

# AuE-6600 | Dynamic Performance of Vehicles

## Homework 5

### Problem 1

Give limits on the Understeer Gradient, so that the characteristic velocity of a vehicle with wheelbase 3.1 m will be in the desired range of 80-120 km/h. What is maximum achievable steering sensitivity in this range (yaw velocity response)? Assuming a steering gear ratio of 19, what steering wheel angle does the driver have to provide for cornering with  $a_y = 5 \text{ m/s}^2$  lateral acceleration?

### Solution 1

1. Give limits on the Understeer Gradient, so that the characteristic velocity of a vehicle with wheelbase 3.1 m will be in the desired range of 80-120 km/h.

```
% Given data
l = 3.1; % m
v_min = 80; % km/h
v_min = v_min/3.6; % m/s
v_max = 120; % km/h
v_max = v_max/3.6; % m/s
% Calculate UG
UG_min = 1/(v_max^2);
UG_max = 1/(v_min^2);
fprintf("Limits on the understeer gradient are %.4f rad-s^2/m and %.4f rad-s^2/m", UG_min, UG_max)
```

Limits on the understeer gradient are 0.0028 rad-s<sup>2</sup>/m and 0.0063 rad-s<sup>2</sup>/m

2. What is maximum achievable steering sensitivity in this range (yaw velocity response)?

```
% Calculate steering sensitivity
steer_sensitivity_min = v_min/(2*l);
steer_sensitivity_max = v_max/(2*l);
fprintf("Steering sensitivity is in the range of %.4f Hz and %.4f Hz\n" + ...
        "Maximum steering sensitivity is %.4f Hz", ...
        steer_sensitivity_min, steer_sensitivity_max, max(steer_sensitivity_min, steer_sensitivity_max))
```

Steering sensitivity is in the range of 3.5842 Hz and 5.3763 Hz  
Maximum steering sensitivity is 5.3763 Hz

3. Assuming a steering gear ratio of 19, what steering wheel angle does the driver have to provide for cornering with  $a_y = 5 \text{ m/s}^2$  lateral acceleration?

```
% Given data
steer_ratio = 19;
a_y = 5; % m/s^2
% Calculate turning radius
R_min = v_min^2/a_y;
R_max = v_max^2/a_y;
% Calculate steering angle
```

```

delta_min = v_min/(R_min*steer_sensitivity_min);
delta_max = v_max/(R_max*steer_sensitivity_max);
% Calculate steering wheel angle
steer_angle_min = delta_min*steer_ratio;
steer_angle_max = delta_max*steer_ratio;
fprintf("The driver have to provide steering wheel angle of %.4f rad for cornering with a_y = 5 m/s^2 at v_x = 22.2222 m/s\n");
fprintf("The driver have to provide steering wheel angle of %.4f rad for cornering with a_y = 5 m/s^2 at v_x = 33.3333 m/s\n");
steer_angle_min, v_min, steer_angle_max, v_max);

```

The driver have to provide steering wheel angle of 1.1927 rad for cornering with  $a_y = 5 \text{ m/s}^2$  at  $v_x = 22.2222 \text{ m/s}$   
The driver have to provide steering wheel angle of 0.5301 rad for cornering with  $a_y = 5 \text{ m/s}^2$  at  $v_x = 33.3333 \text{ m/s}$

## Problem 2

Consider the following Bicycle model vehicle:

- Mass: 120 slug
- Wheelbase: 9 ft.
- Weight Distribution: Defined below.
- Front Cornering Stiffness: 350 lb/deg
- Rear Cornering Stiffness: 350 lb/deg

This vehicle is being driven on a 320 ft radius (left turn) skid pad.

For the weight distributions 60% front ( $a=3.6 \text{ ft}$ ,  $b=5.4 \text{ ft}$ ), 50% front ( $a=4.5 \text{ ft}$ ,  $b=4.5 \text{ ft}$ ), and 40% front ( $a=5.4 \text{ ft}$ ,  $b=3.6 \text{ ft}$ ), answer the following:

- Calculate the six stability derivatives for this vehicle at a speed of 30 mph.
- Determine the stability factor.
- Determine the critical speed. If it does not exist, say "does not exist".
- Determine the distance from the neutral steer point ( $d$ ) to the front tire.
- Determine the static margin.
- Plot the theoretical vehicle stabilizing moment against velocity from 0 to 75 mph. That is, plot  $N_\beta \cdot \beta + N_r \cdot r$  vs.  $v_x$ . (See hint below.)
- Plot the vehicle control moment against the vehicle stabilizing moment for velocities from 0 to 75 mph. That is, plot  $N_\delta \cdot \delta$  vs.  $N_\beta \cdot \beta + N_r \cdot r$ . (See hint below.)

You should plot the results for all three models in one figure for questions F and G.

Hint for part F:

Select a range of velocities from 0 to 75 mph in increments of, say, 1 mph. For each of these velocities you need to calculate theoretical values for  $N_\beta$ ,  $\beta$ ,  $N_r$ , and  $r$ . The theoretical  $\beta$  can be derived as:

$$\beta = \frac{b}{R} - \frac{a * m * v^2}{l * R * C_{\alpha R}}$$

Hint for part G:

Use the understeer gradient and the lateral acceleration at each velocity to find  $\delta$  at each velocity.

## Solution 2

1. Calculate the six stability derivatives for this vehicle at a speed of 30 mph.

```
% Given data
m = 120; % slug
m = m*14.594; % kg
l = 9; % ft
l = l/3.281; % m
C_alpha_F = 350; % lb/deg
C_alpha_F = C_alpha_F*4.4482*180/pi; % N/rad
C_alpha_R = 350; % lb/deg
C_alpha_R = C_alpha_R*4.4482*180/pi; % N/rad
R = 320; % ft
R = R/3.281; % m
v_x = 30; % mph
v_x = v_x/2.237; % m/s
a = [3.6 4.5 5.4]; % ft
a = a/3.281; % m
b = [5.4 4.5 3.6]; % ft
b = b/3.281; % m
% Calculate stability derivatives
YB = ones(1,3).*(-(C_alpha_F+C_alpha_R)); % N/rad
Yr = ((b*C_alpha_R)-(a*C_alpha_F))/(v_x); % N-s/rad
Yd = ones(1,3).*(C_alpha_F); % N/rad
NB = (b*C_alpha_R)-(a*C_alpha_F); % N-m/rad
Nr = -((a.^2*C_alpha_F)+(b.^2*C_alpha_R))/(v_x); % N-m-s/rad
Nd = ones(1,3).*(a*C_alpha_F); % N-m/rad
stability_derivatives = [YB' Yr' Yd' NB' Nr' Nd'];
fprintf("The stability derivatives are printed in a tabular form below\n" + ...
        "Rows represent weight distributions: 60%% front (a=3.6 ft, b=5.4 ft), 50%% front (a=4.5 ft, b=4.5 ft), and 40%% front (a=5.4 ft, b=3.6 ft)\n" + ...
        "Columns represent stability derivatives: YB (N/rad), Yr (N-s/rad), Yd (N/rad), NB (N-m/rad), Nr (N-m-s/rad), Nd (N-m/rad)\n");
```

The stability derivatives are printed in a tabular form below

Rows represent weight distributions: 60% front (a=3.6 ft, b=5.4 ft), 50% front (a=4.5 ft, b=4.5 ft), and 40% front (a=5.4 ft, b=3.6 ft)

Columns represent stability derivatives: YB (N/rad), Yr (N-s/rad), Yd (N/rad), NB (N-m/rad), Nr (N-m-s/rad), Nd (N-m/rad)

```
disp(stability_derivatives);
```

```
1.0e+05 *

-1.7840    0.0365    0.8920    0.4894   -0.2603    0.9787
-1.7840         0    0.8920         0   -0.2502    1.2234
-1.7840   -0.0365    0.8920   -0.4894   -0.2603    1.4681
```

2. Determine the stability factor.

```
% Calculate UG
UG = (m*((C_alpha_R*b)-(C_alpha_F*a)))/(l*C_alpha_F*C_alpha_R);
% Calculate stability factor
```

```
K = UG/l; % rad-s^2/m^2
fprintf("The stability factors are printed in a vector form below\n" + ...
        "Rows represent weight distributions: 60%% front (a=3.6 ft, b=5.4 ft), 50%% front (a=4.5 ft, b=4.5 ft), and 40%% front (a=3.6 ft, b=3.6 ft)\n" + ...
        "Column represents stability factor: K (rad-s^2/m^2)");
```

The stability factors are printed in a vector form below  
 Rows represent weight distributions: 60% front (a=3.6 ft, b=5.4 ft), 50% front (a=4.5 ft, b=4.5 ft), and 40% front (a=3.6 ft, b=3.6 ft)  
 Column represents stability factor: K (rad-s<sup>2</sup>/m<sup>2</sup>)

```
disp(K');
```

```
0.0014
0
-0.0014
```

3. Determine the critical speed. If it does not exist, say “does not exist”.

```
% Calculate critical speed
v_crit = sqrt(-1./K);
fprintf("The critical speeds are printed in a vector form below\n" + ...
        "Rows represent weight distributions: 60%% front (a=3.6 ft, b=5.4 ft), 50%% front (a=4.5 ft, b=4.5 ft), and 40%% front (a=3.6 ft, b=3.6 ft)\n" + ...
        "Column represents critical speed: v_crit (m/s)");
```

The critical speeds are printed in a vector form below  
 Rows represent weight distributions: 60% front (a=3.6 ft, b=5.4 ft), 50% front (a=4.5 ft, b=4.5 ft), and 40% front (a=3.6 ft, b=3.6 ft)  
 Column represents critical speed: v\_crit (m/s)

```
for i=1:length(v_crit)
    if isreal(v_crit(i))
        disp(v_crit(i))
    else
        disp('does not exist')
    end
end
```

```
does not exist
does not exist
26.4310
```

4. Determine the distance from the neutral steer point (d) to the front tire.

```
% Calculate neutral steer point (NSP)
NSP = C_alpha_R/(C_alpha_F+C_alpha_R);
% Calculate distance from the neutral steer point to the front tire
d = NSP*l;
fprintf("The distance from the neutral steer point to the front tire is %.4f m", d);
```

The distance from the neutral steer point to the front tire is 1.3715 m

5. Determine the static margin.

```
% Calculate static margin
SM = ((ones(1,3)*d)-a)./(ones(1,3)*l);
fprintf("The static margins are printed in a vector form below\n" + ...
        "Rows represent weight distributions: 60%% front (a=3.6 ft, b=5.4 ft), 50%% front (a=4.5 ft, b=4.5 ft), and 40%% front (a=3.6 ft, b=3.6 ft)\n" + ...
        "Column represents static margin: SM");
```

```
"Column represents static margin: SM (unless or %%)");
```

The static margins are printed in a vector form below

Rows represent weight distributions: 60% front (a=3.6 ft, b=5.4 ft), 50% front (a=4.5 ft, b=4.5 ft), and 40% front (a=5.4 ft, b=3.6 ft)

Column represents static margin: SM (unless or %)

```
disp(SM');
```

```
0.1000  
0  
-0.1000
```

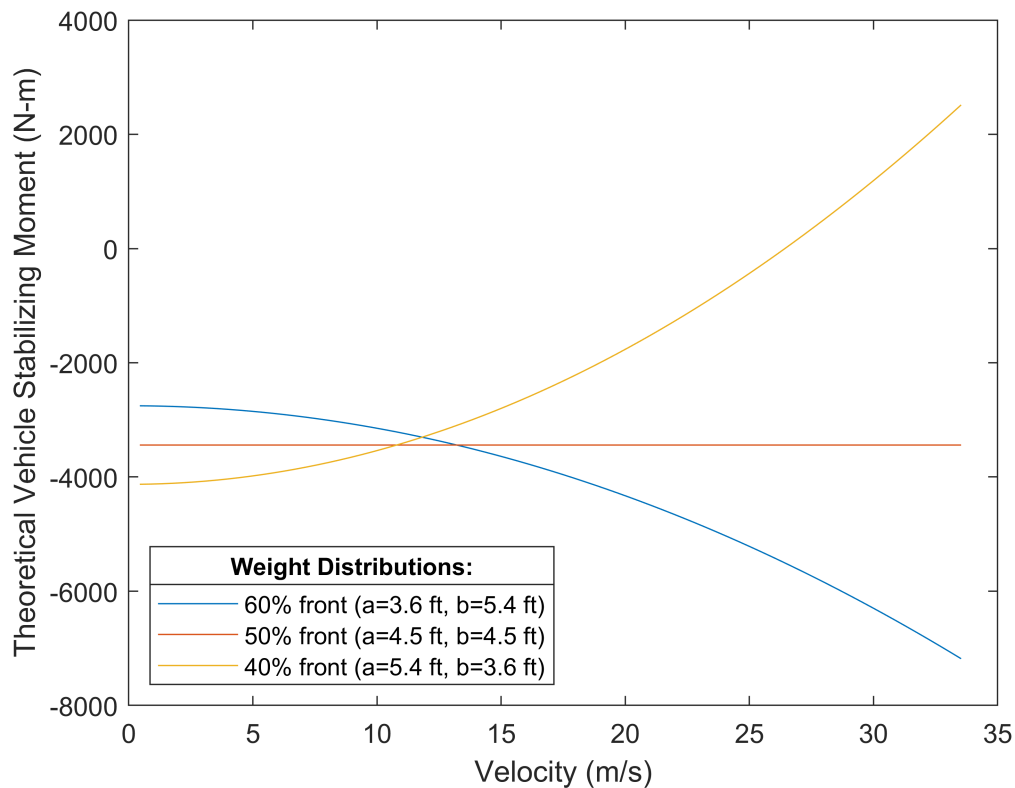
6. Plot the theoretical vehicle stabilizing moment against velocity from 0 to 75 mph. That is, plot  $N_\beta \cdot \beta + N_r \cdot r$  vs.  $v_x$ .

Hint:

Select a range of velocities from 0 to 75 mph in increments of, say, 1 mph. For each of these velocities you need to calculate theoretical values for  $N_\beta$ ,  $\beta$ ,  $N_r$ , and  $r$ . The theoretical  $\beta$  can be derived as:

$$\beta = \frac{b}{R} - \frac{a * m * v^2}{l * R * C_{\alpha R}}$$

```
v_x = 0:75; % mph  
v_x = v_x/2.237; % m/s  
NB = [];  
B = [];  
Nr = [];  
r = [];  
for i=1:length(v_x)  
    NB(:,i) = (b*C_alpha_R)-(a*C_alpha_F);  
    B(:,i) = (b/R)-(a*m*v_x(i)^2)/(l*R*C_alpha_R);  
    Nr(:,i) = -((a.^2*C_alpha_F)+(b.^2*C_alpha_R))/(v_x(i)');  
    r(:,i) = v_x(i)/R;  
end  
X = v_x;  
Y = (NB.*B)+(Nr.*r);  
plot(X,Y(1,:))  
hold on;  
plot(X,Y(2,:))  
plot(X,Y(3,:))  
hold off;  
xlabel("Velocity (m/s)")  
ylabel("Theoretical Vehicle Stabilizing Moment (N-m)")  
lgd = legend("60% front (a=3.6 ft, b=5.4 ft)", "50% front (a=4.5 ft, b=4.5 ft)", "40% front (a=5.4 ft, b=3.6 ft)")  
title(lgd,'Weight Distributions:')
```



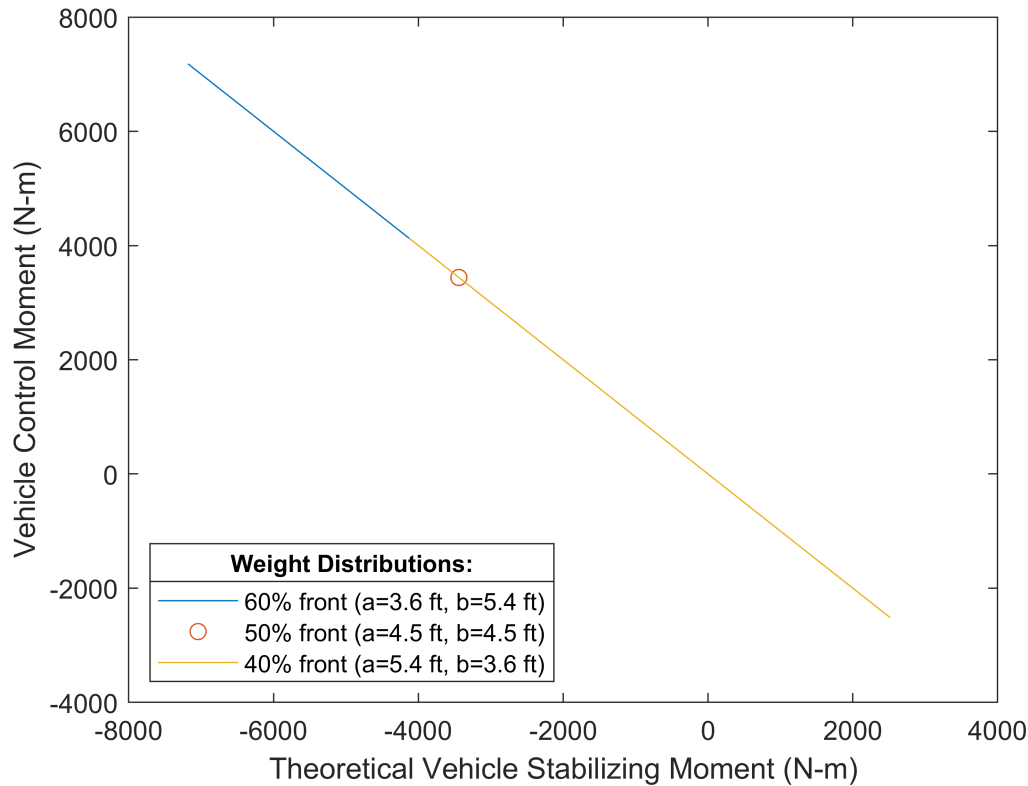
7. Plot the vehicle control moment against the vehicle stabilizing moment for velocities from 0 to 75 mph. That is, plot  $N_{\delta} \cdot \delta$  vs.  $N_{\beta} \cdot \beta + N_r \cdot r$ .

Hint:

Use the understeer gradient and the lateral acceleration at each velocity to find  $\delta$  at each velocity.

```
Nd = [];
d = [];
for i=1:length(v_x)
    Nd(:,i) = ones(1,3).*(a*C_alpha_F);
    a_y = v_x(i)^2/R;
    UG = (m*((C_alpha_R*b)-(C_alpha_F*a)))/(l*C_alpha_F*C_alpha_R);
    d_A = l/R;
    d(:,i) = d_A+(UG*a_y);
end
X = (NB.*B)+(Nr.*r);
Y = Nd.*d;
plot(X(1,:),Y(1,:))
hold on;
plot(X(2,:),Y(2,:), 'o')
plot(X(3,:),Y(3,:))
hold off;
xlabel("Theoretical Vehicle Stabilizing Moment (N-m)")
ylabel("Vehicle Control Moment (N-m)")
lgd = legend("60% front (a=3.6 ft, b=5.4 ft)", "50% front (a=4.5 ft, b=4.5 ft)", "40% front (a=5.4 ft, b=3.6 ft)");
```

```
title(lgd,'Weight Distributions:')
```



### Problem 3

#### Vehicle Parameters:

- Mass: 1637 kg
- Yaw inertia: 3326 kg-m<sup>2</sup>
- Wheelbase: 2.736 m
- Weight distribution: 60% to front
- Front cornering stiffness: 802 N/deg
- Rear cornering stiffness: 785 N/deg
- Steering ratio: 15:1 (15 degree at the steering wheel = 1 degree at the front wheel)

#### Maneuver Description:

In this problem, you are required to simulate the bicycle model for the maneuver that is described below. Based on the description, you should create a vector of inputs for the simulation.

The roadwheel steering angle is the input to your bicycle model. In the first maneuver, provide a step input for this steering angle. The vehicle is first being driven down a straight line at 74 mph for 7 seconds after which the driver holds the handwheel position constant at 45 degrees for 60 seconds. The handwheel position is then returned to 0 degrees and the maneuver is terminated

#### Answer the following:

Using a state-space approach, determine the states,  $\beta$  and  $\dot{\psi}$ , of the bicycle model for the complete maneuver. Assume a linear tire model. Provide plots for each maneuver (1)  $\beta$  v/s time, (2)  $\dot{\psi}$  v/s time, (3)  $\alpha_f$  v/s time, and (4)  $\alpha_r$  vs time for the entire length of the simulation. (Total 4 plots)

### Solution 3

```

m = 1637; % kg
Iz = 3326; % kg-m^2
l = 2.736; % m
a = 0.4*l;
b = l-a;
C_alpha_F = 802; % N/deg
C_alpha_F = C_alpha_F*(180/pi); % N/rad
C_alpha_R = 785; % N/deg
C_alpha_R = C_alpha_R*(180/pi); % N/rad
SR = 15;
v_x = 74; % mph
v_x = v_x/2.237; % m/s

% Single-Track Model
a11 = -((C_alpha_R+C_alpha_F)/(m*v_x));
a12 = (((C_alpha_R*b)-(C_alpha_F*a))/(m*v_x^2))-1;
a21 = ((C_alpha_R*b)-(C_alpha_F*a))/(Iz);
a22 = -((C_alpha_R*b^2)+(C_alpha_F*a^2))/(Iz*v_x);
b1 = (C_alpha_F)/(m*v_x);
b2 = (C_alpha_F*a)/(Iz);
A = [a11 a12; a21 a22];
B = [b1; b2];

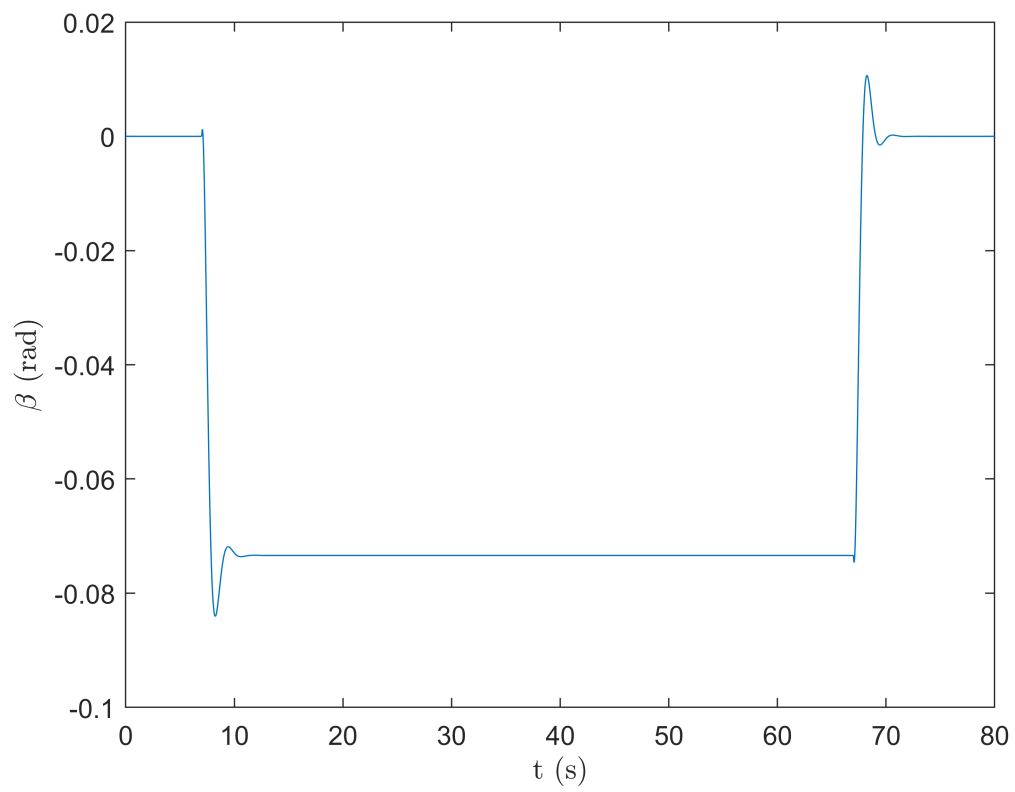
% Initialization
dt = 0.001; % s
X = [];
X(:,1) = [0;0];
X_dot = [];
u = [ones(1,7000)*0 ones(1,60000)*(deg2rad(45)/SR) ones(1,13000)*0]; % steering input (rad) at

% Simulation at each millisecond
for t=1:80000
    X_dot(:,t) = A*X(:,t)+B*u(t);
    X(:,t+1) = X(:,t) + X_dot(:,t)*dt;
end
alpha_F = [0 u] - (X(2,:)*a)/v_x - X(1,:);
alpha_R = (X(2,:)*b)/v_x - X(1,:);

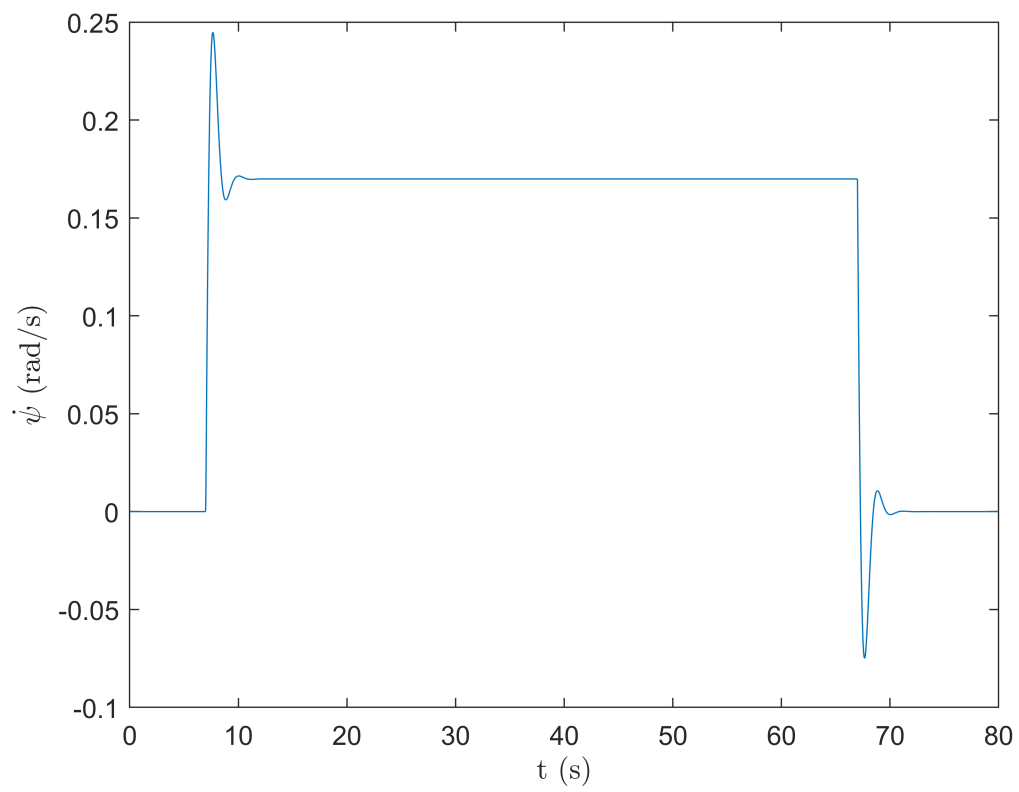
% Plot
t = 0:80000; % ms
plot(t/1000,X(1,:))
xlabel("t (s)", 'interpreter', 'latex')
ylabel("$\beta$ (rad)", 'interpreter', 'latex')

```

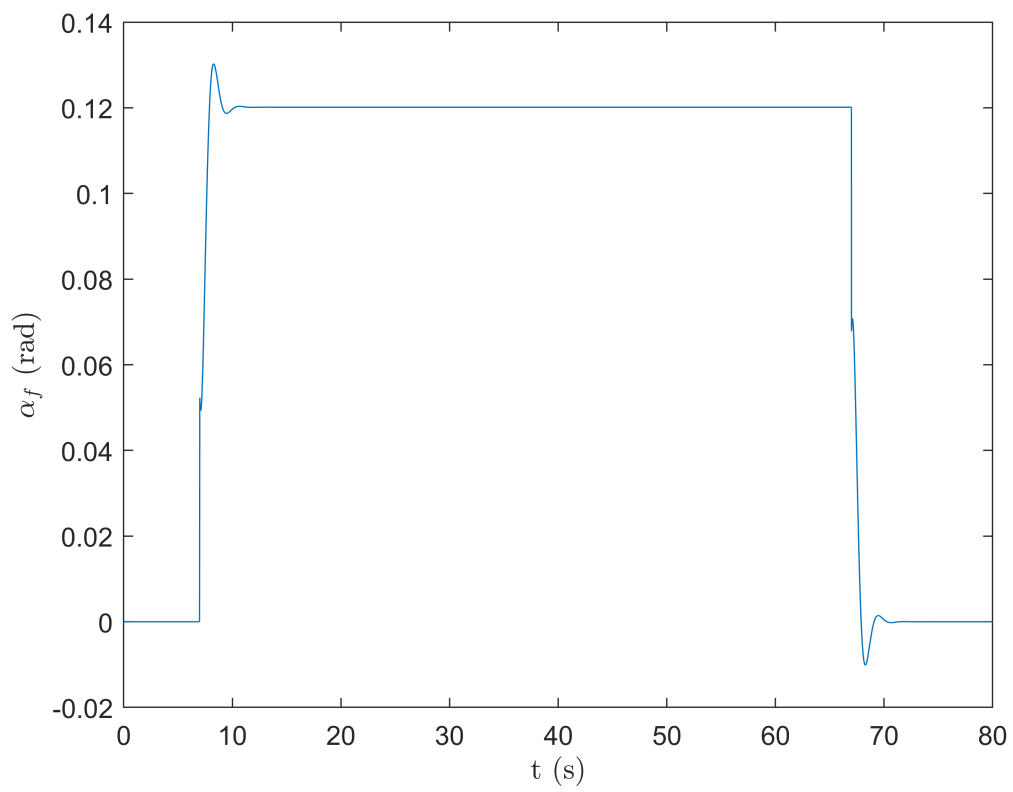




```
plot(t/1000,X(2,:))  
xlabel("t (s)",'interpreter','latex')  
ylabel("$\dot{\psi}$ (rad/s)",'interpreter','latex')
```



```
plot(t/1000,alpha_F)
xlabel("t (s)", 'interpreter', 'latex')
ylabel("$\alpha_f$ (rad)", 'interpreter', 'latex')
```



```
plot(t/1000,alpha_R)
xlabel("t (s)", 'interpreter', 'latex')
ylabel("$\alpha_r$ (rad)", 'interpreter', 'latex')
```

