
Algorithm 1 NorSand model algorithm

- 1: Assembling the tangent matrix D_{ijkl}
 - 2: $\delta\sigma_{ij} = D_{ijkl}\delta\epsilon_{kl}$
 - 3: $\sigma_{trial} = \sigma + \delta\sigma$
 - 4: $J_2 = \frac{1}{6}((\sigma_{11} - \sigma_{22})^2 + (\sigma_{11} - \sigma_{33})^2 + (\sigma_{33} - \sigma_{22})^2 + 6(\sigma_{12}^2 + \sigma_{23}^2 + \sigma_{33}^2))$
 - 5: $p_{trial} = \sigma_{ij}\delta_{ij}/3$, $q_{trial} = \sqrt{3J_2}$
 - 6: Then we going to calculating the yield surface
 - 7: $M_i = M_{tc} \cdot (1 - \frac{\chi N|\psi|}{M_{tc}})$
 - 8: $p_{max} = p_i \exp(\frac{\chi\psi}{M_{tc}})$
 - 9: $F = q_{trial} - p_{trial}M_i(1 - \ln(\frac{p_{trial}}{p_i}))$, $F_2 = p_{trial} - p_{max}$
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Algorithm 2 Procesures to generate the random loading path via gaussian process and principal rotation

Given: Given: The amplitud for principle strains

Algorithm 3 Summary of the procedure used to calculate the total stress with regard to the give strain increment

Given: The total stress σ , the total strain ϵ at current step, and the accumulated plastic strain ϵ (used as the internal variable), $\Delta\epsilon$ is to be applied to the configuration; Yield function f

Ensure: $f(\sigma, H) \leq 0$

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1:  $\Delta\hat{\sigma} = \mathbf{D}_e \cdot \Delta\epsilon$   $\triangleright$  Calculate the stress increment assuming elastic behavior
2:  $\hat{\sigma} = \sigma + \Delta\hat{\sigma}$   $\triangleright$  Calculate the trial stress
3:  $f(\hat{\sigma})$   $\triangleright$  Calculate the value of the yield function, with  $\hat{\sigma}$  as the state of stress,
4: if  $f(\hat{\sigma}) \leq 0$  then
5:    $\sigma = \hat{\sigma}$   $\triangleright$  The strain increment is elastic. In this case, the trial stress is correct; we return.
6:   return  $\sigma$ 
7: else
8:   if The previous stress is plastic then
9:      $r = 0$   $\triangleright$   $r$  is the portion of incremental strain taken elastically.
10:    Call ELASTOPLASTIC RETURN MAPPING( $\Delta\epsilon^{ep}$ )
11:   else  $\triangleright$  There is a transition from elstic to plastic
12:     Determine  $r$  via  $F(\sigma + r \cdot \Delta\epsilon) = 0$ 
13:      $\sigma = \mathbf{D}_e \cdot r \Delta\epsilon$ 
14:      $\Delta\epsilon^{ep} = (1 - r) \cdot \Delta\epsilon$   $\triangleright$   $\Delta\epsilon^{ep}$  is the elastoplastic strain increment
15:     Call ELASTOPLASTIC RETURN MAPPING( $\Delta\epsilon^{ep}$ )
16:   end if
17: end if
18: return  $\sigma$ 

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Algorithm 4 Elastoplastic return mapping (Convergence of this algorithm needs verification)

Given: The strain increment $\Delta\epsilon$, the hardening function $H(\bar{\epsilon}^p)$, and the yield function $f(\boldsymbol{\sigma}, H)$

Ensure: $f(\boldsymbol{\sigma}, H) = 0$

- 1: $f_{tol} = 1e-2$
 - 2: $k = 1, \sigma_k^{(n+1)} = \sigma^{(n)} + \mathbf{D}_e \Delta\epsilon \triangleright$ Calculate the trial stress as the begining of the return mapping iteration
 - 3: **while** $f(\sigma_k^{(n+1)}, H(\bar{\epsilon}_k^p)) > f_{tol}$ **do** $\triangleright f = g$ in Association Flow assumption
 - 4: $\mathbf{a}_k = \mathbf{b}_k = (\partial f / \partial \boldsymbol{\sigma})_k$
 - 5: $B_k = \delta \bar{\epsilon}^p / \delta \lambda = \sqrt{2/3} \|\mathbf{a}_k\|$
 - 6: $A_k = -\delta f_k / \delta \bar{\epsilon}_k^p \cdot B_k$
 - 7: $\delta \lambda = f_k / (\mathbf{a}_k^T \mathbf{D}_e \mathbf{a}_k)$
 - 8: $\delta \boldsymbol{\sigma} = -f_k \mathbf{D}_e \mathbf{b}_k / (A_k + \mathbf{a}_k^T \mathbf{D}_e \mathbf{b}_k)$
 - 9: $\delta \bar{\epsilon}^p = f_k B_k / (A_k + \mathbf{a}_k^T \mathbf{D}_e \mathbf{b}_k)$
 - 10: $\boldsymbol{\sigma}_{k+1}^{(n+1)} = \boldsymbol{\sigma}_k^{(n+1)} + \delta \boldsymbol{\sigma}$
 - 11: $\bar{\epsilon}_{k+1}^p = \bar{\epsilon}_k^p + \delta \bar{\epsilon}^p$
 - 12: $\boldsymbol{\epsilon}_{k+1}^p = \boldsymbol{\epsilon}_k^p + \mathbf{a}_k \delta \lambda$
 - 13: $k = k + 1$
 - 14: **end while**
 - 15: **return** $\boldsymbol{\sigma}, \boldsymbol{\epsilon}_{k+1}^p, \bar{\epsilon}_{k+1}^p$
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