = %f', value(G(2,1)))
    fprintf('Cc = %f', value(G(1,2)))
    fprintf('Dc = %f', value(G(1,1)))
end
end

```

OUTPUT:

```

-----
Standard LMI Method | CASE 1: γ = 3
-----
SeDuMi 1.3 by AdvOL, 2005-2008 and Jos F. Sturm, 1998-2003.
Alg = 2: xz-corrector, theta = 0.250, beta = 0.500
eqs m = 6, order n = 11, dim = 35, blocks = 4
nnz(A) = 20 + 0, nnz(ADA) = 36, nnz(L) = 21
it :      b*y      gap    delta   rate   t/tP*   t/tD*   feas cg cg  prec
 0 :          2.71E+01 0.000
 1 : -5.65E+00 9.11E+00 0.000 0.3364 0.9000 0.9000 1.41 1 1 3.2E+00
 2 : -1.25E+01 2.87E+00 0.000 0.3153 0.9000 0.9000 0.91 1 1 9.6E-01
 3 : -1.70E+01 6.35E-01 0.000 0.2209 0.9000 0.9000 0.66 1 1 2.5E-01
 4 : -1.98E+01 5.13E-02 0.000 0.0808 0.9900 0.9900 0.78 1 1 2.1E-02
 5 : -2.01E+01 1.90E-03 0.000 0.0369 0.9900 0.9900 0.99 1 1 8.3E-04
 6 : -2.01E+01 1.03E-04 0.407 0.0545 0.9900 0.9900 1.00 1 1 4.5E-05
 7 : -2.01E+01 7.99E-06 0.254 0.0773 0.9900 0.9900 1.00 1 1 3.5E-06

```

```

8 : -2.01E+01 7.20E-07 0.438 0.0902 0.9900 0.9900 1.00 1 1 3.2E-07
9 : -2.01E+01 1.51E-07 0.000 0.2100 0.9000 0.9000 1.00 2 2 6.7E-08
10 : -2.01E+01 1.86E-08 0.017 0.1233 0.9450 0.9450 1.00 2 2 8.3E-09
11 : -2.01E+01 1.61E-09 0.060 0.0865 0.9900 0.9900 1.00 2 2 7.2E-10

iter seconds digits      c*x          b*y
11       0.2    9.8 -2.0062574492e+01 -2.0062574496e+01
|Ax-b| = 4.8e-10, [Ay-c]_+ = 9.5E-10, |x|= 1.1e+01, |y|= 1.1e+01

Detailed timing (sec)
      Pre           IPM           Post
3.090E-01     5.140E-01     3.300E-02
Max-norms: ||b||=1, ||c|| = 9,
Cholesky |add|=0, |skip| = 0, ||L.L|| = 6.52152.

X*:
 6.9382   -1.0201
-1.0201   3.9239

Y*:
 4.2969   -2.3744
-2.3744   4.9036
rank([X y*I; y*I Y]) = 4
Solving LMI problem resulted in full order controller with nc = 2
Extracted u1 & Σ1 so as to obtain reduced order controller with nc = 1
Y12 = 2x1
-1.7170
 1.5871
Y22 = 1
P = 3x3
 4.2969   -2.3744   -1.7170
-2.3744   4.9036   1.5871
-1.7170   1.5871   1.0000
Gamma = 7x2
-2.3744   -1.7170
 4.9036   1.5871
 1.5871   1.0000
 0         0
 0         0
 0         0
 1.0000   0
Lambda = 2x7
 1         0         0         0         1         0         0
 0         0         1         0         0         0         0
Q = 7x7
 0     4.2969     0     -2.3744     0         0         0
 4.2969   -4.7488   -1.7170   4.9036     0     1.0000   0
 0     -1.7170     0     1.5871     0         0         0
-2.3744   4.9036   1.5871   -9.0000     0         0         0
 0         0         0         0     -9.0000     0         0
 0     1.0000     0         0         0     -1.0000     0
 0         0         0         0         0         0     -1.0000
Warning in BASICLMI: the solvability conditions are not satisfied
-----
Standard LMI Method | CASE 2: γ = 4
-----
SeDuMi 1.3 by AdvOL, 2005-2008 and Jos F. Sturm, 1998-2003.
Alg = 2: xz-corrector, theta = 0.250, beta = 0.500
eqs m = 6, order n = 11, dim = 35, blocks = 4

```

```

nnz(A) = 20 + 0, nnz(ADA) = 36, nnz(L) = 21
it :      b*y      gap    delta   rate   t/tP*   t/tD*   feas cg cg prec
 0 :          4.74E+01 0.000
 1 : -7.71E+00 1.53E+01 0.000 0.3239 0.9000 0.9000 1.46 1 1 2.8E+00
 2 : -1.67E+01 4.33E+00 0.000 0.2820 0.9000 0.9000 1.04 1 1 8.1E-01
 3 : -2.02E+01 8.97E-01 0.000 0.2072 0.9000 0.9000 0.83 1 1 1.8E-01
 4 : -2.23E+01 4.34E-02 0.000 0.0484 0.9900 0.9900 0.85 1 1 8.9E-03
 5 : -2.25E+01 2.43E-03 0.160 0.0560 0.9675 0.9675 1.00 1 1 5.0E-04
 6 : -2.25E+01 2.68E-04 0.198 0.1101 0.9450 0.9450 1.00 1 1 5.5E-05
 7 : -2.25E+01 2.09E-05 0.319 0.0779 0.9900 0.9900 1.00 1 1 4.3E-06
 8 : -2.25E+01 9.96E-06 0.205 0.4772 0.9000 0.9000 1.00 1 1 2.1E-06
 9 : -2.25E+01 2.48E-06 0.000 0.2490 0.9000 0.9000 1.00 1 1 5.2E-07
10 : -2.25E+01 2.29E-07 0.369 0.0922 0.9900 0.9900 1.00 2 2 4.9E-08
11 : -2.25E+01 8.19E-08 0.171 0.3580 0.9000 0.9000 1.00 2 2 1.8E-08
12 : -2.25E+01 6.92E-09 0.149 0.0845 0.9900 0.9900 1.00 2 2 1.5E-09
13 : -2.25E+01 6.74E-10 0.139 0.0974 0.9900 0.9900 1.00 2 2 1.5E-10

iter seconds digits      c*x          b*y
13       0.0  10.2 -2.2456285268e+01 -2.2456285269e+01
|Ax-b| = 8.7e-11, [Ay-c]_+ = 2.7E-10, |x|= 7.9e+00, |y|= 1.2e+01

