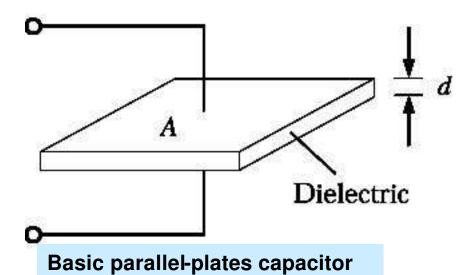
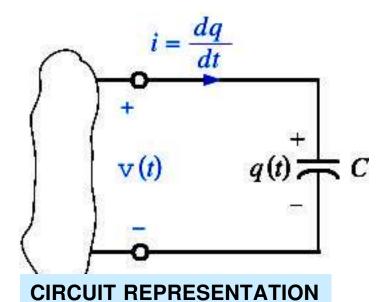
### **CONDENSADORES E BOBINES**

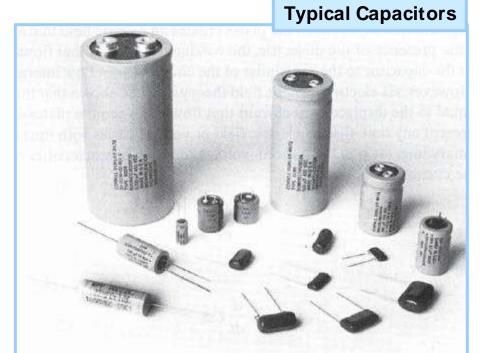
**DISPOSITIVOS PASSIVOS DE ARMAZENAMENTO DE ENERGIA** 

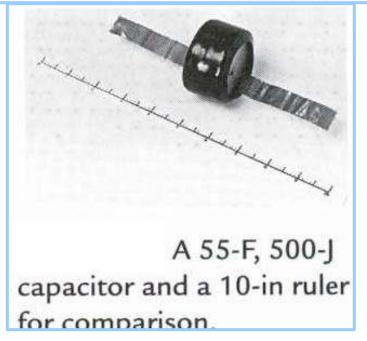
### CONDENSADOR

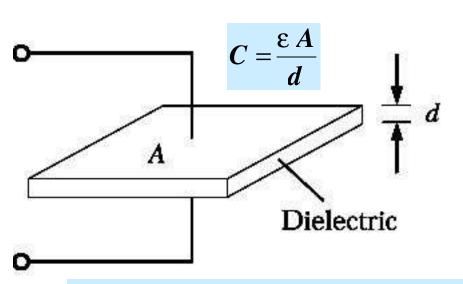


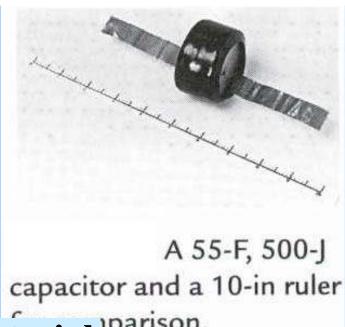


CONVENÇÃO PASSIVA PARA A CORRENTE









# E Constante dielectrica do material

$$55F = \frac{8.85 \times 10^{-12} A}{1.016 \times 10^{-4}} \Rightarrow A = 6.3141 \times 10^8 m^2$$

Valores de capacidade são baixos.Microfarads é típico Circuitos integrados é ainda mais baixo ... pico farads é típico Condensadores obedecem À Lei de Coulomb :

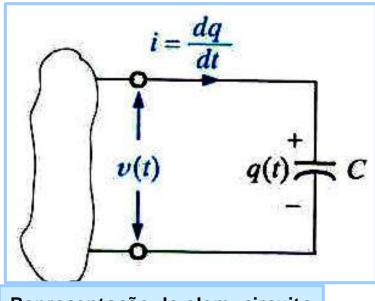
$$Q = CV_C$$

C é a capacidade do condensador

carga tensão el.

Um Farad(F) é a capacidade de um dispositivo Que armazena um coulomb de carga a um volt.

$$Farad = \frac{Coulomb}{Volt}$$



Representação do elem. circuito

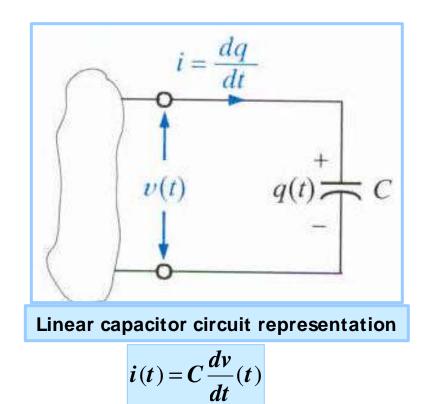
EXAMPLE Queda de tensão de um cond. De 2 micro Farads que armazene 10mC de carga

$$V_C = \frac{1}{C}Q = \frac{1}{2*10^{-6}}10*10^{-3} = 5000$$
 v

Capacitance in Farads, charge in Coulombs result in voltage in Volts

CONDENSADORES PODEM SER PERI GOSOS!!!!!!!!!

Condensadores apenas armazenam e libertam carga. NÃO "CRI AM" CARGA.



$$Q_C = CV_C$$
 LEI DA CAPACIDADE!

Se a tensão varia a carga varia e portanto há uma corrente Que flui......

Podemos exprimir a tensão em função Da corrente.

$$V_C(t) = \frac{1}{C}Q = \frac{1}{C} \int_{-\infty}^t i_C(x) dx$$

Forma integral.

Uma consequência é que ...

$$V_C(t-) = V_C(t+); \forall t$$

Tensão aos terminais do condensador TEM QUE SER CONTÍNUA.

... Ou a corrente em função da tensão Aos seus terminais

$$i_C = \frac{dQ}{dt} = C\frac{dV_C}{dt}$$

Forma diferencial da lei da capacitância

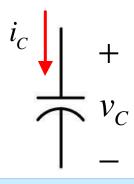
E daí ??

$$V_C = Const \Rightarrow i_C = 0$$

Comportamento estacionário ou DC

Se a tensão é constante o condensador COMPORTA-SE COMO UM CIRCUITO ABERTO.

### Condensador como elemento de circuito



$$i_C(t) = C \frac{dv_c}{dt}(t)$$

$$v_C(t) = \frac{1}{C} \int_C^t i_C(x) dx$$

$$i_R = \frac{1}{R}v_R$$

$$v_R = Ri_R$$
Ohm's Law

$$\int_{-\infty}^{t} = \int_{-\infty}^{t_0} + \int_{t_1}^{t}$$

$$v_{C}(t) = \frac{1}{C} \int_{-\infty}^{t_{0}} i_{C}(x) dx + \frac{1}{C} \int_{t_{0}}^{t} i_{C}(x) dx$$

$$v_C(t) = v_C(t_0) + \frac{1}{C} \int_{t_0}^{t} i_C(x) dx$$

### Condensador como armazenador de energia

$$i_C$$
 +  $v_C$ 

Potência instantânea

$$p_C(t) = v_C(t)i_C(t)$$

$$i_C(t) = C \frac{dv_c}{dt}(t)$$

$$p_C(t) = Cv_C(t) \frac{dv_c}{dt}$$

$$p_C(t) = C \frac{d}{dt} \left( \frac{1}{2} v_C^2(t) \right)$$
 Energia é integral da potência 
$$w_C(t_2, t_1) = \int_{t}^{t_2} p_C(x) dx$$

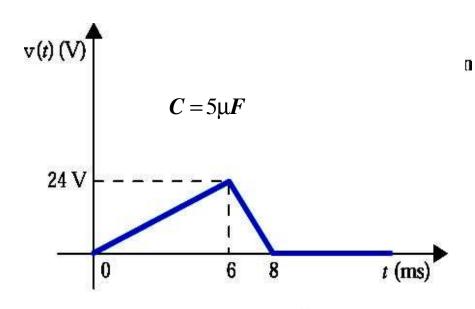
$$\boldsymbol{p}_{\boldsymbol{C}}(t) = \frac{1}{\boldsymbol{C}} \frac{\boldsymbol{d}}{\boldsymbol{d}t} \left( \frac{1}{2} \boldsymbol{q}_{\boldsymbol{c}}^{2}(t) \right)$$

Se t1 é menos infinito temos "energia armazenada em t2."

Se ambos os limites são infinitos temos A energia total armazenada.

$$\mathbf{w}_{C}(t_{2},t_{1}) = \frac{1}{2}\mathbf{C}v_{C}^{2}(t_{2}) - \frac{1}{2}\mathbf{C}v_{C}^{2}(t_{1})$$

$$w_{C}(t_{2},t_{1}) = \frac{1}{C}q_{C}^{2}(t_{2}) - \frac{1}{C}q_{C}^{2}(t_{1})$$



Energia armazenada de 0 - 6 msec

$$|\mathbf{w}_{C}(0,6)| = \frac{1}{2}\mathbf{C}v_{C}^{2}(6) - \frac{1}{2}\mathbf{C}v_{C}^{2}(0)$$

$$w_C(0,6) = \frac{1}{2}5*10^{-6}[F]*(24)^2[V^2]$$

Carga armazenada aos 3msec

$$q_C(3) = Cv_C(3)$$

 $q_C(3) = 5*10^{-6}[F]*12[V] = 60\mu C$ 

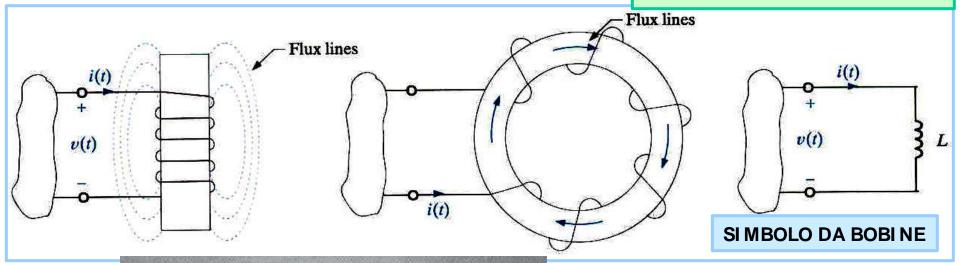
Exemplo

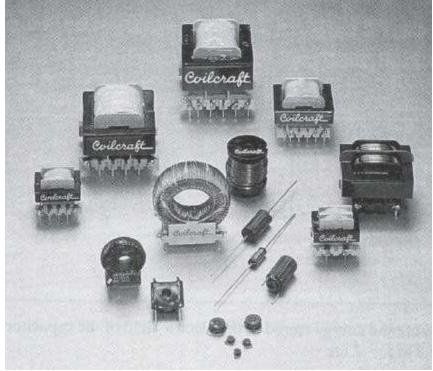
"energia total armazenada?" ....

"carga total armazenada?" ...

### **BOBINES**

## ATENÇÃO À CONVENÇÃO PARA TENSÃO E CORRENTE





Um fluxo variável no tempo I nduz um campo electro--magnético, surgindo uma Tensão (induzida) aos Terminais da bobine.

## FLUXO MAGNÉTICO VARIÁVEL NO TEMPO INDUZ UMA TENSÃO NA BOBINE

$$v_L = \frac{d\phi}{dt}$$
 Lei da indução

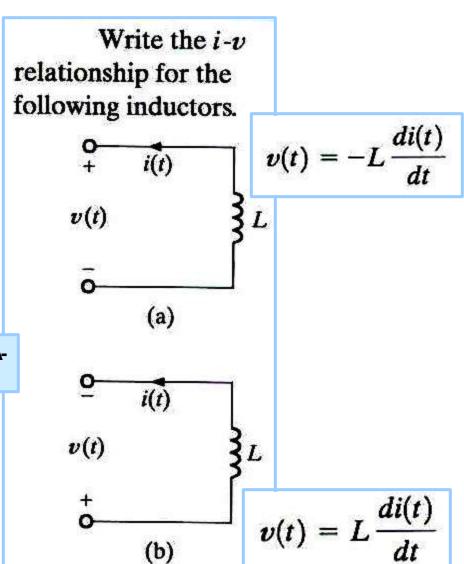
Para uma bobine "normal" (linear), o fluxo é Proporcional à corrente.

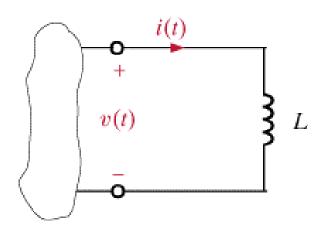
$$\phi = Li_L \Rightarrow v_L = L\frac{di_L}{dt}$$

A CONSTANTE DE PROPORCIONALIDADE L CHAMA-SE INDUTÂNCIA

### A INDUTÂNCIA MEDE-SE EM HENRY

$$HENRY = \frac{Volt}{Amp/sec}$$





$$v_L = L \frac{di_L}{dt}$$
 Differential form of induction law

$$i_L(t) = \frac{1}{L} \int_{-\infty}^{t} v_L(x) dx$$

Integral form of induction law

$$i_L(t) = i_L(t_0) + \frac{1}{L} \int_{t_0}^t v_L(x) dx; \ t \ge t_0$$

Conseq. Directa da forma integral...

 $i_L(t-)=i_L(t+); \quad \forall t$  A corrente tem que ser contínua...

Outra consequência ....

$$i_L = Const. \Rightarrow v_L = 0$$
 Comportamento DC

### Potência e energia armazenada

$$p_L(t) = v_L(t)i_L(t) \quad \mathbf{w} \quad p_L(t) = L\frac{di_L}{dt}(t)i_L(t) = \frac{d}{dt} \left(\frac{1}{2}Li_L^2(t)\right)$$

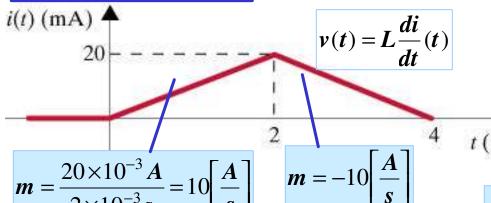
$$w_L(t_2,t_1) = \int_{t_1}^{t_2} \frac{d}{dt} \left( \frac{1}{2} L i_L^2(x) \right) dx$$
Current in Amps, Inductance in Henrys yield energy in Joules

$$w(t_2,t_1) = \frac{1}{2}Li_L^2(t_2) - \frac{1}{2}Li_L^2(t_1)$$
 Energy stored on the interval Can be positive or negative

$$w_L(t) = \frac{1}{2}Li_L^2(t)$$
 "Energy stored at time t" Must be non-negative. Passive element!!!

### **LEARNING EXAMPLE**

#### L=10mH. FIND THE VOLTAGE



#### **ENERGY STORED BETWEEN 2 AND 4 ms**

$$w(4,2) = \frac{1}{2}Li_L^2(4) - \frac{1}{2}Li_L^2(2)$$

$$w(4,2) = 0 - 0.5*10*10^{-3}(20*10^{-3})^2$$
 J

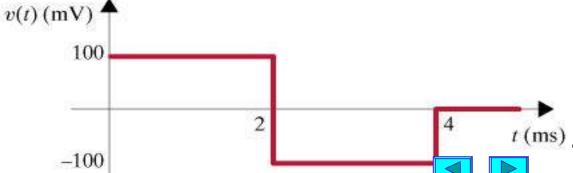
### THE DERIVATIVE OF A STRAIGHT LINE IS ITS SLOPE

$$\frac{di}{dt} = \begin{cases} 10(A/s) & 0 \le t \le 2ms \\ -10(A/s) & 2 < t \le 4ms \\ 0 & elsewhere \end{cases}$$

THE VALUE IS NEGATIVE BECAUSE THE INDUCTOR IS SUPPLYING ENERGY PREVIOUSLY STORED

$$\frac{di}{dt}(t) = 10(A/s) 
L = 10 \times 10^{-3} H$$

$$\Rightarrow v(t) = 100 \times 10^{-3} V = 100 mV$$



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### The Dual Relationship for Capacitors and Inductors

Capacitor	Inductor
$i(t) = C \frac{dv(t)}{dt}$	$v(t) = L \frac{di(t)}{dt}$
$v(t) = \frac{1}{C} \int_{t_0}^t i(x) dx + v(t_0)$	$i(t) = \frac{1}{L} \int_{t_0}^{t} v(x) dx + i(t_0)$
$p(t) = Cv(t) \frac{dv(t)}{dt}$ $C \to L$ $v \to i$	$p(t) = Li(t) \frac{di(t)}{dt}$
$w(t) = \frac{1}{2}Cv(t)^2 \qquad i \to v$	$w(t) = \frac{1}{2}Li^2(t)$

### Condensadores em série

$$v(t) = v_1(t) + v_2(t) + v_3(t) + \cdots + v_N(t)$$

$$v_i(t) = \frac{1}{C_i} \int_{t_0}^t i(t) dt + v_i(t_0)$$

$$C_s = \frac{C_1 C_2}{C_1 + C_2}$$

Combinação serie de 2 condensadores

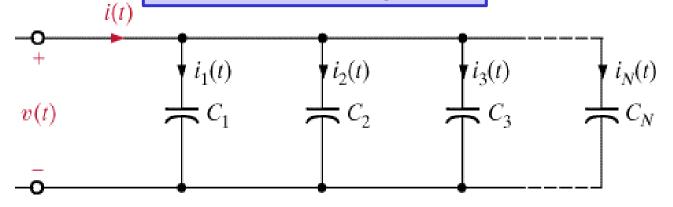
$$v(t) = \left(\sum_{i=1}^{N} \frac{1}{C_i}\right) \int_{t_0}^{t} i(t) dt + \sum_{i=1}^{N} v_i(t_0)$$

$$\frac{1}{C_S} = \sum_{i=1}^N \frac{1}{C_i} = \frac{1}{C_1} + \frac{1}{C_2} + \dots + \frac{1}{C_N}$$

$$G\mu F \qquad 3\mu F \qquad C_S = 2\mu F$$

$$v(t_0) = \sum_{i=1}^N v_i(t_0)$$
 Semelhante a resist. Em paralelo

### **Condensadores em paralelo**



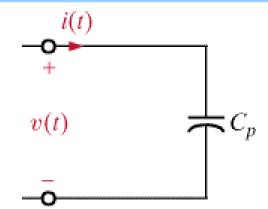
$$i(t) = i_1(t) + i_2(t) + i_3(t) + \cdots + i_N(t)$$

$$i_k(t) = C_k \frac{dv}{dt}(t)$$

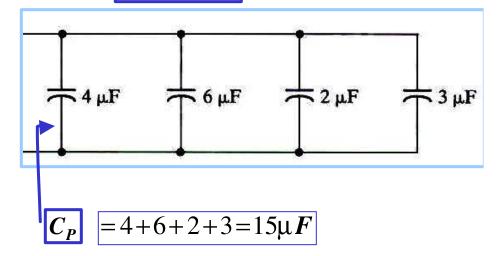
$$i(t) = C_1 \frac{dv(t)}{dt} + C_2 \frac{dv(t)}{dt} + C_3 \frac{dv(t)}{dt} + \dots + C_N \frac{dv(t)}{dt}$$

$$= \bigg(\sum_{i=1}^N C_i\bigg) \frac{dv(t)}{dt}$$

$$C_p = C_1 + C_2 + C_3 + \cdots + C_N$$

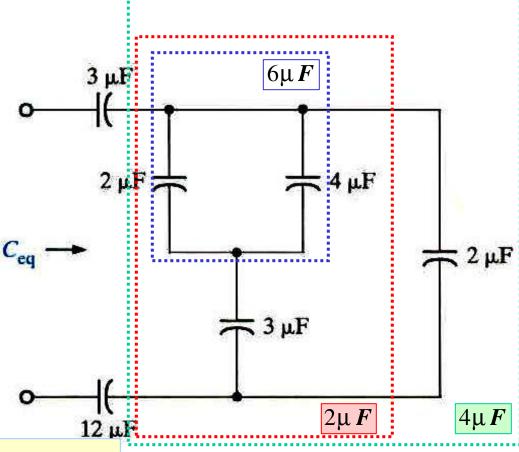


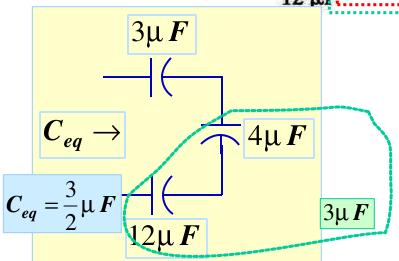
### **EXEMPLO**



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### **EXEMPLO**





### **SERIES INDUCTORS**

 $= v_N(t) +$ 

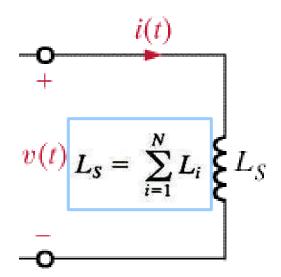
$$v(t)$$
  $t_{N}$   $t_{N}$ 

$$v(t) = v_1(t) + v_2(t) + v_3(t) + \cdots + v_N(t)$$

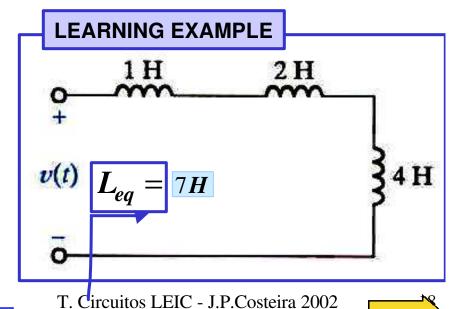
$$v_k(t) = L_k \frac{di}{dt}(t)$$

$$v(t) = L_1 \frac{di(t)}{dt} + L_2 \frac{di(t)}{dt} + L_3 \frac{di(t)}{dt} + \dots + L_N \frac{di(t)}{dt}$$
$$= \left(\sum_{i=1}^N L_i\right) \frac{di(t)}{dt}$$

$$L_{S} = \sum_{i=1}^{N} L_{i}$$



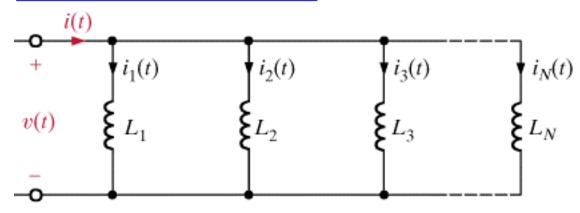
$$v(t) = L_S \frac{di}{dt}(t)$$

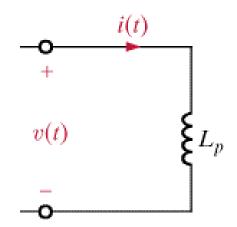






### **PARALLEL INDUCTORS**



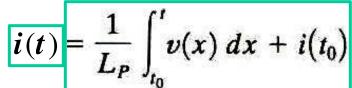


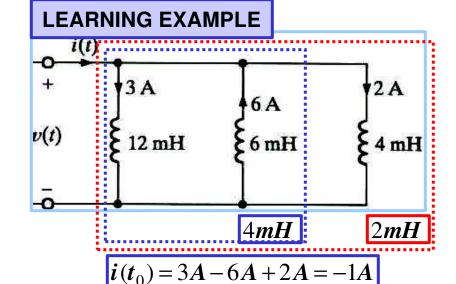
$$i(t) = i_1(t) + i_2(t) + i_3(t) + \dots + i_N(t)$$
$$i_j(t) = \frac{1}{L_j} \int_{t_0}^t v(x) \, dx + i_j(t_0)$$

$$i(t) = \left(\sum_{j=1}^{N} \frac{1}{L_{j}}\right) \int_{t_{0}}^{t} v(x) dx + \sum_{j=1}^{N} i_{j}(t_{0})$$

$$\frac{1}{L_p} = \frac{1}{L_1} + \frac{1}{L_2} + \frac{1}{L_3} + \dots + \frac{1}{L_N}$$

$$i(t_0) = \sum_{j=1}^{N} i_j(t_0)$$





INDUCTORS COMBINE LIKE RESISTORS
CAPACITORS COMBINE LIKE CONDUCTANCES

osteira 2002



### **SUMMARY**

The important (dual) relationships for capacitors and inductors are as follows:

$$q = Cv$$

$$i(t) = C \frac{dv(t)}{dt} \qquad v(t) = L \frac{di(t)}{dt}$$

$$v(t) = \frac{1}{C} \int_{-\infty}^{t} i(x) dx \qquad i(t) = \frac{1}{L} \int_{-\infty}^{t} v(x) dx$$

$$p(t) = Cv(t) \frac{dv(t)}{dt} \qquad p(t) = Li(t) \frac{di(t)}{dt}$$

$$W_C(t) = 1/2Cv^2(t) \qquad W_L(t) = 1/2Li^2(t)$$

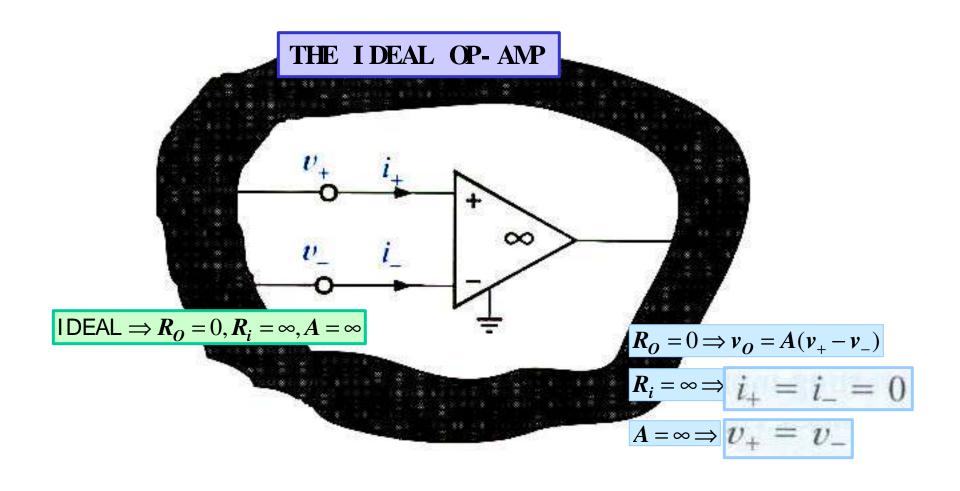
- The passive sign convention is used with capacitors and inductors.
- In dc steady state a capacitor looks like an open circuit and an inductor looks like a short circuit.
- Leakage resistance is present in practical capacitors and inductors.
- When capacitors are interconnected, their equivalent capacitance is determined as follows: Capacitors in series combine like resistors in parallel and capacitors in parallel combine like resistors in series.
- When inductors are interconnected, their equivalent inductance is determined as follows: Inductors in series combine like resistors in series and inductors in parallel combine like resistors in parallel.
- RC operational amplifier circuits can be used to differentiate or integrate an electrical signal.





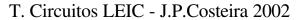
### RC OPERATIONAL AMPLIFIER CIRCUITS

### INTRODUCES TWO VERY IMPORTANT PRACTICAL CIRCUITS BASED ON OPERATIONAL AMPLIFIERS



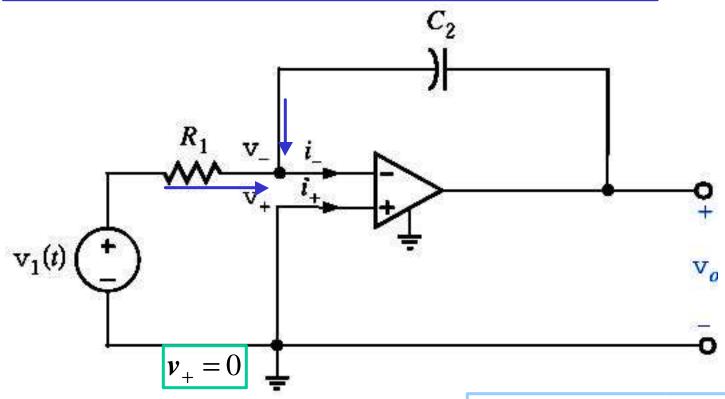








### RC OPERATIONAL AMPLIFIER CIRCUITS -THE INTEGRATOR



$$\frac{v_1 - v_-}{R_1} + C_2 \frac{d}{dt} (v_o - v_-) = i_-$$

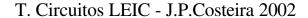
### **IDEAL OP-AMP ASSUMPTIONS**

$$\begin{array}{ccc} v_{-} = v_{+} & (A = \infty) \\ i_{-} = 0 & (R_{i} = \infty) \end{array} \qquad \begin{array}{c} v_{1} \\ \hline R_{1} \end{array} = -C_{2} \frac{dv_{o}}{dt}$$

$$v_o(t) = \frac{-1}{R_1 C_2} \int_{-\infty}^{t} v_1(x) dx$$
$$= \frac{-1}{R_1 C_2} \int_{0}^{t} v_1(x) dx + v_o(0)$$

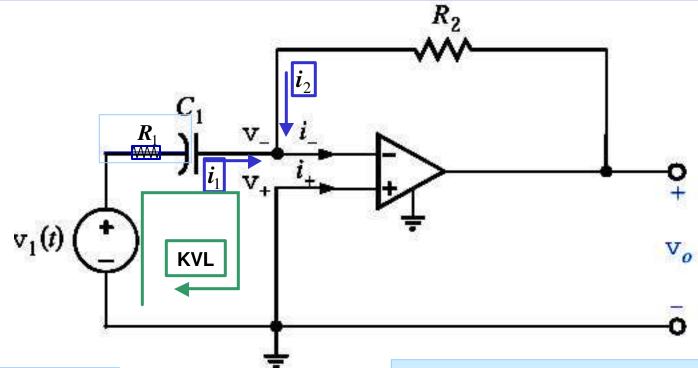








#### RC OPERATIONAL AMPLIFIER CIRCUITS - THE DIFFERENTIATOR



$$\mathbf{v}_{+} = 0$$

$$KCL@v_{-}: i_{1}+i_{2}=i_{-}$$

#### **IDEAL OP-AMP ASSUMPTIONS**

$$\begin{aligned}
\mathbf{v}_{-} &= \mathbf{v}_{+} & (\mathbf{A} &= \infty) \\
\mathbf{i}_{-} &= 0 & (\mathbf{R}_{i} &= \infty)
\end{aligned}
\mathbf{i}_{1} + \frac{\mathbf{v}_{0}}{\mathbf{R}_{2}} = 0$$

$$v_1(t) = R_1 i_1 + \frac{1}{C_1} \int_{-\infty}^{t} i_1(x) dx$$
 DIFFERENTIATE

$$\mathbf{R}_{1}\mathbf{C}_{1}\frac{d\mathbf{i}_{1}}{dt} + \mathbf{i}_{1} = \mathbf{C}_{1}\frac{d\mathbf{v}_{1}}{dt}(t)$$

replace 
$$i_1$$
 in terms of  $v_0$   $(i_1 = -\frac{v_0}{R_2})$ 

$$R_1C_1\frac{dv_o}{dt} + v_o = -R_2C_1\frac{dv_1}{dt}(t)$$

IF R1 COULD BE SET TO ZERO WE WOULD HAVE AN IDEAL DIFFERENTIATOR.

IN PRACTICE AN IDEAL DIFFERENTIATOR AMPLIFIES ELECTRIC NOISE AND DOES NOT OPERATE.

THE RESISTOR INTRODUCES A FILTERING ACTION. ITS VALUE IS KEPT AS SMALL AS POSSIBLE TO APPROXIMATE A DIFFERENTIATOR



