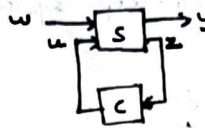


$$\dot{x}_p = A_p x_p + B_p u + D_p w$$

$$y = C_p x_p + B_y u + D_y w$$

$$z = M_p x_p + D_z w$$



F8 Aircraft

Comparing with given system equations:

$$A_p = \begin{bmatrix} 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 1.5 & -1.5 & 0 & 0.0057 & 1.5 & 0 & 0 & 0 \\ -12 & 12 & -0.6 & -0.0344 & -12 & 0 & 0 & 0 \\ -0.852 & 0.29 & 0 & -0.014 & -0.29 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & -0.73 & 2.8294625 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1.25 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & -1000 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & -1000 \end{bmatrix}$$

$$B_p = \begin{bmatrix} 0 & 0 \\ 0.16 & 0.8 \\ -19 & -3 \\ -0.0115 & -0.0087 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}$$

$$D_p = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0.1149 & 0 & 0 \\ 4 & 0 & 0 \\ 0 & 1024 & 0 \\ 0 & 0 & 1024 \end{bmatrix}$$

$$C_p = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$B_y = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0.01 & 0 \\ 0 & 0.01 \end{bmatrix}$$

$$D_y = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$M_p = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & -139.020647321 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & -139.020647321 \end{bmatrix}$$

$$D_z = \begin{bmatrix} 0 & 142.857142857 & 0 \\ 0 & 0 & 142.857142857 \end{bmatrix}$$

Lumped system matrices:

$$A = A_p$$

$$B = [D_p \quad B_p]$$

$$C = [C_p \quad M_p]$$

$$D = \begin{bmatrix} D_y & B_y \\ D_z & 0 \end{bmatrix}$$

Open-loop system:

$$S_{OL} = ss(A, B, C, D)$$

Input to open-loop system:

$$w(t) = \begin{bmatrix} 10 \\ 0 \\ 0 \end{bmatrix} \delta(t)$$

↑ unit impulse disturbance

$$\text{where } \delta(t) = \begin{cases} 1; & 0 \leq t \leq \frac{0.01}{\Delta t} \\ 0; & t > \frac{0.01}{\Delta t} \end{cases}$$

$$u(t) = 0 \quad \forall t$$

Open-loop system simulation:

• Simulate open-loop system S_{ol} using "lsim" for $t=0$ to $t=10$ sec. with $\Delta t = 0.01$ sec.

• Plot $w(t)$ vs. t ← wind gust disturbance (input)
Plot $y_1(t)$ vs. t ← aircraft pitch angle (output)

Full order optimal H_∞ dynamic controller design

$$S = \text{tfss}(A, B, C, D)$$

$$n_z = \text{size}(M_p, 1)$$

$$n_u = \text{size}(B_p, 2)$$

$$r = [n_z \quad n_u]$$

$$[gopt, G] = \text{hinflmi}(S, r)$$

$$\|e\|_2 < \gamma^*$$

controller

$$[A_c, B_c, C_c, D_c] = \text{hiss}(G)$$

Closed-loop system:

$$A_{cl} = \begin{bmatrix} A_p + B_p D_c M_p & B_p C_c \\ B_c M_p & A_c \end{bmatrix}$$

$$B_{cl} = \begin{bmatrix} D_p + B_p D_c D_z \\ B_c D_z \end{bmatrix}$$

$$C_{cl} = \begin{bmatrix} C_p + B_y D_c M_p & B_y C_c \end{bmatrix}$$

$$D_{cl} = D_y + B_y D_c D_z$$

$$S_{cl} = \text{ss}(A_{cl}, B_{cl}, C_{cl}, D_{cl})$$

Design Validation:

- Stability: Eigenvalues: $\text{Re}(\lambda_i(A_{cl})) < 0 \leftarrow$ closed loop system stability guaranteed
(Poles)
- Performance: H_2 norm: $\|P_{ee}\| = \text{hinfnorm}(S_{cl})$
($\|P_{ee}\|$) $\|P_{ee}\| < \gamma^*$ \leftarrow optimal (guaranteed) H_2 performance
 \uparrow \uparrow
hinfnorm γ_{opt}

Input to closed-loop system:

- $w(t) = \begin{bmatrix} 10 \\ 0 \\ 0 \end{bmatrix} \delta(t)$ \leftarrow unit impulse signal
where $\delta(t) = \begin{cases} 1; & 0 \leq t \leq \underbrace{0.01}_{\Delta t} \\ 0; & t > 0.01 \end{cases}$

Closed-loop system simulation:

- Simulate closed-loop system S_{cl} using "lsim" for $t=0$ to $t=10$ sec. with $\Delta t = 0.01$ sec.
- Plot $w(t)$ vs. $t \leftarrow$ wind gust disturbance (input)
Plot $y_1(t)$ vs. $t \leftarrow$ aircraft pitch angle (output)

Problem 3

CODE:

```
% PROBLEM 3

% Clear workspace
close all
clear
clc

% Define the system matrices
Ap = [0 0 1 0 0 0 0 0;
      1.5 -1.5 0 0.0057 1.5 0 0 0;
      -12 12 -0.6 -0.0344 -12 0 0 0;
      -0.825 0.29 0 -0.014 -0.29 0 0 0;
      0 0 0 0 -0.73 2.82940625 0 0;
      0 0 0 0 0 -1.25 0 0;
      0 0 0 0 0 0 -1000 0;
      0 0 0 0 0 0 0 -1000];
Bp = [0 0;
      0.16 0.8;
      -19 -3;
      -0.0115 -0.0087;
      0 0;
      0 0;
      0 0;
      0 0];
Dp = [0 0 0;
      0 0 0;
      0 0 0;
      0 0 0;
      0.1149 0 0;
      4 0 0;
      0 1024 0;
      0 0 1024];
Cp = [1 0 0 0 0 0 0 0;
      0 1 0 0 0 0 0 0;
      0 0 0 0 0 0 0 0;
      0 0 0 0 0 0 0 0];
By = [0 0;
      0 0;
      0.01 0;
      0 0.01];
Dy = [0 0 0;
```

```

    0 0 0;
    0 0 0;
    0 0 0];
Mp = [1 0 0 0 0 0 -139.020647321 0
      0 1 0 0 0 0 0 -139.020647321];
Dz = [0 142.857142857 0
      0 0 142.857142857];

% Lumped system matrices
A = Ap;
B = [Dp Bp];
C = [Cp; Mp];
D = [Dy By; Dz zeros(size(Dz,1), size(By,2))];

% State-space system
Sol = ss(A, B, C, D)

% Define the lumped (disturbance + control) input
t = 0:0.01:10;
w_amplitude = [10; 0; 0];
w_duration = 0.01;
w_impulse = w_amplitude * (t >= 0 & t < w_duration);
u = zeros(size(Bp,2), size(w_impulse,2));
w = [w_impulse; u];

% Simulate the open-loop system response
[y_ol, t_out, x_ol] = lsim(Sol, w', t);

% Plot the results
figure;
sgtitle('Open-Loop System Response');
subplot(2, 1, 1);
plot(t, w(1, :));
legend('Input (Wind Gust Disturbance)');
subplot(2, 1, 2);
plot(t, y_ol(:, 1));
legend('Output (Aircraft Pitch Angle)');

% H $\infty$  controller design
S = ltisys(A, B, C, D);
nz = size(Mp, 1);
nu = size(Bp, 2);

```

```

r = [nz nu];
[gopt, G] = hinflmi(S, r)

% H $\infty$  controller matrices
disp('H $\infty$  controller:')
[Ac, Bc, Cc, Dc] = ltiss(G)

% Closed-loop system matrices
disp('Closed-loop system:')
Acl = [Ap+Bp*Dc*Mp, Bp*Cc; Bc*Mp, Ac]
Bcl = [Dp+Bp*Dc*Dz; Bc*Dz]
Ccl = [Cp+By*Dc*Mp, By*Cc]
Dcl = Dy+By*Dc*Dz

% Closed-loop system
Scl = ss(Acl, Bcl, Ccl, Dcl);

% Verification of designed H $\infty$  controller
disp('H $\infty$  norm:')
hinf_norm = hinfnorm(Scl)
disp('Closed-loop poles:')
eig_Acl = eig(Acl)
if((hinf_norm < gopt) && all(real(eig_Acl) < 0.0))
    disp('Verification of H $\infty$  norm and stability constraints successful!')
else
    disp('Verification of H $\infty$  norm and stability constraints failed!')
end

% Define the lumped (disturbance + control) input
t = 0:0.01:10;
w_amplitude = [10; 0; 0];
w_duration = 0.01;
w_impulse = w_amplitude * (t >= 0 & t < w_duration);
w = w_impulse;

% Simulate the open-loop system response
[y_cl, t_out, x_cl] = lsim(Scl, w', t);

% Plot the results
figure;
sgtitle('Closed-Loop System Response');
subplot(2, 1, 1);