Detailed timing (sec)
      Pre        IPM        Post
1.200E-02    3.201E-02    2.997E-03
Max-norms: ||b||=1, ||c|| = 16,
Cholesky |add|=0, |skip| = 0, ||L.L|| = 4.35694.
X*:
  6.9145  -0.8214
 -0.8214   4.9001
Y*:
  4.9551  -2.0759
 -2.0759   5.6866
rank([X y*I; y*I Y]) = 4
Solving LMI problem resulted in full order controller with nc = 2
Extracted u1 & E1 so as to obtain reduced order controller with nc = 1
Y12 = 2x1
 -1.6106
  1.5346
Y22 = 1
P = 3x3
  4.9551  -2.0759  -1.6106
 -2.0759   5.6866   1.5346
 -1.6106   1.5346   1.0000
Gamma = 7x2
 -2.0759  -1.6106
  5.6866   1.5346
  1.5346   1.0000
   0       0
   0       0
   0       0
  1.0000   0
Lambda = 2x7
  1       0       0       0       1       0       0
   0       0       1       0       0       0       0
Q = 7x7
   0     4.9551       0   -2.0759       0       0       0
 4.9551  -4.1518  -1.6106   5.6866       0   1.0000       0

```

```

      0   -1.6106       0   1.5346       0       0       0
-2.0759    5.6866   1.5346  -16.0000       0       0       0
      0       0       0       0  -16.0000       0       0
      0   1.0000       0       0       0  -1.0000       0
      0       0       0       0       0       0  -1.0000
Controller matrix (G):
-2.6758   1.3083
 8.5579  -5.0717
Ac = -5.071654
Bc = 8.557912
Cc = 1.308284
Dc = -2.675828
-----
Standard LMI Method | CASE 3: γ = 5
-----
SeDuMi 1.3 by AdvOL, 2005-2008 and Jos F. Sturm, 1998-2003.
Alg = 2: xz-corrector, theta = 0.250, beta = 0.500
eqs m = 6, order n = 11, dim = 35, blocks = 4
nnz(A) = 20 + 0, nnz(ADA) = 36, nnz(L) = 21
it : b*y      gap    delta   rate   t/tP*   t/tD*   feas cg cg prec
 0 :      7.35E+01 0.000
 1 : -1.03E+01 2.28E+01 0.000 0.3097 0.9000 0.9000 1.48 1 1 2.6E+00
 2 : -2.10E+01 5.93E+00 0.000 0.2602 0.9000 0.9000 1.11 1 1 7.3E-01
 3 : -2.36E+01 1.27E+00 0.000 0.2149 0.9000 0.9000 0.92 1 1 1.6E-01
 4 : -2.57E+01 5.44E-02 0.000 0.0427 0.9900 0.9900 0.87 1 1 7.1E-03
 5 : -2.58E+01 2.00E-03 0.024 0.0368 0.9900 0.9900 1.00 1 1 2.6E-04
 6 : -2.58E+01 2.24E-04 0.206 0.1119 0.9450 0.9450 1.00 1 1 2.9E-05
 7 : -2.58E+01 1.85E-05 0.480 0.0825 0.9900 0.9900 1.00 1 1 2.4E-06
 8 : -2.58E+01 8.75E-06 0.164 0.4733 0.9000 0.9000 1.00 1 1 1.2E-06
 9 : -2.58E+01 1.63E-06 0.000 0.1859 0.9000 0.9000 1.00 1 1 2.2E-07
10 : -2.58E+01 1.36E-07 0.471 0.0837 0.9900 0.9900 1.00 1 2 1.8E-08
11 : -2.58E+01 2.69E-08 0.000 0.1976 0.9000 0.9000 1.00 2 2 3.6E-09
12 : -2.58E+01 1.17E-09 0.359 0.0434 0.9900 0.9900 1.00 2 2 1.6E-10

iter seconds digits      c*x          b*y
 12        0.0  10.1 -2.5756604760e+01 -2.5756604762e+01
|Ax-b| =  8.3e-11, [Ay-c]_+ =  4.2E-10, |x|=  6.6e+00, |y|=  1.3e+01

Detailed timing (sec)
      Pre        IPM        Post
3.300E-02    2.400E-02    2.002E-03
Max-norms: ||b||=1, ||c|| = 25,
Cholesky |add|=0, |skip| = 0, ||L.L|| = 4.93398.
X*:
    7.4856   -0.7233
   -0.7233    5.8495
Y*:
    5.8149   -1.9387
   -1.9387    6.6066
rank([X γ*I; γ*I Y]) = 4
Solving LMI problem resulted in full order controller with nc = 2
Extracted u1 & Σ1 so as to obtain reduced order controller with nc = 1
Y12 = 2x1
   -1.5604
    1.5103
Y22 = 1
P = 3x3

```

