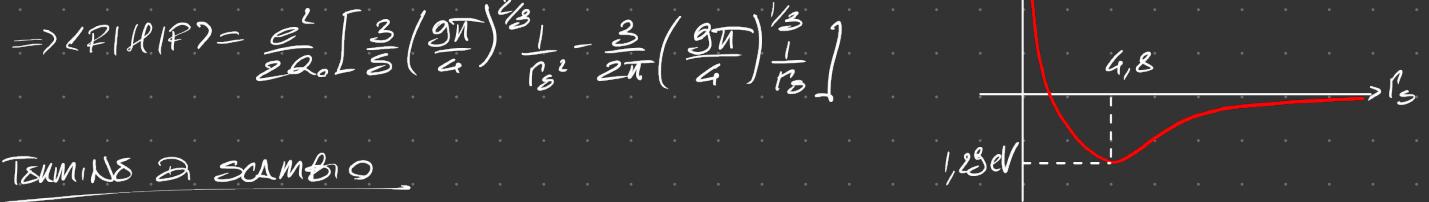




$$\frac{\langle \hat{P} \rangle}{N} = \frac{3}{5} \frac{k^2 R_F^2}{2m} - \frac{1}{n} \frac{e^2}{4\pi^3} K_F^4 = \frac{3}{5} \frac{k^2}{2m} K_F^2 - \frac{3}{4\pi} \frac{e^2}{Q_0} K_F Q_0 = \frac{e^2}{2Q_0} \left[ \frac{3}{5} (Q_0 K_F)^2 - \frac{3}{2\pi} (Q_0 K_F) \right] \rightarrow \text{DEF SPATIALE MODA} \quad \left( \frac{V}{N} \right)^{1/3} = \left[ \frac{4}{3} \pi (R_S) \right]^{3/2} \xrightarrow{\text{EDITE}} \frac{1}{n} = \frac{3\pi^2}{K_F^3} = \frac{V}{N} = \frac{4}{3} \pi (R_S) Q_0^3 \Rightarrow (K_F Q_0)^2 = \frac{3\pi^2}{4\pi} \frac{3}{4} \frac{V}{R_S^3} \rightarrow Q_0 K_F = \left( \frac{3\pi}{4} \right)^{1/3} \frac{1}{R_S}$$



TERMINI DI SCAMBIO

$$E_x[n] = -\frac{e^2}{2} \frac{3}{2\pi} (2\pi^2)^{1/3} \int_{\theta} \Delta n(x)$$

$$\text{THERMODYNAMICA} \quad dE = -PdV + \mu dN \rightarrow \times \text{sys omogeneo} \quad (\text{INVAN TABIBI})$$

$$\begin{cases} \mathcal{E} = \frac{E}{N} = \mathcal{E}[n] \\ \mu = \frac{\partial \mathcal{E}}{\partial N} = \frac{\partial \mathcal{E}}{\partial n} \\ P = -\frac{\partial \mathcal{E}}{\partial V} = n(\mu - \mathcal{E}) \end{cases}$$

MISTALCI

- Al  $P_S \approx 2,87$
- Nel  $P_S \approx 3,33$
- K  $P_S \approx 6,86$
- Rb  $P_S \approx 5,20$

- OSS
- $P_S < 6 \Rightarrow$  TRANSIZIONE DI FASE
  - $P_S > 6 \Rightarrow$  CALORE DI VAPORAZIONE
  - Si misura essere da CMB
- $$\frac{e^2}{2Q_0} \left( \frac{2,10}{P_S} - \frac{1,8}{P_S} \right)$$

CONSIDERANDO IL VOLUME PARZIALE  $V = \frac{5}{3} \pi R_S^3 N$

$$Q_0 = \text{VOLUME PARZIALE} \quad \Rightarrow P_S = \frac{P_0}{Q_0} \quad \text{CMB DENSITA' sys.}$$

$P_S \rightarrow 0 \Rightarrow$   $\theta \rightarrow$  PARTEBAS PICCOLA (GAS ESTREMISMO)

$$\underline{HE} \quad H = \sum h_i(i) + \frac{1}{2} \sum_{i,j} S(i,j) \rightarrow \text{CONGRUENZA DELLA STAZIONARITÀ} \quad \langle i,j | H | i,j \rangle = \sum_{i,j} S_{ij}$$

$$\langle \phi | H | \phi \rangle = \sum \langle a_i | h | a_i \rangle + \frac{1}{2} \sum_{i,j} \langle a_i | S_{ij} | a_j \rangle + \delta_{ij} \langle a_i | a_j \rangle \rightarrow \text{AL ALI: OLTRE I TUTTI I CONTRIBUENTI PORTANO A STAZIONARITÀ DELLA STAZIONARITÀ}$$

$$E_{AP} = \min_{\{a_i\}} \langle \phi | H | \phi \rangle - \sum_j S_{ij} [c_{ai}, a_j] - \delta_{ij} \rightarrow \text{IMPIEGO} \quad \frac{\delta E}{\delta a_i} = 0 \quad \forall i \rightarrow a_i \rightarrow a_i + \eta_i \rightarrow E[a_i - a_i + \eta_i] - E[a_i - a_i] = \kappa \eta_i + C(\eta_i) \rightarrow \text{CONSIDERAZIONE DI UNO}$$

$$S_{ij} = \langle a_i | h | a_i \rangle + \sum_j \langle a_i | S_{ij} | a_j \rangle - \delta_{ij} \langle a_i | a_j \rangle = 0 + \eta_i \rightarrow h(a_i) + \sum_j \langle a_i | S_{ij} | a_j \rangle = \epsilon_i(a_i) \rightarrow \text{Trovata la soluz.} \Rightarrow \text{FAMIGLIA}$$

$$\Rightarrow E_{AP} = \sum \langle a_i | h | a_i \rangle + \frac{1}{2} \sum_{i,j} \langle a_i | S_{ij} | a_j \rangle - \delta_{ij} \langle a_i | a_j \rangle = \frac{1}{2} \sum_i [\epsilon_i - \langle a_i | h | a_i \rangle]$$

$$\text{PROBLEMA SOLO} \quad \langle x_m | \rightarrow \langle x_m | h | a_i \rangle + \sum_j \langle x_m | a_i | S_{ij} | a_j \rangle = E_i(a_i) = h a_i(x_m) + \sum_j \sum_{j,m} \int_{\text{d}x} \int_{\text{d}x'} \delta(x-x') \delta(x'-x'') \langle x_m | g_j(x'm') | g_j(x'm') \rangle \langle x'm' | a_j(x'm') | a_j(x'm') \rangle = \sum_i a_i(x_m)$$

$$(h a_i)(x_m) + \sum_j \sum_{j,m} \int_{\text{d}x} \int_{\text{d}x'} \delta(x-x') \delta(x'-x'') \delta_{ij} \delta_{jm} \delta_{im} \delta_{jm} \delta_{im} \delta_{ij} \delta_{jm} \delta_{im} \delta_{jm} \delta_{im} \delta_{ij} = E_i(a_i(x_m))$$

$$\left[ \frac{\hbar^2}{2m} \nabla^2 + U(x) \right] a_i(x_m) + \int_{\text{d}x} \int_{\text{d}x'} \delta(x-x') \int_{\text{d}x''} |g_j(x'm')|^2 a_i(x_m) = \left[ \frac{\hbar^2}{2m} \nabla^2 - U(x) \right] a_i(x_m) + O_{ii}(x) a_i(x_m)$$

$$\text{SE CONSIDERIAMO} \quad \text{INVAN TABIBI} \quad [H, p] = 0 \Rightarrow V = V(x-j) \Rightarrow \text{OGNI N-UPA} \quad \text{SODDISFA L'HP}$$

$$\sum \frac{p_i^2}{2m} \delta_{ii} m_i + \sum_j \langle k_j m_j | S_{ij} | k_j m_j \rangle - \log m_j \delta_{ii} m_i = E_i | k_i m_i \rangle \quad \times \text{INVAN V CONSERVA MOMENTO} \Rightarrow \delta + k_j = \delta + k_j \Rightarrow \delta = \delta \quad m_i = m_i$$

$$\frac{\hbar^2}{2m} K_i^2 | k_i m_i \rangle + \sum_j \langle k_i m_i | k_j m_j | S_{ij} | k_j m_j \rangle - \sum_j \langle k_i m_i | k_j m_j | S_{ji} | k_i m_i \rangle = E_i | k_i m_i \rangle$$

$$\Rightarrow \langle k_i m_i | k_j m_j | S_{ij} | k_i m_i \rangle = \langle k_i m_i | S_{ij} | k_j m_j \rangle = \int_{\text{d}x} \int_{\text{d}x'} V(x-x') \langle k_i m_i | x-x' | k_j m_j \rangle = \frac{1}{V} \int_{\text{d}x} \int_{\text{d}x'} V(x-x') = \frac{V_0}{V}$$

$$\Rightarrow \frac{\hbar^2}{2m} K_i^2 | k_i m_i \rangle + \sum_j \frac{\hbar^2}{V} \delta_{ij} m_i - E_{xc} = E_i | k_i m_i \rangle \rightarrow E_{xc} = \langle k_i m_i | k_j m_j | S_{ij} | k_i m_i \rangle = \delta_{mm} \langle k_i m_i | S_{ij} | k_i m_i \rangle = \delta_{mm} \int_{\text{d}x} \int_{\text{d}x'} V(x-x') \langle k_i m_i | x-x' | k_i m_i \rangle = \delta_{mm} \int_{\text{d}x} \int_{\text{d}x'} V(x-x') \tilde{e}^{-\frac{(k_i-k_j)x}{\hbar}} = \frac{\delta_{mm}}{V} \tilde{V}(k_i - k_j)$$

$$\Rightarrow \frac{\hbar^2}{2m} K_i^2 | k_i m_i \rangle + \sum_j \frac{\hbar^2}{V} \delta_{ij} m_i - \sum_j \frac{\delta_{mm}}{V} \tilde{V}(k_i - k_j) | k_i m_i \rangle = E_i | k_i m_i \rangle \rightarrow | k_i m_i \rangle \text{ AUTOSTATO} \quad E_i = \frac{\hbar^2}{2m} K_i^2 + \frac{\hbar^2}{V} \sum_j \delta_{ij} m_i - \frac{1}{V} \sum_j \delta_{mm} \tilde{V}(k_i - k_j)$$

$$\times \text{HE DENSEO} \quad \langle \phi \rangle = \text{HF} \Rightarrow E(\kappa) = \frac{\hbar^2}{2m} \frac{1}{V} \sum_{i,k} \frac{e^2 k^2}{(2\pi)^3} = \frac{\hbar^2}{2m} \frac{1}{V} \frac{e^2}{(2\pi)^3} K_F^2 = \frac{\hbar^2}{2m} \frac{2e^2 K_F}{\pi} f(K_F)$$

$$f(x) = \frac{1}{2} + \frac{1-x^2}{4x} \ln \frac{1+x}{1-x} \rightarrow \text{HP DA PESSIMA MAPPA DEI VAL. DI SINISTRA PUNTO}$$

$$\text{CONSIDERANDO DENSITA' STAT. X UNITA' DI SPAT. VOL.} \quad P(E) = \frac{1}{V} \sum_k S(E(k) - E) \approx \int_{(2\pi)^3} \frac{S(E(k) - E)}{(2\pi)^3} \frac{K^2(k)}{E(k) |k|}$$

$$\rightarrow \text{PER IL K_F} \quad f(K_F) \Big|_{K_F} = f(1) \rightarrow \text{DIVINA DIVINA} \Rightarrow P(E_F) \text{ PROBLEMATICO} \rightarrow \text{NON CONCIDE CON DATI SPATIALI}$$

$$\rightarrow \text{DEF SPATIALE MODA} \quad \left( \frac{V}{N} \right)^{1/3} = \left[ \frac{4}{3} \pi (R_S) \right]^{3/2} \xrightarrow{\text{PAMM}} \frac{1}{n} = \frac{3\pi^2}{K_F^3} = \frac{V}{N} = \frac{4}{3} \pi (R_S) Q_0^3 \Rightarrow (K_F Q_0)^2 = \frac{3\pi^2}{4\pi} \frac{3}{4} \frac{V}{R_S^3} \rightarrow Q_0 K_F = \left( \frac{3\pi}{4} \right)^{1/3} \frac{1}{R_S}$$

EVOLOZIONE TEMPORALE  $H = \sum a_i a_i^\dagger C_a^\dagger C_a \Rightarrow C_a(t) = e^{iHt/a} C_a e^{-iHt/a} = e^{i\omega t} C_a$  ANCHE  $C_a^\dagger(t) = e^{i\omega t} C_a^\dagger$

se H compiato  $\Rightarrow$  DECRESCE A INSTATI  $H = H_0 + V_t \rightarrow$  EVOLZ. CONSUETTA DA FAMIGLIA A SP A 2 PARMI

$\begin{cases} C(t,t') C(t't') = C(t't) \\ C(tt') = \text{11} \\ C^\dagger(t't') = C(t't) \end{cases} \rightarrow$  PROPAGATORI (NO SHOT NOVELLO ISOTROPO)  $\rightarrow \square C(ttt') C(t'tt') = \partial_t C(ttt')$

$\Rightarrow \square C(ttt') C(t'tt') = \square C(ttt') \square C(t'tt') = \square C(ttt')$   $\rightarrow$  MOLTA EVOLZ. ALLA SEMPRE D'UNA

$$\Rightarrow \text{DIF SOLO DA } t \quad \partial_t C(ttt') C(t'tt') = \frac{H(t)}{a} \rightarrow \square C(ttt') C(t'tt') = H(t) C(ttt')$$

$$\rightarrow \text{NON COMMUTAT.} \Rightarrow \text{IN GNL NON SO MISURABILI}$$

$$H_t = H_0 + V_t \rightarrow C(t,t) = e^{-\frac{iH_0 t}{a}} C_I(t,t) \rightarrow C_I(t,t') = C_I(t,t) C_I^\dagger(t',t) = e^{-\frac{iH_0 t}{a}} C(t,t) C_I^\dagger(t',t) e^{-\frac{iH_0 t'}{a}}$$

$$\rightarrow \text{EQ EQUIL. X PIOPPI DI INSTATI} \quad \partial_t \partial_t C_I(t,t') = \partial_t \partial_t \left[ e^{-\frac{iH_0 t}{a}} C(t,t') e^{-\frac{iH_0 t'}{a}} \right] = -H_0 C_I + e^{-\frac{iH_0 t}{a}} \square C_I e^{-\frac{iH_0 t'}{a}} = e^{-\frac{iH_0 t}{a}} V_0 e^{-\frac{iH_0 t'}{a}}$$

$$\rightarrow \int \partial_t \partial_t C_I(t,t') = V_{tt}(t) C_I(t,t') \rightarrow \text{ER MOLTA INSTATI}$$

$$\rightarrow \text{PER CADUTA} \Rightarrow \text{EQ VACUUM} \quad C_I(t,t') = \text{11} + \frac{1}{(2\pi)^3} \int_{\text{d}t''} V_{tt''}(t) C_I(t'',t') = \text{11} + \sum_{\ell=1}^{\infty} \frac{1}{(2\pi)^3} \int_{\text{d}t''} \int_{\text{d}t_1} \int_{\text{d}t_2} \int_{\text{d}t_3} V_{tt''}(t) C_I(t_1,t_2) \dots C_I(t_{\ell-1},t_{\ell}) - V_{tt''}(t_1) \rightarrow \text{PER LA TUTTA} \quad \text{+ CAMBIO SIGN}$$

FUNZIONI DI GREEN A 2 PT.  $\square G_{ab} = \langle GS | T C_a(t) C_b^\dagger(t') | GS \rangle$  Dopo che le due z/2 erano evolute da H insieme  $\rightarrow H|GS\rangle = E|GS\rangle$

$$\square C(t,t') \langle GS | C_a(t) C_b^\dagger(t') | GS \rangle = \langle GS | C_a(t) C_a^\dagger(t') C_b(t') C_b^\dagger(t') | GS \rangle = e^{-\frac{iH_0 t}{a}} e^{-\frac{iH_0 t'}{a}} \langle GS | C_a(t) C_b^\dagger(t') | GS \rangle \rightarrow \text{AMMELLA TRANSIZ. TRA STATO CON} \quad \text{+ INSTATI} \quad \text{+ INSTATI} \quad \text{+ INSTATI}$$

$$\text{DEF PESONE} \quad \square G_{mm}(\underline{x}t, \underline{x}t') = \langle GS | T q_m(\underline{x}t) q_m^\dagger(\underline{x}t') | GS \rangle$$

$$\rightarrow \text{DFT ITMIDI} \quad T A_n(\underline{x}_n) - A_n(\underline{x}_n) = (\pm) \square A_{n_1}(\underline{x}_{n_1}) - A_{n_2}(\underline{x}_{n_2}) \rightarrow \varepsilon_{n_1} + \text{BOSS} - x \text{ BOSS} - x \text{ FDTMIDI}$$

$$\rightarrow \text{PROPR} \quad T A_n(\underline{x}_n) - A_n(\underline{x}_n) = (\pm) \frac{\pi}{T} \overline{A_{n_1}(\underline{x}_{n_1})} - A_{n_2}(\underline{x}_{n_2})$$

$$\rightarrow \text{PROPR} \quad \text{DATO} \quad \hat{O} = \sum C_p \langle p | \theta | p' \rangle C_{p'} \quad \& \text{H CON } |GS\rangle \Rightarrow \langle GS | \hat{O} | GS \rangle = ?$$

$$\rightarrow \langle GS | C_r C_r | GS \rangle = \langle GS | C_r^\dagger C_r | GS \rangle = \frac{1}{2\pi} \int_{-\pi}^{\pi} \langle GS | C_r^\dagger(t) C_r(t) | GS \rangle = \frac{1}{2\pi} \int_{-\pi}^{\pi} \langle GS | T C_r^\dagger(t) C_r(t) | GS \rangle = \pm \frac{1}{2\pi} \int_{-\pi}^{\pi} \langle GS | T C_r^\dagger(t) C_r(t) | GS \rangle = \pm \frac{1}{2\pi} \int_{-\pi}^{\pi} G_{rr}(t) dt$$

$$\Rightarrow \langle GS | \hat{O} | GS \rangle = \pm \frac{1}{2\pi} \int_{-\pi}^{\pi} \langle r | \theta | r' \rangle G_{rr'}(t) dt$$

ESSEMPIO DENSITA' A SPAT. P1

$$\langle GS | \hat{n}_m(\underline{x}) | GS \rangle = \langle GS | q_m^\dagger(\underline{x}) q_m(\underline{x}) | GS \rangle = \langle GS | q_m^\dagger(\underline{x}) q_m(\underline{x}) | GS \rangle$$

$$t' = t + \eta Z_2 = \lim_{\eta \rightarrow 0} (\pm) \langle GS | T q_m^\dagger(\underline{x}t) q_m^\dagger(\underline{x}t') | GS \rangle = \pm \langle G_{mm}(\underline{x}t, \underline{x}t') | GS \rangle$$



$$H = \sum_{\alpha} h_{\alpha} C_{\alpha}^+ C_{\alpha} \times N \text{ FORMULI}$$

$$\begin{aligned} \langle G_{mm'}(\underline{x}, \underline{x}') \rangle &= \langle \text{GS} | T \hat{q}_m(\underline{x}) \hat{q}_{m'}^+(\underline{x}') | \text{GS} \rangle \\ &= \sum_{\alpha, \alpha'} \frac{-i \omega_{\alpha} C_{\alpha} + i \Delta_{\alpha}}{\underline{x} - \underline{x}' + i \eta} \langle \text{GS} | C_{\alpha}^+ C_{\alpha'} | \text{GS} \rangle \end{aligned}$$

Si no se considera el efecto de la velocidad:

$$\sum_{\alpha, \alpha'} [\theta(\underline{x} - \underline{x}') \langle \text{GS} | C_{\alpha}^+ C_{\alpha'} | \text{GS} \rangle - \theta(\underline{x}' - \underline{x}) \langle \text{GS} | C_{\alpha'}^+ C_{\alpha} | \text{GS} \rangle]$$

$$\langle T A_{\alpha} B_{\alpha'} \rangle = \theta(\underline{x} - \underline{x}') \langle A_{\alpha} B_{\alpha'} \rangle + \theta(\underline{x}' - \underline{x}) \langle B_{\alpha'} A_{\alpha} \rangle$$

$$= \sum_{\alpha, \alpha'} [\theta(\underline{x} - \underline{x}') \langle \text{GS} | S_{\alpha, \alpha'} C_{\alpha}^+ C_{\alpha'} | \text{GS} \rangle - \theta(\underline{x}' - \underline{x}) \langle \text{GS} | S_{\alpha, \alpha'} C_{\alpha'}^+ C_{\alpha} | \text{GS} \rangle]$$

$$= \sum_{\alpha, \alpha'} e^{-i \omega_{\alpha} (\underline{x} - \underline{x}')} \langle \text{GS} | S_{\alpha, \alpha'} [ \theta(\underline{x} - \underline{x}') \theta(\omega_{\alpha} - \omega_{\alpha'}) - \theta(\underline{x}' - \underline{x}) \theta(\omega_{\alpha'} - \omega_{\alpha}) ] | \text{GS} \rangle$$