```

```

plot(t, w(1, :));
legend('Input (Wind Gust Disturbance)');
subplot(2, 1, 2);
plot(t, y_cl(:, 1));
legend('Output (Aircraft Pitch Angle)');

```

OUTPUT:

Sol =

A =

	x1	x2	x3	x4	x5	x6	x7	x8
x1	0	0	1	0	0	0	0	0
x2	1.5	-1.5	0	0.0057	1.5	0	0	0
x3	-12	12	-0.6	-0.0344	-12	0	0	0
x4	-0.825	0.29	0	-0.014	-0.29	0	0	0
x5	0	0	0	0	-0.73	2.829	0	0
x6	0	0	0	0	0	-1.25	0	0
x7	0	0	0	0	0	0	-1000	0
x8	0	0	0	0	0	0	0	-1000

B =

	u1	u2	u3	u4	u5
x1	0	0	0	0	0
x2	0	0	0	0.16	0.8
x3	0	0	0	-19	-3
x4	0	0	0	-0.0115	-0.0087
x5	0.1149	0	0	0	0
x6	4	0	0	0	0
x7	0	1024	0	0	0
x8	0	0	1024	0	0

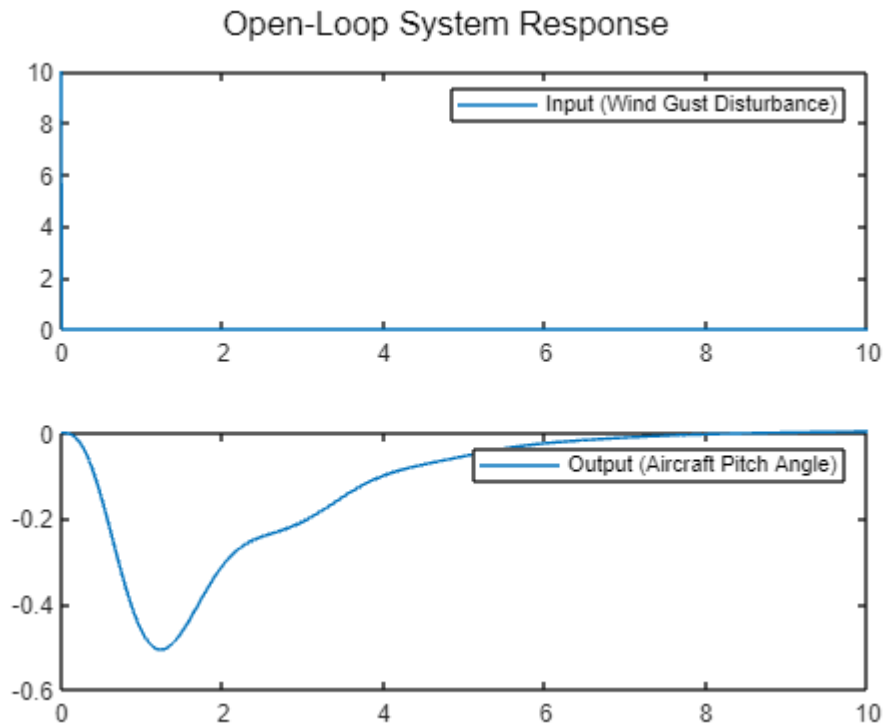
C =

	x1	x2	x3	x4	x5	x6	x7	x8
y1	1	0	0	0	0	0	0	0
y2	0	1	0	0	0	0	0	0
y3	0	0	0	0	0	0	0	0
y4	0	0	0	0	0	0	0	0
y5	1	0	0	0	0	0	-139	0
y6	0	1	0	0	0	0	0	-139

D =

	u1	u2	u3	u4	u5
y1	0	0	0	0	0
y2	0	0	0	0	0
y3	0	0	0	0.01	0
y4	0	0	0	0	0.01
y5	0	142.9	0	0	0
y6	0	0	142.9	0	0

Continuous-time state-space model.