```

5.8149 -1.9387 -1.5604
-1.9387 6.6066 1.5103
-1.5604 1.5103 1.0000
Gamma = 7x2
-1.9387 -1.5604
6.6066 1.5103
1.5103 1.0000
0 0
0 0
0 0
1.0000 0
Lambda = 2x7
1 0 0 0 1 0 0
0 0 1 0 0 0 0
Q = 7x7
0 5.8149 0 -1.9387 0 0 0
5.8149 -3.8774 -1.5604 6.6066 0 1.0000 0
0 -1.5604 0 1.5103 0 0 0
-1.9387 6.6066 1.5103 -25.0000 0 0 0
0 0 0 0 -25.0000 0 0
0 1.0000 0 0 0 -1.0000 0
0 0 0 0 0 0 -1.0000
Controller matrix (G):
-3.1340 1.6176
11.9541 -7.5012
Ac = -7.501234
Bc = 11.954090
Cc = 1.617626
Dc = -3.134028
-----
Alternating Projection Method | CASE 1: γ = 3
-----
SeDuMi 1.3 by AdvOL, 2005-2008 and Jos F. Sturm, 1998-2003.
Alg = 2: xz-corrector, theta = 0.250, beta = 0.500
eqs m = 6, order n = 11, dim = 35, blocks = 4
nnz(A) = 20 + 0, nnz(ADA) = 36, nnz(L) = 21
it : b*y      gap    delta   rate   t/tP*   t/tD*   feas cg cg prec
0 :          2.71E+01 0.000
1 : -5.65E+00 9.11E+00 0.000 0.3364 0.9000 0.9000 1.41 1 1 3.2E+00
2 : -1.25E+01 2.87E+00 0.000 0.3153 0.9000 0.9000 0.91 1 1 9.6E-01
3 : -1.70E+01 6.35E-01 0.000 0.2209 0.9000 0.9000 0.66 1 1 2.5E-01
4 : -1.98E+01 5.13E-02 0.000 0.0808 0.9900 0.9900 0.78 1 1 2.1E-02
5 : -2.01E+01 1.90E-03 0.000 0.0369 0.9900 0.9900 0.99 1 1 8.3E-04
6 : -2.01E+01 1.03E-04 0.407 0.0545 0.9900 0.9900 1.00 1 1 4.5E-05
7 : -2.01E+01 7.99E-06 0.254 0.0773 0.9900 0.9900 1.00 1 1 3.5E-06
8 : -2.01E+01 7.20E-07 0.438 0.0902 0.9900 0.9900 1.00 1 1 3.2E-07
9 : -2.01E+01 1.51E-07 0.000 0.2100 0.9000 0.9000 1.00 2 2 6.7E-08
10 : -2.01E+01 1.86E-08 0.017 0.1233 0.9450 0.9450 1.00 2 2 8.3E-09
11 : -2.01E+01 1.61E-09 0.060 0.0865 0.9900 0.9900 1.00 2 2 7.2E-10

iter seconds digits      c*x          b*y
11       0.0   9.8 -2.0062574492e+01 -2.0062574496e+01
|Ax-b| = 4.8e-10, [Ay-c]_+ = 9.5E-10, |x|= 1.1e+01, |y|= 1.1e+01

Detailed timing (sec)
Pre           IPM          Post
1.100E-02    3.900E-02    2.997E-03

```

```

Max-norms: ||b||=1, ||c|| = 9,
Cholesky |add|=0, |skip| = 0, ||L.L|| = 6.52152.
SeDuMi 1.3 by AdvOL, 2005-2008 and Jos F. Sturm, 1998-2003.
Alg = 2: xz-corrector, theta = 0.250, beta = 0.500
eqs m = 11, order n = 9, dim = 65, blocks = 2
nnz(A) = 20 + 0, nnz(ADA) = 121, nnz(L) = 66
it :      b*y      gap    delta   rate   t/tP*   t/tD*   feas cg cg prec
 0 :          8.16E+00 0.000
 1 : -2.50E+00 3.13E+00 0.000 0.3836 0.9000 0.9000 2.27 1 1 2.7E+00
 2 : 1.31E-01 8.96E-01 0.000 0.2861 0.9000 0.9000 3.42 1 1 3.8E-01
 3 : 5.07E-03 1.99E-02 0.000 0.0222 0.9900 0.9900 1.25 1 1 1.2E-01
 4 : 1.19E-07 3.91E-07 0.000 0.0000 1.0000 1.0000 1.01 1 1 2.3E-05
 5 : 5.71E-14 1.85E-13 0.442 0.0000 1.0000 1.0000 1.00 1 1 1.1E-11

iter seconds digits      c*x          b*y
      5       0.0     8.9  1.1776667857e-13  5.7097292825e-14
|Ax-b| = 3.0e-14, [Ay-c]_+ = 5.7E-14, |x|= 5.0e-01, |y|= 1.1e+01

Detailed timing (sec)
      Pre           IPM           Post
5.501E-02    2.299E-02    9.002E-03
Max-norms: ||b||=1, ||c|| = 1.387637e+01,
Cholesky |add|=0, |skip| = 0, ||L.L|| = 1.
Converged at iteration 2
X*:
  6.9382  -1.0201
 -1.0201   3.9239
Y*:
  4.2969  -2.3744
 -2.3744   4.9036
Solving LMI problem resulted in a reduced-order controller with nc = 1
  Warning in BASICLMI: the solvability conditions are not satisfied
-----
Alternating Projection Method | CASE 2: y = 4
-----
SeDuMi 1.3 by AdvOL, 2005-2008 and Jos F. Sturm, 1998-2003.
Alg = 2: xz-corrector, theta = 0.250, beta = 0.500
eqs m = 6, order n = 11, dim = 35, blocks = 4
nnz(A) = 20 + 0, nnz(ADA) = 36, nnz(L) = 21
it :      b*y      gap    delta   rate   t/tP*   t/tD*   feas cg cg prec
 0 :          4.74E+01 0.000
 1 : -7.71E+00 1.53E+01 0.000 0.3239 0.9000 0.9000 1.46 1 1 2.8E+00
 2 : -1.67E+01 4.33E+00 0.000 0.2820 0.9000 0.9000 1.04 1 1 8.1E-01
 3 : -2.02E+01 8.97E-01 0.000 0.2072 0.9000 0.9000 0.83 1 1 1.8E-01
 4 : -2.23E+01 4.34E-02 0.000 0.0484 0.9900 0.9900 0.85 1 1 8.9E-03
 5 : -2.25E+01 2.43E-03 0.160 0.0560 0.9675 0.9675 1.00 1 1 5.0E-04
 6 : -2.25E+01 2.68E-04 0.198 0.1101 0.9450 0.9450 1.00 1 1 5.5E-05
 7 : -2.25E+01 2.09E-05 0.319 0.0779 0.9900 0.9900 1.00 1 1 4.3E-06
 8 : -2.25E+01 9.96E-06 0.205 0.4772 0.9000 0.9000 1.00 1 1 2.1E-06
 9 : -2.25E+01 2.48E-06 0.000 0.2490 0.9000 0.9000 1.00 1 1 5.2E-07
10 : -2.25E+01 2.29E-07 0.369 0.0922 0.9900 0.9900 1.00 2 2 4.9E-08
11 : -2.25E+01 8.19E-08 0.171 0.3580 0.9000 0.9000 1.00 2 2 1.8E-08
12 : -2.25E+01 6.92E-09 0.149 0.0845 0.9900 0.9900 1.00 2 2 1.5E-09
13 : -2.25E+01 6.74E-10 0.139 0.0974 0.9900 0.9900 1.00 2 2 1.5E-10

iter seconds digits      c*x          b*y
 13       0.0     10.2 -2.2456285268e+01 -2.2456285269e+01

```

$|Ax-b| = 8.7e-11$, $[Ay-c]_+ = 2.7E-10$, $|x|= 7.9e+00$, $|y|= 1.2e+01$

Detailed timing (sec)
 Pre IPM Post
 2.100E-02 2.800E-02 2.002E-03
 Max-norms: $\|b\|=1$, $\|c\|=16$,
 Cholesky |add|=0, |skip|=0, $\|L.L\|=4.35694$.
 SeDuMi 1.3 by AdvOL, 2005-2008 and Jos F. Sturm, 1998-2003.
 Alg = 2: xz-corrector, theta = 0.250, beta = 0.500
 eqs m = 11, order n = 9, dim = 65, blocks = 2
 nnz(A) = 20 + 0, nnz(ADA) = 121, nnz(L) = 66

it :	b*y	gap	delta	rate	t/tP*	t/tD*	feas	cg	cg	prec
0 :		8.16E+00	0.000							
1 :	-2.49E+00	3.13E+00	0.000	0.3838	0.9000	0.9000	2.28	1	1	2.7E+00
2 :	1.30E-01	8.94E-01	0.000	0.2857	0.9000	0.9000	3.42	1	1	3.8E-01
3 :	5.01E-03	1.97E-02	0.000	0.0221	0.9900	0.9900	1.25	1	1	1.2E-01
4 :	1.17E-07	3.85E-07	0.000	0.0000	1.0000	1.0000	1.01	1	1	2.3E-05
5 :	3.01E-14	9.08E-14	0.202	0.0000	1.0000	1.0000	1.00	1	1	5.5E-12

iter seconds digits c*x b*y
 5 0.0 9.4 5.0899527759e-14 3.0144842876e-14
 $|Ax-b| = 1.7e-14$, $[Ay-c]_+ = 3.0E-14$, $|x|= 5.0e-01$, $|y|= 1.3e+01$

Detailed timing (sec)
 Pre IPM Post
 2.997E-03 1.001E-02 9.958E-04
 Max-norms: $\|b\|=1$, $\|c\|=1.382892e+01$,
 Cholesky |add|=0, |skip|=0, $\|L.L\|=1$.
 Converged at iteration 2

X*:
 6.9145 -0.8214
 -0.8214 4.9001

Y*:
 4.9551 -2.0759
 -2.0759 5.6866

Solving LMI problem resulted in a reduced-order controller with nc = 1
 Controller matrix (G):
 -2.6758 1.3083
 8.5579 -5.0717

Ac = -5.071654
 Bc = 8.557912
 Cc = 1.308284
 Dc = -2.675828

Alternating Projection Method | CASE 3: $\gamma = 5$

SeDuMi 1.3 by AdvOL, 2005-2008 and Jos F. Sturm, 1998-2003.
 Alg = 2: xz-corrector, theta = 0.250, beta = 0.500
 eqs m = 6, order n = 11, dim = 35, blocks = 4
 nnz(A) = 20 + 0, nnz(ADA) = 36, nnz(L) = 21

it :	b*y	gap	delta	rate	t/tP*	t/tD*	feas	cg	cg	prec
0 :		7.35E+01	0.000							
1 :	-1.03E+01	2.28E+01	0.000	0.3097	0.9000	0.9000	1.48	1	1	2.6E+00
2 :	-2.10E+01	5.93E+00	0.000	0.2602	0.9000	0.9000	1.11	1	1	7.3E-01
3 :	-2.36E+01	1.27E+00	0.000	0.2149	0.9000	0.9000	0.92	1	1	1.6E-01
4 :	-2.57E+01	5.44E-02	0.000	0.0427	0.9900	0.9900	0.87	1	1	7.1E-03
5 :	-2.58E+01	2.00E-03	0.024	0.0368	0.9900	0.9900	1.00	1	1	2.6E-04

6 :	-2.58E+01	2.24E-04	0.206	0.1119	0.9450	0.9450	1.00	1	1	2.9E-05
7 :	-2.58E+01	1.85E-05	0.480	0.0825	0.9900	0.9900	1.00	1	1	2.4E-06
8 :	-2.58E+01	8.75E-06	0.164	0.4733	0.9000	0.9000	1.00	1	1	1.2E-06
9 :	-2.58E+01	1.63E-06	0.000	0.1859	0.9000	0.9000	1.00	1	1	2.2E-07
10 :	-2.58E+01	1.36E-07	0.471	0.0837	0.9900	0.9900	1.00	1	2	1.8E-08
11 :	-2.58E+01	2.69E-08	0.000	0.1976	0.9000	0.9000	1.00	2	2	3.6E-09
12 :	-2.58E+01	1.17E-09	0.359	0.0434	0.9900	0.9900	1.00	2	2	1.6E-10

iter seconds digits c*x b*y
 12 0.0 10.1 -2.5756604760e+01 -2.5756604762e+01
 |Ax-b| = 8.3e-11, [Ay-c]_+ = 4.2E-10, |x|= 6.6e+00, |y|= 1.3e+01

Detailed timing (sec)

Pre	IPM	Post								
2.002E-03	2.700E-02	2.002E-03								
Max-norms:	b =1, c = 25,									
Cholesky	add =0, skip = 0, L.L = 4.93398.									
SeDuMi 1.3 by AdvOL, 2005-2008 and Jos F. Sturm, 1998-2003.										
Alg = 2: xz-corrector, theta = 0.250, beta = 0.500										
eqs m = 11, order n = 9, dim = 65, blocks = 2										
nnz(A) = 20 + 0, nnz(ADA) = 121, nnz(L) = 66										
it	b*y	gap	delta	rate	t/tP*	t/tD*	feas	cg	cg	prec
0 :		8.33E+00	0.000							
1 :	-2.75E+00	3.18E+00	0.000	0.3812	0.9000	0.9000	2.25	1	1	2.7E+00
2 :	1.48E-01	9.32E-01	0.000	0.2935	0.9000	0.9000	3.43	1	1	3.9E-01
3 :	6.51E-03	2.33E-02	0.000	0.0250	0.9900	0.9900	1.28	1	1	1.2E-01
4 :	1.86E-07	5.57E-07	0.000	0.0000	1.0000	1.0000	1.01	1	1	3.1E-05
5 :	4.75E-14	1.27E-13	0.301	0.0000	1.0000	1.0000	1.00	1	1	6.9E-12

iter seconds digits c*x b*y
 5 0.0 9.2 7.8883843350e-14 4.7484765648e-14
 |Ax-b| = 2.1e-14, [Ay-c]_+ = 4.8E-14, |x|= 5.0e-01, |y|= 1.5e+01

Detailed timing (sec)

Pre	IPM	Post
2.299E-02	9.998E-03	1.006E-03
Max-norms:	b =1, c = 1.497125e+01,	
Cholesky	add =0, skip = 0, L.L = 1.	