Si no se considera el efecto de la velocidad:

$$= \int_0^{\infty} \frac{d\omega}{2\pi} e^{-i\omega(\underline{x} - \underline{x}')} G_{mm'}(\underline{x}, \omega)$$



$$\text{No considerar } \theta(\underline{x} - \underline{x}') = \int_0^{\infty} \frac{d\omega}{2\pi} \frac{e^{-i\omega(\underline{x} - \underline{x}')}}{\omega + i\eta} \quad \text{Diagram: vector at } t \rightarrow \text{constante } 0$$

$$\Rightarrow G_{mm'}(\underline{x}, \underline{x}') = \int_0^{\infty} - \int_0^{\infty} \frac{d\omega}{2\pi} \frac{e^{-i\omega(\underline{x} - \underline{x}')}}{\omega + i\eta} \theta(\omega_a - \omega_p) - \int_0^{\infty} \frac{d\omega}{2\pi} \frac{e^{-i\omega(\underline{x} - \underline{x}')}}{\omega + i\eta} \theta(\omega_f - \omega_a)$$

$$= \int_0^{\infty} \langle \text{GS} | S_{\alpha, \alpha'} | \text{GS} \rangle \left[ \theta(\omega_a - \omega_p) \int_0^{\infty} \frac{d\omega}{2\pi} \frac{e^{-i\omega(\underline{x} - \underline{x}')}}{\omega + i\eta} - \theta(\omega_p - \omega_a) \int_0^{\infty} \frac{d\omega}{2\pi} \frac{e^{-i\omega(\underline{x} - \underline{x}')}}{\omega + i\eta} \right]$$

$$= \int_0^{\infty} \langle \text{GS} | S_{\alpha, \alpha'} | \text{GS} \rangle \left[ \theta(\omega_a - \omega_p) \int_0^{\infty} \frac{d\omega}{2\pi} \frac{e^{-i\omega(\underline{x} - \underline{x}')}}{\omega - \omega_a + i\eta} - \theta(\omega_p - \omega_a) \int_0^{\infty} \frac{d\omega}{2\pi} \frac{e^{-i\omega(\underline{x} - \underline{x}')}}{\omega - \omega_a + i\eta} \right]$$

$$\Rightarrow G_{mm'}^0(\underline{x}, \underline{x}') = \sum_{\alpha} \langle \text{GS} | S_{\alpha, \alpha'} | \text{GS} \rangle \left[ \frac{\theta(\omega_a - \omega_p)}{\omega - \omega_a + i\eta} + \frac{\theta(\omega_p - \omega_a)}{\omega - \omega_a - i\eta} \right] \quad \text{P.S.P. } \omega$$

$$h_{\alpha} = h_{\alpha} C_{\alpha}, \quad H_0 = \sum_{\alpha} h_{\alpha} \hat{n}_{\alpha}$$

$$G_{mm'}^0(\underline{x}, \omega) = \sum_{\alpha} h_{\alpha}(\underline{x}) h_{\alpha}^*(\underline{x}') \left[ \frac{\theta(\omega_a - \omega_p)}{\omega - \omega_a + i\eta} + \frac{\theta(\omega_p - \omega_a)}{\omega - \omega_a - i\eta} \right]$$

$$\text{APLICANDO } \langle \text{GS} | \hat{U}_0(\underline{x}) | \text{GS} \rangle = -i G_{mm}^0(\underline{x}, \underline{x}') = -i \int_0^{\infty} \frac{d\omega}{2\pi} G_{mm}^0(\underline{x}, \omega) e^{i\omega t}$$

$$= -i \sum_{\alpha} |h_{\alpha}(\underline{x})|^2 \int_0^{\infty} \frac{d\omega}{2\pi} e^{-i\omega t} \left[ \frac{\theta(\omega_a - \omega_p)}{\omega - \omega_a + i\eta} + \frac{\theta(\omega_p - \omega_a)}{\omega - \omega_a - i\eta} \right]$$

$$= \sum_{\alpha} |h_{\alpha}(\underline{x})|^2 (-i) \frac{2\pi i}{2\pi} \theta(\omega_p - \omega_a) e^{i\omega_a t} = \sum_{\alpha} |h_{\alpha}(\underline{x})|^2 \theta(\omega_p - \omega_a)$$

$$\uparrow \eta \rightarrow 0 \quad \text{DENSIDAD BINARIA ESTADÍSTICA}$$

$$\text{DENSIDAD GS} = \sum \text{DENSIDAD BINARIA ESTADÍSTICA} \times \epsilon_{\alpha}$$

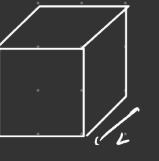
$$\text{Anomalias} \propto \text{SISTEMAS} \text{ VAL DISCRIMINANTES} \in \omega_F$$

CAS IDEAL DE FORMA  $G = \frac{P^2}{2\pi m}$   $|Q| = 1 \text{ KM} \rightarrow \text{IN BOX L} \quad R = \frac{2\pi}{L} \quad \underline{n} \in \mathbb{Z}^3$

$$G_{mm'}^0(\underline{x}, \underline{x}') = \sum_{\underline{k}, \underline{k}'} \langle \underline{x} | \underline{k} \rangle \langle \underline{k}' | \underline{x}' \rangle G^0(\underline{k}, \underline{k}') = \delta_{mm'} \int \frac{d\underline{k} R}{(2\pi)^3} e^{-i\underline{k}(\underline{x}-\underline{x}')} G^0(\underline{k}, \underline{k})$$

$$G^0(R, \omega) = \frac{\theta(E_F - E_F)}{\omega - \frac{E_F + i\eta}{a}} + \frac{\theta(E_F - E_K)}{\omega - \frac{E_K + i\eta}{a}} = \frac{i\Omega_F}{\omega - \frac{E_F + i\eta}{a}} \text{sgn}(\omega_F - \omega)$$

PASSETE A SP R X R D HO IN VAN X TABLA 2



TIPOS FORMAS BASES

CAMPO ESCALONADO

↑ R KS ↑

$$\text{PER QTB } P = \sum_m k \underline{k} C_{km}^+ C_{km} \rightarrow \underline{Q} P = \sum_m k \underline{k} Q C_{km}^+ C_{km} \Rightarrow e^{-iQ P / a} e^{-iQ F / a} = e^{-iQ K} e^{-iQ F} = e^{\underline{Q} P(x)} e = \sum_m \langle \underline{x} | \underline{k} \rangle C_{km}^+ e = Q_m^0(\underline{x})$$

$$\Rightarrow \text{ES } [H, f] = 0 \Rightarrow G_{mm'}(\underline{x}, \underline{x}') \text{ SIMILAR } \underline{x} - \underline{x}' \Rightarrow G_{mm'}(\underline{x}, \underline{x}') = \int \frac{d\underline{k} R}{(2\pi)^3} \frac{d\omega}{2\pi} G_{mm}(\underline{k}, \omega) e^{i\underline{k}(\underline{x}-\underline{x}') - i\omega(\underline{x}-\underline{x}')}}$$

EQ DEL MOT. IN FG  $H = \sum_{ab} h_{ab} C_a^+ C_b + \frac{1}{2} \sum_{abcd} \sum_{abcd} C_a^+ C_b^+ C_c C_d \text{ CON } C_a b \otimes C_d c = \langle b | a | d | c \rangle$

$$[C_r, C_a^+ C_b] = \delta_{ra} C_b \quad \oplus \quad [C_r, C_a^+ C_b C_d C_c] = (\delta_{ra} C_b \pm \delta_{rb} C_a) C_d C_c \Rightarrow [C_r, H] = \sum_{ab} [C_r, C_a^+ C_b] + \frac{1}{2} \sum_{abcd} [C_r, C_a^+ C_b^+ C_c C_d] = \sum_b h_{rb} C_b + \frac{1}{2} \left( \sum_{bcd} \delta_{rbcd} C_b C_c \pm \sum_{bcd} \delta_{rbc} C_b C_d \right)$$

ESTIMACION  $\bullet H = H_1 + H_2 \Rightarrow \sum C_r^+ [C_r, H] = H_1 + 2H_2$

$\bullet i\hbar \partial_t G(t) = i\hbar \partial_t e^{\frac{iHt}{\hbar}} C_r e^{-\frac{iHt}{\hbar}} = [C_r(t), H] = \sum_b h_{rb} C_b(t) + \sum_{bcd} \delta_{rbcd} (C_b^+ C_d C_c)(t)$

TRONAMOS  $E_{GS} = \langle GS | H | GS \rangle$  DA P.M.P  $\langle GS | \hat{H} | GS \rangle \rightarrow E_{GS} = \langle GS | H_1 | GS \rangle + \langle GS | H_2 | GS \rangle$

$$\sum_r \langle GS | C_r^+ (t) i\hbar \partial_t C_r(t) | GS \rangle = \langle GS | H_1 | GS \rangle + 2 \langle GS | H_2 | GS \rangle = h_{rr} \langle GS | \sum_r C_r^+(t) i\hbar \partial_t C_r(t) | GS \rangle = \sum_r h_{rr} \langle GS | C_r^+(t) C_r(t) | GS \rangle = \sum_r h_{rr} \langle GS | C_r^+(t) C_r(t) | GS \rangle = \sum_r h_{rr} \langle GS | C_r^+(t) C_r(t) | GS \rangle = \sum_r h_{rr} \langle GS | C_r^+(t) C_r(t) | GS \rangle = \sum_r h_{rr} \langle GS | C_r^+(t) C_r(t) | GS \rangle = \sum_r h_{rr} \langle GS | C_r^+(t) C_r(t) | GS \rangle$$

EQUATION  $i C_{ab}^0(t, t') = \langle GS | C_a(t) C_b^+(t') | GS \rangle = \theta(t - t') \langle GS | C_a(t) C_b^+(t') | GS \rangle \pm \theta(t' - t) \langle GS | C_b^+(t') C_a(t) | GS \rangle$

$$\rightarrow \text{DESEM} i\hbar \partial_t C_{ab}(t, t') = \delta(t - t') \langle C_a(t) C_b^+(t') | GS \rangle + C_b^+(t') C_a(t) | GS \rangle + \theta(t' - t) \langle C_a(t) C_b^+(t') | GS \rangle + \theta(t - t') \langle C_b^+(t') C_a(t) | GS \rangle$$

$$\Rightarrow -i\hbar \partial_t C_{ab}(t, t') = i\hbar \delta_{ab} \delta(t - t') + \sum_c h_{ac} \langle C_a(t) C_c^+(t') | GS \rangle + \sum_{bcd} \delta_{bcd} \langle C_b^+(t') C_c(t) | GS \rangle \langle C_d(t) C_b^+(t') | GS \rangle$$

$$\Rightarrow [-i\hbar \partial_t C_{ab}(t, t') - i\sum_c h_{ac} C_{cb}(t, t')] - \sum_{bcd} \delta_{bcd} \langle C_b^+(t') C_c(t) | GS \rangle = i\hbar \delta_{ab} \delta(t - t') \quad (*)$$

EN PRESENZA DE O.P.R. 2 CORP.  $\Rightarrow$  EQ MOT. FG A ORDEN EXP.  $\rightarrow$  FORMA NON CHIUSA = FORMA MARCA MARTIN & SCHLESINGER  $\Rightarrow$  TRONCO (4PI) =  $\langle SA | H | 2PI \rangle$

$$\delta_{abcd}^0(t, t, t_3, t_4) = \langle GS | T C_a(t) C_b(t_3) C_d^+(t_4) | GS \rangle = \pm \langle GS | T C_b(t_3) C_a(t_4) C_d^+(t_4) | GS \rangle = \pm i^2 G_{abcd}^0(t, t, t_3, t_4)$$

$$\rightarrow \otimes \times \delta_{ab}$$

$$T(C_b^+ C_d C_c)(t) C_b^+(t') = T C_b^+(t') C_d(t') C_c(t') \Rightarrow \sum_c (i\hbar \delta_{ac} - h_{ac}) C_{cb}(t, t') + i \sum_{bcd} \delta_{bcd} i \hbar \delta_{tt'} C_{db}(t, t')$$

$$\oplus 2 S.A.T.$$

$$\rightarrow \text{CASO NON INDUEBLE} \Rightarrow \sum_c (i\hbar \delta_{ac} - h_{ac}) C_{cb}^0(t, t') = i\hbar \delta_{ab} \delta(t - t') \rightarrow \text{SPW} \sum_c (i\hbar \omega - h_{ac}) C_{cb}^0(\omega) = i\hbar \delta_{ab} \rightarrow (i\hbar \omega \mathbf{1} - \hat{h}) C_{ab}^0(\omega) \mathbf{1}$$

$$\Rightarrow G^0(\omega) = \left( \omega - \frac{\hat{h}}{a} \right)^{-1} \text{ RESOLVENTE} \Rightarrow \frac{1}{f(\omega)} \delta_{ab} \delta(t - t') \Rightarrow G^0(\omega) = \sum_j \frac{1}{\omega - \epsilon_j / a} \rightarrow \text{SINCERITÀ} \text{ ED } \text{RE} \Rightarrow \text{FORM IN C}$$

$$\hat{h} \neq \text{MOM} \Rightarrow \text{DEF } \neq \text{PC} \rightarrow \text{IN BASE } \frac{1}{(1 + \omega)^2} \text{ OP } \hat{h} \text{ & } \omega \hat{h} = -\frac{\hbar^2}{2m} \nabla^2 + \epsilon(\omega) \Rightarrow \left[ \hat{h}\omega + \frac{\hbar^2}{2m} \nabla^2 - \epsilon(\omega) \right] \left[ G_{mm}^0(\underline{x}, \omega) \right] = \hat{h} \delta(\underline{x} - \underline{x}') \delta_{mm}$$

$$\rightarrow \left[ \hat{h}\omega + \frac{\hbar^2}{2m} \nabla^2 - \epsilon(\omega) \right] f(\omega) = g(\omega) \text{ CON } g \text{ SON ASSIGNATE } \epsilon \text{ DI UN NON OMOS.} \Rightarrow f(\omega) = f_0(\omega) + \frac{1}{a} \int_{-\infty}^{\omega} g(\omega') C^0(\omega' - \omega) d\omega'$$

$$\rightarrow \text{OP DI UNA FORMA } C^0 \rightarrow \text{ES NON SOLO } \epsilon \rightarrow \text{ACQUIRIR A G SPW}$$

ISOL CECI MANDA SLOW consider as  $H = H_0 + gV \rightarrow V \neq 0 \text{ const} \Rightarrow$  quasi static case no SLOW THERMOPHYSICS

$$H = H_0 + gV \rightarrow V \neq 0 \text{ const} \Rightarrow \text{quasi static case no SLOW THERMOPHYSICS} \Rightarrow \text{INTERFACIAL}$$

$$\text{def } H_t = H_0 + g e^{-\frac{E(t)}{kT}} V = \begin{cases} H & |t| \rightarrow \infty \\ H_0 & t = 0 \end{cases} \quad \forall E \geq 0 \quad [H_t, H_0] \neq 0$$

$$\Rightarrow C_I(t, t') \text{ IN DISEGNI INFOMAS} \quad C_I(t, 0) = e^{\frac{-\theta}{kT}} C_I(t')$$

$$\rightarrow \text{SOM SS } \Delta \text{ DI } H_0 \Rightarrow \int_{-\infty}^0 \left[ q_{\pm} \right] = \int_{-\infty}^0 \frac{\left( C_I(\theta \pm \Delta) / \Delta_0 \right)}{\left( \Delta_0 / C_I(\theta \pm \Delta) / \Delta_0 \right)} = \left[ q_{\pm} \right] \text{ DI } H_0$$

$\Delta_0 / \Delta_0 \text{ NON DIF} \Rightarrow \text{COINCIDONO A MENO DI UNA PESO}$

NB NON CANTUSSO CS  $\rightarrow$  CS (possible COND CROSING) MA NON ANIONE SS CONSIDERO COSSUM

$$\text{Dim } H_t = H_0 + g e^{\frac{-\theta}{kT}} V \Rightarrow C_I(t, \theta) \text{ SE } t < 0 \rightarrow g = e^{\frac{-\theta}{kT}} \rightarrow H_t = H_0 + g e^{\frac{-\theta}{kT}} V \Rightarrow C_I(t, \theta) = C_I(t + \theta, 0)$$

$$\Rightarrow \frac{\partial}{\partial g} - \frac{\partial}{\partial \theta} \rightarrow \frac{\partial}{\partial g} C_I(t, \theta) = \frac{\partial \theta}{\partial g} \frac{\partial C_I}{\partial \theta}(t + \theta, \theta) = \frac{\partial \theta}{\partial g} \left[ \frac{\partial C_I}{\partial \theta}(t + \theta, \theta) + \frac{\partial C_I}{\partial t}(t + \theta, \theta) \right] = \frac{\partial \theta}{\partial g} \left[ \frac{\partial C_I}{\partial t}(t, \theta) + \frac{\partial C_I}{\partial \theta}(0, \theta) \right]$$

$$g = e^{\frac{-\theta}{kT}} \rightarrow I = \frac{\partial \theta}{\partial g} g \varepsilon \Rightarrow \varepsilon g \frac{\partial}{\partial g} C_I(t, \theta) = \frac{\partial \theta}{\partial g} C_I(t, \theta) H_0 \rightarrow t = 0 \Rightarrow H_{t=0} = H$$

$$\Rightarrow \text{if } g \frac{\partial}{\partial g} C_I(0, \theta) = H(0, \theta) - C(0, \theta) \quad [H_0 + g e^{\frac{-\theta}{kT}} V] \leftarrow C(t, 0) = e^{\frac{-\theta}{kT}} C_I(t, 0) = C^+(0, \theta)$$

$$\text{if } g \frac{\partial}{\partial g} C_I(0, \theta) = H(0, \theta) - C_I(0, \theta) H_0 \quad g C_I(0, \theta) V_{H_0}(s) e^{\frac{-\theta}{kT}}$$

$$\text{if } g \frac{\partial}{\partial g} C_I(0, \theta) / \Delta_0 = (H - \varepsilon_0) C_I(0, \theta) / \Delta_0 \quad g e^{\frac{-\theta}{kT}} C_I(0, \theta) V_{H_0}(s) / \Delta_0$$

$$\varepsilon \in \Delta \Rightarrow s \rightarrow -\Delta \Rightarrow \text{if } g \frac{\partial}{\partial g} C_I(\theta - \Delta) / \Delta_0 = (H - \varepsilon_0) C_I(\theta - \Delta) / \Delta_0 \quad \text{SS SUMMA CHE } \varepsilon \rightarrow 0 \Rightarrow \text{S' ACTUALE AP}$$

$$\rightarrow \varepsilon \frac{\partial}{\partial g} g \frac{\partial}{\partial g} C_I(\theta - \Delta) / \Delta_0 = \langle \Delta_0 / (H - \varepsilon_0) C_I(\theta - \Delta) / \Delta_0 \rangle$$

$$\Rightarrow \varepsilon \frac{\partial}{\partial g} \frac{C_I(\theta - \Delta)}{\langle \Delta_0 / C_I(\theta - \Delta) / \Delta_0 \rangle / \Delta_0} = \frac{(H - \varepsilon_0) C_I(\theta - \Delta) / \Delta_0}{\langle \Delta_0 / C_I(\theta - \Delta) / \Delta_0 \rangle / \Delta_0} - \frac{C_I(\theta - \Delta) / \Delta_0}{\langle \Delta_0 / C_I(\theta - \Delta) / \Delta_0 \rangle / \Delta_0} \frac{\langle \Delta_0 / (H - \varepsilon_0) C_I(\theta - \Delta) / \Delta_0 \rangle / \Delta_0}{\langle \Delta_0 / C_I(\theta - \Delta) / \Delta_0 \rangle / \Delta_0}$$

$$\downarrow \varepsilon \rightarrow Q$$

$$Q = \frac{(H - \varepsilon_0) C_I(\theta - \Delta) / \Delta_0}{\langle \Delta_0 / C_I(\theta - \Delta) / \Delta_0 \rangle / \Delta_0} - \frac{C_I(\theta - \Delta) / \Delta_0}{\langle \Delta_0 / C_I(\theta - \Delta) / \Delta_0 \rangle / \Delta_0} \frac{\langle \Delta_0 / (H - \varepsilon_0) C_I(\theta - \Delta) / \Delta_0 \rangle / \Delta_0}{\langle \Delta_0 / C_I(\theta - \Delta) / \Delta_0 \rangle / \Delta_0}$$

$$\Rightarrow Q = (H - \varepsilon_0) / q_{\pm} - q_{\pm} \times \varepsilon_0 / (H - \varepsilon_0) / q_{\pm}$$

X MISURARES  $C_I$  USO TEXP D'YSON

$q_{\pm} \rightarrow$  SLOW NORMALEZ, 100M X 100

FORMULA DI INTERFAZIE  $H = H_0 + V \quad H(q_{\pm}) = \varepsilon_0 / q_{\pm} \quad H / \Delta_0 = \varepsilon_0 / \Delta_0$

$$\Rightarrow H \hat{=} \text{VACO} \quad \langle \varepsilon_0 | \hat{T} \hat{S}_{II}(\varepsilon_0) - \hat{S}_{II}(H_0) | \varepsilon_0 \rangle = \frac{\langle \Delta_0 | \hat{T} \hat{S}_{II}(\varepsilon_0) - \hat{S}_{II}(H_0) | \varepsilon_0 \rangle}{\langle \Delta_0 | \varepsilon_0 | \Delta_0 \rangle}$$

$$\text{dim} \quad t_1 > t_2 \rightarrow t_N \Rightarrow \langle \varepsilon_0 | \hat{S}_{II}(\varepsilon_0) - \hat{S}_{II}(H_0) | \varepsilon_0 \rangle = \underbrace{\langle q_{+}^{+} | \hat{C}_I^{+}(\varepsilon_0) \hat{S}_{II}(H_0) | t_1 \rangle}_{\langle q_{+}^{+} | q_{+}^{+} \rangle} \underbrace{\langle t_1 | \varepsilon_0 | t_2 \rangle}_{\langle t_1 | t_2 \rangle} \underbrace{\langle t_2 | \hat{S}_{II}(H_0) | \varepsilon_0 \rangle}_{\langle t_2 | t_2 \rangle}$$

$$= \frac{\langle \Delta_0 | C_I^{+}(\varepsilon_0 + \Delta_0) | \Delta_0 \rangle}{\langle \Delta_0 | C_I^{+}(\varepsilon_0 + \Delta_0) | \Delta_0 \rangle} * \underbrace{C_I(\varepsilon_0) C_I(\varepsilon_0) C_I(\varepsilon_0) C_I(\varepsilon_0)}_{C_I(\varepsilon_0)} - \frac{C_I(\varepsilon_0 - \Delta_0) | \Delta_0 \rangle}{\langle \Delta_0 | C_I(\varepsilon_0 - \Delta_0) | \Delta_0 \rangle}$$

$$\frac{\langle \Delta_0 | C_I^{+}(\varepsilon_0 + \Delta_0) | \Delta_0 \rangle}{\langle \Delta_0 | C_I^{+}(\varepsilon_0 + \Delta_0) | \Delta_0 \rangle} \quad \text{SS VIA ECONOMIA}$$

$$\text{TOTAL DI PARTE CC} \quad \text{EXACTA NO SGN} \quad \uparrow \quad \text{t, } \quad \text{VIA ECONOMIA}$$

$$= \frac{\langle \Delta_0 | C_I^{+}(\varepsilon_0) C_I(\varepsilon_0) C_I(\varepsilon_0) | \Delta_0 \rangle}{\langle \Delta_0 | C_I^{+}(\varepsilon_0) C_I(\varepsilon_0) | \Delta_0 \rangle} \rightarrow T = \Pi \oplus \sum_I C_I(\varepsilon_0) T \exp \int \frac{V_{H_0}(t) dt}{t}$$

$$= \frac{\langle \Delta_0 | \hat{T} \hat{S}_{II}(\varepsilon_0) - \hat{S}_{II}(H_0) | \varepsilon_0 \rangle}{\langle \Delta_0 | \varepsilon_0 | \Delta_0 \rangle}$$

X COMPLETANES

$$C_{min}^0(x, x') = \langle C_S | \hat{T} \hat{P}_m(x) \hat{P}_m^+(x') | \rangle = \frac{\langle \Delta_0 | \hat{T} \hat{S}_{II}(\varepsilon_0) \hat{P}_m^+(x') | \rangle}{\langle \Delta_0 | \varepsilon_0 | \Delta_0 \rangle}$$

SO STAZIONARIO A S NA

VACONATO DI V  $\Rightarrow$  ON BOTH DUE COMPL  $\Rightarrow$  POSS DI S'PLICHE

PROPIETÀS UBBDO

$$\left[ \frac{\partial \omega + \frac{\hbar^2}{2m} \nabla^2}{\varepsilon_0} \right] G(x, x') = \delta_3(x - x') \quad \text{SS MEAN X S'PLICHE} \quad \Rightarrow G_{min} = G \delta_{min}$$

$$\left[ \frac{\hbar^2}{2m} \nabla^2 \right] G(x, x') = \delta_3(x - x') + G(x) G(x') \quad \text{SS S'PLICHE} \quad \Rightarrow G = \text{PARIT C'ABINA}$$

$$\Rightarrow G(x, x') = G^0(x, x') + \frac{1}{\pi} \int_{-\infty}^{\infty} d\omega G^0(x, \omega) G^0(\omega, x') \rightarrow \text{PARIBUS}$$

$$\begin{array}{c} \omega = \omega + z \\ \hline x & x' & \omega \\ \uparrow & \uparrow & \uparrow \\ \omega & \omega + z & \omega \end{array} \quad \text{INSTANT} \quad \begin{array}{c} \omega = \omega + z \\ \hline x & x' & \omega \\ \uparrow & \uparrow & \uparrow \\ \omega & \omega + z & \omega \end{array} \quad \text{BORN S'PLICHE} \quad \begin{array}{c} \omega = \omega + z \\ \hline x & x' & \omega \\ \uparrow & \uparrow & \uparrow \\ \omega & \omega + z & \omega \end{array} \quad \text{SS KIN SO MS} \Rightarrow \text{S'PLICHE}$$

SS PARIBUS AC'AB  
 $\omega + \frac{\hbar^2}{2m} \nabla^2$   
TUNO A TUNO

S'PLICHE  
A COSANO  
INTUAZ C

TEOREMA DA UNIÃO ESTÁTICA, IGS, BASEIA-SE ASSOCIAR CANÔNICAS  $\alpha_n^\pm$  NON AUTÔMAG

$$[\alpha_n^\pm, \alpha_j^\pm] = \emptyset \quad [\alpha_n^-, \alpha_j^+] = S_{kj} \quad \text{TC} \quad \alpha_n^- |_{GS} = \emptyset \quad \Rightarrow \text{SOMA CACONTO}$$

$$\text{SO IF } \alpha_n^- |_{F'} = \emptyset \rightarrow \begin{cases} \text{CROSS } Q_{km}^+ |_{F'} = \emptyset & \text{IRICR} \\ \text{DISTINCT } Q_{km}^+ |_{F'} & \text{IRICR} \end{cases}$$

$$\langle F | \alpha_n^+ = \emptyset \rightarrow \begin{cases} F | Q_{km} = \emptyset & \text{IRICR} \\ \langle F | Q_{km}^+ = \emptyset & \text{IRICR} \end{cases}$$

$$Q_m^-(x) = \sum_{\underline{x}} Q_{\underline{x}m} (\underline{x}| \underline{x}) = \sum_{\substack{\underline{x} \in R_F \\ \underline{x} \in R_F}} (\underline{x}| \underline{x}) Q_{\underline{x}m} + \sum_{\substack{\underline{x} \in R_F \\ \underline{x} \in R_F}} (\underline{x}| \underline{x}) Q_{\underline{x}m}^{(+)} = Q_m^{(+)}(\underline{x}) + Q_m^{(-)}(\underline{x})$$

$$\langle F | Q_m^{(+)}(\underline{x}) = \emptyset \quad Q_m^{(-)} |_{F'} = \emptyset \quad \rightarrow \text{VALO TFO A}$$

$$A - A_i^{(+)} + A_i^{(-)} \rightarrow [A_i^{(+)}, A_j^{(+)}] = [A_i^{(-)}, A_j^{(-)}] = \emptyset \quad [A_i^{(-)}, A_j^{(+)}] = C1 \neq \emptyset$$

DEF [Op. ordinam nonam]

$$N[A_i - A_N] = (+) \overbrace{A_i^{(+)}}^{\text{CROSS}} - \overbrace{A_N^{(-)}}^{\text{NON ORDIN}} \quad (+ \text{sx}, - \text{dx})$$

→ NON ORDIN VODO

$$A_i A_L = (A_i^+ + A_i^-)(A_L^+ + A_L^-) = N[A_i A_L] + [A_i^-, A_L^+] \quad \text{CROSS}$$

$$\text{DEF [comunig]} \quad A_i A_L = N[A_i A_L] + \overbrace{A_i A_L}^{\text{CROSS}} \rightarrow \overbrace{A_i A_L}^{\text{CROSS}} = [A_i^-, A_L^+]$$

$$\Rightarrow \langle S(A_i A_L) |_{GS} \rangle = \overbrace{A_i A_L}^{\text{CROSS}} \rightarrow \langle N \rangle = \emptyset$$

→ SO  $A_i - A_N \Rightarrow$  TORNOSCAK

$$\text{DEF [ANALOG TORN]} \quad N[A_i - A_N] = (\pm) \overbrace{N[A_i - A_N]}^{\text{CROSS}}$$

$$\text{DEF [comunig]} \quad \overbrace{A_i (A_i - A_N) A_L}^{\text{CROSS}} = (A_i - A_N) \overbrace{A_i A_L}^{\text{CROSS}}$$

$$\text{DEF } \times \text{DEF } \quad \textcircled{1} \quad A_i^- A_i^+ - A_N^+ = (IA_i^-, A_i^+ |_{\pm}) \quad A_2^+ - A_1^+ + A_1^- A_2^- A_2^+ - A_1^+ = \overbrace{A_0 A_1 A_2^+}^{\text{CROSS}} - A_1^+ \pm A_1^+ [A_0, A_2^+] \pm A_2^+ - A_1^+ \\ = \overbrace{A_0 A_1 A_2^+}^{\text{CROSS}} - A_1^+ + \overbrace{A_0 A_1 A_2^+}^{\text{CROSS}} - A_1^+ + \overbrace{A_0 A_1^+ A_2^- A_2^+}^{\text{CROSS}} - A_1^+ + (\pm) A_i^+ - A_N^+ A_0^+$$

$$\textcircled{2} \times \text{NOV} \quad A_0 N[A_i - A_N] = N[A_0 A_i - A_N] + \sum_{k=1}^n N[\overbrace{A_0 A_k - A_N}^{\text{CROSS}}]$$

$$\textcircled{3} \text{BANZAS} \quad A_0 N[A_i - A_N] = N[A_0 - A_N] + \sum_k N[\overbrace{A_0 A_k - A_N}^{\text{CROSS}}]$$

$$\text{TOOL} \quad A_i - A_N = N[A_i - A_N] + \sum_{\substack{\text{CROSS} \\ \text{CROSS}}} N[A_i - A_N] + \sum_{\substack{\text{CROSS} \\ \text{CROSS}}} N[A_i^+ - A_N^+] + \sum_{\substack{\text{CROSS} \\ \text{CROSS}}} N[A_i^- - A_N^-]$$

$$\uparrow \quad \uparrow \quad \uparrow \\ N_{n_0} \quad N_{n_1} \quad N_{n_2} \\ n_{\text{PAUL}} \Rightarrow \text{CDSM} \\ n_{\text{BSP}} \Rightarrow \text{ASPM}$$

$$\Rightarrow \langle GS | A_i - A_N |_{GS} \rangle = \begin{cases} \emptyset & n_{\text{BSP}} \\ \sum_{\substack{\text{CROSS} \\ \text{CROSS}}} N[A_i^+ - A_N^+] & n_{\text{PAUL}} \end{cases}$$

dim (x NOV)

$$A_i A_2 = N[A_i A_2] + \overbrace{A_i A_2}^{\text{CROSS}} \rightarrow \text{IF } A_i - A_N = \sum_{k=0}^{L/2} N_{n_k}$$

$$A_0 A_i - A_N = A_0 (N_{n_0} + N_{n_1} + \dots) \leftarrow A_0 N[A_i - A_N] = N[A_0 - A_N] + \sum_{k=0}^{L/2} N[A_0 - A_k - A_N] \\ = N_{n_{00}} + N[A_0 N_{n_0}] + N[A_0 N_{n_1}] + N[A_0 N_{n_2}] + \dots = N_{n_{00}} + N_{n_{01}} + \dots$$

$$\square \quad \square \quad \square$$

EXEMPLO

$$\langle F | \widehat{A}_1(x) \widehat{A}_1(x') | F \rangle = \langle F | \overbrace{Q_1^+(x) Q_1^-(x)}^{\text{CROSS}} \overbrace{Q_1^+(x') Q_1^-(x')}^{\text{CROSS}} | F \rangle = \\ = \langle F | Q_1^+(x) Q_1^-(x) | F \times F | Q_1^+(x') Q_1^-(x') | F \rangle + \langle F | Q_1^+(x) Q_1^-(x') | F \times F | Q_1^+(x') Q_1^-(x') | F \rangle \\ \Rightarrow \langle F | \widehat{A}_1(x) \widehat{A}_1(x') | F \rangle - \langle F | \widehat{A}_1(x) | F \times F | \widehat{A}_1(x') | F \rangle = \langle F | Q_1^+(x) Q_1^-(x') | F \times F | Q_1^+(x) Q_1^-(x') | F \rangle \\ \text{NÃO BANZAS } \underset{x \rightarrow x'}{\cancel{\text{CROSS}}} \Rightarrow \text{SSOCIAÇÕES FORTI}$$

TEOREMA DA CIRCUITO  $\text{obs } \langle G_{\text{GS}}, A_n | \text{GS} \rangle = \begin{cases} 0 & \text{se } n \text{ é dísp. falso} \\ \sum_{k \text{ constante}} \text{tot se } n \text{ é Falso} \rightarrow \text{constante} = \text{falso} + 2^k \end{cases}$   $\Rightarrow \text{PONTE} \text{ N. PARÍC} = \prod \text{PONTE} + 2^k \rightarrow \text{CÁLCULO DE PONTE}$

INTRODUÇÃO A 2 CONDIÇÕES

$V = \frac{E}{2V} \sum_{q \neq q_m} \sum_{q \neq q_m} Q^+_{q_m} Q^+_{R_m} Q^+_{R+q_m} Q^-_{q_m} \Rightarrow \langle PIV | V \rangle = \langle F | Q^+_{F_m} Q^-_{F-q_m} | F \rangle \langle F | Q^+_{R_m} Q^-_{R+q_m} | F \rangle - \langle F | Q^+_{q_m} Q^-_{R+q_m} | F \rangle \langle F | Q^+_{R_m} Q^-_{F-q_m} | F \rangle$

$\Leftrightarrow 0 \Leftrightarrow q = Q$

$\times \text{EVOLUÇÃO E BASTA ANDAR} \rightarrow \text{EVOLUÇÃO DIFERENTES MELHORES} \text{ (L. CLASSE) } \alpha_k^I$

$H = \sum k \omega_c C_c^+ C_c \rightarrow C_c(t) = e^{-i\omega_c t} C_c \quad C_c^+(t) = e^{i\omega_c t} C_c^+ \Rightarrow \text{ADICIONA E SUBTRAÍ}$

TEOREMA  $| \text{GS} \rangle, \alpha_k^\pm, H \rightarrow \times \text{TEOREMA DA N. PARÍC} \text{ COM } \alpha_k^\pm(t) = \int_k(t) \alpha_k^\pm \Rightarrow \langle \alpha_k^\pm(t) | \text{GS} \rangle = 0 \quad \forall t \Rightarrow [\alpha_j^-(t), \alpha_k^+(t)]_\pm = [\alpha_j^-(t), \alpha_k^+(t)]_\pm = 0 \quad [\alpha_j^-(t), \alpha_k^+(t)]_\pm = \delta_{kj} g(t, t')$

$\Rightarrow T[A_1(t_1) \dots A_n(t_n)] = N[A_1(t_1) \dots A_n(t_n)] + \sum_m N[A_1 \dots \overset{m}{A_m} \dots A_n] + N[A_1 \dots \underset{m}{A_m} \dots A_n] + \dots$

STEP 1  $T[A_1(t_1) A_2(t_2)] = \theta(t_1 - t_2) A_1(t_1) A_2(t_2) \pm \theta(t_2 - t_1) A_2(t_2) A_1(t_1) = \theta(t_1 - t_2) \left( N[A_1(t_1) A_2(t_2)] + \overline{A_1(t_1) A_2(t_2)} \right) \pm \theta(t_2 - t_1) \left( N[\overline{A_2(t_2)} A_1(t_1)] + \overline{A_2(t_2)} \overline{A_1(t_1)} \right)$

$= [\theta(t_1 - t_2) + \theta(t_2 - t_1)] N[A_1(t_1) A_2(t_2)] + \theta(t_1 - t_2) \overline{A_1(t_1) A_2(t_2)} + \theta(t_2 - t_1) \overline{A_2(t_2) A_1(t_1)} = N[A_1(t_1) A_2(t_2)] + \overline{A_1(t_1) A_2(t_2)} \xrightarrow{\text{comb. adic. e subtração}}$

$\Rightarrow \langle \text{GS} | T[A_1(t_1) A_2(t_2)] | \text{GS} \rangle = A_1(t_1) \overline{A_2(t_2)} \rightarrow \text{obs} (\text{mod. valor absoluto} \times \text{signo}) \quad A_1(t_1) \overline{A_2(t_2)} = \pm A_2(t_2) \overline{A_1(t_1)}$

$\Rightarrow \langle \text{GS} | T[G_{m_1}(1) G_{m_2}^+(2)] | \text{GS} \rangle = {}^0 G_{m_1 m_2}^0(12) \rightarrow G_{m_1 m_2}^0 = 0 \text{ se } \text{GS} \text{ é Falso} \text{ ou } \hat{N} \neq 0 \text{ se } \text{GS} \text{ é verdadeiro e não se aplica}$

$\Rightarrow \langle \text{GS} | T[G_{m_1}(1) G_{m_2}^+(2)] | \text{GS} \rangle = {}^0 G_{m_1 m_2}^0(12) \xrightarrow{\text{compara com } 0} \text{ADICIONA}$

STEP 2  $\times \text{H. P. INVERSA} \text{ SE } N[T[A_1(t_1) \dots A_n(t_n)]] = \sum_{k=0}^n N_{nk} \rightarrow N_{nk} = \sum_{\substack{k \text{ constante} \\ \text{TOTAL}}} N \left[ \frac{m}{\cancel{1}} \right] \rightarrow \times \text{ADICIONA} \quad T[A_0(t_0) A_1(t_1) \dots A_n(t_n)] = (\pm) {}^0 A_0 T[A_1 \dots \cancel{A_0} \dots A_n]$

$= (\pm) {}^0 A_0 \left( N[A_0 \dots \cancel{A_0} \dots A_n] + \sum_m N[\cancel{A_0} \dots A_1 \dots \cancel{A_0} \dots A_n] + \dots \right)$

ONDE OSOS CONSTANTE INDISP DA T  $A_0 N[A_0 \dots A_n] = N[A_0 \dots A_n] + \sum_k N[A_0 \dots \cancel{A_k} \dots A_n] \Rightarrow (\pm) {}^0 N[A_0 \dots \cancel{A_k} \dots A_n] + (\pm) {}^0 \sum_k N[\cancel{A_k} A_0 \dots \cancel{A_k} \dots A_n] + (\pm) {}^0 \sum_m N[\cancel{A_k} A_0 \dots \cancel{A_k} \dots \cancel{A_m} \dots A_n] + (\pm) {}^0 \sum_k N[\cancel{A_k} A_0 \dots \cancel{A_k} \dots \cancel{A_m} \dots A_n]$

NECESSARIO E A POSITIVO E TOTAL  $\rightarrow N[A_0 \dots A_n]$

II  $\rightarrow \cancel{A_0} A_n = \langle T[A_0] A_n \rangle \text{ MAIS H. P. T. MAX} \Rightarrow T = 1 \rightarrow \text{S. P. S.} \Rightarrow \pm \text{ P. V. V.} \Rightarrow \text{NO S. P. S.} \Rightarrow N[A_0 \dots \cancel{A_n}] \times \text{RES. T. MAX}, \text{ MELHOR } A_0(A_0 \dots A_n) = (\pm)^n A A' (A_0 \dots A_n)$

$\Rightarrow N[A_0 \dots \cancel{A_n}] + N[A_0 \dots A_n] + \blacksquare$

APPLICATIONS  ${}^0 G(1234) = \langle \text{GS} | T[G(1) G(2) G^+(3) G^+(4)] | \text{GS} \rangle = {}^0 G^0(13) {}^0 G^0(24) \pm {}^0 G^0(14) {}^0 G^0(23) \rightarrow \text{INT. DA PARÍC. NÃO INVERSA} \text{ SE PONTE S. P. S.} \Rightarrow \text{P. G. COM PONTE ESSAS}$

+ INGEN.  $G(1234) = G(13) G(24) \pm G(14) G(23) + G(1234)$

$\xrightarrow{\text{P. G. COM PONTE ESSAS}}$





~~EQ D'EGISON X HF~~  $G^0$  MISURA D'EGISON X SCAMBIO PARTICOLO DI  $\Sigma^*$

$$\times G^0 \text{ PARTICOLO} \quad [i\partial_x - h(x)] G^0 = S_{mn} + S_3(x-x') \delta(t-t')$$

$$\times HF \quad G_{mm'}^{HF}(xx') = G_{mm'}^0(xx') + \frac{i}{\alpha} \sum_{m''m'''} \int dx_2 G_{mm''}^0(x_2) \left[ \int dy_2 U^0(2g) G_{m'm''}^{HF}(gyx) \right] \\ - \frac{i}{\alpha} \sum_{m''m'''} \int dx_2 G_{mm''}^0(x_2) G_{m'm''}^{HF}(x_2x') \int dy_2 U^0(2g) G_{m'm''}^{HF}(gy)$$

### INTERAZIONE DI PROPAGAZIONE

IN EGGS MB C'è TUTTA E PARTE "VISTITA"

DA INSIEME DI PROPAGAZIONI

$$= \begin{array}{c} \uparrow \\ \downarrow \\ \text{---} \end{array} + \begin{array}{c} \uparrow \\ \downarrow \\ \text{---} \end{array} + \begin{array}{c} \uparrow \\ \downarrow \\ \text{---} \end{array}$$

$$\rightarrow I \text{ OLTRE} \quad \begin{array}{c} \uparrow \\ \downarrow \\ \text{---} \end{array} = \frac{i}{\alpha} \int dx_1 dx_2 G^0(x_1x_2) G^0(x_1x_2) G^0(x_1y) G^0(x_2y)$$

SE ESCO DA UN CONCETTO PIÙ DI 3 PROBLEMI  $G^0$  A SUMMA DI QUATTRO IN DIFERENZA DI SPATI  $C(x, x_2)$ .

$$\begin{array}{c} \uparrow \\ \downarrow \\ \text{---} \end{array} = \frac{i}{\alpha} \int dx_1 dx_2 G^0(x_1x_2) G^0(x_1x_2) G^0(x_1y) G^0(x_2y) \\ = \begin{array}{c} \uparrow \\ \downarrow \\ \text{---} \end{array} + \dots \\ = \begin{array}{c} \uparrow \\ \downarrow \\ \text{---} \end{array} + \begin{array}{c} \uparrow \\ \downarrow \\ \text{---} \end{array} + \begin{array}{c} \uparrow \\ \downarrow \\ \text{---} \end{array} + \dots \quad \text{POSSIBILITÀ DI} \\ \rightarrow G(x, x_2) = G^0(x, x_2) + \int dy_1 dy_2 U^0(x_1y_1) \bar{U}^0(y_2y_1) G^0(y_1x_2)$$

DIVIDIAMO IL CONCETTO IN CUI MANIFESTA IL PROBLEMA  $G^0$

$$\text{DA } G = \langle E_0 | TS q^+ q^- | E_0 \rangle \quad \text{ESPLIAMO S E ELETTRONICO CON 3 } G^0 \quad \begin{array}{c} \uparrow \\ \downarrow \\ \text{---} \end{array} \quad \begin{array}{c} \uparrow \\ \downarrow \\ \text{---} \end{array} \quad \begin{array}{c} \uparrow \\ \downarrow \\ \text{---} \end{array}$$

USANDO CHE  $S$  È IL  $\delta^{(0)}_{x_1 \rightarrow x_2}$  NO SI PUÒ FAR CONCETTO V PARTICOLO  $\Rightarrow$  NO SCAMBIO  $\Rightarrow$  NO SCAMBIO

$$\frac{i}{\alpha} \sum_{k=2}^{\infty} \frac{1}{(\beta k)^k} \int \langle TV_i - V_k q^+ q^- \rangle \delta^{(0)}_{x_1 \rightarrow x_2} dt_1 - dt_k = \frac{i}{\alpha} \sum_{k=2}^{\infty} \frac{1}{(\beta k)^k} \int dt_1 \dots dt_k \int dy_1 dy_2 U^0(x_1y_1) \langle T q^+_1 q^+_2 q^-_3 q^-_4 \rangle V_k V_k \dots V_k$$

$$= \frac{i}{\alpha} \sum_{k=2}^{\infty} \frac{1}{(\beta k)^k} \int dt_1 \dots dt_k \int dy_1 dy_2 U^0(x_1y_1) G^0(x_1x_2) \dots G^0(x_kx_2) \dots G^0(x_ky_2) \dots G^0(y_2y_1) \dots G^0(y_2y_1)$$

$$= \frac{i}{\alpha} \sum_{k=2}^{\infty} \frac{1}{(\beta k)^k} \int dt_1 \dots dt_k \int dy_1 dy_2 U^0(x_1y_1) G^0(x_1x_2) \dots G^0(x_kx_2) \dots G^0(x_ky_2) \dots G^0(y_2y_1)$$

$$= \frac{i}{\alpha} \sum_{k=2}^{\infty} \frac{1}{(\beta k)^k} \int dt_1 \dots dt_k \int dy_1 dy_2 U^0(x_1y_1) G^0(x_1x_2) \dots G^0(x_kx_2) \dots G^0(x_ky_2) \dots G^0(y_2y_1)$$

$$= \frac{i}{\alpha} \sum_{k=2}^{\infty} \frac{1}{(\beta k)^k} \int dt_1 \dots dt_k \int dy_1 dy_2 U^0(x_1y_1) G^0(x_1x_2) \dots G^0(x_kx_2) \dots G^0(x_ky_2) \dots G^0(y_2y_1)$$

$$= \frac{i}{\alpha} \int dx_1 dx_2 G^0(x_1x_2) G^0(x_1x_2) \left[ \frac{1}{\alpha} \int dy_1 dy_2 U^0(x_1y_1) G^0(x_1y_1) \langle TV_i - V_k q^+ q^- \rangle \right]^k \quad \text{ACCORDAMENTO CON CIRCUITO} \Rightarrow \langle E_0 | TS q^+ q^- | E_0 \rangle^k = \langle E_0 | T q^+ q^- | E_0 \rangle^k$$

$$\Rightarrow \langle E_0 | T q^+ q^- | E_0 \rangle^k = \langle E_0 | \hat{O} | E_0 \rangle^k \Rightarrow \langle E_0 | \hat{O} | E_0 \rangle = \langle E_0 | \hat{O}_A | E_0 \rangle - \langle E_0 | \hat{O}_B | E_0 \rangle \Rightarrow \langle E_0 | \hat{O}_A | E_0 \rangle = \langle E_0 | \hat{O}_B | E_0 \rangle$$

$$\Rightarrow \langle E_0 | \hat{O}_A | E_0 \rangle = S_{AA} \quad \text{NO SCAMBIO} \Rightarrow \langle E_0 | \hat{O}_B | E_0 \rangle = S_{BB} \quad \text{SCAMBIO}$$

$$G(x, x_2) = G^0(x, x_2) + \int dy_1 dy_2 U^0(x_1y_1) \bar{U}^0(y_2y_1) G^0(y_1x_2) \text{ CON } \int dy_1 dy_2 U^0(x_1y_1) \bar{U}^0(y_2y_1) = \frac{1}{\alpha} \langle E_0 | S_{AB} | E_0 \rangle$$

$$= \sum_{k=0}^{\infty} \frac{1}{(\beta k)^k} \frac{1}{k!} \sum_{k'=k}^{\infty} \frac{1}{(\beta k')^{k-k}} \frac{1}{(k')!} I - I = \sum_{k=0}^{\infty} \frac{1}{(\beta k)^k} \frac{1}{k!} \int dt_1 \dots dt_k \langle TV_i - V_k q^+ q^- \rangle \sum_{k'=0}^{\infty} \frac{1}{(\beta k')^{k'}} \frac{1}{k'!} \int ds_1 \dots ds_k \langle TV_i - V_k q^+ q^- \rangle$$

MESSAGGIO TECNICO

$$= \langle E_0 | TS q^+ q^- | E_0 \rangle \langle E_0 | TS q^+ q^- | E_0 \rangle = \langle E_0 | T q^+ q^- | E_0 \rangle \langle E_0 | T q^+ q^- | E_0 \rangle$$

② PENSANDO A 8 2 3 E PARTE DI SCAMBIO  $\Rightarrow \pm \langle E_0 | T q^+ q^- | E_0 \rangle$  

③ CONTAGGIO D'INTESA CON TUTTO  $\Rightarrow$  G CONCESSA 

EQ DEL MOTORE  $\Rightarrow$  DUE NIDI

$$[i\partial_x - h(x)] G(x-x't') = S_{mn} S_3(x-x') \delta(t-t') + \sum_m \int dy S(xy) G_{mm'}^{HF}(x-x't') G_{m'm'}^{HF}(yt')$$

SS TUTTO CONCESSA

$$+ \sum_m \int dy S(xy) \left[ G_{mm'}^{HF}(x-x't') G_{m'm'}^{HF}(yt') - G_{mm'}^{HF}(xt') G_{m'm'}^{HF}(yt') \right]$$

$\Rightarrow$  EQ CHIUSA X IL PROPAGATORI  $\rightarrow$  APPROXIMAZIONE HF (IN TERMINI DI PROPAGATORI)

EQ QUADRATICA DI  $G$

$$[i\partial_x - h(x)] G_{mm'}^{HF}(x-x't') = S_{mn} S_3(x-x') \delta(t-t') + \sum_m \int dy S(xy) G_{mm'}^{HF}(x-x't') G_{m'm'}^{HF}(yt') - i G_{mm'}^{HF}(x-x't') \sum_m \int dy S(xy) G_{m'm'}^{HF}(yt')$$

$$\Rightarrow [i\partial_x - h(x) - C_H(x)] G_{mm'}^{HF}(x-x't') = S_{mn} S_3(x-x') \delta(t-t') + \sum_m \int dy S(xy) G_{mm'}^{HF}(x-x't') G_{m'm'}^{HF}(yt')$$

IS SP CS

$$[i\partial_x - h(x) - C_H(x)] G_{mm'}^{HF}(x-x't') = S_{mn} S_3(x-x') \delta(t-t') + \sum_m \int dy S(xy) G_{mm'}^{HF}(x-x't') e^{i\omega t} \quad (*)$$

SS SPPI MAMM PROPAGATORI DI PARTICOLE INDIP  $\rightarrow G_{mm'}^{HF}(x-x') = \sum_n C_n(xm) C_n^{*}(xm')$   $\rightarrow C_n$  CP ONSDORUM

INSERENDO IN MAMM E MOTTO  $\times C_n(xm')$   $\oplus \int dy \delta^{(0)}_{m'm} \sum_m$   $\Rightarrow$  IN ONSDORUM SI OTTIENE

$$\int \frac{C_n(xm)}{\omega - \omega_n \pm i\eta \operatorname{sgn}(\omega_n - \omega_f)} = \alpha C_n(xm) + \sum_m \int dy S(xy) \frac{C_n(ym')}{\omega - \omega_n \pm i\eta \operatorname{sgn}(\omega_n - \omega_f)} \int \frac{dy}{2\pi} G_{mm'}^{HF}(xy) e^{i\omega y}$$

$$\text{CON CIRCUITO } \langle \hat{O}_A | \hat{O}_B | E \rangle = \sum_m \sum_n |C_n(xm)|^2 \delta(\omega_f - \omega_n)$$

ORA PENSANDO A  $\omega - \omega_n$   $\Rightarrow$  SIS EQ HF

$$[h(x) + C_H(x)] \langle \hat{O}_A | \hat{O}_B | E \rangle - \sum_m \delta(\omega_f - \omega_n) \langle \hat{O}_B | \hat{O}_B | E \rangle \int dy S(xy) C_n(ym') C_n^{*}(ym'') = \text{fisico } C_n(x)$$

SS  $C_{AB}(xm) = f_A(x) \delta_B(m)$   $\Rightarrow$  ORTOPORTANTÉ SPIN  $\sum_{m''} S_{AB}(m'') S_{AB}(m'') = S_{AB}$

$$\Rightarrow IS EQ \quad [h(x) + C_H(x)] \langle f_A(x) - \sum_{\omega_B < \omega_f} f_B(x) \int dy S(xy) f_B^{*}(y) \rangle = \text{fisico } f_A(x)$$

SOMMA DI TUTTI I DISegNI TOPOLOGICI DESTINATI CONCESSI

IN CUI S'HA PARTE CON SPIN P E S'HA PARTE CON SPIN P

IN CUI S'HA PARTE CON SPIN P E S'HA PARTE CON SPIN P

POLEAZZIONE PRODUZIONE

$$\Pi(12) = \text{Diagramma} + \text{Diagramma con loop} + \text{Diagramma con loop e loop} \rightarrow \text{disegnabile o no}$$

$$\Rightarrow \Pi = \bar{\Pi}^* + \bar{\Pi}^* \pi_0 (\bar{\Pi}^* + \bar{\Pi}^* \pi_0 (\bar{\Pi}^* -)) = \bar{\Pi}^* + \bar{\Pi}^* \pi_0 \bar{\Pi} = \bar{\Pi}^* + \bar{\Pi}^* \bar{\Pi}^* \bar{\Pi}$$

ESPLICATI

$$\bar{\Pi}_{\text{prod}}^{(12)} = \bar{\Pi}^*(12) + \int d\vec{x} d\vec{y} \sum_{\text{loop}} \bar{\Pi}^*(13) G^0(34) \bar{\Pi}^*(42)$$

$$\approx G^0_{\text{prod}} = S_{\text{prod}} C^0 \Rightarrow \bar{\Pi}_{\text{prod}} = \bar{\Pi}^*(12) + \int d\vec{x} d\vec{y} \bar{\Pi}^*(13) G^0(34) \bar{\Pi}^*(42)$$

$$C = C^0 + C^0 \bar{\Pi}^* C^0 = C^0 + C^0 (\bar{\Pi}^* + \bar{\Pi}^* \bar{\Pi}^*) C^0 \Rightarrow [C = C^0 + C^0 \bar{\Pi}^* C^0]$$

SE H INVAL X TASSAZZ  $\Rightarrow$  ANCHE  $\Pi$  E  $\bar{\Pi}^*$  (BUT  $\Pi \times \bar{\Pi}^*$ )  $\Rightarrow$  ANCHE  $C$

$$C(xg) = \int \frac{d^3 k}{(2\pi)^3} \frac{d\omega}{2\pi} C(k\omega) e^{i\vec{k}(x-g) - i\omega(t_x - t_g)}$$

$$\Rightarrow C(k\omega) = C^0(k\omega) + C^0(k\omega) \bar{\Pi}^*(k\omega) C(k\omega)$$

$$\Rightarrow C(k\omega) = \frac{C^0(k\omega)}{1 - C^0(k\omega) \bar{\Pi}^*(k\omega)}$$

$$\bar{\Pi}(k\omega) = \frac{\bar{\Pi}^*(k\omega)}{1 - C^0(k\omega) \bar{\Pi}^*(k\omega)}$$

X POT ENTRICO  $C^0(x-x') = S(x-x') \delta(t-t')$   $\Rightarrow C^0(k\omega) = S(k)$

$$\Rightarrow C(k\omega) = \frac{S(k)}{E(k\omega)}, \bar{\Pi}(k\omega) = \frac{\bar{\Pi}^*(k\omega)}{E(k\omega)} \xrightarrow{\text{PONTE DI DISTINZIONE CON}} E(k\omega) = 1 - S(k) \bar{\Pi}^*(k\omega)$$

ANCHE SE  $C^0$  ENTRICO  $C$  DIP DEL TEMPO X E' CASO DISCONTINUO  
NEDOSTA DEL MODELLO

CASO COULOMB  $C^0(k\omega) = \frac{4\pi e^2}{k^2} \Rightarrow C(k\omega) = \frac{4\pi e^2}{k^2 - E(k\omega) \bar{\Pi}^*(k\omega)}$

$\rightarrow$  CONDIZIONE A CONGO NELLA DI COULEMB E' MOLTO  
DURO SCALDARE DEL MODELO PER DISPERGIMENTO

CALCOLO PARZIALE DI  $\Pi^*$   $\text{Diagramma} = \text{Diagramma} + \text{Diagramma con loop}$

$$\bar{\Pi}(xg) = \frac{1}{i\hbar} \langle E(1) T S(1)(x) S(1)(g) | E \rangle \text{ COME ASSISTENZA DATO DAGLI  
L'ESPRESSO ANALITICO}$$

$\rightarrow$  PREDISPOSIZIONE  $\frac{1}{i\hbar}$  + DISG. INDIRETTO

$$\text{Diagramma con loop} = \bar{\Pi}(xg) = \frac{1}{i\hbar} (-1) 2 G^0(xg) G^0(gx)$$

$\rightarrow$  IN SP

REGOLE DI FERMATIUS (KS SPLUR) (CONSIDERANDO DA TRANSFORMATA)  $G = \sum G^0(j)$

$$G^0(x-x') = \left(\frac{i}{\hbar}\right)^K (-1) \sum_{\text{SPIN}} \int d\vec{z}_1 d\vec{z}_2 \dots d\vec{z}_K G^0(z_i z_j) G^0(x-z_i) G^0(x-z_j) G^0(x'-z_i) G^0(x'-z_j)$$

SE  $G^0$  FORMANO 2 TPI DI SPIN

$$V = \frac{1}{2} \int d\vec{x} d\vec{y} G^0(q) G^0(q)$$

- ① start  $\longrightarrow$  END
- ② cool

SE HO INVAL X TASSAZZ SE I X  $G^0$  CAS X INVERSIONI

$$\begin{aligned} & \uparrow \text{RWA} \quad G^0(z_1 z_2) = \int \frac{d^3 k}{(2\pi)^3} \frac{d\omega}{2\pi} e^{i\vec{k}(z_1 - z_2) - i\omega(t_1 - t_2)} \\ & \downarrow \end{aligned} \quad G^0(q_1 z_2) = \int \frac{d^3 q}{(2\pi)^3} \frac{d\omega}{2\pi} e^{i\vec{q}(z_1 - z_2) - i\omega(t_1 - t_2)} G^0(q\omega)$$

IN SP POSSO NO CANCELLARE START/END

IN SP E  $G^0$  NON HA ORDINE NATURALE  $\Rightarrow$  DECISO IO

IN SP E  $G^0$  NON HA ORDINE NATURALE  $\Rightarrow$  DECISO IO

IN SP E  $G^0$  NON HA ORDINE NATURALE  $\Rightarrow$  DECISO IO

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IN SP E <math

$$\frac{P+q}{q} \xrightarrow{\omega+i\eta} = \frac{1}{\hbar} (-1) \int \frac{d^3 p}{(2\pi)^3} \frac{d\omega}{2\pi} \left[ \frac{\Theta(p-R_F)}{\omega - \epsilon_{p,q} + i\eta} + \frac{\Theta(p-R_F)}{\omega - \epsilon_{p,q} - i\eta} \right] \left[ \frac{\Theta(p+q-R_F)}{\omega + i\eta} + \frac{\Theta(p+q-R_F)}{\omega - i\eta} \right] = \overline{\Pi}(q, \omega)$$

INTEGRANDO IN  $\omega \rightarrow \frac{1}{\omega^2}$  CONV CON POU SONO S SOTTO  $\rightarrow$  GII INTEGR CONV CONV  $\Rightarrow$  CHIUSO DENTRO MIPAU

$\Rightarrow$  CONTRIB SERA INTEGR CON POU OFFSET  $\rightarrow 2/6$

$$\overline{\Pi}(q, \omega) = -\frac{2i}{\hbar} \int \frac{d^3 p}{(2\pi)^3} \frac{2\pi i}{2\pi} \left[ \frac{\Theta(p-R_F) \Theta(p+q-R_F)}{\omega - \epsilon_{p,q} - \epsilon_{p,q} + i\eta} + \frac{\Theta(p-R_F) \Theta(p+q-R_F)}{\omega + i\eta - \epsilon_{p,q} - \epsilon_{p,q} + i\eta} \right]$$

$\rightarrow$  PLEMEL-SORHOTSKI  $\frac{1}{x-y \pm i\eta} = \frac{P}{x-y} + i\pi \delta(x-y)$   $\rightarrow$  VACC SS INTEGR SS DNA ABBUS

$$P = \text{Re } \overline{\Pi}(q, \omega) = \frac{2}{\hbar} \int \frac{d^3 p}{(2\pi)^3} \frac{\Theta(p-R_F) \Theta(p+q-R_F) - \Theta(p-R_F) \Theta(p+q-R_F)}{\omega - \epsilon_{p,q} - \epsilon_{p,q}}$$

$$\text{Im } \overline{\Pi}(q, \omega) = -\frac{2\pi i}{\hbar} \int \frac{d^3 p}{(2\pi)^3} \Theta(p-R_F) \Theta(p+q-R_F) \delta(\omega - \epsilon_{p,q} - \epsilon_{p,q}) + \Theta(p-R_F) \Theta(p+q-R_F) \delta(\omega + i\eta - \epsilon_{p,q} - \epsilon_{p,q})$$

$\partial \text{Im } \overline{\Pi} \rightarrow$  HO DNA PARTEC DENTRO SONA POU DENTRO DI CA DENTRO DI UNO DI THI

INTEGR DI RE SPENDO CAS

$$\Theta(p-R_F) [1 - \Theta(p+q-R_F)] [\Theta(p-R_F) - \Theta(p+q-R_F)] = \Theta(p-R_F) - \Theta(p+q-R_F)$$

$$\text{Re } \overline{\Pi}(q, \omega) = \frac{2}{\hbar} \int \frac{d^3 p}{(2\pi)^3} \frac{\Theta(p-R_F) - \Theta(p+q-R_F)}{\omega - \epsilon_{p,q} - \epsilon_{p,q}} - p \xrightarrow{\text{caso estremo}} \frac{2}{\hbar} \int \frac{d^3 p}{(2\pi)^3} \Theta(p-R_F) \left[ \frac{1}{\omega - \epsilon_{p,q} - \epsilon_{p,q}} - \frac{1}{\omega + i\eta - \epsilon_{p,q} - \epsilon_{p,q}} \right]$$

[CASO DI RUMS X D20 (CASO ESTREMICO)]

$$\Theta(p-R_F) \rightarrow \begin{cases} p+q > R_F \\ p < R_F \end{cases} \Rightarrow \epsilon_{p,q} - \epsilon_{p,q} \geq 0 \Rightarrow \omega \geq 0$$

$$\text{II PT} \quad \begin{cases} p+q < R_F \\ p > R_F \end{cases} \Rightarrow \epsilon_{p,q} - \epsilon_{p,q} < 0 \Rightarrow \omega < 0$$

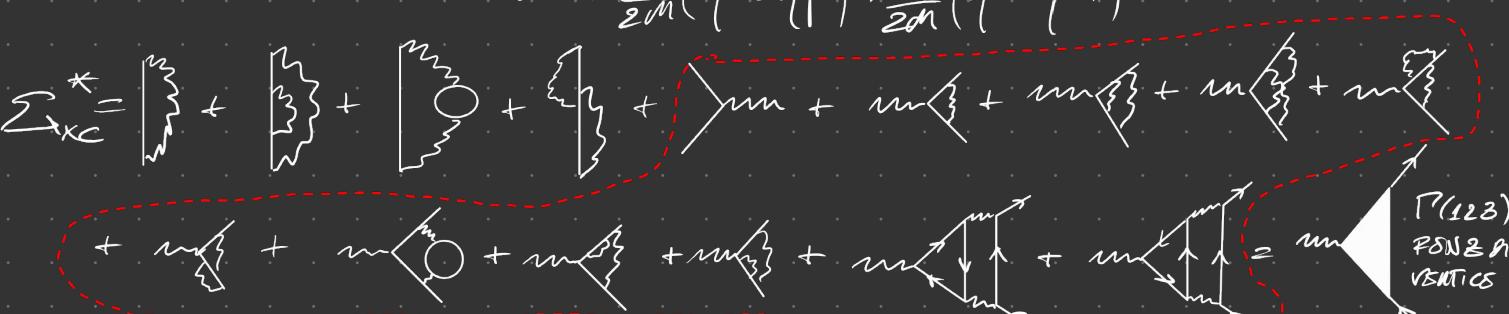
D > Q

$$\frac{p+q}{R_F} = \frac{\omega}{\hbar} \leq \frac{\hbar^2}{2m} (q^2 + 2|p||p|) \rightarrow$$

$$\frac{\hbar^2}{2m} (q^2 + 2|p||p|) \leq \frac{\hbar^2}{2m} (q^2 + 2qR_F) \Rightarrow \Theta(p-R_F) \Rightarrow \text{SECONDO}$$



$$\hbar D = \frac{\hbar^2}{m} R_F q = 2\epsilon_q q$$



FUNZ DI VISIT

P<sup>0</sup> = min POSSO MARAVI  
TUTTI SOTTO



EQ DA HESIN

$$G = G^0 + G^0 \Sigma^* G$$

Dgson I

$$U = U^0 + U^0 \Pi^* U$$

Dgson II

$$\Pi^* = \frac{1}{\hbar} \int d^3 p \frac{\Theta(p-R_F) \Theta(p+q-R_F)}{\omega - \epsilon_{p,q} - \epsilon_{p,q}}$$

$$\Sigma^* = \frac{1}{\hbar} \int d^3 p \frac{\Theta(p-R_F) \Theta(p+q-R_F)}{\omega + i\eta - \epsilon_{p,q} - \epsilon_{p,q}}$$

$$\Pi^*(12) = \frac{1}{\hbar} (-1) \int d\omega d\omega \text{P}(123) G(32) G(12)$$

$$\text{P}(123) = \text{P}_{(123)} + \int d\omega d\omega G^0(12) G^0(13) \frac{S \Sigma^*(23)}{S G^0(45)}$$

$$\text{RUMEL DI BETHE-SALPESON}$$

RUMEL CRESCE LEVANDO G<sup>0</sup> E SPEDENDO CON IL MANCO IL PAPA E LE MEZZE STA TABACCA XRS MANCO CONOSCE  $\Sigma^*$   
 $\Rightarrow$  LISS SOLO ACCORD

E APPROX FRIADESTA  $\rightarrow$  APPROX GW IN ODI  $\boxed{T = T^0}$

$$\Rightarrow$$
 EQ HESIN  $\rightarrow$  EQ INTEGRABILITA  $\Pi^* = \frac{1}{\hbar} \Sigma^* =$

$$\Sigma^* = F(G^0(20) G^0(03) G^0(02)) \Rightarrow G^0 \rightarrow G^0 + SG^0 \oplus \Sigma^* \rightarrow \Sigma^* + SG^0$$

per prendere il funzionale è valido

$$1 \times 1 \text{ IS } G^0 \rightarrow SG \text{ UN IN SG}$$

$$SG(\Sigma) = \int d\omega d\omega \frac{S \Sigma(23)}{S G(45)}$$

IN APPROX GW MENTRE IL  $\Sigma$  DI DIAG DIVENTA FATTORIALE UNA ESSENZA LA VACUA O CONSERVA FINITO

$$\text{RAPPRESENTAZIONE DI LEHMANN PER PROFILATORI} \quad H(t) \rightarrow S \rho \omega \Rightarrow \text{RAPPRESENTAZIONE} \quad H(t) \rightarrow S \rho \omega \Rightarrow \text{RAPPRESENTAZIONE}$$

$$G_{\mu\mu}(x, x') = \langle \delta_0^N | T q_\mu(x) q_\mu^\dagger(x') | \delta_0^N \rangle \quad \text{CONSIDERANDO} \quad H | \delta_n^N \rangle = \epsilon_n^N | \delta_n^N \rangle$$

$\oplus$  EXPATIE TONO

$$= \Theta(t-t') \langle \delta_0^N | q_\mu^\dagger(x) q_\mu^\dagger(x') | \delta_0^N \rangle - \Theta(t'-t) \langle \delta_0^N | q_\mu^\dagger(x) q_\mu^\dagger(x') | \delta_0^N \rangle$$

$q_\mu^\dagger$  CURE PARTEC = INDETERMINATO COMPLETAMENTE SU PARTEC

$$= \sum_n \left[ \Theta(t-t') e^{-i\omega(\epsilon_n^{N+1} - \epsilon_0^N)(t-t')} \langle \delta_0^N | q_\mu^\dagger(x) q_\mu^\dagger(x') | \delta_0^N \rangle - \Theta(t'-t) e^{-i\omega(\epsilon_n^{N+1} - \epsilon_0^N)(t-t')} \langle \delta_0^N | q_\mu^\dagger(x) q_\mu^\dagger(x') | \delta_0^N \rangle \right]$$

Ora CASA IL TEMPO DI SPETTROSCOPIA  $\Rightarrow$  SLOWS

$$= i \sum_n \left[ \int \frac{d\omega}{2\pi} \frac{e^{-i\omega(t-t')}}{\omega + i\eta} \langle q_\mu^\dagger(x) q_\mu^\dagger(x') \rangle - \int \frac{d\omega}{2\pi} e^{-i\omega(t-t')} \langle q_\mu^\dagger(x) q_\mu^\dagger(x') \rangle \right]$$

MISURAZIONE DEL CONTRIBUTO  $\Delta E$   $\oplus$  MANIERA A DETERMINARE

$$\Rightarrow G_{\mu\mu}(x, x') = \int \frac{d\omega}{2\pi} e^{-i\omega(t-t')} \sum_n \left[ \frac{\langle \delta_0^N | q_\mu^\dagger(x) | \epsilon_{n+1}^{N+1} \times \epsilon_n^{N+1} q_\mu^\dagger(x') | \delta_0^N \rangle}{\omega - \epsilon_{n+1}^{N+1} - \epsilon_0^N + i\eta} + \frac{\langle \delta_0^N | q_\mu^\dagger(x) | \epsilon_n^{N+1} \times \epsilon_n^{N+1} q_\mu^\dagger(x') | \delta_0^N \rangle}{\omega - \epsilon_n^{N+1} - \epsilon_0^N - i\eta} \right]$$

$$\Rightarrow G_{\mu\mu}(x, x') = \sum_n [-] \quad \text{POSSO ACCORDARMI ENTI ED EP + XKE LO SOMMI SONO} \neq \text{SHIFTATO TUTTO A UN NUMERO}$$

$$\text{ORA } \epsilon_n^{N+1} - \epsilon_0^N = \epsilon_n^{N+1} \pm \epsilon_0^N - \epsilon_0^N \oplus \epsilon_n^{N+1} = \epsilon_n^{N+1} - \epsilon_0^N > 0 \times \text{DEF ENA SCOTTAZ} \quad \epsilon \mu = \epsilon_0^N - \epsilon_0^N \text{ FOTOCAMICO}$$

PER N  $\rightarrow \infty$  NON DA N MA DA PENSARE

$$\text{DEM} \times N-1 \quad \epsilon_n^{N+1} - \epsilon_0^N = \frac{\epsilon_n^{N+1} - \epsilon_0^N + \epsilon_{n-1}^{N+1} - \epsilon_0^N}{N}$$

$$\Rightarrow G_{\mu\mu}(x, x') = \sum_n \frac{\langle \delta_0^N | q_\mu^\dagger(x) | \epsilon_{n+1}^{N+1} \times \epsilon_n^{N+1} q_\mu^\dagger(x') | \delta_0^N \rangle}{\omega - \epsilon_{n+1}^{N+1} - \epsilon_0^N + i\eta} + \sum_n \frac{\langle \delta_0^N | q_\mu^\dagger(x) | \epsilon_n^{N+1} \times \epsilon_n^{N+1} q_\mu^\dagger(x') | \delta_0^N \rangle}{\omega + \epsilon_n^{N+1} - \epsilon_0^N - i\eta}$$

SOMMA TRA STANTI DISCOSTRAZIONI  $\Rightarrow$  POI COSEMI IN PIÙ

$$\begin{aligned} &\text{FACENDO CONSIDERAZIONI DI FONDO} \\ &\text{SI CONSIDERANO ACCORDAMENTO} \\ &\text{PIÙ FINTA MA} \\ &\text{MANTENGONO IL SEGNALE} \end{aligned}$$

$$\text{INVAR X TRASLAZIONE SP-TEMPO} \quad [H, f] = 0 \Rightarrow |\epsilon_n(x)\rangle \Rightarrow \sum_n \leftrightarrow \sum_{nR} \text{AZIONE TRASLAZIONE}$$

$$e^{i\omega t} q_\mu^\dagger(x) e^{-i\omega t} = q_\mu^\dagger(x-\omega t) = e^{-i\omega t} q_\mu^\dagger(0) e^{i\omega t} = \text{SCUOLO TONO}$$

POTREO SCRIVERE CHE GS SIA  $R=0$  (PERMETTENDO UN BALLO CONTO)

$$G_{\mu\mu}(x, x') = \sum_{nR} \left[ \frac{\langle \delta_0^N | q_\mu^\dagger(x) | \epsilon_{n+1}^{N+1} \times \epsilon_n^{N+1} q_\mu^\dagger(x') | \delta_0^N \rangle}{\omega - \epsilon_{n+1}^{N+1} - \epsilon_0^N + i\eta} + \sum_k \frac{\langle \delta_0^N | q_\mu^\dagger(x) | \epsilon_{n+1}^{N+1} \times \epsilon_n^{N+1} q_\mu^\dagger(x') | \epsilon_k^{N+1} \times \epsilon_{k-1}^{N+1} q_\mu^\dagger(0) | \delta_0^N \rangle}{\omega + \epsilon_{n+1}^{N+1} - \epsilon_0^N - i\eta} \right]$$

$$= \sum_{nR} e^{i\omega(x-x')} \left[ \frac{\langle \delta_0^N | q_\mu^\dagger(0) | \epsilon_{n+1}^{N+1} \times \epsilon_n^{N+1} q_\mu^\dagger(x') | \delta_0^N \rangle}{\omega - \epsilon_{n+1}^{N+1} - \epsilon_0^N + i\eta} + \frac{\langle \delta_0^N | q_\mu^\dagger(0) | \epsilon_n^{N+1} \times \epsilon_{n-1}^{N+1} q_\mu^\dagger(x') | \delta_0^N \rangle}{\omega + \epsilon_n^{N+1} - \epsilon_0^N - i\eta} \right]$$

$$\Rightarrow G_{\mu\mu}(k\omega) = \sqrt{\sum_n} \left[ \frac{|\langle \delta_0^N | q_\mu^\dagger(0) | \epsilon_{n+1}^{N+1} \times \epsilon_n^{N+1} q_\mu^\dagger(0) | \delta_0^N \rangle|^2}{\omega + \epsilon_{n+1}^{N+1} - \epsilon_0^N + i\eta} + \frac{|\langle \delta_0^N | q_\mu^\dagger(0) | \epsilon_n^{N+1} \times \epsilon_{n-1}^{N+1} q_\mu^\dagger(0) | \delta_0^N \rangle|^2}{\omega - \epsilon_n^{N+1} - \epsilon_0^N - i\eta} \right]$$

$$A(k\omega) = \sqrt{\sum_n} |S| \quad S = \langle \delta_0^N | q_\mu^\dagger(0) | \epsilon_{n+1}^{N+1} \times \epsilon_n^{N+1} q_\mu^\dagger(0) | \delta_0^N \rangle$$

### TEORIA DELLA RISPOSTA CINETICA

$$\text{H INFATI} \rightarrow \text{POTENZIALE CON V(t)} = \omega \text{ PER } t < 0$$

$$\rightarrow \text{SUPP DI SPETTROSCOPIA} \quad |\phi(t) = |GS\rangle \text{ DI } H \Rightarrow \text{SO } t \geq 0 \quad \langle q(t) | \phi(t) \rangle = \langle \phi(t) | \phi(t) \rangle = e^{i\omega t} \langle \phi(0) | \phi(0) \rangle$$

SO CONSIDER O<sub>t</sub> CHE HA PROPRIA SVOLGE TEMPORALE INDIPENDENTI

$$\langle \phi(t) | O_t | \phi(t) \rangle = \langle GS | \langle \phi(t), O_t | \phi(t) \rangle | GS \rangle = \langle GS | \langle \phi(t), O_t | \phi(t) \rangle | GS \rangle \text{ CON SVOLGE INDEPENDENTI DI O<sub>t</sub> SECONDO I 2 EVOLVIMENTI}$$

E' POSSIBILE SCRIVERE TUTTO AL LIVELLO

$$O_t(t, \omega) = \text{EXP} \left[ \frac{i}{\hbar} \int_0^t dt' V_h(t') \right] \Rightarrow \langle GS | \left( 1 - \frac{1}{\hbar} \int_0^t dt' V_h(t') \right) O_t(t, \omega) \left( 1 + \frac{1}{\hbar} \int_0^t dt' V_h(t') \right) | GS \rangle = \langle \phi(t) | O_t | \phi(t) \rangle - \langle GS | O_t | GS \rangle$$

$$= \frac{1}{\hbar} \int_0^t dt' \langle GS | [O_t(t'), V_h(t')] | GS \rangle \rightarrow \text{LINEARE IN V}$$

### PERTURBAZIONE ESTERNA

$$H_t = H + \int d\omega \chi(\omega) \phi(\omega t) \rightarrow \text{DIP TEMPORALE DA CAMPO ESTERNO} \quad \phi(\omega t) = 0 \text{ SE } t < 0$$

$$\text{VALORE A MISURA} \hat{n} \rightarrow \langle \phi(t) | \hat{n} | \phi(t) \rangle - \langle GS | \hat{n} | GS \rangle = \frac{1}{\hbar} \int dt' \int d\omega \chi(\omega) \langle GS | \hat{n}_h(\omega), \hat{n}_h(\omega') | GS \rangle \phi(\omega')$$

$$\text{VALORE DENSITÀ IN } \omega \text{ } \hat{n}(\omega) = \frac{1}{\hbar} \int dt' d\omega \chi(\omega) \langle \phi(t), \phi(t') \rangle \phi(\omega') \rightarrow \text{OSSERVAZIONE DI H}$$

$$\langle \phi(t) | \phi(t') \rangle = \langle GS | [\hat{n}_h(\omega), \hat{n}_h(\omega')] | GS \rangle \rightarrow \text{VALORE SO INDETTO DA FONZ ESTERNA E UNO IN QUESTA DA UNA RISPOSTA IN GS NON CONSIDERATA}$$

$$\theta \text{ CONSIDERA CADUTA} \rightarrow \text{FONZ DI RISPOSTA INTANDEATA} \phi(t, t') \text{ DI PDA } t-t'$$

$$\text{INvar x traslazion sp-tempo} \rightarrow \mathcal{D}(x, x') \text{ DI PDA } x-x' \text{ E } t-t' \rightarrow \text{DIM CONTRIBUTO DI CAMPO}$$

$$[f, H] = 0 \Rightarrow \text{NUOVO SVOLGE TEMPORALE DI CADUTA SO GS} \Rightarrow \text{DI PDA } x-x' \rightarrow \text{NUOVO} \rightarrow \text{CONTRIBUTO DI SP-TEMPORALE} \rightarrow \text{SP-TEMPORALE}$$

$$S_n(x, t) = \int \frac{ds k}{(2\pi)^3} \frac{dk}{2\pi} e^{i k x - i \omega t} \rightarrow S_n(k\omega) \Rightarrow \mathcal{D}(k\omega) = \frac{1}{\hbar} \int dk \mathcal{D}(k\omega) \phi(k\omega)$$

$$\text{IN SP-TEMPORALE} \rightarrow \text{VALORE MODULARE}$$

$$\text{IN MATERIALE CON ATTIVITÀ} \rightarrow \text{COSTANTE DI KINETICA}$$

$$\rightarrow \text{ESISTENZA CONSIDERATA}$$

$$\text{DEF } \mathcal{D}(x, x') = \langle GS | \mathcal{T} S_n(x, t) S_n(x', t') | GS \rangle = i\hbar \overline{I(x, x')}$$

$$\text{INVERSO A PREMERE X INVAR TRASLATE SP-TEMPO} \rightarrow \mathcal{D}(k\omega)$$

$$\text{NELL'LEHMANN X SA E SB} \quad \oplus \quad \langle \mathcal{C}_{AB}^R(t, t') \rangle = \langle GS | [A_h(t), B_h(t')] | GS \rangle \theta(t-t') \rightarrow \text{ENCIOPPO}$$

$$\text{DEF } \mathcal{C}_{AB}^T(t, t') = \langle GS | \mathcal{T} S_A_h(t) S_B_h(t') | GS \rangle = \theta(t-t') \langle GS | S_A_h(t) S_B_h(t') | GS \rangle - \theta(t-t') \langle GS | S_B_h(t) S_A_h(t') | GS \rangle$$

$$\text{SUSCETTIBILITÀ CONSIDERATA}$$

$$\text{IN SP-TEMPORALE} \rightarrow \text{VALORE MODULARE}$$

$$\text{IN MATERIALE CON ATTIVITÀ} \rightarrow \text{COSTANTE DI KINETICA}$$

$$\rightarrow \text{ESISTENZA CONSIDERATA}$$

$$\text{DEF } \mathcal{C}_{AB}^R(\omega) = \langle GS | [A_h(\omega), B_h(\omega)] | GS \rangle = \theta(\omega) \langle GS | A_h(\omega) B_h(\omega) | GS \rangle - \theta(\omega) \langle GS | B_h(\omega) A_h(\omega) | GS \rangle$$

$$\text{# PDM DI C, C'}$$

$$\text{DEF } \mathcal{C}_{AB}^T(\omega) = \int \frac{ds k}{(2\pi)^3} \frac{dk}{2\pi} e^{i k x - i \omega t} \langle GS | [A_h(\omega), B_h(\omega)] | GS \rangle$$

$$\text{N=0 E' ANCHE } \oplus \text{ SP-TEMPORALE}$$

$$\text{E' STERIO } (\epsilon_n - \epsilon_0)/\hbar$$

$$\text{DEF } \mathcal{C}_{AB}^R(\omega) = \int \frac{ds k}{(2\pi)^3} \frac{dk}{2\pi} e^{i k x - i \omega t} \langle GS | [A_h(\omega), B_h(\omega)] | GS \rangle$$

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$$\text{DEF } \mathcal{C}_{AB}^T(\omega) = \int \frac{ds k}{(2\pi)^3} \frac{dk}{2\pi} e^{i k x - i \omega t} \langle GS | [A_h(\omega), B_h(\omega)] | GS \rangle$$

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$$\text{# PDM DI C, C'}$$

$$\text{DEF } \mathcal{C}_{AB}^T(\omega) = \int \frac{ds k}{(2\pi)^3} \frac{dk}{2\pi} e^{i k x - i \omega t} \langle GS | [A_h(\omega), B_h(\omega)] | GS \rangle$$

$$\text{N=0 E' ANCHE } \oplus \text{ SP-TEMPORALE}$$

$$\text{E' STERIO } (\epsilon_n - \epsilon_0)/\hbar$$

SCHERZINGE IMPONEREA IN Q D'ANALISI 2e IN REG  $\Rightarrow H_{KQ} = 2e^2 \int dx \frac{1(x)}{|x|} \rightarrow$  PERTURB IMPORTAT ACCORDA A  $t = -\infty$

$$S\eta(x,t) = \frac{1}{\alpha} \int dt' dx' \delta(x-x') \delta(t-t') \phi(x') \Rightarrow \phi(x) = -\frac{2e^2}{|x|}$$

$$S\eta(\underline{\omega}) = \frac{1}{\alpha} \mathcal{D}(\underline{\omega}\omega) \phi(\underline{\omega}\omega) \Rightarrow \phi(\underline{\omega}\omega) = -2e^2 \frac{4\pi}{K^2} 2\pi S(\omega)$$

$$\begin{aligned} S\eta(x,t) &= \int \frac{dx K}{(2\pi)^3} e^{iKx} \int \frac{d\omega R}{\alpha} (\underline{\omega}\omega) (-2e^2) \frac{4\pi}{K^2} = -2e^2 \frac{4\pi}{K^2} \int_0^\infty K^2 dK \int \frac{d\omega R}{\alpha} \frac{e^{iKx} \cos \theta}{\sin^2 \theta} \\ &= -\frac{2e^2}{4\pi^2} \int K dK \frac{4\pi}{K^2} \frac{1}{\alpha} \mathcal{D}(\underline{\omega}\omega) e^{iKx} \end{aligned}$$

ESIGUO

$$\text{SOMMO CHE } \mathcal{D}(xx') = \underline{\pi}(xx') \Rightarrow \text{COI CALCOLATORE } \mathcal{D}(xx') = \frac{R}{\alpha} \underline{\pi}(xx') \Rightarrow \mathcal{D}(\underline{\omega}\omega) = \frac{\underline{\pi}(\underline{\omega}\omega)}{1 - 8(K) \underline{\pi}(\underline{\omega}\omega)}$$

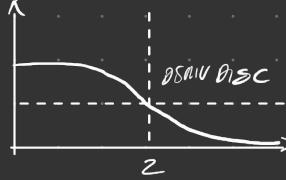
$$\Rightarrow \text{PERICO DIMINUISCE } \underline{\pi} = \text{Re} \underline{\pi} + i \text{Im} \underline{\pi} \text{sgn}(\omega) \Rightarrow \underline{\pi} = \frac{\underline{\pi} R}{1 - 8\underline{\pi} R} \Rightarrow \frac{\mathcal{D}(\underline{\omega}\omega)}{\alpha} = \frac{R}{\underline{\pi}(\underline{\omega}\omega)} = \frac{iK}{1 - \frac{4\pi e^2}{K^2} \underline{\pi}(\underline{\omega}\omega)}$$

$$\Rightarrow S\eta(r) = -\frac{2}{4\pi^2 r} \int K dK \frac{\frac{4\pi e^2}{K^2} \underline{\pi}(\underline{\omega}\omega)}{1 - \frac{4\pi e^2}{K^2} \underline{\pi}(\underline{\omega}\omega)} e^{iKr} \rightarrow \text{NON SO } \underline{\pi} \text{ MA SOLO CHE } \underline{\pi} = \text{Re} \underline{\pi} (\text{P. IM. NELLA})$$

$$\Rightarrow \text{APPROX } \underline{\pi} \approx \underline{\pi}^0$$

IL CALCOLO ESATO  $\rightarrow$  VADO A  $R \rightarrow \infty \Rightarrow e^{iKr}$  OSCILLA UN BOMBO  $\Rightarrow$  INIZIALE VA A 0 VELOCEM  $\Rightarrow$  DOMINA ZONA  $K \rightarrow 0$  IN INIZIO

$$\Rightarrow \boxed{K \rightarrow 0} \quad \underline{\pi}(\underline{\omega}\omega) \approx \underline{\pi}^0(\underline{\omega}\omega) = -\frac{MK_F}{4\pi^2 R^2} g\left(\frac{K}{K_F}\right) \rightarrow g(x) = \frac{1}{2} - \frac{1}{2x} \left(1 - \frac{x}{a}\right) \text{ G} \left| \frac{2-x}{2+x} \right|$$



$$g \text{ NAMMENDA DA INTERVALLI} \rightarrow \boxed{g(\omega) = 1} \rightarrow \text{APPROX THOMAS-FERMI} \quad \boxed{g(x) \approx 1}$$

$$S\eta(r) = -\frac{2}{4\pi^2 r} \int K dK \frac{\frac{4\pi e^2}{K^2} \left(-\frac{MK_F}{4\pi^2 R^2}\right)}{R^2 + \frac{MK_F^2 e^2}{4\pi^2 R^2}} \quad R_F = \frac{MK_F e^2}{4\pi^2 R^2} = \frac{K_F}{2a} \quad \left(2a = \frac{R^2}{me^2}\right)$$

$$K_F \approx 1 \quad \text{NON COSÌ} \neq \text{DA}$$

DENSITÀ INTERNA COND

$$\rightarrow S\eta(r) = -\frac{2}{4\pi^2 r} \int K dK \frac{K^2}{K^2 + K_F^2} e^{iKr} = \frac{2\pi a}{r} \frac{1}{1 + K_F^2/a^2} \quad \text{THOMAS-FERMI}$$



IN REALTA' DUE VALORI MISURABILI  $\Rightarrow$  DUE FORMULE

$$\Rightarrow S\eta(r) \sim \frac{2}{r} \cos(2K_F r) \quad \text{E' Ogni A DENSITÀ FISI DI KF}$$

$$\text{DUE VALORI MISURABILI MAGGIORI!} \quad \Rightarrow \underline{\pi} \text{ HA PARTE REALE E' RE} \rightarrow \text{POSSÈ E' RE} \Rightarrow \text{INTESA SEPARABILI}, \quad \text{OASI FUNZ RETTIFICA PER KF} \rightarrow \underline{\pi}(\underline{\omega}\omega) = \frac{\underline{\pi}^*}{1 - 8(K) \underline{\pi}(\underline{\omega}\omega)}$$

$$\text{POSI} \quad \Omega = 1 - 8(K) \underline{\pi}(\underline{\omega}\omega) \rightarrow \text{PER KF} \Rightarrow \omega(\omega) = \underline{\omega}(\omega) + i \omega_c(\omega) \rightarrow \text{ROT} \Rightarrow \omega_c < 0 \rightarrow \Omega = 1 - 8(K) \underline{\pi}(\omega, \omega + i\omega_c) \rightarrow \text{IMPONGO} \omega_2 \text{ PICCOLO} \Rightarrow \text{SEPARO PT RE E IM E' E' L'INTESA}$$

$$1 - 8(K) \left[ \text{Re} \underline{\pi}(\underline{\omega}\omega) + i \text{Im} \underline{\pi}(\underline{\omega}\omega) + \frac{i\omega_c}{\omega} \text{Re} \underline{\pi}(\underline{\omega}\omega) \right] \frac{1}{\omega - \omega} \rightarrow \text{PT RE} \quad \Omega = 1 - 8(K) \text{Re} \underline{\pi}(\underline{\omega}\omega) (+ \text{PT IM} \times \omega_c \rightarrow \omega) \quad \text{PT IM} \quad \Omega = -8(K) \text{Im} \underline{\pi}(\underline{\omega}\omega) + \omega_c \frac{\partial}{\partial \omega} \text{Re} \underline{\pi}(\underline{\omega}\omega) \Big|_{\omega=0} \rightarrow \text{PT RE} \quad \omega_c$$

$$C_{AB}(\omega) = \sum_n A_{nB} B_{nA} \delta\left(\omega - \frac{\omega_n - \omega_0}{\tau_n}\right) - B_{nA} A_{nB} \delta\left(\omega + \frac{\omega_n - \omega_0}{\tau_n}\right)$$

FUNZ RETTIFICA PER KF  
=> ANALOGA IN PIANO E SP

$$C_{AB}^T(\omega) = \int_{-\infty}^{\infty} d\omega' \frac{C_{AB}(\omega')}{\omega - \omega' + i\eta \text{sgn}(\omega')}$$

$$\text{SS } \boxed{A = \hat{n}(x) [ \epsilon | B = \hat{n}(x) ]} \Rightarrow \text{SCHEM MATH AUTOESTATE DI H}$$

$$\phi(x) = e^{-\frac{\eta}{2} \Delta x^2} e^{+\frac{\eta}{2} \Delta x^2} \Rightarrow \hat{n}(x) = e^{-\frac{\eta}{2} \Delta x^2} e^{+\frac{\eta}{2} \Delta x^2}$$

IN BASES  $|\Sigma_A(R)\rangle$   $\rightarrow \langle \Sigma_B(\omega) | \Sigma_A(R) \rangle = \text{EVOL DI PRODUKT}$

$$i \mathcal{D}^R(\underline{\omega}\omega) = \int_{-\infty}^{\infty} d\omega' \frac{\mathcal{D}(\underline{\omega}\omega)}{\omega - \omega' + i\eta}$$

$$\mathcal{D}(\underline{\omega}\omega) = \int d\omega' \frac{\mathcal{D}(\underline{\omega}\omega')}{\omega - \omega' + i\eta \text{sgn}(\omega)}$$

FACENDO COSTO  $\mathcal{D}(K\omega) \in \mathbb{R}$

$$\text{OSSO } \frac{1}{\omega - \omega' + i\eta} = \frac{1}{\omega - \omega'} + \frac{\pi}{\omega} \delta(\omega - \omega') \Rightarrow \mathcal{D}(\underline{\omega}\omega) = \int d\omega' \frac{\mathcal{D}(\omega\omega')}{\omega - \omega'} - \frac{\pi}{\omega} \mathcal{D}(K\omega)$$

$$\mathcal{D}(\underline{\omega}\omega) = \int d\omega' \frac{\mathcal{D}(\omega\omega')}{\omega - \omega'} - \frac{\pi}{\omega} \text{sgn}(\omega) \mathcal{D}(K\omega)$$

$\rightarrow \mathcal{D}(K\omega) \in \mathbb{R}$

$$\text{HO CHE } \text{Re } \mathcal{D}(K\omega) = \text{Re } \mathcal{D}(K\omega) \quad \& \quad \text{Im } \mathcal{D}(K\omega) = \overline{\text{Im } \mathcal{D}(K\omega)} \text{sgn}(\omega)$$

OCCORRENZA DI PLASMA E' SPERAT SU SOL

$\Rightarrow$  E' INFUSION DI CO ACCORDI PONENDO EN MULTIPLO DI UNA COSTA QUANTITA'

$\rightarrow$  POSSO ED ESTRASS METRICO  $\Rightarrow$  EN PIANO X ATTUAZ DI OSCILLAZ CONDUTTIVITA' NEI METRI

SE UN OMNIBUS CON SGNS

$$\omega_p = \frac{4\pi e^2}{m} n \rightarrow \omega_p \text{ NKEV} > E_F$$

$\hookrightarrow$  INSHP DA L  $\Rightarrow$  PROBLEMA CHIUSURA X SISTOL

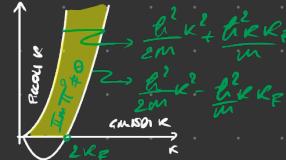
$$S\eta(x,t) = \int \frac{dx K}{(2\pi)^3} \frac{d\omega}{2\pi} e^{iKx - \omega t} \frac{iKx - \omega t}{\pi^2 \mathcal{D}(\underline{\omega}\omega)} \phi(\underline{\omega}\omega)$$

$$\underline{\pi}(\underline{\omega}\omega) = \frac{\underline{\pi}^*}{1 - 8(K) \underline{\pi}(\underline{\omega}\omega)} \quad \omega_{\text{POLL}} = 2\pi \text{ FONTE DISTORSIONE} \quad \mathcal{E}(\underline{\omega}\omega) = 1 - 8(K) \underline{\pi}(\underline{\omega}\omega)$$

$$\Rightarrow \mathcal{E}^R(\underline{\omega}\omega) = 1 - 8(K) \underline{\pi}^R(\underline{\omega}\omega)$$

$$\begin{aligned}
 Q &= 1 - \delta(\underline{\omega}) \operatorname{Re} \tilde{\Pi}^*(\underline{\omega} \omega_1(\underline{\omega})) \\
 \omega_2(\underline{\omega}) &= \frac{\overline{\Pi^m \Pi^*(\underline{\omega} \omega_2(\underline{\omega}))}}{\frac{\partial}{\partial \omega} \operatorname{Re} \tilde{\Pi}^*(\underline{\omega} \omega)} \Big|_{\omega_1(\underline{\omega})} \\
 \Rightarrow \tilde{\Pi}(\underline{\omega}) &= \frac{\mathcal{Z}(\underline{\omega})}{\omega - [\omega_1(\underline{\omega}) + i\omega_2(\underline{\omega})]} + \frac{\text{LOSS}}{\Pi(\underline{\omega})} \rightarrow \text{CONTINUEDO ROLLO} \\
 \text{TRIVATO IL ROLLO INFERIORE} \quad \tilde{\Pi}^*(\underline{\omega}) &= \int \frac{d\underline{\omega}}{(2\pi)^3} \mathcal{Z}(\underline{\omega}) e^{-i\underline{\omega} \underline{x}} \int_{\pm\infty} \frac{d\omega}{2\pi} \frac{e^{-i\omega t}}{\omega - \omega_1 - i\omega_2} \phi(\omega) \\
 &\rightarrow \omega_2 < 0 \rightarrow \text{TRACCE INFERIORI} \quad \text{di OCCASIONE}
 \end{aligned}$$

Caso Coolidge,  $\text{APPROX } \bar{\pi} = \bar{\pi}^k \rightarrow$  x versos a cada moto constante no 2 regiões em que  $\bar{\pi}^k \bar{\pi} = 0$



$$I = \frac{C\pi e^2}{K^2} \frac{2}{t_1} \int_{(2\pi)^3} dq \Theta(K_F q) \left[ \frac{1}{\omega - \frac{E_q^0}{\hbar} - \frac{E_{q+K}}{\hbar}} - \frac{1}{\omega - \frac{E_q^0}{\hbar} + \frac{E_{q+K}}{\hbar}} \right] = \frac{C\pi e^2}{K^2} \frac{2}{t_1} \int_{(2\pi)^3} dq \Theta(K_F q) \frac{2(E_q^0 - E_{q+K}^0)}{\omega^2 - \left(\frac{E_q^0 - E_{q+K}^0}{\hbar}\right)^2} = \text{Solid Geom}$$

$$= \frac{q\pi e^2}{K^2} \frac{2}{\alpha} \left\{ \frac{dq}{(2\pi)^3} \Theta(K_F - q) 2 \left( \frac{\hbar^2 K^2}{2m} + \frac{\hbar K q}{m} \right) \left[ 1 + \left( \frac{\hbar^2 K^2}{2m} + \frac{\hbar K q}{m} \right)^2 \right]^{1/2} \right\} \quad \text{and so } \Theta \Rightarrow \Theta_K \oplus \text{constant}$$

$$\Rightarrow \underline{1} = \frac{4\pi e^2}{K^2 \omega^2} \frac{4}{\hbar} \int_{(2\pi)^3} \frac{dq}{\partial(K_F - q)} \left[ \left( \frac{\hbar K^2}{2m} + \frac{\hbar K q}{m} \right) + \frac{1}{\omega^2} \left( \frac{\hbar K^2}{2m} + \frac{\hbar K q}{m} \right)^2 + \dots \right] \rightarrow \text{minimize Coulomb} = R^2 \text{ in term to cancel out terms} \rightarrow \text{ACM} \times \delta S \text{ for cost profile}$$

$$I = \frac{4\pi e^2}{\omega^2} \frac{4}{\hbar} \frac{\hbar}{2m} \left\{ \frac{1}{(2\pi)^3} \int \frac{ds q}{\hbar} \delta(K_F q) + \frac{4\pi e^2}{K^2 \omega^2} \frac{\hbar}{\hbar \omega^2} \int \frac{ds q}{(2\pi)^3} \delta(K_F - q) \right\} \left[ \left( \frac{\hbar K^2}{2m} \right)^3 + 3 \left( \frac{\hbar K^2}{2m} \right)^2 \frac{\hbar K q}{m} + 3 \left( \frac{\hbar K^2}{2m} \right) \left( \frac{\hbar K q}{m} \right)^2 + \left( \frac{\hbar K q}{m} \right)^3 \right] + \dots$$

K ACCORDE POC GRANDE  
 E INCONTRABILE

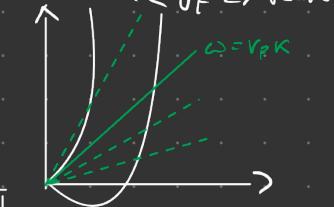
$$\Rightarrow I = \frac{4\pi e^2}{m\omega^2} n + \frac{4\pi e^2}{K^2 \omega^4} \leq \int \frac{ds q}{(2\pi)^3} \Theta(K - q) 3 \left( \frac{\pi K^2}{2m} \right) \left( \frac{\pi}{m} \right)^2 K_q K_j q_j \varphi_j$$

$$\rightarrow \text{Harmonic motion for outer particle}$$

$$25(R) = 25(0) + \dots \Rightarrow \omega^2 = \text{constant} R^{-2}$$

$$\rightarrow \text{Log-log graph} = \text{straight line}$$

$$\left. \begin{array}{l} > V_F \Rightarrow \text{OVS} \\ < V_F \Rightarrow \text{NON CO VSO} \end{array} \right\} \text{INTEN. CONC.}$$



$$\text{THE CANONICAL CONSEQUENCES OF COMPOSITION ARE}$$

$$x' = U^t x U \quad p' = U^t p U \quad S' = U^t S U$$

$$\rightarrow [x_i, p_j] = [x_i^!, p_j^!] = i \hbar \epsilon_{ij} \quad [s_i, s_j] = [s_i^!, s_j^!] = -i \hbar \epsilon_{ijk} s_k$$

ES IX, S INVAN

$$x' = x, \quad S' = S, \quad P'_i Q = [P_i - i\theta \left( O_2, 0 \right)] / Q$$

X AVENS IN VAN LOC INTRODUCO. TIE P-AI DESVULTA  
CONVIVANTE

$$= \overline{n_i} + A_i - \overset{\circ}{\text{th}} \overset{+}{\text{O}} \overset{+}{\text{O}} \overset{-}{\text{O}} - A_i^! \rightarrow \text{impres} \times \overline{n_i} = \overline{n_i}^! \times \text{loc}$$

$$\Rightarrow A_i = f_i - \hat{f}_i(\cup^+ \cup^-)$$

$$[\pi_i, \overline{ag}] = [p_i A_i, p_{\overline{g}} A_{\overline{g}}] = -i\theta D_{\overline{g}} + i\theta D_g A_i + I A_i A_{\overline{g}}$$

INVAL X PASSO GLOBAIS  $\rightarrow$  SUMA  $O(1)$   $q^i = e^{iX} q^i$   
 SE PASSO A SUMA  $O(1)_{loc}$   $q^i(x) = e^{-iX(x)} q^i(x)$  INCON LA FISICA NON È INVARIANTE COSE DIVERSI PASSAGGI DA  $p_i$  A  $\tilde{p}_i$   
 $O \in O(1)_{loc}$  E  $O = e^{-iX(x)}$   $\Rightarrow A_i(x) = A_i - \text{grad}_i X(x)$

SOPRASSOGLIO ALGUNA TUTTA CHE MI INTRODUCCE UNA RIVAR X DISTANZA  $\varphi(x) = U\psi(x)$ ,  $U \in SO(N)$   
 → IMPONENDO IN UN LOC.  $A_\mu^i = A_\mu - \frac{1}{2} \epsilon_{ijk} \partial_k \varphi_i \rightarrow$  MATER  $\in SO(N)$  CHE DIPENDE X  
 HERMITIANA  $\partial^\mu \varphi_i = 0$

LIVELLI DI CANTO FISSI SINCS. PARTEC.  $\dot{h} = \frac{f^2}{2m} \rightarrow e^{-i\omega t}$  IN CAMPO ELETTRICO  $\frac{1}{2m}(\vec{p} + \frac{e}{c}\vec{A})^2 = \frac{1}{2}m\omega^2 \rightarrow \underline{\underline{e}} = \frac{\omega}{c} = \frac{f + \frac{e}{c}\vec{A}}{m}$

PRESO  $\underline{\underline{e}} = \frac{1}{2}\hat{z} \rightarrow$  UBERTÀ' DI SEZIONE  $A \rightarrow \underline{\underline{A}} = (A_x, A_y, 0)^T$

$$\underline{B} = \begin{pmatrix} \hat{i} & \hat{j} & \hat{k} \\ \partial_x & \partial_y & \partial_z \end{pmatrix} \rightarrow B_x = \partial_x A_y - \partial_y A_x \rightarrow \text{curl } \underline{A} \neq$$

so Be ONE A meno di trenta minuti diventano I i canzoni che

$$\hat{Y} = \left( \frac{\partial Y}{\partial T} \right)^{-1} \hat{T} + \left( \frac{\partial Y}{\partial \sigma} \right)^{-1} \left[ \sigma_0 \right]^{0.5}$$

$$\text{DEF } \hat{P} = \mathcal{E}_x \left( \sqrt{\frac{eB_0}{mc}} t \right)^{-\frac{1}{2}}, \quad \hat{Q} = \mathcal{E}_y \left( \sqrt{\frac{eB_0}{mc}} t \right)^{\frac{1}{2}} \rightarrow [P, Q] = -i\hbar \Rightarrow \text{RAMANUJAN} \quad \frac{1}{2} m (\hat{P}_x^2 + \hat{Q}_y^2) + \frac{P_e^2}{2m} = \frac{1}{2} m \frac{eB_0 t}{mc} (\hat{P}_x^2 + \hat{Q}_y^2) + \frac{P_e^2}{2m} = \hbar \omega_c \left( \frac{\hat{P}_x^2 + \hat{Q}_y^2}{2} \right) + \frac{P_e^2}{2m} \rightarrow \text{TERMINA CHIOTICO IN 2 \oplus OSCILLATIONS AROUND EIGEN } n + \frac{1}{2} \Rightarrow \text{SPETTO OSCILLATIVO TRASLATO IN 2}$$

PARTICLES IN BOX → CONSERVATION  $p_x, p_y, p_z \rightarrow$  A POINT IN 3D. XES CAUSE OF gde. DIFFUSION.  $p_x \in$

ACCORDO CONTI LANDAO S VEDEROS I MIGLI SCORSI DI A X SU NOSTRA → 2 STD ① GANZE LANDAO  $\vec{A}_1 = \begin{pmatrix} 0 \\ xB \\ 0 \end{pmatrix}$  → PUNTA A PONTE A HOKKIMA 2.000CA

$$\text{② GAUGS SIMMETRICO} \quad \vec{A}_S = \begin{pmatrix} -\frac{eB}{2} \\ \frac{eB}{2} \\ 0 \end{pmatrix} \rightarrow \text{NAMURA XES' COORD CILINDRICAS}$$

$$\text{SPEED OF LIGHT CAN'T FOND } [hK] = \left[ \frac{eB}{c} \right] \quad \left( K = \frac{1}{L} \right) \Rightarrow L^2 = \frac{hc}{eB} \rightarrow \text{RISKO } S =$$

$$\Rightarrow \text{EQ AUTOVAL INS. } \frac{1}{2m} \left( -\frac{\hbar^2}{L^2} \frac{d^2}{ds^2} + \frac{\hbar^2}{L^2} (s + k_f L)^2 \right) a(s) = E a(s) \Rightarrow -\frac{d''}{2} + (s + k_f L)^2 \frac{a}{s} = \left( \frac{m_L^2}{\hbar^2} \right) a E = \frac{E}{\hbar^2 m} a \quad \text{DEMO CACOCAMUS ESTA MANSIZZIA}$$

→ SINTA POSSIBILITÀ: È NON È OVVIAMENTE UNA CONFINATO XSE IN UNA BARRIERA → GEOM  
  
 SE SIAMO CONTANTI DAI BORDI ⇒ SOL  $e^{\frac{i}{\hbar} \sqrt{E - V_0} x}$  Hn(x) → STIMMA  $\frac{m}{\hbar^2} \frac{\partial^2 C}{\partial x^2}$   
 CENTRALIZZATE IN  $-V_0$  CON OSCILLAZIONI SULLA L E AUTONAL  $\theta \omega_L \left( \frac{n+1}{2} \right)$   
 $L = \frac{2,56 \text{ nm}}{\sqrt{B - V_0}}$  → SCALA MICHA. ESSI DECIDONO AUTOFUNZ  $\Rightarrow$  A DIST L DAL BORDO NON AVESSENTE L'ESTERNO

⇒ NSC BDK CIV CANDAO. 800 EPA BAKI → DESARROLLO ANM → APLICANDO AL BANCO ESTADO DE PANTAS

+ MIRAMICINO AL BAGNO + SINNACREA LA PANEBOGLIA → CLASSICO AL CENTRO COMUNALE ROMA, AL BAGNO UNA SALSINA CON IL CACIO E' CONSOLO

→ QUANTO SONO DEGNAZI I CV DI CAVADAS NSC BULK?   $\frac{L \times Lg B}{\phi_0}$  EQUAZIONE DIP DA A -

$$= \frac{1}{A=0} + \frac{e}{c} \int dx \underline{J}(x) \underline{A}(xt) + \frac{e^2}{2mc^2} \int dx \underline{A}^2(xt) \hat{n}(x) \rightarrow \text{IS SQ CONTRADICT X PLAS POSSIE SEMENGE QDSEIA COMENTS IN PNOB IN ASENZA DI } \vec{A} \rightarrow \text{IS } \vec{S} + p_m$$

(10) è di conseguenza

$$N_{H_A}(x) = e^{\frac{i}{\hbar} H_A t} \hat{N}(x) e^{-\frac{i}{\hbar} H_A t} \rightarrow -\frac{i}{\hbar} \frac{\partial}{\partial t} N_{H_A}(x) = e^{\frac{i}{\hbar} H_A t} [H_A, \hat{N}(x)] e^{-\frac{i}{\hbar} H_A t}$$

$\hookrightarrow$  NON COMMUTATIVITÄT

$[\hat{N}, \hat{C}] = 0 \Rightarrow$  ANSTEIGA NON COMMUTA  $\rightarrow$  DEF  $\hat{P}(x) = -e^{\frac{i}{\hbar} H(x)} \hat{N}(x) e^{-\frac{i}{\hbar} H(x)}$  DEGENERATION

## Risposta: Undine

ACORDOS A A ON ESTE TEMPO E PRIMA ESSO AS IAS) DA H<sub>A=0</sub> N → ALVO E

$$\langle \psi(t) | \int e^{(x t)} |\psi(t)\rangle = (\text{cos}) \int e^{(x t)} (\text{cos}) + \frac{1}{\varphi \pi} \int dt' \delta(t-t') (\text{cos}) \int \left[ \int e^{(x t)}, V_{\Delta x \otimes} \right] (\text{cos})$$

$$\underline{J} = e \underline{J} - \frac{e^2}{mc^2} \hat{n} A(\underline{x}, t) = -\frac{e^2}{mc^2} n(\underline{x}) A_l(\underline{x}, t) + \frac{1}{i\hbar} \frac{e}{c} \int dt' d\underline{x}' \delta(t-t') \langle \text{as} | \left[ \underline{J}_e(\underline{x}, t), \int_m (\underline{x}', t') \right] | \text{GS} \rangle A_m(\underline{x}', t')$$

OSSERVAZIONE: Dopo aver preso in considerazione la quantizzazione delle forme di campo, si trova che l'equazione di Maxwell diventa

NSL GS  $\int u \left(\frac{1}{x}\right) dx = 0$  ma il II term no

→ Voglio ~~no~~ e and in A  $\Rightarrow$  NSD committments 080 8020

$$\oint_{\ell} (\underline{x} \cdot \underline{t}) = -\frac{e}{mc^2} \int_{as} \underline{n}(\underline{x}) A_\ell(\underline{x} \cdot \underline{t}) - \frac{e^2}{\hbar} \int dt' ds \underline{x}' \sum_{lm}^{RET} (\underline{x} \cdot \underline{x}') A_m(\underline{x}' \cdot \underline{t}')$$

$$D_{lm}^{RST}(x) = \theta(t-t') \langle \text{gs} | \left[ J_l(x), J_m(x') \right] \rangle \text{gs} \quad \text{PARA LOS DOS FERMIONES} \rightarrow \text{CONSTANTE DONDE } l=1$$

$$\text{so faccio tando } \mathcal{D}_{\text{em}}^T(xx') = \langle \mathcal{G}_S | T S_f^{(x)} S_f^{(x')} | \mathcal{G}_S \rangle \rightarrow \text{modulo}$$

$$J_e(x) = \int d\tau' d_3 x' \left[ -\frac{e^2}{mc} n(x') S_{em} S_\sigma(x-x') \delta(\tau-\tau') - \frac{e^2}{m c} \partial_{em}^{RET}(x, x', \tau') \right] A_m(x', \tau') \quad \text{a not intusessa compo } \underline{\underline{\epsilon}} \rightarrow \frac{1}{c} \frac{\partial A_e}{\partial t} = E_e \xrightarrow{\text{SWS}} \frac{i\omega}{c} A_e(x, \omega) = E_e(x, \omega) \quad \begin{matrix} \text{Posso mesclar os} \\ \text{j lin in } \underline{\underline{\epsilon}} \Rightarrow \text{tensos} \\ \text{constitui} \end{matrix}$$

$$\int e(\underline{x}\omega) = \int d\underline{x}' \sigma_{em}(\underline{x}\underline{x}'\omega) E_m(\underline{x}'\omega) \text{ leaves down (no invariance)} \text{ and } \sigma_{em}(\underline{x}\underline{x}'\omega) = \frac{e^2}{2m\omega} n(\underline{x}) \delta_{em} \delta(\underline{x}-\underline{x}') + \frac{e^2}{8\pi\omega} D_{em}^{ROT}(\underline{x}\underline{x}'\omega)$$

ss IN VAK X TABLAZ  $\delta_e(\omega) = \sigma_{em}(\omega) E_m(\omega) \rightarrow D_{em} \times \text{losses em sban} \rightarrow \text{moxco continua sban}$

ESAME D'ESE

$$H_E = H - e \int d_3x' n(x) \int d_3x' p_{\text{ext}}(x|t') \quad \Rightarrow \text{INTERAzione DENSITÀ e INTESA - SXT} \quad \Rightarrow \text{TA NEUTRALE CONSEGUENZA}$$

$$\delta n(x,t) = \frac{1}{a} \int d_3x' dt' \mathcal{D}(x,t|x'|t') (-e) \int d_3x'' p_{\text{ext}}(x''|t'') \phi(x'|t')$$

$$p_{\text{ind}}(x,t) = \frac{1}{a} \int d_3x' dt' \mathcal{D}(x,t|x'|t') \int d_3x'' dt'' \frac{\partial^2}{\partial t'^2} \delta(t'-t'') p_{\text{ext}}(x''|t'') = \int d_3x' \frac{R}{\pi(x')} \int d_3x'' O^0(x'|x'') p_{\text{ext}}(x'') \rightarrow \text{SOMMA DENSITÀ - DENSITÀ}$$

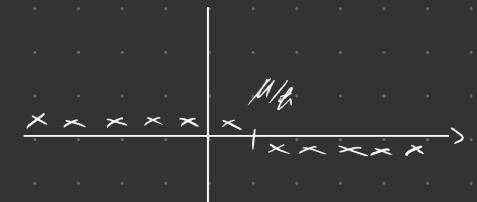
$$\boxed{J_E = 4\pi (p_{\text{ext}} p_{\text{ind}})}$$

$$\text{EWSR (INVERSE SPL-SPL)} \Rightarrow \text{RE}(R\omega) = \pi \left[ 1 + R^*(K\omega) S(K\omega) \right] \left( \frac{S_{\text{ext}}(K\omega)}{E_{\text{ext}}(K\omega)} \right) \rightarrow \text{SO MONO & SYM GEN} \rightarrow \text{NO ROTATION} \rightarrow \text{SPP (SOMOHA)} \\ \text{RE} D = \text{GAP}_{\text{SPL}} \Rightarrow \text{COMP } R \rightarrow \Rightarrow D \propto R \Rightarrow D \propto E \bar{E} \quad \text{RES X WAVE NUMBER ANALOGY}$$

## QUADRO PARTICOLARE

ENVELOPE COMUNE PROPAGAZIONE  $G_{\mu\mu}(\underline{x}, \underline{x}', \omega) = \sum_n \frac{\langle \underline{E}_n^N | \underline{q}_{\mu}(\underline{x}) | \sum_{n'} \underline{E}_{n'}^{N+1} \underline{q}_{\mu}^+(\underline{x}') | \underline{\delta}\omega^N \rangle}{\omega - \frac{1}{\hbar} (\mu + \underline{E}_n^{N+1}) + i\eta} + \frac{\langle \underline{E}_n^N | \underline{q}_{\mu}^+(\underline{x}') | \sum_{n'} \underline{E}_{n'}^{N+1} \underline{q}_{\mu}(\underline{x}) | \underline{\delta}\omega^N \rangle}{\omega - \frac{1}{\hbar} (\mu - \underline{E}_n^{N+1}) - i\eta}$

SE  $\omega \rightarrow \pm \infty \Rightarrow G = \frac{1}{\omega} \sum_n \left( \frac{\langle \underline{E}_n^N | \underline{q}_{\mu}(\underline{x}) | \underline{q}_{\mu}^+(\underline{x}') | \underline{\delta}\omega^N \rangle}{\omega - \frac{1}{\hbar} (\mu + \underline{E}_n^{N+1}) + i\eta} + \frac{\langle \underline{E}_n^N | \underline{q}_{\mu}^+(\underline{x}') | \underline{q}_{\mu}(\underline{x}) | \underline{\delta}\omega^N \rangle}{\omega - \frac{1}{\hbar} (\mu - \underline{E}_n^{N+1}) - i\eta} \right)$  + correction



$$= \frac{1}{\omega} \langle \underline{E}_k^N | \underline{q}_{\mu}(\underline{x}), \underline{q}_{\mu}^+(\underline{x}') | \underline{\delta}\omega^N \rangle = \frac{1}{\omega} S_{\mu\mu} \delta(\underline{x} - \underline{x}') \rightarrow \text{SE OTTO CONSIDERARSI X TASSO DI SPIN} \quad G(\underline{k}\omega) = S_{\mu\mu} G(\underline{k}\omega)$$

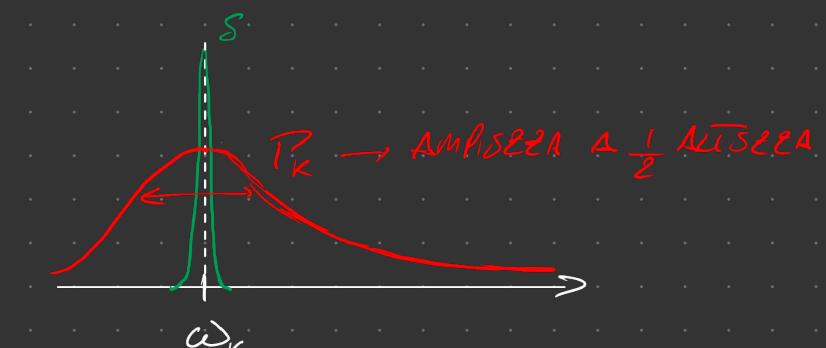
$$\Rightarrow G(\underline{k}\omega) = \int \frac{d\omega' A(\underline{k}\omega')}{\omega - \omega' + i\eta \operatorname{sgn}(\omega - \frac{\mu}{\hbar})} \rightarrow \begin{cases} A(\underline{k}\omega) \geq 0 \\ \int_{-\infty}^{\omega} d\omega' A(\underline{k}\omega') = 1 \end{cases} \rightarrow \text{SEMPLICE SOVRAPP CON DUE MIE DI PESO DI PROBABILITÀ DI PARTECIPAZIONE}$$

## CASE ESEMPLIFICATI [PESO PARTICOLARE]

$$A(\underline{k}\omega) = \delta\left(\omega - \frac{\epsilon_0(\underline{k})}{\hbar}\right) \rightarrow \delta \text{ CONFERMA SU LOCALISAZIONE DI PESO PARTCOLARE} \Rightarrow \text{PROBABILITÀ}$$

SE PRO INSTEADO  $\Rightarrow$  SE AVERGAGE S  $\rightarrow$  APPROX CONSIDERAZIONE

$$A(\underline{k}\omega) = \frac{P_k}{\pi} \frac{1}{(\omega - \omega_k)^2 + P_k^2} \xrightarrow{P_k \rightarrow 0} A^0 \Rightarrow G(\underline{k}\omega) = \frac{1}{\omega - \omega_k + i P_k \operatorname{sgn}(\omega - \frac{\mu}{\hbar})}$$



$\Pi(\underline{k}) = \# \text{ OCCURENZE STATO } k \rightarrow$  CALCOLARE DA  
DECAY

$\rightarrow$  AMPLIAZIONE: CASO DI UNICO PESO MOLTIPLICATO PER DECAY TRAMO CONTO X AMPLIAMENTO

$$G(\underline{k}\omega) = \int_{-\infty}^{\omega} \frac{d\omega' A(\underline{k}\omega')}{\omega - \omega'} - i\pi A(\underline{k}\omega) \operatorname{sgn}(\omega - \frac{\mu}{\hbar})$$

$$G(\underline{k}\omega) = \frac{1}{\omega - \omega_k + i P_k \operatorname{sgn}(\omega - \frac{\mu}{\hbar})} \rightarrow 1 \text{ PESO} \rightarrow \text{CASO QUANDO FACCIO TASSO FORMULARE ZERDO PESO} \\ \Rightarrow 1 \text{ PESO CASO NO} \rightarrow \text{TASSO DI SPIN}$$

$$\text{IM } G \text{ CAMBIA } \operatorname{sgn} \frac{\mu}{\hbar} \left\{ \begin{array}{l} < 0 \quad \omega > \mu/\hbar \\ > 0 \quad \omega < \mu/\hbar \end{array} \right. \rightarrow \omega \text{ IN } \omega = \mu/\hbar$$

$$\exists \text{ ALTRA DIFERENZA DI } G \rightarrow G(\underline{k}\omega) = \frac{1}{\omega - \frac{\epsilon_0(\underline{k})}{\hbar} - \Sigma^*(\underline{k}\omega)} \text{ SE OGNI} \rightarrow \text{SERIAO} \times \omega \text{ DI PESO DI IM} = \frac{1}{(\omega - \frac{\epsilon_0(\underline{k})}{\hbar} - \operatorname{Re} \Sigma^*) - i \text{ IM } \Sigma^*}$$

$$\Rightarrow \text{IM } G(\underline{k}\omega) = \frac{\text{IM } \Sigma^*(\underline{k}\omega)}{\left[ \omega - \frac{\epsilon_0(\underline{k})}{\hbar} - \operatorname{Re} \Sigma^* \right]^2 + \text{IM } \Sigma^{*2}} \rightarrow \text{O} \text{ IL} \omega = \frac{\mu}{\hbar} \text{ E} \Sigma^* = 0 \Rightarrow \text{SENZA PESO DI IM} \text{ MA} \Sigma^* \neq 0$$

$$\rightarrow \omega \text{ SE } \omega \text{ È DI SPIN FORMA } k \text{ T.C. } \frac{\mu}{\hbar} - \frac{\epsilon_0(\underline{k})}{\hbar} - \Sigma^*(\underline{k}\omega) = 0$$

$$\text{PER } [\text{CONSIDERAZIONE} - \text{CASE}] \text{ IL PESO DELL'UNICO SPIN FORMA È PESO DI SPIN} \times \text{NO } 1/2 \quad \int \frac{dK}{(2\pi)^3} \theta(G(\underline{k}, \frac{\mu}{\hbar})) = \hat{N} \quad \text{IM } \Sigma^*(\underline{k}\omega) = 0$$

CONSIDERAZIONI SE HEG D'UNO CAMPIONE  $\Rightarrow$  SUL HEL  $\rightarrow$  SPETTRI (WAVEFUNCTION) IL VAL  $\frac{4\pi}{3} K_F^3$  MANTIENE UNA ACCORDANZA INTEGRALE  
 $\rightarrow$  CON CAMPIONE EGGS ANCHE ISOMORFO MA I NODI SONO ANCHE DISTINZIONI IN SUL

$$G(\underline{\omega}, \omega) = \frac{1}{\omega - \frac{\epsilon_0(\underline{\omega})}{\hbar} - \Sigma^*(\underline{\omega}, \omega)} \quad \text{UNA QUASIPARTICELLA DEVE DECEDERE DAL FONDO DEL PROBLEMA} \rightarrow \omega - \frac{\epsilon_0(\underline{\omega})}{\hbar} - \Sigma^*(\underline{\omega}, \omega) = 0 \quad \text{CON} \omega(\underline{\omega}) = \omega(\underline{\omega}) + i\frac{\hbar}{2} \Sigma^*(\underline{\omega}, \omega)$$

$$\Rightarrow G \text{ FONDO DI L'ATTRAZIONE} \quad G(\underline{\omega}, \omega) = \frac{\epsilon(\underline{\omega})}{\omega - \omega_{p0}(\underline{\omega})} + G^{RSG}(\underline{\omega}, \omega) \quad \hookrightarrow \text{ANALITICA}$$

$\hookrightarrow$  ASSUMIGLI A QUASI LA UNA PARTICELLA MA CON PIÙ IMMAGINI FINITE  $\omega_2 \Rightarrow$  ROBA CHE NON C'È

È COME SE DA POCHE SPECTRALI AVESSEMO ESTENDO S DAVANTI A  $\epsilon(\underline{\omega}) \leq 1$   $\Rightarrow$  SE  $\epsilon(\underline{\omega}) > 1$  ALLORA  $\omega_2$

$$\omega_1 + i\omega_2 - \frac{\epsilon_0(\underline{\omega})}{\hbar} - \Sigma^*(\underline{\omega}, \omega_1 + i\omega_2) = 0 \quad \omega_2 = (\text{VITA PARTICELLA})^{-1} \Rightarrow \text{O VOGNO PICCOLO} \rightarrow Q = \omega_1 + i\omega_2 - \frac{\epsilon_0(\underline{\omega})}{\hbar} - \Sigma^*(\underline{\omega}, \omega_1) - i\omega_2 \frac{\partial \Sigma^*}{\partial \omega} \Big|_{\omega_1}$$

$$\text{ET TIRI} \quad Q = \omega_1(\underline{\omega}) - \frac{\epsilon_0(\underline{\omega})}{\hbar} - \text{Re} \Sigma^*(\underline{\omega}, \omega_1(\underline{\omega}))$$

$$\text{ET IMMAGINE} \quad Q = \omega_2(\underline{\omega}) - \text{Im} \Sigma^*(\underline{\omega}, \omega_1(\underline{\omega})) - \omega_2(\underline{\omega}) \frac{\partial \text{Re} \Sigma^*}{\partial \omega} \Big|_{\omega=\omega_1} \Rightarrow \omega_2 = \frac{\text{Im} \Sigma^*(\underline{\omega}, \omega_1(\underline{\omega}))}{1 - \frac{\partial \text{Re} \Sigma^*}{\partial \omega} \Big|_{\omega_1(\underline{\omega})}} \quad \text{ZQ DAVIS IMMAGINE} \Rightarrow \text{SE SUL PONTE}$$

$$\epsilon(\underline{\omega}) = \lim_{\omega \rightarrow \omega_{p0}} G(\underline{\omega}, \omega) / (\omega - \omega_{p0}) = \lim_{\omega \rightarrow \omega_{p0}} \frac{\omega - \omega_{p0}}{\omega - \frac{\epsilon_0(\underline{\omega})}{\hbar} - \Sigma^*(\underline{\omega}, \omega)}$$

QUASI PARTICELLA = FOGLIO SIMPLICE

$$\omega_{\text{TIME}} \rightarrow \lim_{\omega \rightarrow \omega_1} \frac{\omega - \omega_1}{(\omega - \omega_1) \left[ 1 - \frac{\partial \text{Re} \Sigma^*}{\partial \omega} \Big|_{\omega_1} \right]} = \frac{1}{1 - \frac{\partial \text{Re} \Sigma^*}{\partial \omega} \Big|_{\omega_1}} \Rightarrow \omega_2 = \epsilon(\underline{\omega}) \text{IMAGINE} \Sigma^*(\underline{\omega}, \omega_1)$$

DI G CON PESO  $\epsilon(\underline{\omega})$

IN QUANTITÀ 1 È VIVENTE IN

REGIONS DI R VIANO SUP

$\rightarrow$  IN PESO DI QP A SUL PONTE È DISCONTINUITÀ DEL # OCCUPAZ (COME SPETTRO IN  $\omega$  X )  
 $\rightarrow$  # OCCUPAZ 1 IN 10000

DI PESO ( $\omega_2$  ACCORDO)

TEORIA DI MIGDAL SUL PONTE SI' SUL DI ASC X # OCCUPAZ  $N(\underline{\omega}) = \langle GS | Q_{B^+}^+ Q_{B^-} | GS \rangle$

$$\rightarrow \text{SUL PONTE VERA A PRESSIONE DELL'QP} \quad N(\underline{\omega}) = \sum_m \langle GS | Q_{B^+}^+ Q_{B^-} | GS \rangle = \int_{-\infty}^{\omega} \frac{d\omega}{2\pi i} G(\underline{\omega}, \omega) e^{i\omega \eta} = \int_{-\infty}^{\omega} \frac{d\omega}{2\pi i} \frac{\epsilon(\underline{\omega})}{\omega - \omega - i\omega} e^{i\omega \eta} + N(\underline{\omega}) = N(\underline{\omega}) + \epsilon(\underline{\omega}) \theta \left( \frac{\omega}{\hbar} - \omega_1(\underline{\omega}) \right)$$

$\Rightarrow$  IL PESO DELL'QP È  $\text{Re} \omega_1 \pm \text{Im} \omega_1$  ACCORDO CON L'INTUIZIONE

$$G(\underline{\omega}, \omega) = \int_{-\infty}^{\omega} \frac{d\omega}{2\pi} e^{i\omega \eta} \left( \frac{\epsilon(\underline{\omega})}{\omega - \omega_p} + G(\underline{\omega}, \omega) \right) \quad \omega > \omega_p \Rightarrow \int_{-\infty}^{\omega} \frac{d\omega}{2\pi} e^{i\omega \eta} \frac{-\frac{\hbar}{2\pi} i\epsilon(\omega(\underline{\omega})) + i\omega_1(\underline{\omega})}{\omega - \omega_p} = \int_{-\infty}^{\omega} \frac{d\omega}{2\pi} e^{i\omega \eta} \frac{\epsilon(\omega(\underline{\omega}))}{\omega - \omega_p}$$

INTERPRETAZIONE:  $\omega_1$  È STIMA DI UNA DISPERSIONE  $\rightarrow \epsilon(\omega) - \hbar\omega(\omega) \times$  AMMAGNA EVOLUZIONE TEMPORALE

→ QUASI PARITY = MANIFESTAZ. CONTINUA DELL'ATTRAZIONE AL MINDSTRETCHING → SISTEMA CHIMICO DI  $e^-$  MA ≠ MASSA. S'ESSENTE DUELLA SCHEDE ENERGETICHE.

LE PARTIC SOLO IN DISTANZA  $\Rightarrow$  EFF COORDINATO  $\rightarrow$  PROPAGAZ DI TUTTI I L'INSIGNS POMANTI IN DEDENZA DA CONSUMO DI FORZA  $\Rightarrow$  QP

$$\Rightarrow x \text{ AND } \omega_1 = \frac{\partial \omega_1}{\partial K} = \frac{t K_F}{m^*} \rightarrow \text{massa effettiva} \rightarrow \text{se non possiamo uscire} \Rightarrow m^* \neq t K_F \rightarrow \omega_1(K) - \underline{\omega_0(K)} - \sum^* (\underline{K} \omega_1(K)) = 0 \text{ (condizionale forza)}$$

$$\rightarrow \text{SUSCOPPO} \quad \omega_1(K_F) + \frac{\hbar K_F}{m^*} - \frac{E_0(K_F)}{\hbar} - \frac{\hbar}{m} K_F (K - K_F) - \sum_{\mathbf{k}}^* (K_F \omega_1(K_F)) - \frac{\partial \sum_{\mathbf{k}}^*}{\partial K} (K - K_F) - \frac{\partial \sum_{\mathbf{k}}^*}{\partial \omega} \frac{\partial \omega_1}{\partial K} (K - K_F) + \dots = 0$$

$\rightarrow$   $\kappa_{\text{DFP}}$  &  $\kappa_{\text{DFP}}$  form a linear system

$$\text{and } Q = \sum_{k=0}^{\infty} K_k \omega_k \rightarrow \frac{1}{m} - \frac{1}{m} - \sum_{k=0}^{\infty} \left( K_k \frac{\partial}{\partial \omega} \right) = 0 \Rightarrow \frac{\partial K_F}{\partial \omega} - \frac{\partial K_F}{\partial m} - \frac{\partial \sum_{k=0}^{\infty} K_k \omega_k}{\partial m} \Big|_{K_F} = 0 \quad 2.$$

→ l'interazione con le cellule non modifica molto la  $m^*$  ma si modifica drasticamente il contenuto di  $e^-$ -fotonini ( $80-100\%$ )

**STOUNDA 2**

\* corzomb in HSG

$$\sum^*(k) = \begin{array}{c} \text{Diagram A} \\ + \end{array} \quad \begin{array}{c} \text{Diagram B} \\ + \end{array}$$

~~NON C'È IN FOG. NERO~~

In  $g = \emptyset$ , this is contained

$$\Rightarrow \phi_{\text{FPA}}(q) = \frac{6\pi e^2}{q^2 - 6\pi e^2 n(q)} \rightarrow \text{A DUVIMINADA} \frac{1}{q^2} \text{ S'ACOMPAGNADA DA} \frac{1}{n(q)}$$

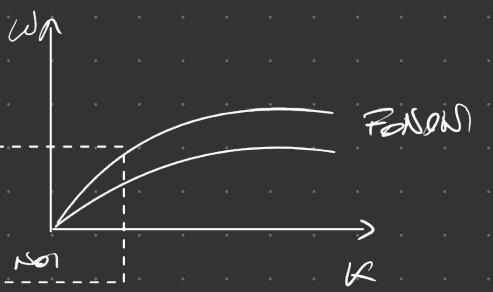
→ Schaduwgaloos fürt ERKENNTNIS DRUGGENZA Log  $\Rightarrow$  Te PORRUBA ac U ORDNS

RESANDO A FOT DE F. E. FERD  
DISTURBIAZ PUSANDO DIAS. ES UNAS PREGONER  
IN OBLI SUCC COMO CONDE RON.

$$\begin{aligned}
 & + \quad \text{Diagram: Two vertical lines with a horizontal wavy line connecting them. The left line has a circle at its top. The right line has two circles at its top. A horizontal arrow points up between the lines. Below the diagram is the expression } -\frac{1}{q^4} \\
 & + \quad \text{Diagram: Similar to the first, but the right line has three circles at its top. Below the diagram is the expression } -\frac{1}{q^6} \\
 = & \quad \text{Diagram: A single vertical line with a horizontal wavy line attached to its left side. Below the diagram is the label RPA} \\
 & = O_{RPA} = O^\circ + O^{\circ\bar{n}\circ\circ} + O^{\circ\bar{n}\circ\circ\bar{n}\circ\circ} + \dots \\
 & + \quad \text{Diagram: Similar to the first, but the right line has four circles at its top. Below the diagram is the expression } -\dots
 \end{aligned}$$

$$\Rightarrow \text{Wavy Line} = \text{mm} + \text{m} \text{ } \textcircled{O} \text{ } \text{mm}$$

BASÍTICA ELASTICITAT (A causa d'una verma TARTÀRA coms més de 80% d'estàncio omes 8 seccions MESTRENTADA SSI R plecs ( $\Rightarrow$  SERRA PASSO) NOTICORANS



PUMA CANT MEET CONDITION  $\rightarrow$  FOR GENERALIZED SCALAR PROB  $\rightarrow$  VARIOUS TENSORS STRESS THAT A CANNOT BE DEFORMATIONS

METEO CONSTANTE  $\rightarrow$  APPLICA DISPREMULZIONE CON  $\alpha(x)$  PIAZZA E PIACERE CADUTA (VACCINO DELL'OCCHIO)

$\underline{x} + \underline{a}(\underline{x})$   $\Rightarrow$  dessempo com o caminho variado das  
 $\underline{x}'$  é igual ao tempo mestre com  
 a mesma  $\underline{s}$

$$g_{jk}(x) = \left( \delta_{ij}^o + \frac{\partial u_i}{\partial x_j} \right) \left( \delta_{ki}^o + \frac{\partial u_i}{\partial x_k} \right) = g_{jk}^o + \left( \frac{\partial u_k}{\partial x_j} + \frac{\partial u_j}{\partial x_k} \right)$$

$\equiv \delta_{jk} + 2\beta_{jk} \rightarrow$  STAIN (DEPOLARISATION)  
TENSION

$$ds'^2 = dx'^1 dx'^1_0 = \frac{\partial x'^1}{\partial x_j} dx^j \frac{\partial x^1_0}{\partial x_k} dx^k$$

$$= g_{jk}(x) dx^j dx^k \quad \sum g_{jk}(x) = \frac{\partial x^i}{\partial x^j} \frac{\partial x^i}{\partial x^k}$$

$$\left. \begin{array}{l} M \geq 0 \Leftrightarrow \exists R \in \mathbb{C} \\ M = R^T R \\ \Rightarrow \sum_i M_{ii} \geq 0 \forall i \end{array} \right\} \leftarrow \begin{array}{l} \text{MATH NON NSS XQS} \\ \text{PROD DI 2 MATR CUNA} \\ \text{TUTTI POSITIVI DOCE' ALCUNA} \end{array}$$

$$\rightarrow \text{cons varianc (volume)} \quad d_3\bar{x}^1 = \left| \det \frac{\partial \bar{x}^1}{\partial x} \right| d_3x = \int g(x)^\top d_3x \Rightarrow \bar{g} = \int \det(1+2D)^\top \text{ con } D \text{ simm Ricci } \Rightarrow \det(1+2D) = 1 + \text{Tr}D + O(\epsilon^2)$$

$$\Rightarrow \delta V = d_3\bar{x}^1 - d_3x = \text{div} \underline{a} V \Rightarrow \text{div} \underline{a} = \frac{\delta V}{V} \rightarrow \text{a div } \underline{a} \text{ si calcola con uno stesso termine a cui si somma il vol}$$

$$\rightarrow \text{cambia anche densità} \rightarrow \text{uso conservaz conformità} \quad \rho_0 d_3x = (\rho_0 + \delta p(x)) d_3\bar{x}^1 = [\rho_0 + \delta p(x)] (1 + \text{div} \underline{a}) d_3x \Rightarrow \delta p(x) = -\rho_0 \text{div} \underline{a}$$

cioè applicando deformazioni al mezzo riducendo conformità

$\rightarrow$  come si discrivono in un mezzo conforme tensioni di stress deviato  $\sigma_{ij}(x)$

$\times$  Poco di densità e tensione di tracce  $\sigma_{ij} = -P \delta_{ij} \Rightarrow \sigma_{rr} = -3P$  (tracce)

In gen der  $P = -\frac{1}{3}\sigma^k_k$

Modo V desum da esp S in mezzo conforme  $\Rightarrow$  tensioni in questo modo forze sottili manca



$$F_i = \int_S d\omega \sigma_{ij} n_j^j = \int_{\text{V}} d_3x D^j \sigma_{ij}$$

processo

$\int_{\text{V}} d_3x D^j \sigma_{ij}$   $\rightarrow$  tensione  $\sigma = \text{Forza} \times \text{unità di vol}$

$\times$  scrivere  $\sigma_{ij}$  mi sposta verso a mezzi elastic

In mezzi costanti  $\sigma_{ij}(x) = C_{ij}^{kl}(x) D_{kl}(x)$  summa re  $\sigma_{ij}$  (x vs  $\sigma_{ij}$  summa)

$\hookrightarrow$  solo esistono cose variane in più in più

se il mezzo ha solo omogeneità  $\Rightarrow$  nulla da x

se no summa  $\sigma_{ij} \leftrightarrow kl \Rightarrow$  costante di simmetria

inoltre  $\sigma_{ij}$  simm x conservaz mom ant

costante in modo

$$\rho_0 \ddot{\sigma}_{ij} = \lambda \ddot{\sigma}_{ij} D^k u_k + 2\mu \ddot{\sigma}^k D_{ij} = \lambda \ddot{\sigma}_{ij} D_k u_k + \mu \ddot{\sigma}^k \left( \frac{\partial D^k}{\partial x^j} + \frac{\partial D^k}{\partial x^i} \right) = (\lambda + \mu) \ddot{\sigma}_{ij} D_k u_k + \mu \nabla^2 \ddot{\sigma}_{ij} \Rightarrow$$

versualmente  $\rho_0 \ddot{\sigma}_{ij} = (\lambda + \mu) \text{grad}(\text{div} \underline{a}) + \mu \nabla^2 \ddot{\sigma}_{ij}$

da queste due sono 2  $\rightarrow$  ① diffusione  $\rho_0 \frac{\partial^2}{\partial t^2} \text{div} \underline{a} = (\lambda + 2\mu) \nabla^2 \text{div} \underline{a}$

② rotazione  $\rho_0 \frac{\partial^2}{\partial t^2} \text{rot} \underline{a} = \mu \nabla^2 \text{rot} \underline{a}$



$$d\dot{f}_i = \sigma_{ij}(x) n^j d\omega$$

com pressione  
forza su da  
 $\rightarrow$  tensione la deforma  
si allunga ac  
equilibrio

Posso scrivere legge di Hooke x questa  
Forza x unità di vol  
 $\rightarrow$  consi densità composta x uscita  
tensione e piccola  
 $\Rightarrow$  ac I and (quale che sia la relazione)

$$\rho_0 \ddot{\sigma}_{ij} = \sigma^k \ddot{\sigma}_{ij}$$

$\times$  mezzi elastici

$$\ddot{\sigma}_{ij}(x) = \lambda \delta_{ij} D^k u_k(x) + 2\mu D_{ij}(x)$$

entro 2 quantità cui si deve usare modo indip  
sotto leste  $\rightarrow D^k \& D_{ij}$

$\lambda, \mu$  cost di lame (dim di pressione)

$$\rightarrow \text{due cose da cui la 1a} \neq$$

① VOL CONSIDERATO  $\Sigma_L = \sqrt{\frac{\lambda+2\mu}{\rho_0}} \Rightarrow \left( \frac{1}{2\Sigma_L^2} \frac{\partial^2}{\partial t^2} - \nabla^2 \right) \operatorname{div} \underline{u} = 0 \Rightarrow \operatorname{div} \underline{u}$  campo scalare che descrive la variaz. di vol → ONDO DI PROGRESSIONE LONDITIO  $\Sigma_L = \text{VOL SECONDO KELVIN}$

②  $\Sigma_T = \sqrt{\frac{\mu}{\rho_0}}$  ONDO TRASVERSALE  $\rightarrow (\operatorname{rot} \underline{u})_i = \epsilon_{ijk} \partial_j u_k = \perp \underline{u}$  ONDO + FREQUENZA COSTANTE INFATI (ES.  $\lambda = 0$  COMUNQ.)  $\Sigma_T \leq \sqrt{2} \Sigma_L$

I VARI MODI SONO LEGATI A VAL DI  $\lambda, \mu$

compon. Al  $\Sigma_L \approx 6100 \frac{m}{s}$   
 $H_2O$  1600 + LEGGERO IC MATER + VELOC.  $\delta$  →  $\times H$  CORDO NO  $\Sigma_{max} = 3600 m/s$   
 DIAMANTE 1200

$\times$  AMPLIONDILS SONO OPORTUNA → SPR K (TUTTI SIRMILO A CAMPO ELEM)  
 $\underline{u}_j(\underline{x}, t) = \sum_k u_j(kt) \frac{e^{ik\underline{x}}}{\sqrt{V}}$  →  $\underline{u}_j(kt) = \frac{K_j}{k} K^l a_p(kt) + \left( S_{jl} - \frac{K_j K_l}{k^2} \right) a^l$   
 TUTTI COTROL = CAMPO VOL SEMPLIS ECOMPONIB IN 2 PT  $\begin{cases} 1 \text{ A ROTAZIO} \\ \text{DIV } \underline{0} \end{cases} \rightarrow \operatorname{div} \underline{u} = 0 \Rightarrow \text{AMPLIO PT} \perp k$   
 $\operatorname{rot} \underline{u} \Rightarrow \text{UNICO PT} \parallel k$

IN SP K  $\rho_0 \frac{\partial^2}{\partial t^2} \underline{u}_j(kt) = -\mu K^2 \underline{u}_j(kt) - (\lambda + \mu) K^l K^l a_p(kt) \rightarrow$  APPLICO, PROGRESSIONE LONG & TRANS →  $\begin{cases} \rho_0 \ddot{u}_j^L = -(\lambda^2 + 2\mu) K^2 \underline{u}_j^L \\ \rho_0 \ddot{u}_j^T = -\mu K^2 \underline{u}_j^T \end{cases} \rightarrow$  EQ ONDO DISACCOPPIATI

$\Rightarrow$  SONO GENSATI  $\vec{u}(x, t) = \frac{1}{\sqrt{V}} \sum_{k \in \Lambda} \vec{e}_k(k) \left[ e^{i k x - i \omega_k t} d_{k\lambda} - e^{-i k x + i \omega_k t} d_{k\lambda}^* \right] \frac{1}{\rho_0} \rightarrow \vec{e}_3(k) = \frac{\vec{k}}{k}$  DIRE LONGA  
 $\vec{e}_{1/2}(k) \perp k$  DIRE TRANS (DIP DA CONSERVAZIONE)

EN POS DIM CHE CR. TIMEV/LONG  $\Rightarrow$  CONSIDERARE EN CONSERVATIVI  $\begin{cases} \frac{\partial^2 \underline{u}^L}{\partial t^2} = 2\Sigma_L^2 \nabla^2 \underline{u}^L \text{ CON } \operatorname{ROT} \underline{u}^L = 0 \\ \frac{\partial^2 \underline{u}^T}{\partial t^2} = 2\Sigma_T^2 \nabla^2 \underline{u}^T \text{ CON } \operatorname{DIV} \underline{u}^T = 0 \end{cases} \Rightarrow$  EN TOT  $E = \frac{1}{2} \rho_0 \int d_{3\lambda} \left[ \left( \frac{\partial u_i}{\partial t} \right)^2 + 2\Sigma_L^2 (\operatorname{div} \underline{u}^L)^2 + \left( \frac{\partial u_i^T}{\partial t} \right)^2 + 2\Sigma_T^2 (\operatorname{rot} \underline{u}^T)^2 \right]$  EN CONSERVATIVA  $\rightarrow \rho_0 \left( \frac{\partial u_i}{\partial t} \right)^2$  DENSITA' DI EN CINERIAS MUSICA EN VOL

IN  $t=0$   $\underline{E} = \sum_{k \in \Lambda} \rho_0 \omega_k^2(k) \left[ d_{k\lambda}^* d_{k\lambda} + c.c. \right]$

ADDESSA PACCIO ON CAZZO XRS SONO RE MA QUANDO E' CHIAZZO E' ON TROTTO

$\rightarrow$  CALCOLIAMO IL # DI OSCILLATORI FISSI A FREQ FIX  $\omega$  (O MODI NORMALI  $\leq \lambda$ )  $N(\omega) = \sum_{k \in \Lambda} \Theta(\omega - \omega_k(k)) = \sum_{k \in \Lambda} \Theta(\omega - \omega_3(k)) + 2 \sum_{k \in \Lambda} \Theta(\omega - \omega_{1/2}(k)) = V \int \frac{d_3(k)}{(2\pi)^3} \left[ \Theta(\omega - \Sigma_L k) + 2 \Theta(\omega - \Sigma_T k) \right] = \frac{V}{(2\pi)^3} \frac{4}{3} \pi \int \left( \frac{\omega}{2\Sigma_L} \right)^3 + 2 \left( \frac{\omega}{2\Sigma_T} \right)^3$

$$\Rightarrow N(\omega) = \frac{V}{6\pi^2} \omega^3 \left[ \frac{1}{2\Sigma_L^3} + \frac{2}{2\Sigma_T^3} \right]$$

SO HO MUSICA DI N MODI OSCILLANTI NON SOLO AL MODI NORMA MA 3N OSCILLATORI  $\Rightarrow$  CANTAT  $\omega_D$  DALLE TUE 3N =  $N(\omega_D)$  COME COTTOFF  $\rightarrow$  IN  $\underline{E}$  SONO INSIEME PARTIORS  $\Theta(\omega_D - \omega(k))$