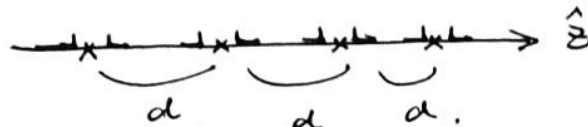


Problem 6.1

a) Radiation Pattern:



The electric field of the array antenna can be expressed as, where the center frequency is 97 MHz.

$$\underline{E}(\omega, \varphi) = -j \frac{z_0}{2\lambda} \frac{e^{-jkr}}{r} \cdot \underline{P}(\hat{r})$$

$$= \underline{E}_1(\omega, \varphi) \cdot AF$$

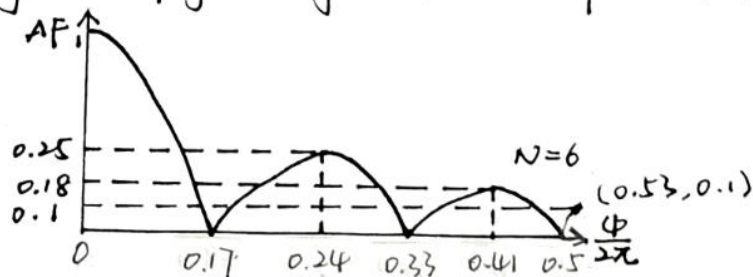
Where the electric field radiated by a single dipole can be expressed as below, whose radiation pattern is same as a dipole.

$$\underline{E}_1(\omega, \varphi) = -j \frac{z_0}{2\lambda} \frac{1}{r_1} \hat{P}_1(\omega, \varphi) \cdot \text{height} \cdot e^{jkr_1} \cdot \underline{I}_1$$

The normalized area factor is,

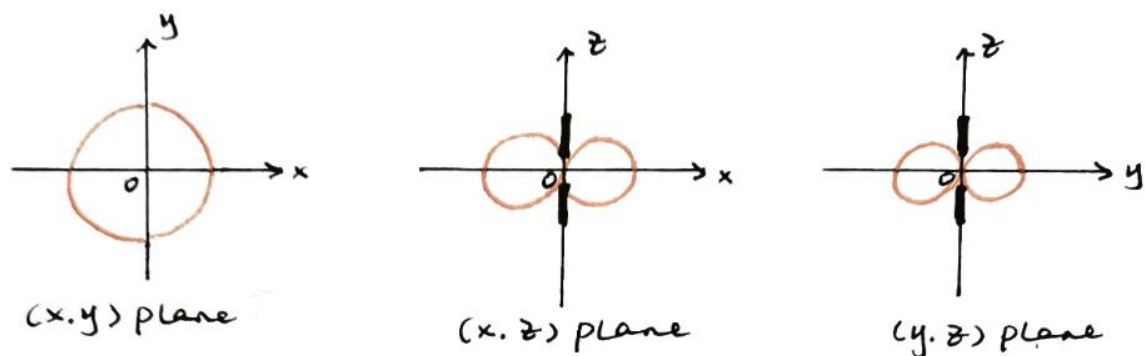
$$AF = \frac{1}{N} \left| \frac{\sin \frac{N\psi}{2}}{\sin \frac{\psi}{2}} \right|$$

where  $\psi = kd \cos \theta + \Phi$ ,  $\Phi$  is assumed equal for each element in the uniform array. The visible range  $\theta \in [0, \pi]$ , where  $\psi/2\pi \in [-0.53, 0.53]$ . Checking the figure of the area factor with  $N=6$ ,

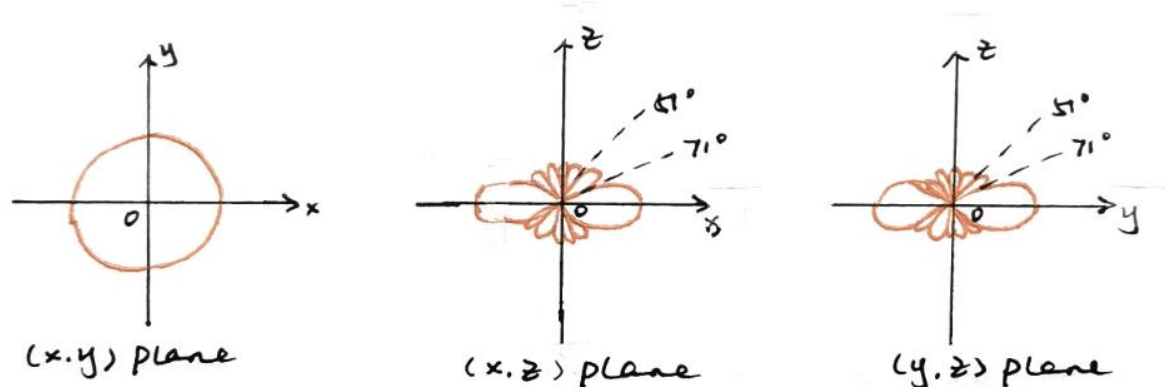


The total radiation pattern can be plotted as the dipole radiation pattern times the AF radiation pattern.

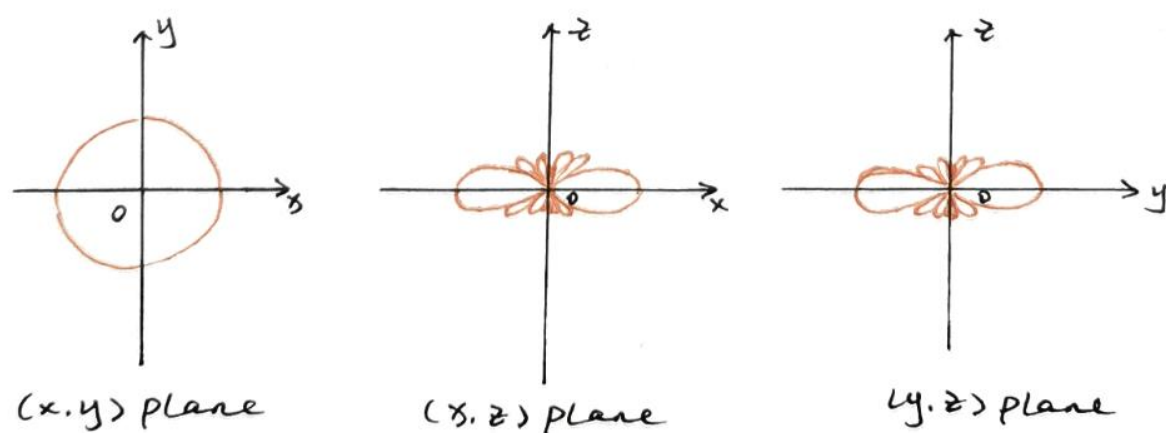
The radiation pattern of the dipole at each plane are,



The radiation patterns of the area factor at each plane are,

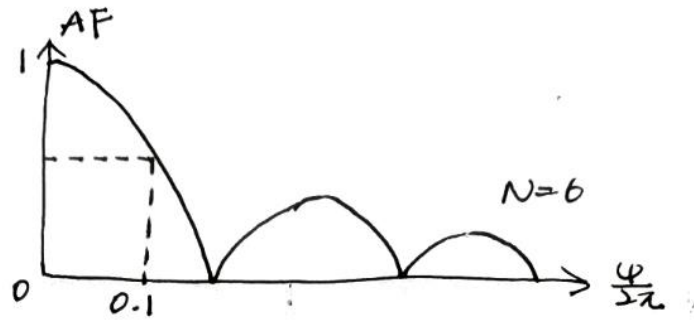


The total radiation patterns at each plane are,



b) HPBW and aperture of the main beam:

According to the figure of the Area Factor with  $\frac{\psi}{2\pi}$ ,



With  $\frac{\psi}{2\pi} = \frac{kd}{2\pi} \cos\theta = 0.1$ ,  $0.53 \cos\theta = 0.1$ ,  
therefore  $\theta = 1.3810 \text{ [rad]} \approx 79.12^\circ$

$$\text{HPBW} = 2 \times (90^\circ - 79.12^\circ) = 21.76^\circ$$

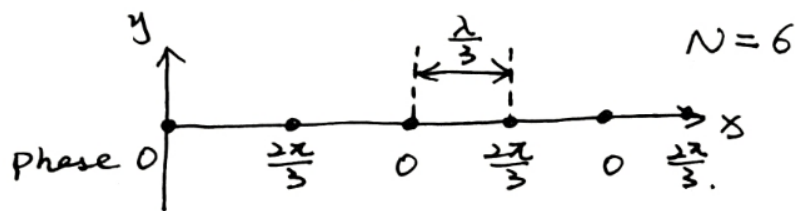
c) Maximum gain:

The gain of the antenna can be calculated from,

$$\begin{aligned} G &= \frac{\frac{a_p}{a_\Sigma}}{(\frac{a_p}{a_\Sigma})_{\text{iso}}} \\ &= G_0 \cdot \sum_{i=1}^N g_i(\omega, \omega). \end{aligned}$$

## Problem 6.2

1. Qualitative radiation pattern:



The electric-field is expressed as,

$$\underline{E}(\omega, \varphi) = \underline{E}_1(\omega, \varphi) \cdot AF$$

where,  $\underline{E}_1(\omega, \varphi) = -j \frac{Z_0}{2\lambda} \frac{1}{r_i} \hat{P}_i(\omega, \varphi) \text{hetf} \cdot e^{jk r_i} \cdot \underline{I}$

$$AF = \sum_{i=1}^N e^{-jk(r_i - r_1)} \cdot e^{(\varphi_i - \varphi_1)j}$$

As the spaces between the elements are equal,

$$r_i - r_1 = -(i-1) d \cos \theta$$

However, the phases of the elements are different,

$$\varphi_2 - \varphi_1 = \frac{2\pi}{3}$$

$$\varphi_5 - \varphi_1 = 0$$

$$\varphi_3 - \varphi_1 = 0$$

$$\varphi_6 - \varphi_1 = \frac{2\pi}{3}$$

$$\varphi_4 - \varphi_1 = \frac{2\pi}{3}$$

Therefore,

$$AF = \sum_{i=1}^N e^{jk[(i-1)d \cos \theta + (\varphi_i - \varphi_1)]}$$

Notating  $x_i = k[(i-1)d \cos \theta + (\varphi_i - \varphi_1)]$

When,  $i=1, 3, 5$ ,  $x_i = k(i-1)d \cos \theta$

$$i=2, 4, 6, \quad x_i = k(i-1)d \cos \theta + \frac{2\pi}{3}$$

Then, the sum can be calculated respectively as two parts,

$$\begin{aligned} AF_1 &= \sum_{i=1,3,5} e^{jk(i-1)d \cos \theta} = \sum_{n=0,2,4} e^{jkn d \cos \theta} \\ &= e^{j2kd \cos \theta} \cdot \frac{\sin(jkd \cos \theta \cdot 3)}{\sin(jkd \cos \theta)} \end{aligned}$$

$$\begin{aligned} AF_2 &= \sum_{i=2,4,6} e^{jk(i-1)d \cos \theta + \frac{2\pi}{3}} = e^{\frac{2\pi}{3}} \cdot \sum_{i=2,4,6} e^{jk(i-1)d \cos \theta} \\ &= e^{j3kd \cos \theta + \frac{2\pi}{3}} \cdot \frac{\sin(jkd \cos \theta \cdot 3)}{\sin(jkd \cos \theta)} \end{aligned}$$

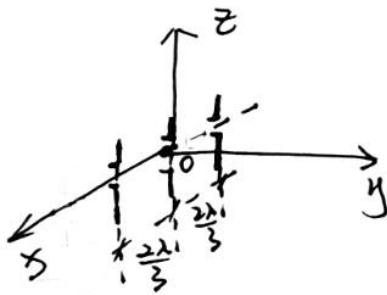
Then, the total area factor is,

$$AF = AF_1 + AF_2$$

$$= e^{2jkd \cos \theta} \frac{\sin(jkd \cos \theta \cdot 3)}{\sin(jkd \cos \theta)} \left(1 + e^{jkd \cos \theta + \frac{2\pi}{3}}\right)$$

OR, the full array antenna can be separated as two equi-spaced and constant-phased array antenna, with both  $N=3$ . Setting the original point as third element.

The first array antenna is like,



$$AF_1 = \sum_{i=1}^3 e^{j(i-1)\psi}$$

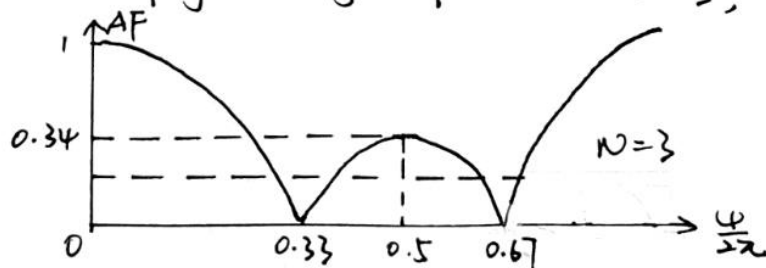
$$\psi = kd \cos \theta + \Phi$$

$$\text{where, } d = \frac{2\lambda}{3} - \Phi = 0$$

$$\text{Thus, } \psi = \frac{2\pi}{\lambda} \cdot \frac{2\lambda}{3} \cos \theta = 2\pi \cdot \frac{2}{3} \cos \theta.$$

$$\frac{\psi}{2\pi} = \frac{2}{3} \cos \theta.$$

The visible range with  $\theta \in [0, \pi]$ , with  $\frac{\psi}{2\pi} \in [-0.67, 0.67]$ . According to the figure of AF with  $N=3$ ,



The first-zero is at,  $\frac{\psi_{01}}{2\pi} = 0.33 = \frac{2}{3} \cos \theta_{01} \rightarrow \theta_{01} \approx 60^\circ$

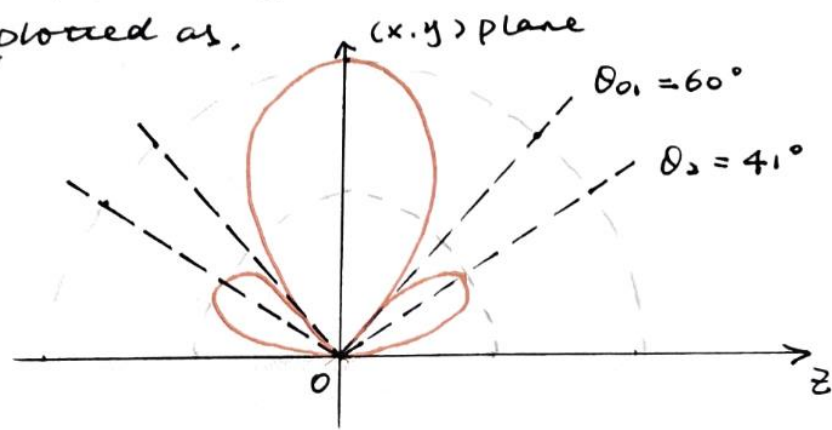
The first-maximum value is at,  $\frac{\psi_1}{2\pi} = 0 = \frac{2}{3} \cos \theta_1$ ,  
 $\theta_1 = 90^\circ$

The second-maximum value is at,  $\frac{\psi_2}{2\pi} = 0.5 = \frac{2}{3} \cos \theta_2$ ,  
 $\theta_2 \approx 41^\circ$ .

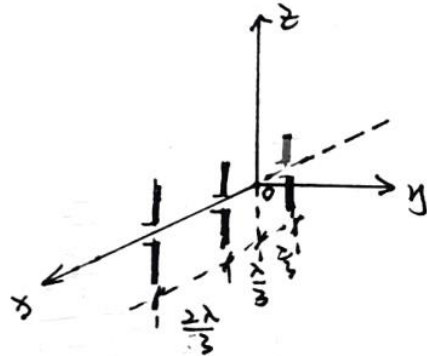
In addition, the second-zero is exactly at  $\theta = 0$  or  $\pi$ .



The radiation pattern of the first array antenna can be roughly plotted as,



The second antenna array is,



$$AF_2 = \sum_{i=1}^3 e^{j(4i-1)\psi}$$

$$\psi = kd \cos \theta + \Phi$$

$$\text{where, } d = \frac{\lambda}{3}, \Phi = \frac{2\pi}{3}$$

$$\text{Thus, } \psi = \frac{2\pi}{\lambda} \cdot \frac{\lambda}{3} \cos \theta + \frac{2\pi}{3}$$

$$\frac{\psi}{2\pi} = \frac{2}{3} \cos \theta + \frac{1}{3}$$

The visible range  $\theta \in [0, \pi]$ , is  $\frac{\psi}{2\pi} \in [-0.33, 1]$

With the first zeros at  $\frac{\psi_{01}}{2\pi} = \frac{2}{3} \cos \theta_{01} + \frac{1}{3} = 0.33$ ,  $\frac{\psi_{02}}{2\pi} = 0.67$ ,

$$\theta_{01} = 1.5758 [\text{rad}] \approx 90^\circ, \theta_{02} = 1.0414 [\text{rad}] \approx 60^\circ$$

The first - maximum value at  $\frac{\psi_{11}}{2\pi} = \frac{2}{3} \cos \theta_{11} + \frac{1}{3} = 0$ ,  $\frac{\psi_{12}}{2\pi} = 1$ ,

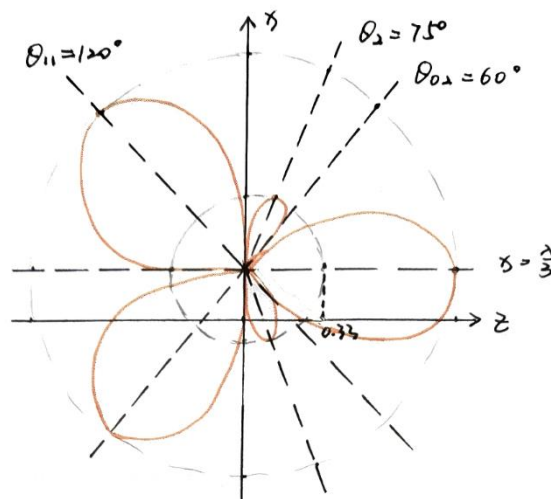
$$\theta_{11} = 2.0944 [\text{rad}] \approx 120^\circ, \theta_{12} = 180^\circ = 0^\circ$$

The second - maximum value at  $\frac{\psi_2}{2\pi} = \frac{2}{3} \cos \theta_2 + \frac{1}{3} = 0.5$ ,

$$\theta_2 = 1.3181 [\text{rad}] \approx 75^\circ$$

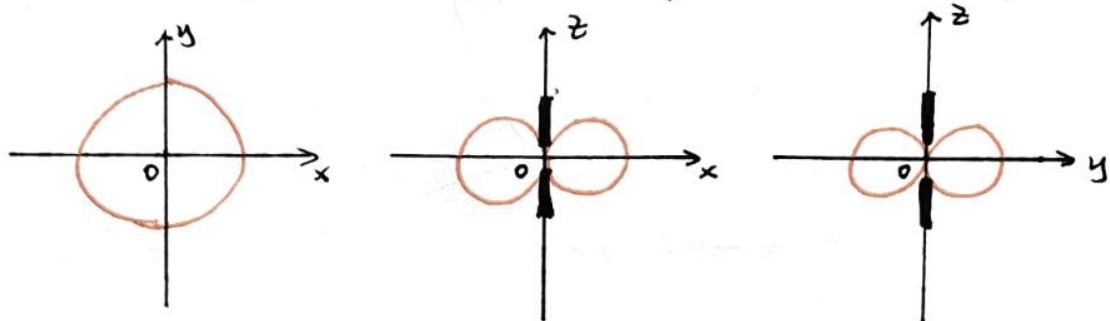
At  $\theta = 0$ ,  $AF = 1$ , At  $\theta = \pi$ ,  $AF = 0$ .

The radiation pattern of the second array antenna can be roughly plotted as.

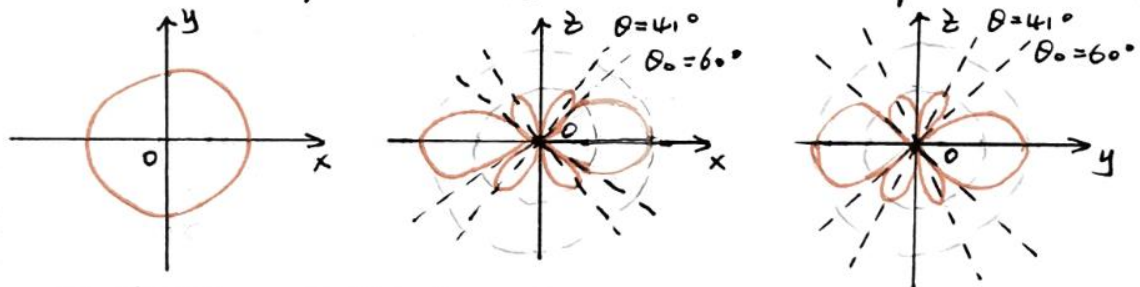


The total radiation pattern is the radiation pattern of the dipole times the sum of the two area factors.

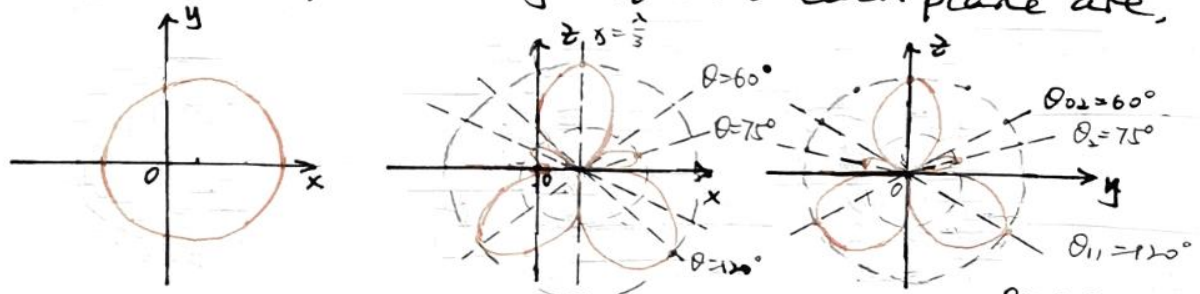
The radiation pattern of the dipole at each plane are,



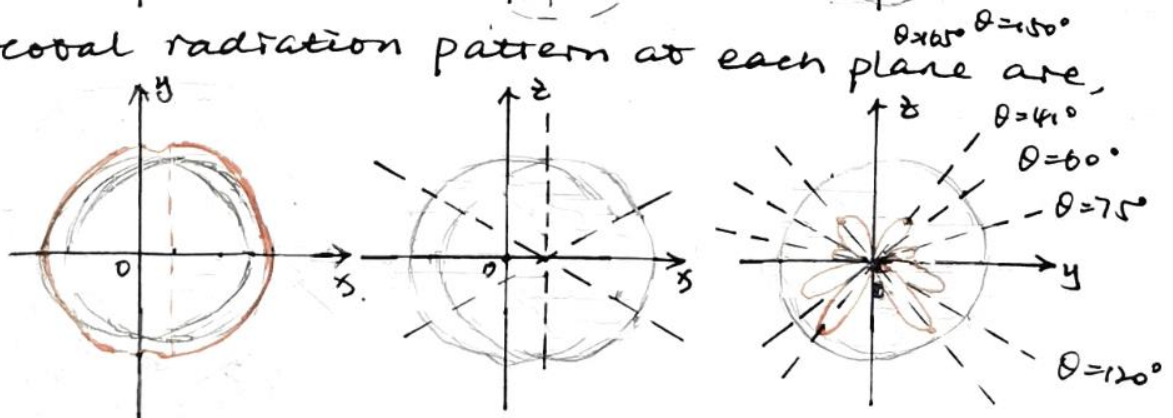
The radiation pattern of  $AF_1$  at each plane are,



The radiation pattern of  $AF_2$  at each plane are,



The total radiation pattern at each plane are,



### Problem 6.3

With HPBW  $< 7^\circ$ , the first-zeros at right and left sides are,

$$\theta_{\Sigma L}^{\perp} = 90^\circ - \frac{7^\circ}{2} = 86.5^\circ$$

$$\theta_{\Sigma R}^{\perp} = 90^\circ + \frac{7^\circ}{2} = 93.5^\circ$$

At the position of HPBW,  $AF[dB] = -3dB$ .

Assuming that  $\Phi = 0$ , and the array is symmetry.

$$AF[dB] = 10 \log_{10} \left[ \left| \frac{\sin\left(\frac{N\psi}{2}\right)}{\sin\left(\frac{\psi}{2}\right)} \right| \right]$$

$$\text{Where } \psi = kd \cos \theta_{\Sigma R}^{\perp} = \frac{2\pi}{\lambda} \cdot d \cdot \cos \theta_{\Sigma R}^{\perp} = 2\pi \cdot 0.6 \cdot \cos 93.5^\circ \\ \approx -0.2301^\circ$$

The value of  $N$  can be then solve as  $N = 13.1525$   
or  $N = 0.4979$ .

As HPBW  $< 7^\circ$ , thus  $\theta_{\Sigma R}^{\perp}$  shall be smaller, and  $N \neq 0$ ,

Therefore,  $N = 13$