Converged at iteration 2

X*:
 7.4856 -0.7233
 -0.7233 5.8495

Y*:
 5.8149 -1.9387
 -1.9387 6.6066

Solving LMI problem resulted in a reduced-order controller with nc = 1
 Controller matrix (G):

-3.1340	1.6176
11.9541	-7.5012

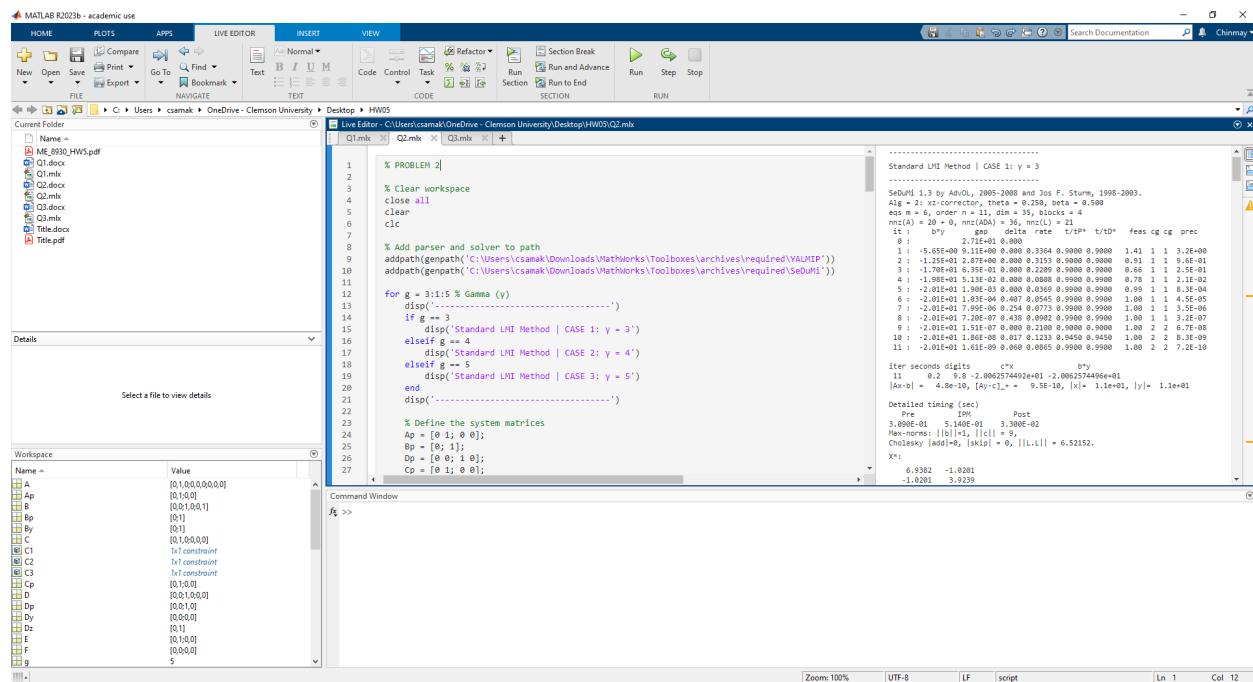
Ac = -7.501234

Bc = 11.954090

Cc = 1.617626

Dc = -3.134028

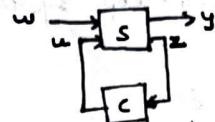
SCREENSHOT:



$$\dot{x}_p = A_p x_p + B_p u + D_p w$$

$$y = C_p x_p + B_y u + D_y w$$

$$z = M_p x_p + D_z w$$



F8 Aircraft

Comparing with given system equations:

$$A_p = \begin{bmatrix} 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1.5 & -1.5 & 0 & 0.0057 & 1.5 & 0 & 0 & 0 & 0 \\ -12 & 12 & -0.6 & -0.0344 & -12 & 0 & 0 & 0 & 0 \\ -0.852 & 0.29 & 0 & -0.014 & -0.29 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & -0.73 & 2.8294625 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$B_p = \begin{bmatrix} 0 & 0 \\ 0.16 & 0.8 \\ -1.9 & -3 \\ -0.0115 & -0.0087 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} \quad D_p = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0.1149 & 0 & 0 \\ 4 & 0 & 0 \\ 0 & 1024 & 0 \\ 0 & 0 & 1024 \end{bmatrix}$$

$$C_p = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad B_y = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0.01 & 0 \\ 0 & 0.001 \end{bmatrix} \quad D_y = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$M_p = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & -139.020647321 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & -139.020647321 \end{bmatrix} \quad D_z = \begin{bmatrix} 0 & 142.857142857 & 0 \\ 0 & 0 & 142.857142857 \end{bmatrix}$$

Lumped system matrices:

$$A = A_p$$

$$B = [D_p \quad B_p]$$

$$C = [C_p \quad M_p]$$

$$D = \begin{bmatrix} D_y & B_y \\ D_z & 0 \end{bmatrix}$$

Open loop system:

$$S_{OL} = ss(A, B, C, D)$$

Input to open-loop system:

$$\cdot w(t) = \begin{bmatrix} 10 \\ 0 \\ 0 \end{bmatrix} \delta(t)$$

↑ unit impulse disturbance

$$\text{where } \delta(t) = \begin{cases} 1 & ; 0 \leq t \leq 0.01 \\ 0 & ; t > 0.01 \end{cases}$$

$$\cdot u(t) = 0 + t$$

Open-loop system simulation:

- Simulate open-loop system, S_{ol} , using "lsim" for $t=0$ to $t=10$ sec. with $\Delta t = 0.01$ sec.
- Plot $w(t)$ vs. t ← wind gust disturbance (input)
- Plot $y_p(t)$ vs. t ← aircraft pitch angle (output)

Full order optimal H_∞ dynamic controller design

$$S = \text{lthsys}(A, B, C, D)$$

$$n_2 = \text{size}(M_p, 1)$$

$$n_u = \text{size}(B_p, 2)$$

$$r = [n_2 \ n_u]$$

$$[g_{\text{opt}}, G] = \text{hinflmi}(S, r)$$

$$[A_c, B_c, C_c, D_c] = \text{ltisss}(G)$$

$\overbrace{\quad}^{\text{controller}}$

Closed-loop system:

$$A_{\text{cl}} = \begin{bmatrix} A_p + B_p D_c M_p & B_p C_c \\ B_c M_p & A_c \end{bmatrix}$$

$$B_{\text{cl}} = \begin{bmatrix} D_p + B_p D_c D_z \\ B_c D_z \end{bmatrix}$$

$$C_{\text{cl}} = \begin{bmatrix} C_p + B_p D_c M_p & B_p C_c \end{bmatrix} \quad D_{\text{cl}} = D_y + B_p D_c D_z$$

$$S_{\text{cl}} = ss(A_{\text{cl}}, B_{\text{cl}}, C_{\text{cl}}, D_{\text{cl}})$$

Design Validation:

- Stability: Eigenvalues: $\operatorname{Re}(\lambda_i(A_{cl})) < 0 \leftarrow \text{closed loop system stability guaranteed}$
- Performance: H_∞ norm: $\|G_{cl}\|_\infty = \text{hinfnorm}(S_{cl})$
 $(\|G_{cl}\|_\infty) \leq \gamma^*$ \leftarrow optimal (*guaranteed*)
 $\xrightarrow{\text{hinf_norm}} \gamma^* \xleftarrow{\text{opt}}$ $\leftarrow H_\infty \text{ performance}$

Input to closed-loop system:

$$\omega(t) = \begin{bmatrix} 10 \\ 0 \\ 0 \end{bmatrix} \delta(t)$$

\uparrow unit impulse signal

$$\text{where } \delta(t) = \begin{cases} 1; & 0 \leq t \leq 0.01 \\ 0; & t > 0.01 \end{cases}$$

Closed-loop system simulation:

- Simulate closed-loop system S_{cl} using "lsim" for $t = 0$ to $t = 10$ sec. with $\Delta t = 0.01$ sec.
- Plot $\omega(t)$ vs. $t \leftarrow$ wind gust disturbance (input)
- Plot $y_1(t)$ vs. $t \leftarrow$ aircraft pitch angle (output)

Problem 3

CODE:

```
% PROBLEM 3
```

```
% Clear workspace
close all
clear
clc

% Define the system matrices
Ap = [0 0 1 0 0 0 0 0;
       1.5 -1.5 0 0.0057 1.5 0 0 0;
       -12 12 -0.6 -0.0344 -12 0 0 0;
       -0.825 0.29 0 -0.014 -0.29 0 0 0;
       0 0 0 0 -0.73 2.82940625 0 0;
       0 0 0 0 0 -1.25 0 0;
       0 0 0 0 0 0 -1000 0;
       0 0 0 0 0 0 0 -1000];
Bp = [0 0;
       0.16 0.8;
       -19 -3;
       -0.0115 -0.0087;
       0 0;
       0 0;
       0 0;
       0 0];
Dp = [0 0 0;
       0 0 0;
       0 0 0;
       0 0 0;
       0.1149 0 0;
       4 0 0;
       0 1024 0
       0 0 1024];
Cp = [1 0 0 0 0 0 0 0;
       0 1 0 0 0 0 0 0;
       0 0 0 0 0 0 0 0;
       0 0 0 0 0 0 0 0];
By = [0 0;
       0 0;
       0.01 0;
       0 0.01];
Dy = [0 0 0;
```

```

    0 0 0;
    0 0 0;
    0 0 0];
Mp = [1 0 0 0 0 0 -139.020647321 0
      0 1 0 0 0 0 -139.020647321];
Dz = [0 142.857142857 0
      0 0 142.857142857];

% Lumped system matrices
A = Ap;
B = [Dp Bp];
C = [Cp Mp];
D = [Dy By; Dz zeros(size(Dz,1), size(By,2))];

% State-space system
Sol = ss(A, B, C, D)

% Define the lumped (disturbance + control) input
t = 0:0.01:10;
w_amplitude = [10; 0; 0];
w_duration = 0.01;
w_impulse = w_amplitude * (t >= 0 & t < w_duration);
u = zeros(size(Bp,2), size(w_impulse,2));
w = [w_impulse; u];

% Simulate the open-loop system response
[y_ol, t_out, x_ol] = lsim(Sol, w', t);

% Plot the results
figure;
sgtitle('Open-Loop System Response');
subplot(2, 1, 1);
plot(t, w(1, :));
legend('Input (Wind Gust Disturbance)');
subplot(2, 1, 2);
plot(t, y_ol(:, 1));
legend('Output (Aircraft Pitch Angle)');

% H $\infty$  controller design
S = ltisys(A, B, C, D);
nz = size(Mp, 1);
nu = size(Bp, 2);

```

```

r = [nz nu];
[gopt, G] = hinflmi(S, r)

% H $\infty$  controller matrices
disp('H $\infty$  controller:')
[Ac, Bc, Cc, Dc] = ltiss(G)

% Closed-loop system matrices
disp('Closed-loop system:')
Acl = [Ap+Bp*Dc*Mp, Bp*Cc; Bc*Mp, Ac]
Bcl = [Dp+Bp*Dc*Dz; Bc*Dz]
Ccl = [Cp+By*Dc*Mp, By*Cc]
Dcl = Dy+By*Dc*Dz

% Closed-loop system
Scl = ss(Acl, Bcl, Ccl, Dcl);

% Verification of designed H $\infty$  controller
disp('H $\infty$  norm:')
hinf_norm = hinfnorm(Scl)
disp('Closed-loop poles')
eig_Acl = eig(Acl)
if((hinf_norm < gopt) && all(real(eig_Acl) < 0.0))
    disp('Verification of H $\infty$  norm and stability constraints successful!')
else
    disp('Verification of H $\infty$  norm and stability constraints failed!')
end

% Define the lumped (disturbance + control) input
t = 0:0.01:10;
w_amplitude = [10; 0; 0];
w_duration = 0.01;
w_impulse = w_amplitude * (t >= 0 & t < w_duration);
w = w_impulse;