Minimization of gamma:

Solver for linear objective minimization under LMI constraints

Iterations : Best objective value so far

1	
2	
3	3650.305369
4	679.874263
5	415.718365
6	196.917091
7	124.993308
8	124.993308
9	39.263120
10	32.197975
11	21.790789
12	21.790789
13	4.993262
14	4.993262
15	2.508027
16	1.610124
17	1.610124
18	1.224387
19	1.224387
20	1.224387
21	1.003425
22	1.003425
23	1.003425
24	0.941879


```

25          0.941879
26          0.941879
27          0.941879
28          0.912216
29          0.912216
30          0.912216
31          0.896765
32          0.896765
33          0.896765
***          new lower bound:      0.820170
34          0.896765
35          0.887844
36          0.887844
37          0.887844
***          new lower bound:      0.867568
38          0.884997
39          0.883333
* switching to QR
40          0.883333
***          new lower bound:      0.877811

```

```

Result: feasible solution of required accuracy
best objective value:      0.883333
guaranteed absolute accuracy: 5.52e-03
f-radius saturation: 0.458% of R = 1.00e+08

```

```

Optimal Hinf performance: 8.823e-01
gopt = 0.8823

```

```

G = 10x10
 77.0684 -206.4493 -45.4703 -89.5611 -35.5194 -12.4998 106.3172 -
2.3242   3.8637   7.0000
-220.1100 183.7132   2.3812 116.5260  57.5111   1.5305 -226.7402
4.7605  -1.7312      0
 397.2066 -510.2170 -63.3345 -269.2750 -121.1621 -18.7382 432.1665 -
5.0789  -3.3582      0
   5.7829 -3.5433   1.5761 -4.9621   1.2446   0.7772   7.5619
1.3169   3.6942      0
 293.4949 -341.9114 -33.2695 -188.0955 -88.9407 -10.9885 313.4063 -
1.8555   1.3533      0
  -7.7820   8.1529   0.3504   4.6494   2.2216   0.1100  -8.8267 -
0.2847  -0.0942      0
-263.0885 307.1698  29.7766 169.0752  79.4155   9.7083 -282.4749
0.6617  -0.6630      0
 -60.3310 101.1714  16.6276  48.7081  21.1076   4.7857  -70.3890
0.5497  -0.2233      0
-102.4696 -63.6786 -48.4705   1.8408  11.4945 -12.2981 -80.1751
0.1321  -0.0537      0
      0      0      0      0      0      0      0
0      0      -Inf

```

```

H $\infty$  controller:

```

```

Ac = 7x7
 77.0684 -206.4493 -45.4703 -89.5611 -35.5194 -12.4998 106.3172
-220.1100 183.7132   2.3812 116.5260  57.5111   1.5305 -226.7402
 397.2066 -510.2170 -63.3345 -269.2750 -121.1621 -18.7382 432.1665
   5.7829 -3.5433   1.5761 -4.9621   1.2446   0.7772   7.5619
 293.4949 -341.9114 -33.2695 -188.0955 -88.9407 -10.9885 313.4063
  -7.7820   8.1529   0.3504   4.6494   2.2216   0.1100  -8.8267

```

-263.0885 307.1698 29.7766 169.0752 79.4155 9.7083 -282.4749

Bc = 7x2

-2.3242 3.8637
4.7605 -1.7312
-5.0789 -3.3582
1.3169 3.6942
-1.8555 1.3533
-0.2847 -0.0942
0.6617 -0.6630

Cc = 2x7

-60.3310 101.1714 16.6276 48.7081 21.1076 4.7857 -70.3890
-102.4696 -63.6786 -48.4705 1.8408 11.4945 -12.2981 -80.1751

Dc = 2x2

0.5497 -0.2233
0.1321 -0.0537

Closed-loop system:

Ac1 = 15x15

10³ x

0	0	0.0010	0	0	0	0	0
0	0	0	0	0	0	0	0
0.0017	-0.0016	0	0.0000	0.0015	0	-0.0269	
0.0109	-0.0916	-0.0348	-0.0361	0.0093	0.0126	-0.0091	-0.0754
-0.0228	0.0164	-0.0006	-0.0000	-0.0120	0	1.5070	-
0.6121	1.4537	-1.7312	-0.1705	-0.9310	-0.4355	-0.0540	1.5779
-0.0008	0.0003	0	-0.0000	-0.0003	0	0.0010	-
0.0004	0.0016	-0.0006	0.0002	-0.0006	-0.0003	0.0001	0.0015
0	0	0	0	0	-0.0007	0.0028	0
0	0	0	0	0	0	0	0
0	0	0	0	0	0	-0.0013	0
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	-1.0000
0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0
1.0000	0	0	0	0	0	0	0
-0.0023	0.0039	0	0	0	0	0	0.3231
0.5371	0.0771	-0.2064	-0.0455	-0.0896	-0.0355	-0.0125	0.1063
0.0048	-0.0017	0	0	0	0	0	-0.6618
0.2407	-0.2201	0.1837	0.0024	0.1165	0.0575	0.0015	-0.2267

Bc1 = 15x3

10³ x

0	0	0
0	0.0277	-0.0112
0	-1.5486	0.6290
0	-0.0011	0.0004
0.0001	0	0
0.0040	0	0
0	1.0240	0
0	0	1.0240
0	-0.3320	0.5520
0	0.6801	-0.2473

Cc1 = 4x15

1.0000	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0
0	0	1.0000	0	0	0	0	0
0	0	0	0	0	0	0	0
0.0055	-0.0022	0	0	0	0	0	-0.7642
0.3104	-0.6033	1.0117	0.1663	0.4871	0.2111	0.0479	-0.7039

```

0.0013    -0.0005         0         0         0         0    -0.1836
0.0746    -1.0247    -0.6368    -0.4847    0.0184    0.1149    -0.1230    -0.8018
Dcl = 4x3

```

```

0         0         0
0         0         0
0    0.7852    -0.3190
0    0.1887    -0.0766

```

H ∞ norm:

hinf_norm = 0.8813

Closed-loop poles:

eig_Acl = 15x1 complex

10³ x

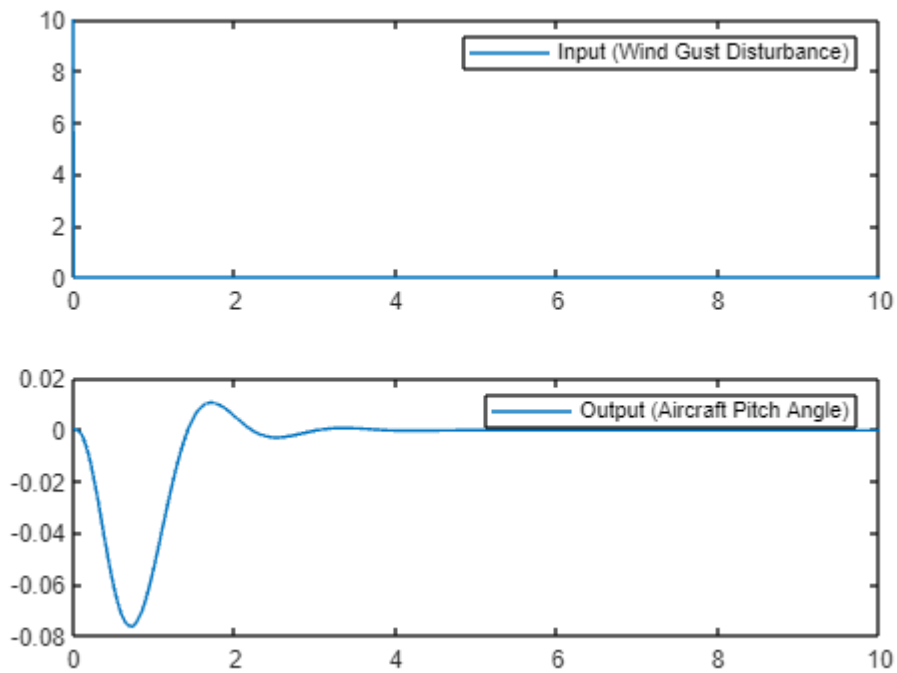
```

-0.1048 + 0.0000i
-0.0311 + 0.0301i
-0.0311 - 0.0301i
-0.0016 + 0.0038i
-0.0016 - 0.0038i
-0.0036 + 0.0011i
-0.0036 - 0.0011i
-0.0035 + 0.0000i
-0.0000 + 0.0000i
-0.0000 - 0.0000i

```

Verification of H ∞ norm and stability constraints successful!

Closed-Loop System Response



SCREENSHOT:

