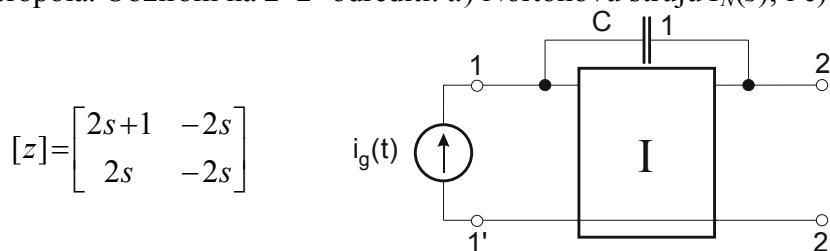


ZAVRŠNI ISPIT IZ ELEKTRIČNIH KRUGOVA 2015-2016 – Rješenja

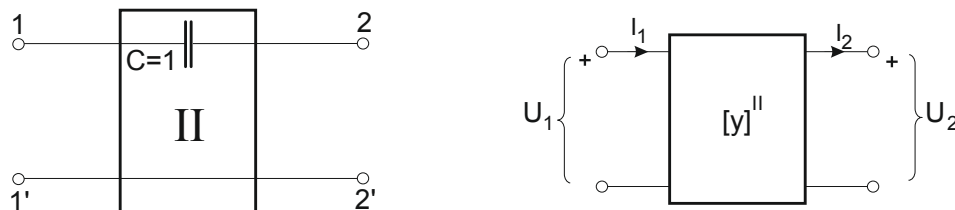
1. Mreža na slici predstavlja paralelni spoj dvaju četveropola. Ako je jedan od njih četveropol I: a) nacrtati drugi četveropol. b) odrediti y -parametre drugog četveropola; c) odrediti y -parametre paralelne kombinacije dva četveropola. Obzirom na 2–2' odrediti: d) Nortonovu struju $I_N(s)$; i e) Nortonovu admittanciju $Y_N(s)$.



$$[z] = \begin{bmatrix} 2s+1 & -2s \\ 2s & -2s \end{bmatrix}$$

Rješenje:

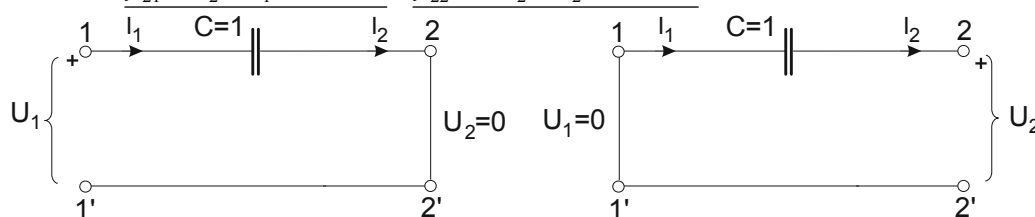
a) drugi četveropol II:



(1 bod)

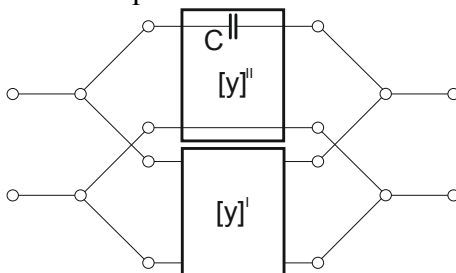
b) y -parametri drugog četveropola. Naponske jednačbe za četveropol uz referentne oznake struja i napona:

$$\begin{aligned} I_1 &= y_{11} \cdot U_1 - y_{12} \cdot U_2 & U_2 = 0, I_2 = I_1 \Rightarrow & U_1 = 0, I_2 = I_1 \Rightarrow \\ I_2 &= y_{21} \cdot U_1 - y_{22} \cdot U_2 & y_{11} = I_1 / U_1 = sC = s & y_{12} = -I_1 / U_2 = sC = s \Rightarrow [y]'' = \begin{bmatrix} y_{11} & -y_{12} \\ y_{21} & -y_{22} \end{bmatrix} = \begin{bmatrix} s & -s \\ s & -s \end{bmatrix} \\ & & y_{21} = I_2 / U_1 = sC = s & y_{22} = -I_2 / U_2 = sC = s \end{aligned}$$



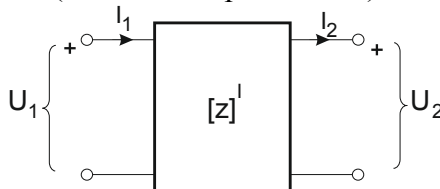
(1 bod)

c) Možemo promatrati dva četveropola I i II u paralelu:



Najprije nađimo y -parametre četveropola I (iz zadanih z -parametara):

$$\begin{aligned} U_1 &= z_{11} \cdot I_1 - z_{12} \cdot I_2 \\ U_2 &= z_{21} \cdot I_1 - z_{22} \cdot I_2 \end{aligned}$$



$$U_1 = (2s+1) \cdot I_1 - 2s \cdot I_2$$

$$U_2 = 2s \cdot I_1 - 2s \cdot I_2 \Rightarrow I_2 = I_1 - \frac{1}{2s} U_2$$

$$U_1 = (2s+1) \cdot I_1 - 2s \cdot \left(I_1 - \frac{1}{2s} \cdot U_2 \right)$$

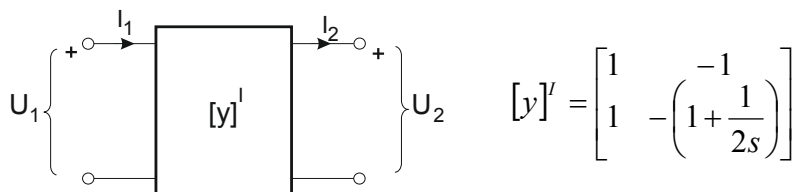
$$U_1 = (2s+1) \cdot I_1 - 2s \cdot I_1 + U_2$$

$$U_1 = 1\Omega \cdot I_1 + U_2$$

$$I_1 = \frac{1}{1\Omega} U_1 - \frac{1}{1\Omega} U_2$$

$$I_2 = \frac{1}{1\Omega} U_1 - \frac{1}{1\Omega} U_2 - \frac{1}{2s} \cdot U_2$$

$$I_2 = \frac{1}{1\Omega} U_1 - U_2 \left(1 + \frac{1}{2s}\right)$$



Ili na drugi način: $[y] = [z]^{-1}$

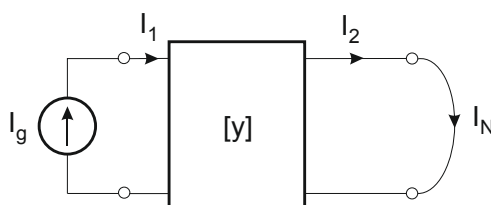
$$y_{11} = \frac{z_{22}}{|\Delta z|} = \frac{2s}{2s} = 1; \quad y_{12} = \frac{z_{12}}{|\Delta z|} = \frac{2s}{2s} = 1; \quad y_{21} = \frac{z_{21}}{|\Delta z|} = \frac{2s}{2s} = 1; \quad y_{22} = \frac{z_{11}}{|\Delta z|} = \frac{2s+1}{2s} = 1 + \frac{1}{2s}$$

$|\Delta z| = (2s+1) \cdot 2s - 4s^2 = 2s$ (Dobije se isti rezultat.)

Sada slijede y -parametri dva četveropola u paralelu:

$$[y] = [y]' + [y]'' = \begin{bmatrix} 1 & -1 \\ 1 & -\left(1 + \frac{1}{2s}\right) \end{bmatrix} + \begin{bmatrix} s & -s \\ s & -s \end{bmatrix} = \begin{bmatrix} 1+s & -(1+s) \\ 1+s & -\left(1+s + \frac{1}{2s}\right) \end{bmatrix} \quad (1 \text{ bod})$$

d) Nortonova struja $I_N(s)$ iz y -parametara:



$$I_1 = y_{11} \cdot U_1 - y_{12} \cdot U_2$$

$$I_2 = y_{21} \cdot U_1 - y_{22} \cdot U_2$$

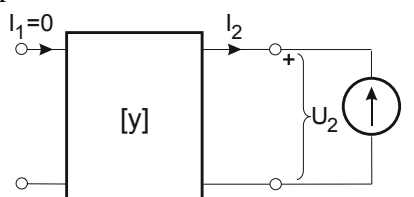
$$i_g(t) = \delta(t) \Rightarrow I_g(s) = 1, \quad I_g = I_1; \quad I_N = I_2$$

$U_2 = 0$ kratki spoj na priključnicama 2-2' kroz koje teče Nortonova struja

$$\frac{I_1}{I_2} = \frac{y_{21}}{y_{11}} \Rightarrow I_2 = \frac{y_{21}}{y_{11}} \cdot I_1 = \frac{1+s}{1+s} \cdot 1 = 1 \Rightarrow I_N(s) = 1 \quad (1 \text{ bod})$$

Drugi način je upotrijebiti izraz: $H_i(s) = \frac{I_2}{I_1} = \frac{Y_L y_{21}}{\Delta y + y_{11} Y_L} \Big|_{Y_L = \infty} = \frac{y_{21}}{y_{11}}$ što će dati isti rezultat.

e) Nortonova admitancija $Y_N(s)$ iz y -parametara:



$I_1 = 0$ prazni hod spoj na priključnicama 1-1' jer je isključen strujni izvor

$$I_1 = -I_2; \quad Y_N = \frac{I}{U_2} = \frac{-I_2}{U_2}; \Rightarrow \begin{aligned} 0 &= y_{11} \cdot U_1 - y_{12} \cdot U_2 \\ -I &= y_{21} \cdot U_1 - y_{22} \cdot U_2 \end{aligned} \Rightarrow y_{11} \cdot U_1 = y_{12} \cdot U_2 \Rightarrow U_1 = (y_{12} / y_{11}) \cdot U_2$$

$$\Rightarrow -I = y_{21} \cdot \frac{y_{12}}{y_{11}} U_2 - y_{22} \cdot U_2 = \frac{y_{12} y_{21} - y_{11} y_{22}}{y_{11}} \cdot U_2 \Rightarrow Y_N = \frac{I}{U_2} = \frac{y_{11} y_{22} - y_{12} y_{21}}{y_{11}} = \frac{\Delta y}{y_{11}}; \quad \Delta y = y_{11} y_{22} - y_{12} y_{21}$$

$$\Delta y = (1+s) \left(1+s + \frac{1}{2s}\right) - (1+s)^2 = (1+s)^2 + \frac{1+s}{2s} - (1+s)^2 = \frac{1+s}{2s}; \quad Y_N(s) = \frac{\Delta y}{y_{11}} = \frac{(1+s)/(2s)}{1+s} = \frac{1}{2s} \quad (1 \text{ bod})$$

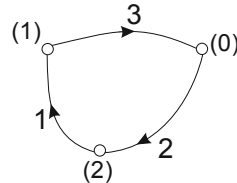
Drugi način je upotrijebiti izraz: $Y_{u12}(s) = y_{22} - \frac{y_{12} y_{21}}{y_{11} + Y_1} \Big|_{Y_1 = 0} = \frac{y_{11} y_{22} - y_{12} y_{21}}{y_{11}}$ što će dati isti rezultat.

2. Električni krug opisan je matricom incidencija \mathbf{A} , matricom admitancija grana \mathbf{Y}_b , i vektorom strujnih izvora grana \mathbf{I}_{0b} . Nacrtati: a) pripadni orijentirani graf i b) električnu mrežu. c) Napisati sustav jednažbi napona čvorova u matičnom obliku za dobivenu mrežu, d) odrediti matrice admitancija čvorova \mathbf{Y}_v i e) vektor strujnih izvora u čvorovima \mathbf{I}_{0v} .

$$\mathbf{Y}_b = \begin{bmatrix} sC_1 & 0 & 0 \\ 0 & sC_2 & 0 \\ rGsC_1 & 0 & G \end{bmatrix}, \quad \mathbf{I}_{0b} = \begin{bmatrix} U_g sC_1 + C_1 u_{C1}(0) \\ 0 \\ rGU_g sC_1 + rGC_1 u_{C1}(0) \end{bmatrix}, \quad \mathbf{A} = \begin{bmatrix} -1 & 0 & 1 \\ 1 & -1 & 0 \end{bmatrix}$$

Rješenje:

a) Orijetirani graf slijedi iz matrice incidencija (reducirane) $\mathbf{A} = \begin{bmatrix} -1 & 0 & 1 \\ 1 & -1 & 0 \end{bmatrix}$



(1 bod)

b) Električna mreža: treba napisati strujno-naponske jednažbe grana

$$\mathbf{I}_b = \mathbf{Y}_b \cdot \mathbf{U}_b + \mathbf{I}_{0b}$$

$$\begin{bmatrix} I_1 \\ I_2 \\ I_3 \end{bmatrix} = \begin{bmatrix} sC_1 & 0 & 0 \\ 0 & sC_2 & 0 \\ rGsC_1 & 0 & G \end{bmatrix} \cdot \begin{bmatrix} U_1 \\ U_2 \\ U_3 \end{bmatrix} + \begin{bmatrix} U_g sC_1 + C_1 u_{C1}(0) \\ 0 \\ rGU_g sC_1 + rGC_1 u_{C1}(0) \end{bmatrix}$$

$$I_1 = U_1 \cdot sC_1 + U_g \cdot sC_1 + C_1 \cdot u_{C1}(0)$$

$$I_2 = U_2 \cdot sC_2$$

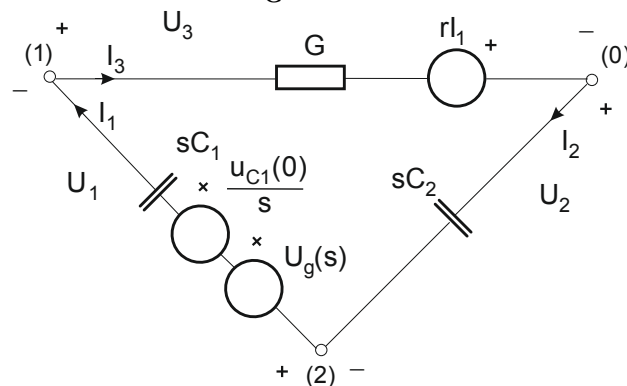
$$I_3 = U_1 rG \cdot sC_1 + U_3 G + rGU_g \cdot sC_1 + rGC_1 \cdot u_{C1}(0)$$

$$I_1 = \left[U_1 + U_g + \frac{u_{C1}(0)}{s} \right] \cdot sC_1$$

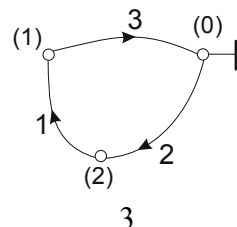
$$I_2 = U_2 \cdot sC_2$$

$$I_3 = U_3 G + rG \cdot sC_1 \left[U_1 + U_g + \frac{u_{C1}(0)}{s} \right] = (U_3 + rI_1) \cdot G$$

$G = \frac{1}{R}$ je vodljivost, odnosno otpor veličine $R = \frac{1}{G}$ je u mreži:



Orijentirani graf (čvor 0 je referentan):



c) Napisati sustav jednažbi napona čvorova u matričnom obliku za dobivenu mrežu:
Sustav jednažbi čvorova glasi: $\mathbf{Y}_v \cdot \mathbf{U}_v = \mathbf{I}_v$ rješenje vektor napona čvorišta \mathbf{U}_v .

b) + c) (2 boda)

d) matrica admitancija čvorova \mathbf{Y}_v :

$$\begin{aligned}\mathbf{Y}_v &= \mathbf{A} \cdot \mathbf{Y}_b \cdot \mathbf{A}^T = \begin{bmatrix} -1 & 0 & 1 \\ 1 & -1 & 0 \end{bmatrix} \cdot \begin{bmatrix} sC_1 & 0 & 0 \\ 0 & sC_2 & 0 \\ rGsC_1 & 0 & G \end{bmatrix} \cdot \begin{bmatrix} -1 & 1 \\ 0 & -1 \\ 1 & 0 \end{bmatrix} = \\ &= \begin{bmatrix} -sC_1 + rGsC_1 & 0 & G \\ sC_1 & -sC_2 & 0 \end{bmatrix} \cdot \begin{bmatrix} -1 & 1 \\ 0 & -1 \\ 1 & 0 \end{bmatrix} = \begin{bmatrix} sC_1 - rGsC_1 + G & -sC_1 + rGsC_1 \\ -sC_1 & sC_1 + sC_2 \end{bmatrix}\end{aligned}$$

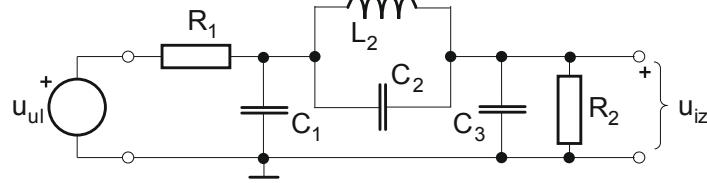
(1 bod)

e) vektor strujnih izvora u čvorovima \mathbf{I}_{0v} :

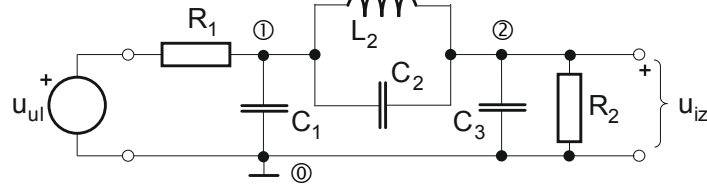
$$\begin{aligned}\mathbf{I}_{0v} &= -\mathbf{A} \cdot \mathbf{I}_{0b} = -\begin{bmatrix} -1 & 0 & 1 \\ 1 & -1 & 0 \end{bmatrix} \cdot \begin{bmatrix} U_g sC_1 + C_1 u_{C1}(0) \\ 0 \\ rGU_g sC_1 + rGC_1 u_{C1}(0) \end{bmatrix} = \\ &= \begin{bmatrix} U_g sC_1 + C_1 u_{C1}(0) - rGU_g sC_1 - rGC_1 u_{C1}(0) \\ -U_g sC_1 - C_1 u_{C1}(0) \end{bmatrix} = \begin{bmatrix} (1-rG)(U_g sC_1 + C_1 u_{C1}(0)) \\ -U_g sC_1 - C_1 u_{C1}(0) \end{bmatrix}\end{aligned}$$

(1 bod)

3. Za električni krug prikazan slikom odrediti: a) naponsku prijenosnu funkciju $H(s)=U_{iz}(s)/U_{ul}(s)$ kao funkciju varijable „ s “ i elemenata (R_i , L_i i C_i). b) Uvrstiti normalizirane vrijednosti elemenata: $R_1=1$, $R_2=1$, $C_1=1$, $C_2=1$, $C_3=1$, $L_2=1$. c) Prikazati raspored polova i nula u kompleksnoj ravnini. d) Izračunati i skicirati amplitudno-frekvencijsku karakteristiku $|T(j\omega)|$. e) O kojem se tipu filtra radi (NP, VP, PP ili PB)?



Rješenje: a) Naponska prijenosna funkcija (metoda napona čvorišta):



$$(1) U_1 \left(\frac{1}{R_1} + sC_1 + sC_2 + \frac{1}{sL_2} \right) - U_2 \left(sC_2 + \frac{1}{sL_2} \right) = U_{ul} \frac{1}{R_1}$$

$$(2) -U_1 \left(sC_2 + \frac{1}{sL_2} \right) + U_2 \left(sC_2 + \frac{1}{sL_2} + sC_3 + \frac{1}{R_2} \right) = 0$$

$$U_2 = U_{iz}$$

$$(2) \Rightarrow U_1 = U_2 \frac{sC_2 + \frac{1}{sL_2} + sC_3 + \frac{1}{R_2}}{sC_2 + \frac{1}{sL_2}} \rightarrow (1) \Rightarrow$$

$$U_2 \frac{sC_2 + \frac{1}{sL_2} + sC_3 + \frac{1}{R_2}}{sC_2 + \frac{1}{sL_2}} \left(\frac{1}{R_1} + sC_1 + sC_2 + \frac{1}{sL_2} \right) - U_2 \left(sC_2 + \frac{1}{sL_2} \right) = U_{ul} \frac{1}{R_1} \Bigg/ \left(sC_2 + \frac{1}{sL_2} \right)$$

$$U_2 \left[s(C_2 + C_3) + \frac{1}{sL_2} + \frac{1}{R_2} \right] \left[s(C_1 + C_2) + \frac{1}{sL_2} + \frac{1}{R_1} \right] - U_2 \left(sC_2 + \frac{1}{sL_2} \right)^2 = U_{ul} \frac{1}{R_1} \left(sC_2 + \frac{1}{sL_2} \right)$$

$$U_{iz} \left[s^2(C_1 + C_2)(C_2 + C_3) + \frac{C_1 + C_2}{L_2} + s \frac{C_1 + C_2}{R_2} + \frac{C_2 + C_3}{L_2} + \frac{1}{s^2 L_2^2} + \frac{1}{sL_2 R_2} + s \frac{C_2 + C_3}{R_1} + \frac{1}{sL_2 R_1} + \frac{1}{R_1 R_2} - s^2 C_2^2 - 2 \frac{C_2}{L_2} - \frac{1}{s^2 L_2^2} \right] = U_{ul} \frac{1}{R_1} \left(sC_2 + \frac{1}{sL_2} \right)$$

$$U_{iz} \left[s^2(C_1 C_2 + C_1 C_3 + C_2 C_3) + \frac{C_1 + C_3}{L_2} + s \frac{C_1 + C_2}{R_2} + \frac{1}{sL_2 R_2} + s \frac{C_2 + C_3}{R_1} + \frac{1}{sL_2 R_1} + \frac{1}{R_1 R_2} \right] = U_{ul} \frac{1}{R_1} \left(sC_2 + \frac{1}{sL_2} \right) \Bigg/ sL_2$$

$$U_{iz} \left[s^3 L_2 (C_1 C_2 + C_1 C_3 + C_2 C_3) + s(C_1 + C_3) + s^2 L_2 \frac{C_1 + C_2}{R_2} + \frac{1}{R_2} + s^2 L_2 \frac{C_2 + C_3}{R_1} + \frac{1}{R_1} + \frac{sL_2}{R_1 R_2} \right] =$$

$$= U_{ul} \frac{1}{R_1} (s^2 L_2 C_2 + 1)$$

$$T(s) = \frac{\frac{1}{R_1}(s^2 L_2 C_2 + 1)}{s^3 L_2 (C_1 C_2 + C_1 C_3 + C_2 C_3) + s^2 L_2 \left(\frac{C_1 + C_2}{R_2} + \frac{C_2 + C_3}{R_1} \right) + s \left(\frac{L_2}{R_1 R_2} + C_1 + C_3 \right) + \frac{1}{R_1} + \frac{1}{R_2}}$$

Dobiveni izraz se može još urediti i prikazati na razne načine:

$$T(s) = \frac{R_2(s^2 L_2 C_2 + 1)}{s^3 L_2 R_1 R_2 (C_1 C_2 + C_1 C_3 + C_2 C_3) + s^2 L_2 [R_1 (C_1 + C_2) + R_2 (C_2 + C_3)] + s [L_2 + R_1 R_2 (C_1 + C_3)] + R_1 + R_2} \quad \text{ili}$$

$$T(s) = \frac{\frac{1}{L_2 R_1 (C_1 C_2 + C_1 C_3 + C_2 C_3)} (s^2 L_2 C_2 + 1)}{s^3 + s^2 \frac{R_1 (C_1 + C_2) + R_2 (C_2 + C_3)}{R_1 R_2 (C_1 C_2 + C_1 C_3 + C_2 C_3)} + s \frac{L_2 + R_1 R_2 (C_1 + C_3)}{L_2 R_1 R_2 (C_1 C_2 + C_1 C_3 + C_2 C_3)} + \frac{R_1 + R_2}{L_2 R_1 R_2 (C_1 C_2 + C_1 C_3 + C_2 C_3)}}, \quad \text{itd.}$$

b) Uvrštene normalizirane vrijednosti elemenata: $R_1=1, R_2=1, C_1=1, C_2=1, C_3=1, L_2=1$:

$$T(s) = \frac{U_{iz}(s)}{U_{ul}(s)} = \frac{s^2 + 1}{3s^3 + 4s^2 + 3s + 2} \quad \text{a) + b) (3 boda)}$$

c) Raspored polova i nula u kompleksnoj ravlini:

$$\text{-polovi: } 3s^3 + 4s^2 + 3s + 2 = 3 \left(s^3 + \frac{4}{3}s^2 + s + \frac{2}{3} \right) = 0$$

Pretpostavimo vrijednost pola: $s_{p1} = -1$

$$s_{p1} = -1 \Rightarrow 3(-1)^3 + 4(-1)^2 + 3(-1) + 2 = 0 \Rightarrow -3 + 4 - 3 + 2 = 0 \quad \text{DA}$$

Podijelimo:

$$\begin{aligned} (3s^3 + 4s^2 + 3s + 2) : (s + 1) &= 3s^2 + \frac{s^2 + 3s + 2}{s + 1} & (s^2 + 3s + 2) : (s + 1) &= s + \frac{2s + 2}{s + 1} & (2s + 2) : (s + 1) &= 2 \\ -3s^3 - 3s^2 & & -s^2 - s & & -2s - 2 & \\ \hline &= s^2 + 3s + 2 & &= 2s + 2 & &= 0 \end{aligned}$$

$$\text{Polovi: } 3s^3 + 4s^2 + 3s + 2 = (s + 1)(3s^2 + s + 2) = 0$$

$$3s^2 + s + 2 = 0 \Rightarrow s_{p2,3} = \frac{-1 \pm \sqrt{1 - 24}}{2 \cdot 3} = \frac{-1 \pm j\sqrt{23}}{6} = -0,1667 \pm j0,799305$$

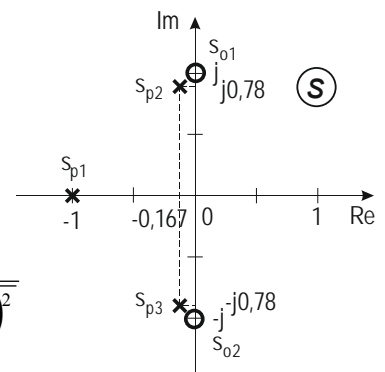
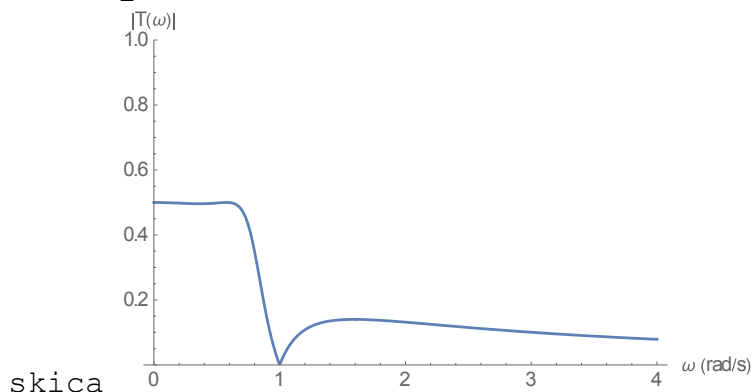
$$\text{-nule: } s^2 + 1 = 0 \Rightarrow s_{o1,2} = \pm j \quad \text{(1 bod)}$$

d) amplitudno-frekvencijska karakteristika:

$$T(j\omega) = \frac{-\omega^2 + 1}{-3j\omega^3 - 4\omega^2 + 3j\omega + 2} \Rightarrow |T(j\omega)| = \frac{|1 - \omega^2|}{\sqrt{(2 - 4\omega^2)^2 + (3\omega - 3\omega^3)^2}}$$

Ako uvrstimo tri karakteristične točke:

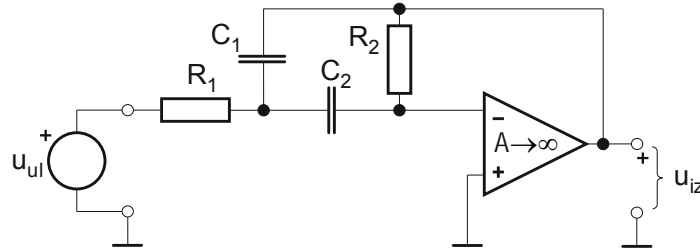
$$s=0 \text{ u } T(s) \Rightarrow T(0) = |T(j\omega)|_{\omega=0} = \frac{1}{2}; \quad s=1 \Rightarrow T(1) = |T(j\omega)|_{\omega=1} = 0; \quad s \rightarrow \infty \text{ u } T(s) \Rightarrow T(\infty) = |T(j\omega)|_{\omega \rightarrow \infty} = 0$$



e) O kojem se tipu filtra radi (NP, VP, PP ili PB)?

Točna su dva odgovora: NP- niski propust (NP Notch) ili PB-pojasna brana d) + e) (1 bod)

4. Za pojasno-propusni električni filter prikazan slikom zadana je naponska prijenosna funkcija $T(s)=U_{iz}(s)/U_{ul}(s)$. a) Usporedbom s općim oblikom PP prijenosne funkcije filtra 2. stupnja odrediti parametre k , ω_p , q_p kao funkcije elemenata filtra. b) Ako su zadane normalizirane vrijednosti parametara $\omega_p=1$ i $q_p=0,7071068$ te ako je $C_1=C_2=1$, izračunati normalizirane vrijednosti otpora R_1 i R_2 i pojačanje k . c) Prikazati raspored polova i nula u kompleksnoj ravnini. d) Izračunati i skicirati amplitudno-frekvencijsku karakteristiku $|T(j\omega)|$. e) Izračunati denormirane elemente filtra za frekvenciju normalizacije $\omega_0=10^3$ rad/s i otpor $R_0=1\text{k}\Omega$.



$$T(s) = \frac{U_{iz}(s)}{U_{ul}(s)} = -\frac{sR_2C_2}{s^2R_1C_1R_2C_2 + s(R_1C_1 + R_1C_2) + 1}$$

Rješenje:

a) Parametri

Napišemo prijenosnu funkciju tako da je koeficijent uz najveću potenciju od s (s^2) jediničan.

$$T(s) = \frac{U_{iz}(s)}{U_{ul}(s)} = -\frac{s \frac{1}{R_1C_1}}{s^2 + s \frac{R_1C_1 + R_1C_2}{R_1C_1R_2C_2} + \frac{1}{R_1C_1R_2C_2}}$$

Usporedba s općim oblikom:

$$T(s) = \frac{U_{iz}(s)}{U_{ul}(s)} = k \cdot \frac{\frac{\omega_p}{q_p} s}{s^2 + \frac{\omega_p}{q_p} s + \omega_p^2}$$

$$\omega_p^2 = \frac{1}{R_1R_2C_1C_2} \Rightarrow \omega_p = \frac{1}{\sqrt{R_1R_2C_1C_2}}$$

$$\frac{\omega_p}{q_p} = \frac{R_1(C_1 + C_2)}{R_1R_2C_1C_2} \Rightarrow q_p = \omega_p \frac{R_1R_2C_1C_2}{R_1(C_1 + C_2)} = \frac{1}{\sqrt{R_1R_2C_1C_2}} \cdot \frac{R_1R_2C_1C_2}{R_1(C_1 + C_2)} = \frac{\sqrt{R_1R_2C_1C_2}}{R_1(C_1 + C_2)}$$

$$k \cdot \frac{\omega_p}{q_p} = \frac{1}{R_1C_1} \Rightarrow k = \frac{1}{R_1C_1} \cdot \frac{q_p}{\omega_p} = \frac{1}{R_1C_1} \cdot \frac{R_1C_1R_2C_2}{R_1(C_1 + C_2)} = \frac{R_2C_2}{R_1(C_1 + C_2)}$$

(1 bod)

b) proračun: u proračunu smo pretpostavili $C_1=C_2=C$ pa će izrazi za ω_p , q_p i k iz točke a) poprimiti jednostavniji oblik:

$$\omega_p = \frac{1}{C\sqrt{R_1R_2}}, \quad q_p = \frac{1}{2}\sqrt{\frac{R_2}{R_1}}, \quad k = \frac{R_2}{2R_1},$$

Izračun jednadžbi iz uvjeta za ω_p i q_p :

$$\text{Iz } q_p = \frac{1}{\sqrt{2}} \text{ slijedi } \frac{1}{\sqrt{2}} = \frac{1}{2}\sqrt{\frac{R_2}{R_1}} \Rightarrow \frac{2}{\sqrt{2}} = \sqrt{\frac{R_2}{R_1}} \Rightarrow 2 = \frac{R_2}{R_1} \Rightarrow R_2 = 2R_1$$

$$\text{Iz } \omega_p=1 \text{ slijedi } 1 = \frac{1}{C\sqrt{R_1R_2}} \Rightarrow C\sqrt{R_1R_2} = 1 \Rightarrow C\sqrt{2R_1^2} = 1 \Rightarrow R_1 = \frac{1}{C\sqrt{2}}$$

Proračun elemenata: Uz odabir $C=1$ je $C_1=1$, $C_2=1$ i računamo:

$$R_1 = \frac{1}{\sqrt{2}}, \quad R_2 = \frac{2}{\sqrt{2}} = \sqrt{2}.$$

Pojačanje u području propuštanja iznosi: $k = \frac{R_2}{2R_1} = \frac{\sqrt{2}}{2 \frac{1}{\sqrt{2}}} = \frac{2}{2} = 1$

(1 bod)

c) raspored polova i nula u kompleksnoj ravnini:

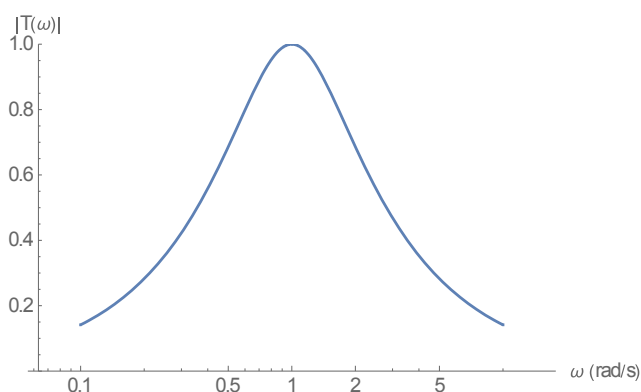
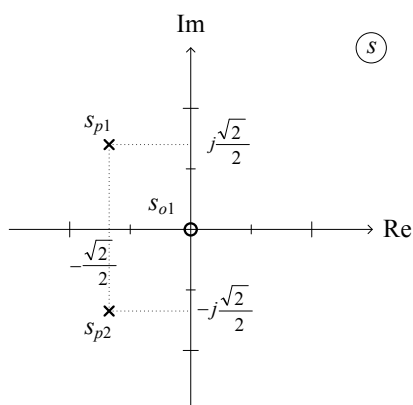
$$H_{PP}(s) = k \frac{(\omega_p / q_p)s}{s^2 + (\omega_p / q_p)s + \omega_p^2} = \frac{\sqrt{2}s}{s^2 + \sqrt{2}s + 1}$$

nule $s_{o1} = 0, s_{o2} = \infty$

polovi $s^2 + \sqrt{2} \cdot s + 1 = 0 \Rightarrow s_{p1,2} = -\frac{\sqrt{2}}{2} \pm \sqrt{\frac{2}{4} - 1} = -\frac{\sqrt{2}}{2} \pm j\frac{\sqrt{2}}{2}$ (1 bod)

d) amplitudno-frekvencijska karakteristika:

$$T(j\omega) = \frac{-\omega \cdot \sqrt{2}}{-\omega^2 + j\omega \cdot \sqrt{2} + 1} \Rightarrow |T(j\omega)| = \frac{|\sqrt{2} \cdot \omega|}{\sqrt{(1 - \omega^2)^2 + (\omega \cdot \sqrt{2})^2}} = \frac{\sqrt{2} \cdot \omega}{\sqrt{1 + \omega^4}} \quad (1 \text{ bod})$$



e) Denormalizacija elemenata po $\omega_0 = 10^3$ rad/s i $R_0 = 1\text{k}\Omega$:

normalizirani elementi

$$R_1 = 1/\sqrt{2}$$

$$R_2 = \sqrt{2}$$

$$C_1 = 1$$

$$C_2 = 1$$

izrazi za denormalizaciju

$$R = R_0 \cdot R_n;$$

$$C = \frac{C_n}{\omega_0 \cdot R_0};$$

$$L = \frac{L_n \cdot R_0}{\omega_0}$$

denormalizirani elementi

$$R_1 = R_0 \cdot 0,7071 = 707,1\Omega$$

$$R_2 = R_0 \cdot 1,4142 = 1414,2\Omega$$

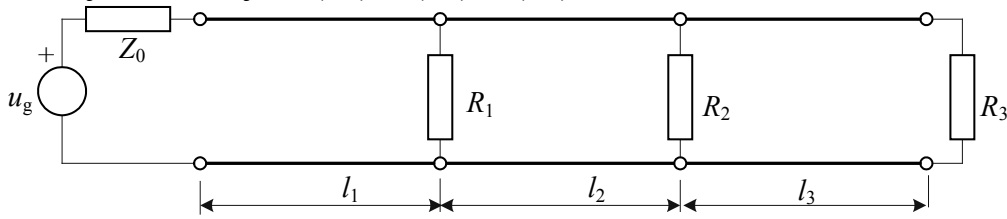
$$C_1 = \frac{1}{\omega_0 R_0} \cdot 1 = C_0 \cdot 1 = 1\mu\text{F}$$

$$C_2 = C_0 \cdot 1 = \mu\text{F}$$

(1 bod)

5. Tri linije bez gubitaka spojene su u kaskadu prema slici. Zadano je: $L=0,25\text{mH/km}$, $C=100\text{nF/km}$, $u_g=10\cos(2,5\pi\cdot 10^5 t)\text{ V}$, $R_2=150\Omega$, $R_3=25\Omega$, $l_1=3\lambda/4$, $l_2=\lambda/2$ i $l_3=\lambda/4$. Odrediti:

- valnu impedanciju i koeficijent prijenosa linija;
- brzinu širenja vala na linijama i duljinu druge i treće linije;
- otpor R_1 da bi prva linija bila prilagođena na izlazu;
- faktore refleksije na krajevima druge i treće linije: Γ_{i2} i Γ_{i3} ;
- napone na kraju svake linije: $u_1(l_1,t)$, $u_2(l_2,t)$, $u_3(l_3,t)$.



Rješenje:

$$\text{a) } Z_0 = \sqrt{\frac{L}{C}} = \sqrt{\frac{2,5 \cdot 10^{-4}}{10^{-7}}} = 50\Omega \quad \gamma = j\beta = j\omega_0 \sqrt{LC} = j2,5 \cdot \pi \cdot 10^5 \sqrt{0,25 \cdot 10^{-10}} = \frac{j5}{4} \pi \text{ [rad/km]}$$

(1 bod)

$$\text{b) } v = \frac{\omega}{\beta} = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{0,25 \cdot 10^{-10}}} = 2 \cdot 10^5 \text{ [km/s]} \quad \lambda = \frac{2 \cdot \pi}{\beta} = \frac{2 \cdot \pi}{1,25 \cdot \pi} = \frac{8}{5} = 1,6 \text{ km}$$

$$l_3 = \frac{\lambda}{4} = 400 \text{ [m]}; \quad l_2 = \frac{\lambda}{2} = 800 \text{ [m]}; \quad (1 \text{ bod})$$

$$\text{c) } \gamma \cdot l_1 = j \cdot \beta \cdot l_1 = j \frac{3\pi}{2} \quad \gamma \cdot l_2 = j \cdot \beta \cdot l_2 = j\pi; \quad \gamma \cdot l_3 = j \cdot \beta \cdot l_3 = j \frac{\pi}{2}$$

$$Z_{ul3} = \frac{R_3 \cosh(\gamma \cdot l_3) + Z_0 \sinh(\gamma \cdot l_3)}{\frac{R_3}{Z_0} \sinh(\gamma \cdot l_3) + \cosh(\gamma \cdot l_3)} = \frac{R_3 \cos(\beta \cdot l_3) + jZ_0 \sin(\beta \cdot l_3)}{j \frac{R_3}{Z_0} \sin(\beta \cdot l_3) + \cos(\beta \cdot l_3)} = \frac{Z_0^2}{R_3} = \frac{2500}{25} = 100\Omega$$

$$R_{eq2} = \frac{R_2 \cdot Z_{ul3}}{R_2 + Z_{ul3}} = \frac{150 \cdot 100}{250} = 60\Omega \quad Z_{ul2} = \frac{R_{eq2} \cos(\beta \cdot l_2) + jZ_0 \sin(\beta \cdot l_2)}{j \frac{R_{eq2}}{Z_0} \sin(\beta \cdot l_2) + \cos(\beta \cdot l_2)} = \frac{-R_{eq2}}{-1} = R_{eq2} = 60\Omega$$

$$R_{eq1} = \frac{R_1 \cdot Z_{ul2}}{R_1 + Z_{ul2}} = \frac{R_1 \cdot R_{eq2}}{R_1 + R_{eq2}} = Z_0 = 50\Omega \quad \Rightarrow \quad R_1 = \frac{Z_0 \cdot R_{eq2}}{R_{eq2} - Z_0} = \frac{50 \cdot 60}{10} = 300\Omega$$

(1 bod)

$$\text{d) } \Gamma_{i2} = \frac{R_{eq2} - Z_0}{R_{eq2} + Z_0} = \frac{10}{110} = \frac{1}{11} \quad \Gamma_{i3} = \frac{R_3 - Z_0}{R_3 + Z_0} = \frac{-25}{75} = -\frac{1}{3} \quad (1 \text{ bod})$$

$$\text{e) } \gamma \cdot l_1 = j\beta \frac{3\lambda}{4} = j \frac{3\pi}{2} \quad U_1(l_1) = U(0) \cdot e^{-j\beta l_1} = 5 \cdot e^{-j3\pi/2} = 5j \quad u_1(l_1, t) = 5 \cos\left(\omega t + \frac{\pi}{2}\right)$$

$$U_2(l_2) = U_1(l_1) \cdot \cos(\beta \cdot l_2) - jU_1(l_1) \cdot \frac{Z_0}{Z_{ul2}} \sin(\beta \cdot l_2) = -U_1(l_1) = -5j \quad u_2(l_2, t) = -5 \cos\left(\omega t + \frac{\pi}{2}\right)$$

$$U_3(l_3) = U_2(l_2) \cdot \cos(\beta \cdot l_3) - jU_2(l_2) \cdot \frac{Z_0}{Z_{ul3}} \sin(\beta \cdot l_3) = -jU_2(l_2) \cdot \frac{Z_0}{Z_{ul3}} \sin(\beta \cdot l_3) = -j(-5j) \frac{1}{2} = -\frac{5}{2}$$

$$u_1(l_3, t) = -2,5 \cdot \cos(\omega t) \quad (1 \text{ bod})$$