% Simulate the open-loop system response
[y_cl, t_out, x_cl] = lsim(Scl, w', t);

% Plot the results
figure;
sgtitle('Closed-Loop System Response');
subplot(2, 1, 1);

```

```

plot(t, w(1, :));
legend('Input (Wind Gust Disturbance)');
subplot(2, 1, 2);
plot(t, y_c1(:, 1));
legend('Output (Aircraft Pitch Angle)');

```

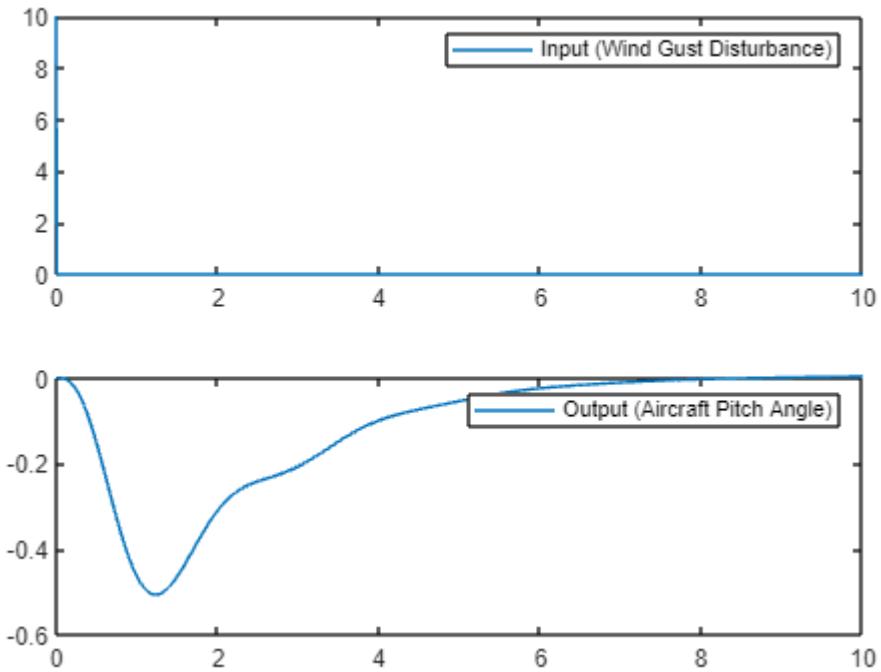
OUTPUT:

Sol =

A =	x1	x2	x3	x4	x5	x6	x7	x8
x1	0	0	1	0	0	0	0	0
x2	1.5	-1.5	0	0.0057	1.5	0	0	0
x3	-12	12	-0.6	-0.0344	-12	0	0	0
x4	-0.825	0.29	0	-0.014	-0.29	0	0	0
x5	0	0	0	0	-0.73	2.829	0	0
x6	0	0	0	0	0	-1.25	0	0
x7	0	0	0	0	0	0	-1000	0
x8	0	0	0	0	0	0	0	-1000
B =	u1	u2	u3	u4	u5			
x1	0	0	0	0	0			
x2	0	0	0	0.16	0.8			
x3	0	0	0	-19	-3			
x4	0	0	0	-0.0115	-0.0087			
x5	0.1149	0	0	0	0			
x6	4	0	0	0	0			
x7	0	1024	0	0	0			
x8	0	0	1024	0	0			
C =	x1	x2	x3	x4	x5	x6	x7	x8
y1	1	0	0	0	0	0	0	0
y2	0	1	0	0	0	0	0	0
y3	0	0	0	0	0	0	0	0
y4	0	0	0	0	0	0	0	0
y5	1	0	0	0	0	0	-139	0
y6	0	1	0	0	0	0	0	-139
D =	u1	u2	u3	u4	u5			
y1	0	0	0	0	0			
y2	0	0	0	0	0			
y3	0	0	0	0.01	0			
y4	0	0	0	0	0.01			
y5	0	142.9	0	0	0			
y6	0	0	142.9	0	0			

Continuous-time state-space model.

Open-Loop System Response



Minimization of gamma:

Solver for linear objective minimization under LMI constraints

Iterations : Best objective value so far

1	
2	
3	3650.305369
4	679.874263
5	415.718365
6	196.917091
7	124.993308
8	124.993308
9	39.263120
10	32.197975
11	21.790789
12	21.790789
13	4.993262
14	4.993262
15	2.508027
16	1.610124
17	1.610124
18	1.224387
19	1.224387
20	1.224387
21	1.003425
22	1.003425
23	1.003425
24	0.941879

```

25          0.941879
26          0.941879
27          0.941879
28          0.912216
29          0.912216
30          0.912216
31          0.896765
32          0.896765
33          0.896765
***          new lower bound:    0.820170
34          0.896765
35          0.887844
36          0.887844
37          0.887844
***          new lower bound:    0.867568
38          0.884997
39          0.883333
* switching to QR
40          0.883333
***          new lower bound:    0.877811

Result: feasible solution of required accuracy
best objective value: 0.883333
guaranteed absolute accuracy: 5.52e-03
f-radius saturation: 0.458% of R = 1.00e+08

Optimal Hinf performance: 8.823e-01
gopt = 0.8823
G = 10x10
   77.0684 -206.4493 -45.4703 -89.5611 -35.5194 -12.4998 106.3172 -
  2.3242   3.8637   7.0000
 -220.1100 183.7132   2.3812 116.5260  57.5111   1.5305 -226.7402
 4.7605  -1.7312   0
 397.2066 -510.2170 -63.3345 -269.2750 -121.1621 -18.7382 432.1665 -
 5.0789  -3.3582   0
   5.7829  -3.5433   1.5761  -4.9621   1.2446   0.7772   7.5619
 1.3169   3.6942   0
 293.4949 -341.9114 -33.2695 -188.0955 -88.9407 -10.9885 313.4063 -
 1.8555   1.3533   0
  -7.7820   8.1529   0.3504   4.6494   2.2216   0.1100  -8.8267 -
 0.2847  -0.0942   0
 -263.0885 307.1698 29.7766 169.0752  79.4155   9.7083 -282.4749
 0.6617  -0.6630   0
 -60.3310 101.1714 16.6276  48.7081  21.1076   4.7857  -70.3890
 0.5497  -0.2233   0
 -102.4696 -63.6786 -48.4705   1.8408  11.4945 -12.2981  -80.1751
 0.1321  -0.0537   0
   0         0         0         0         0         0         0         0
0         0         -Inf

Hinfinity controller:
Ac = 7x7
   77.0684 -206.4493 -45.4703 -89.5611 -35.5194 -12.4998 106.3172
 -220.1100 183.7132   2.3812 116.5260  57.5111   1.5305 -226.7402
 397.2066 -510.2170 -63.3345 -269.2750 -121.1621 -18.7382 432.1665
   5.7829  -3.5433   1.5761  -4.9621   1.2446   0.7772   7.5619
 293.4949 -341.9114 -33.2695 -188.0955 -88.9407 -10.9885 313.4063
  -7.7820   8.1529   0.3504   4.6494   2.2216   0.1100  -8.8267

```

```

-263.0885 307.1698 29.7766 169.0752 79.4155 9.7083 -282.4749
Bc = 7x2
-2.3242 3.8637
4.7605 -1.7312
-5.0789 -3.3582
1.3169 3.6942
-1.8555 1.3533
-0.2847 -0.0942
0.6617 -0.6630
Cc = 2x7
-60.3310 101.1714 16.6276 48.7081 21.1076 4.7857 -70.3890
-102.4696 -63.6786 -48.4705 1.8408 11.4945 -12.2981 -80.1751
Dc = 2x2
0.5497 -0.2233
0.1321 -0.0537
Closed-loop system:
Acl = 15x15
103 ×
0 0 0.0010 0 0 0 0
0 0 0 0 0 0 0
0.0017 -0.0016 0 0.0000 0.0015 0 -0.0269
0.0109 -0.0916 -0.0348 -0.0361 0.0093 0.0126 -0.0091 -0.0754
-0.0228 0.0164 -0.0006 -0.0000 -0.0120 0 1.5070 -
0.6121 1.4537 -1.7312 -0.1705 -0.9310 -0.4355 -0.0540 1.5779
-0.0008 0.0003 0 -0.0000 -0.0003 0 0.0010 -
0.0004 0.0016 -0.0006 0.0002 -0.0006 -0.0003 0.0001 0.0015
0 0 0 0 -0.0007 0.0028 0
0 0 0 0 0 0 0
0 0 0 0 0 -0.0013 0
0 0 0 0 0 0 0
0 0 0 0 0 0 -1.0000
0 0 0 0 0 0 0
0 0 0 0 0 0 0
1.0000 0 0 0 0 0 0
-0.0023 0.0039 0 0 0 0 0.3231 -
0.5371 0.0771 -0.2064 -0.0455 -0.0896 -0.0355 -0.0125 0.1063
0.0048 -0.0017 0 0 0 0 -0.6618
0.2407 -0.2201 0.1837 0.0024 0.1165 0.0575 0.0015 -0.2267
Bcl = 15x3
103 ×
0 0 0
0 0.0277 -0.0112
0 -1.5486 0.6290
0 -0.0011 0.0004
0.0001 0 0
0.0040 0 0
0 1.0240 0
0 0 1.0240
0 -0.3320 0.5520
0 0.6801 -0.2473
Ccl = 4x15
1.0000 0 0 0 0 0 0
0 0 0 0 0 0 0
0 1.0000 0 0 0 0 0
0 0 0 0 0 0 0
0.0055 -0.0022 0 0 0 0 -0.7642
0.3104 -0.6033 1.0117 0.1663 0.4871 0.2111 0.0479 -0.7039

```

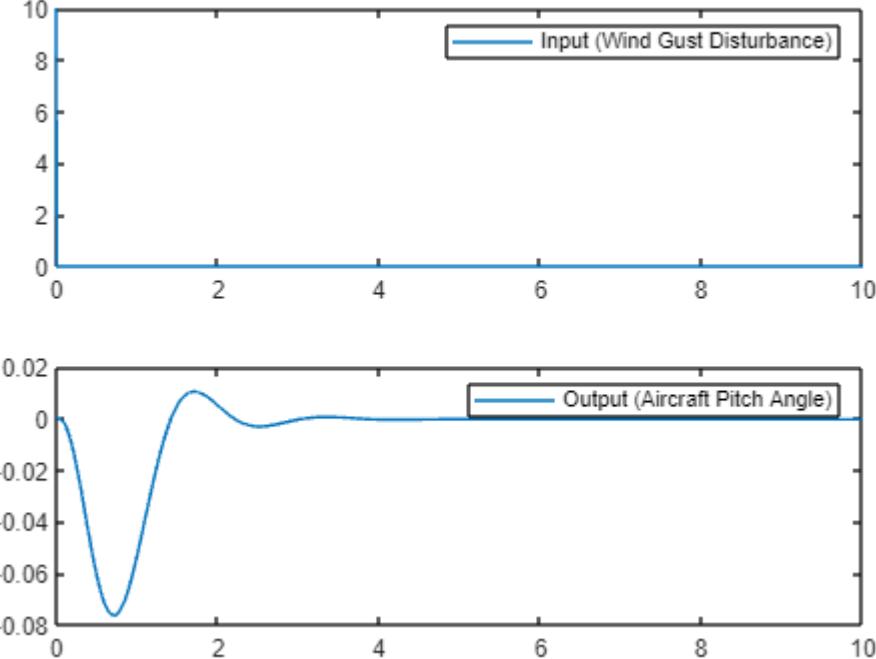
```

0.0013 -0.0005 0 0 0 0 -0.1836
0.0746 -1.0247 -0.6368 -0.4847 0.0184 0.1149 -0.1230 -0.8018
Dcl = 4x3
0 0 0
0 0 0
0 0.7852 -0.3190
0 0.1887 -0.0766
H $\infty$  norm:
hinf_norm = 0.8813
Closed-loop poles:
eig_Acl = 15x1 complex
103 x
-0.1048 + 0.0000i
-0.0311 + 0.0301i
-0.0311 - 0.0301i
-0.0016 + 0.0038i
-0.0016 - 0.0038i
-0.0036 + 0.0011i
-0.0036 - 0.0011i
-0.0035 + 0.0000i
-0.0000 + 0.0000i
-0.0000 - 0.0000i

```

Verification of H ∞ norm and stability constraints successful!

Closed-Loop System Response



SCREENSHOT:

