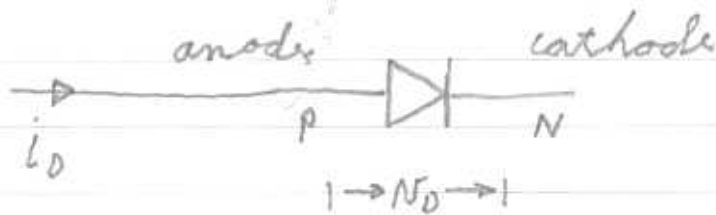
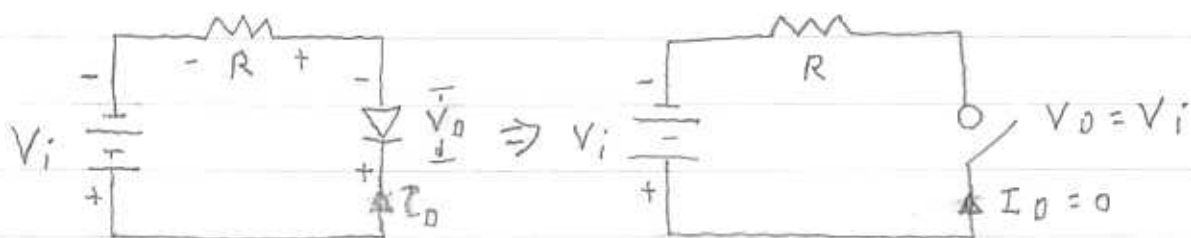
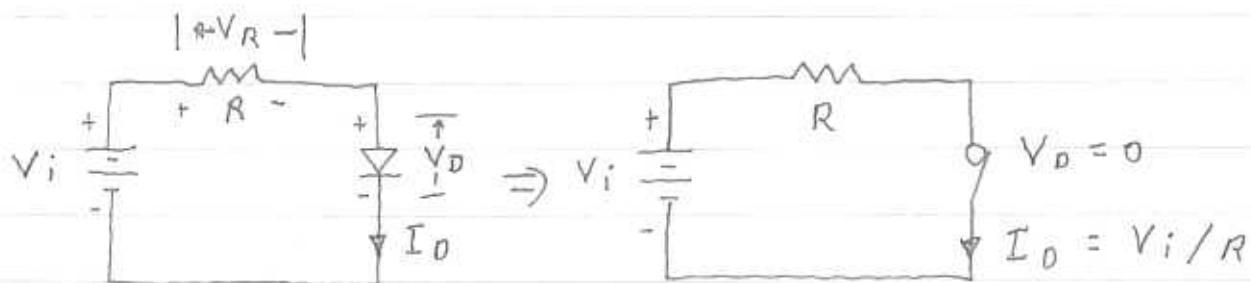


CHAPTER 3 Diodes

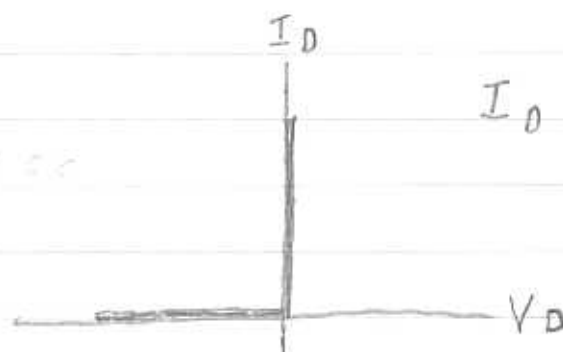


Ideal Diode

Equivalent Circuit

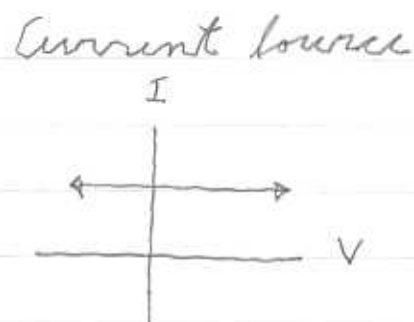
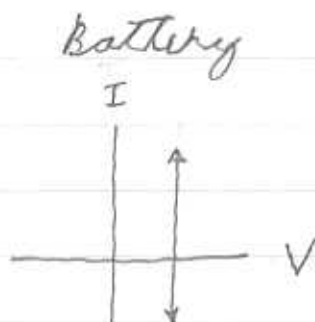
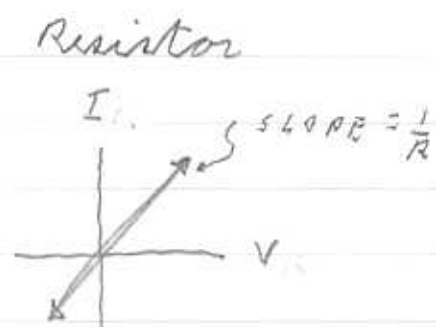


Ideal Diode Characteristics

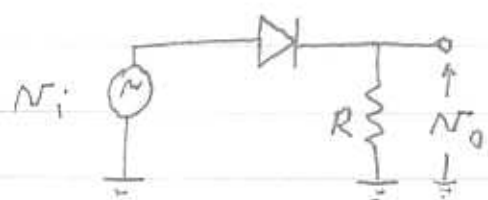


$$I_D = f(V_D)$$

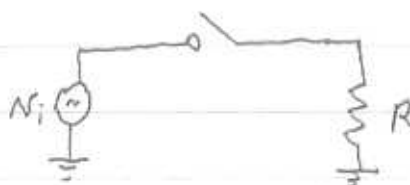
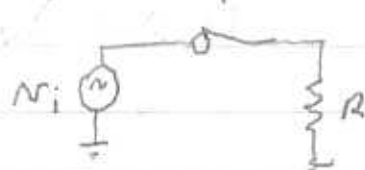
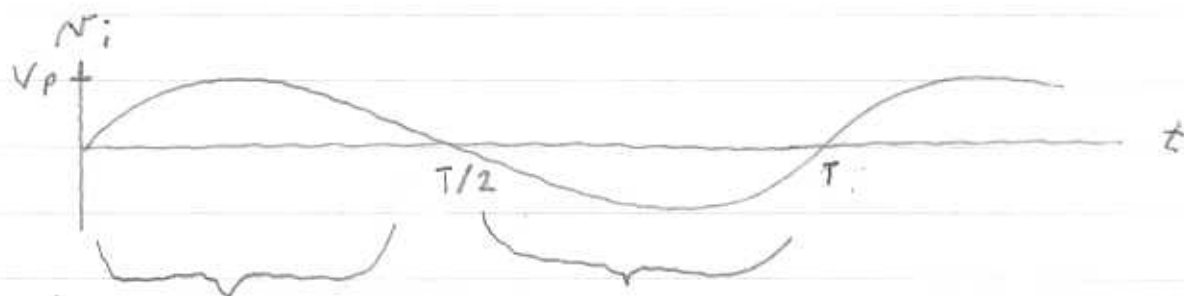
Contrast with:



Rectifier (Generates DC from AC)

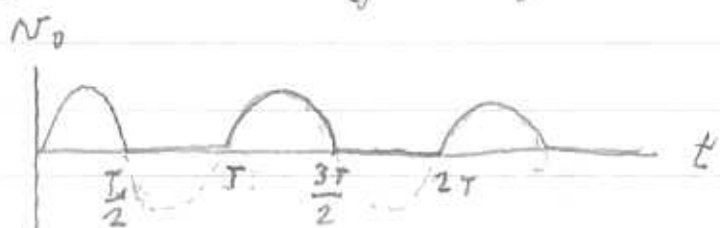


$$N_i = V_p \sin\left(\frac{2\pi}{T} t\right)$$

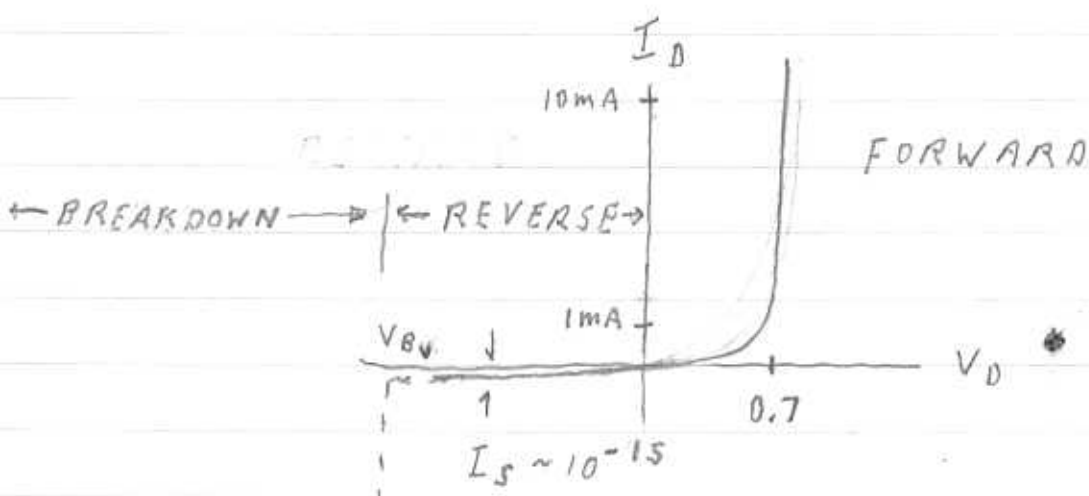
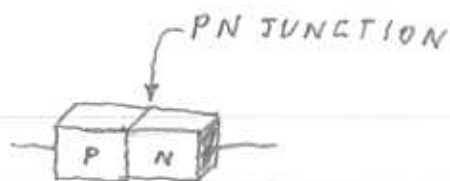


Eg. Current (0 to $\frac{T}{2}$)

Eg. Current ($\frac{T}{2}$ to T)



Real Diode



$$i_D = I_S (e^{N_D/V_T n} - 1)$$

i_D = diode current

N_D = voltage

I_S = saturation current ($I_S \propto$ PN JUNCTION AREA)

n = constant between 1 & 2

$$(1) \quad V_T = kT/q \approx 25 \text{ mV}$$

q = Electron charge

k = Boltzmann's constant

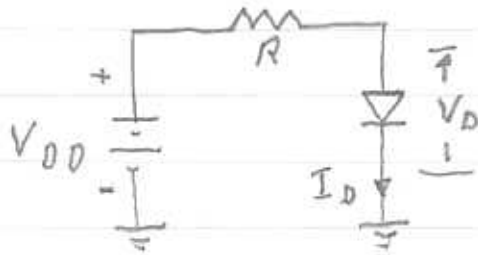
T = $^{\circ}\text{K}$

$$(1a) \quad i_D \approx I_S e^{N_D/V_T n}$$

$$(1b) \quad \therefore N_D \approx n V_T \ln(i_D/I_S)$$

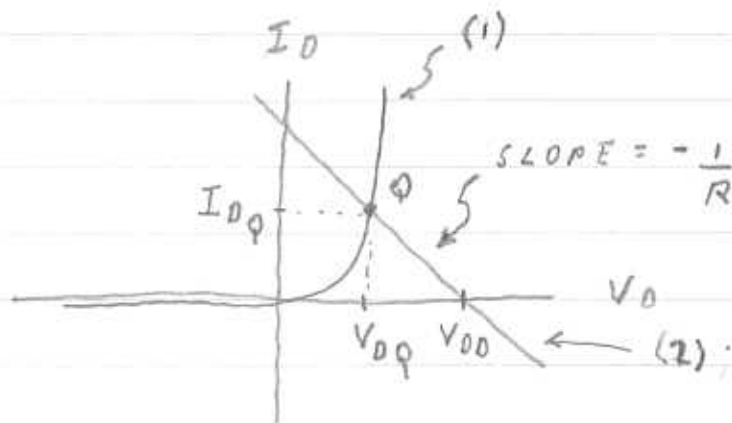
} for $N_D > 100 \text{ mV}$

ANALYSIS OF DIODE CIRCUITS

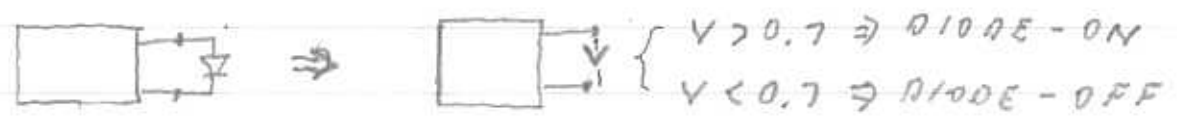
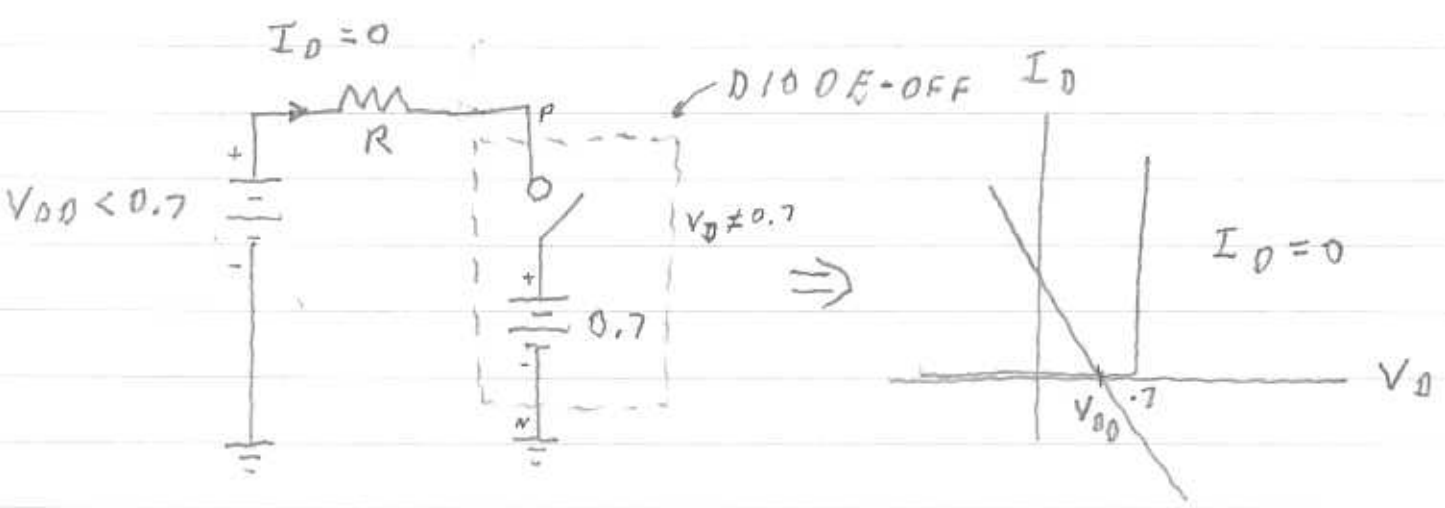
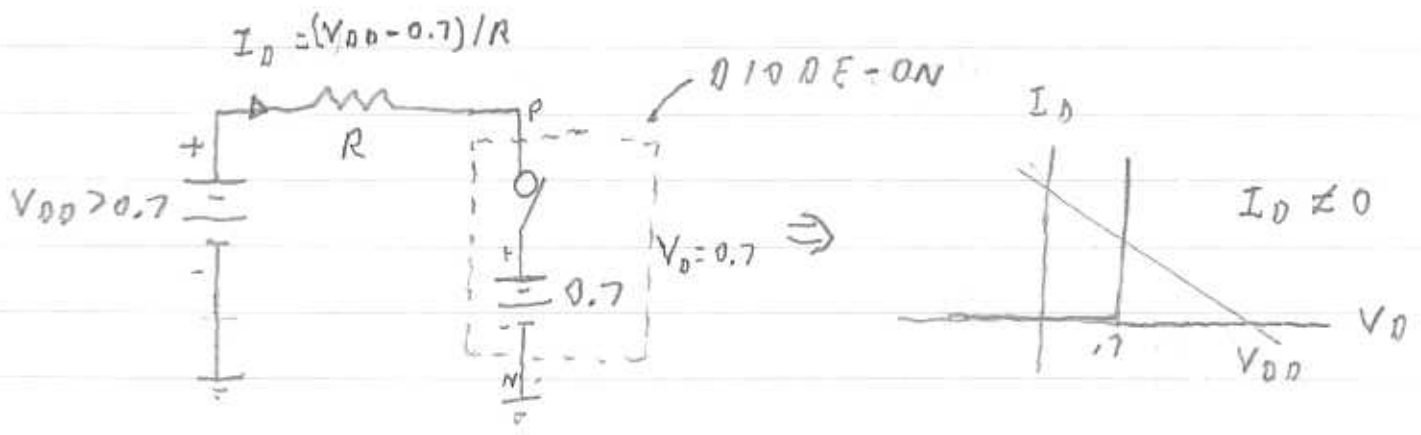
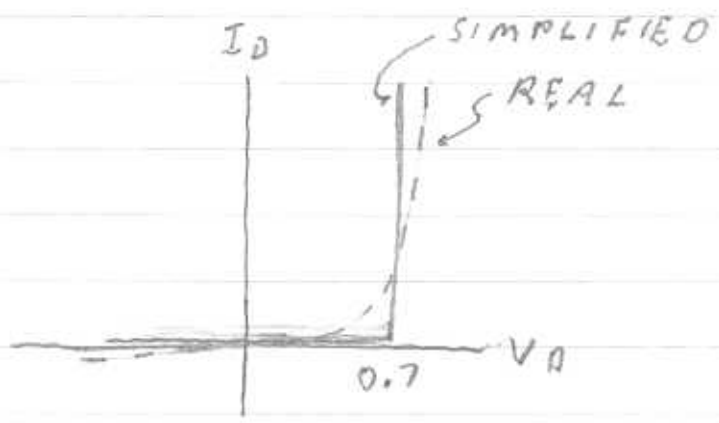


$$\begin{aligned}
 (2) \quad V_{DD} &= V_D + R I_D && \leftarrow \text{load line equation} \\
 (1) \quad I_D &= I_S (e^{V_D/V_T} - 1) && \leftarrow \text{diode characteristics}
 \end{aligned}$$

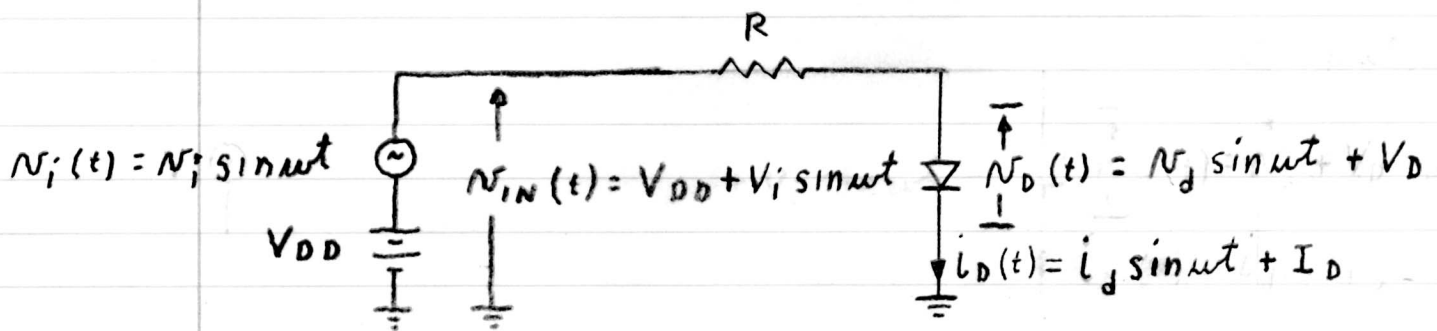
GRAPHICAL ANALYSIS:



SIMPLIFIED DIODE MODEL: USE FOR DC CIRCUIT

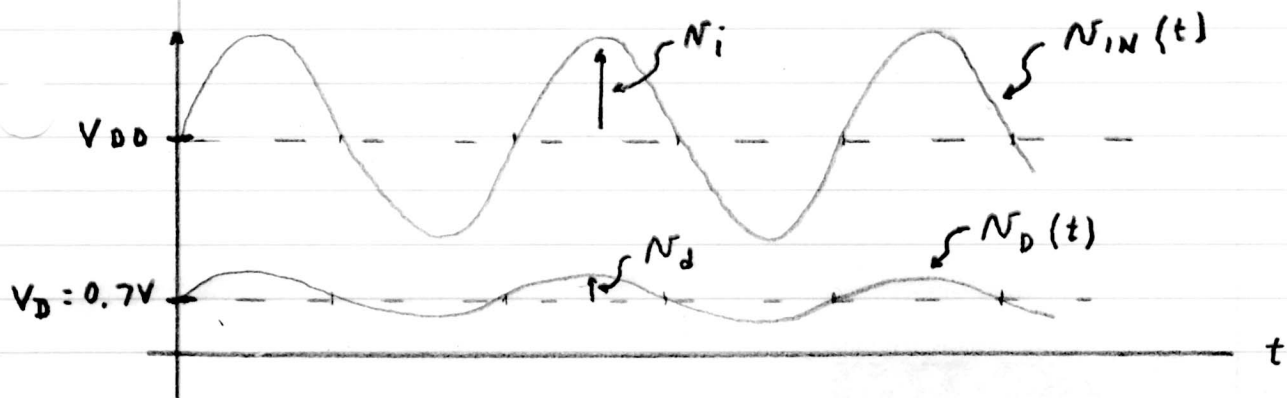


ANALYZE A DIODE CIRCUIT WITH AN AC & DC SOURCE

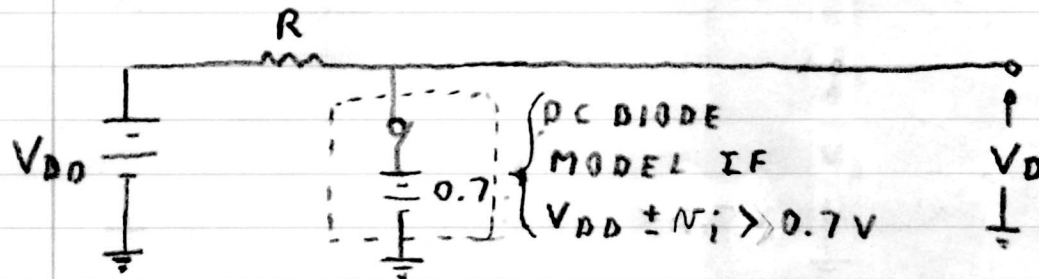


$$(1) i_D(t) = I_S (e^{V_D(t)/V_T} - 1)$$

$$(2) \underbrace{V_{DD} + V_i \sin \omega t}_{V_{DIN}(t)} = V_D(t) + R i_D(t)$$



I) WE WILL FIND V_D AND I_D FROM THE DC CIRCUIT



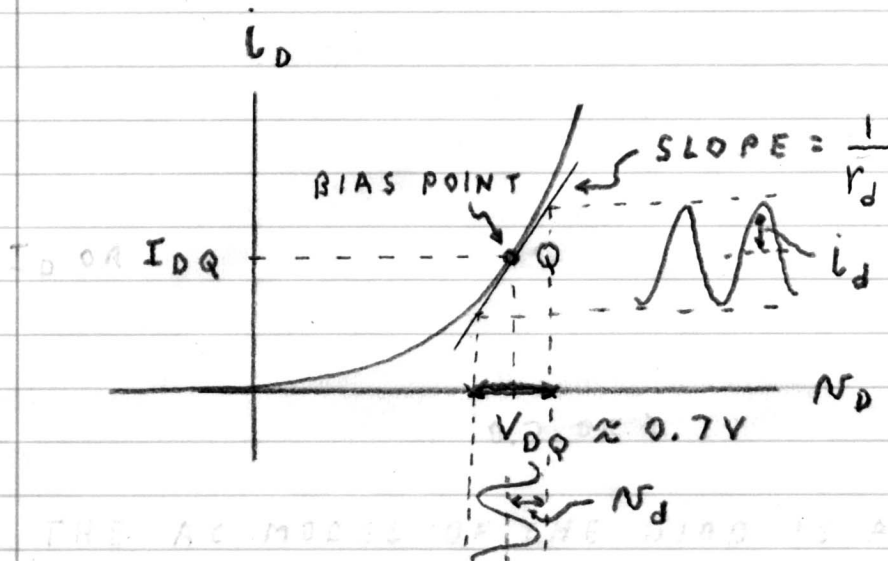
THE V_D & I_D THAT RESULTS FROM THE DC SOURCE IS THE BIAS OR 'Q' POINT

$V_D = 0.7V$
 $I_D = (V_{DD} - 0.7) / R$

II) WE WILL FIND N_d AND I_d FROM THE AC CIRCUIT

BUT FIRST WE MUST FIND THE "AC" MODEL OF THE DIODE.

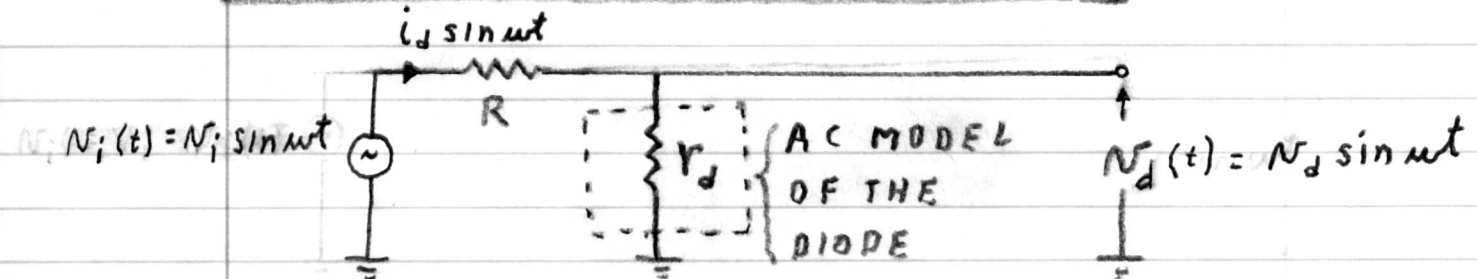
SMALL SIGNAL (AC) DIODE MODEL ; USED FOR AC CIRCUIT UNDER SMALL SIGNAL CONDITIONS



THE AC MODEL OF THE DIODE IS A RESISTOR WHOSE VALUE IS EQUAL TO r_d

THE AC MODEL OF THE DIODE IS A RESISTOR WHOSE VALUE IS EQUAL TO r_d . (r_d IS A DYNAMIC RESISTOR)

AC CIRCUIT (LINEARIZED CIRCUIT)



$$N_d(t) = N_d \sin \omega t = N_i(t) \left[\frac{r_d}{r_d + R} \right] = N_i \left[\frac{r_d}{r_d + R} \right] \sin \omega t$$

$$N_d = \frac{N_i r_d}{r_d + R}$$

THUS: $N_D(t) = V_D + N_D \sin \omega t$

$$N_D(t) = \underset{\substack{\uparrow \\ \text{BIAS VOLTAGE}}}{0.7} + N_i \underbrace{\left[\frac{r_d}{r_d + R} \right]}_{\text{AC SIGNAL}} \sin \omega t$$

FIND r_d

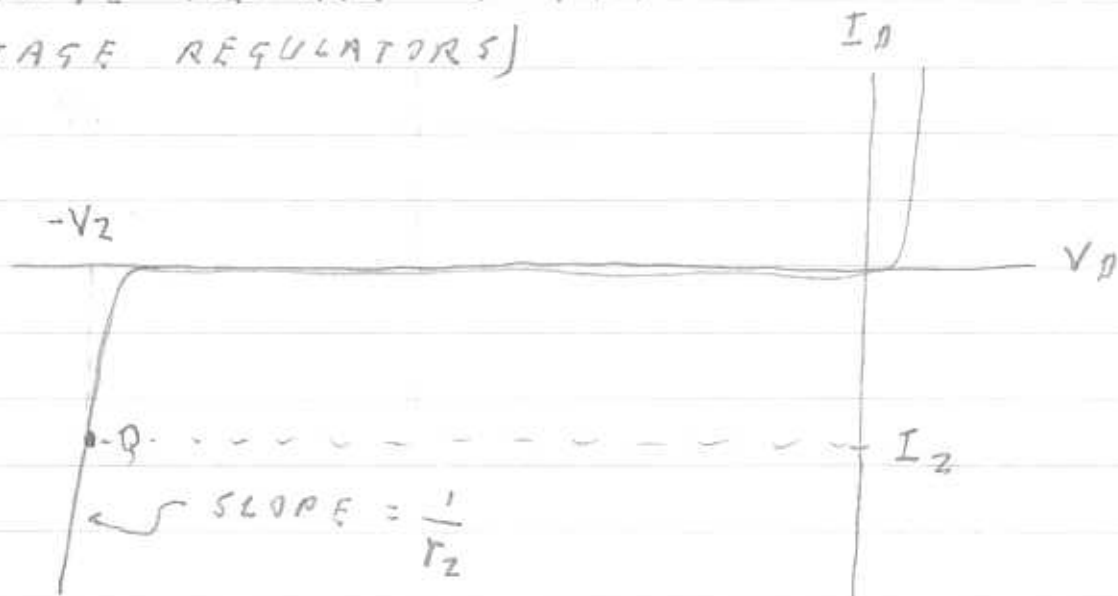
$$r_d = \left. \frac{dV_D}{dI_D} \right|_{I_D = I_{DQ}}$$

$$I_D = I_S (e^{V_D/V_T} - 1) \approx I_S e^{V_D/V_T} ; V_D \geq 100 \text{ mV}$$

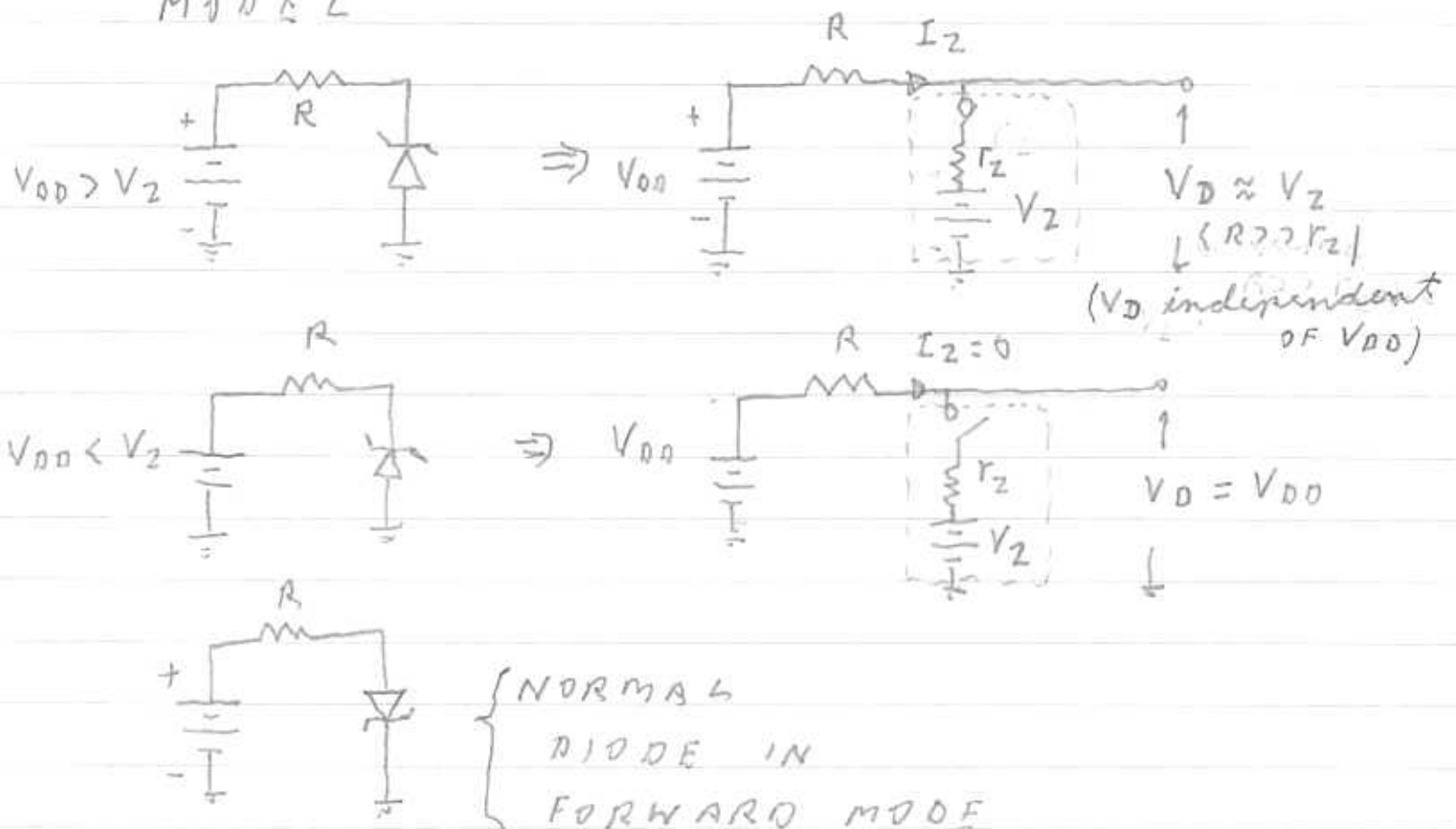
$$1/r_d = \left. \frac{dI_D}{dV_D} \right|_Q = \frac{I_S}{V_T} e^{V_D/V_T} = \left. \frac{I_D}{V_T} \right|_Q = \frac{I_{DQ}}{V_T} \approx \frac{I_{DQ}}{25 \text{ mV}}$$

$$r_d = V_T / I_{DQ}$$

REVERSE BREAKDOWN REGION - ZENER DIODES (VOLTAGE REFERENCE FOR VOLTAGE REGULATORS)

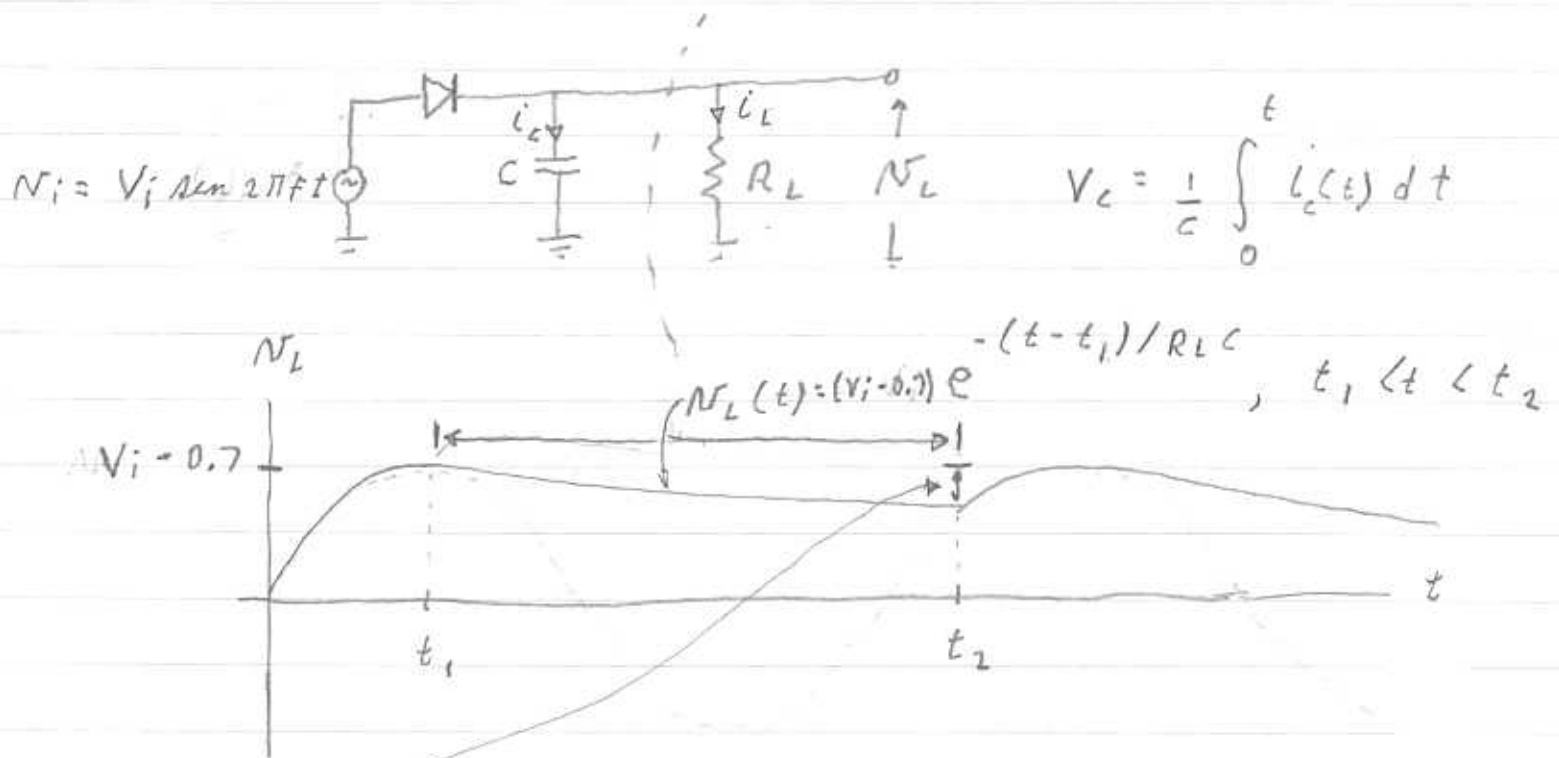


MODEL



USES OF DIODES

Half Wave Rectifier with filtering Capacitor (Produces DC from AC)

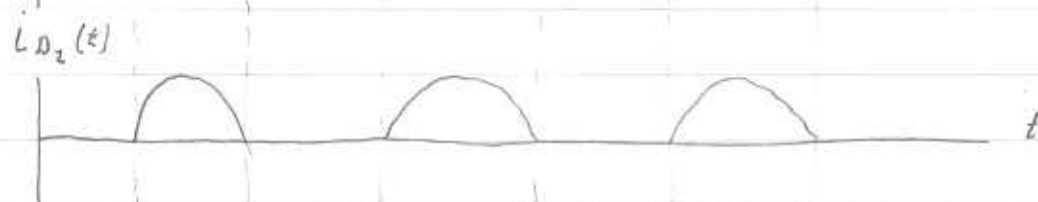
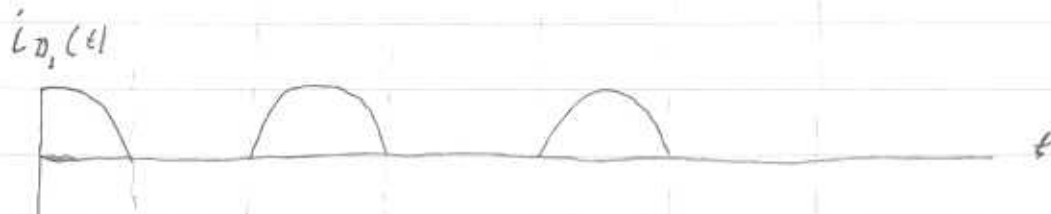
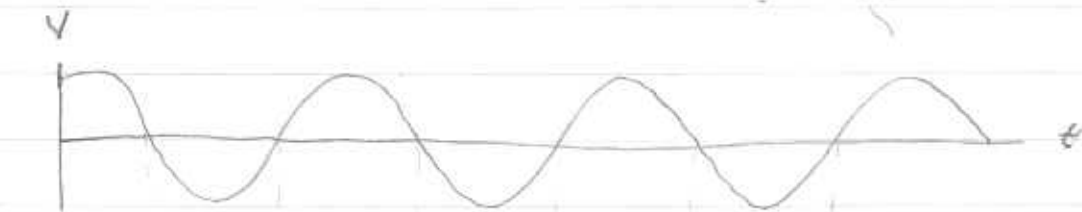
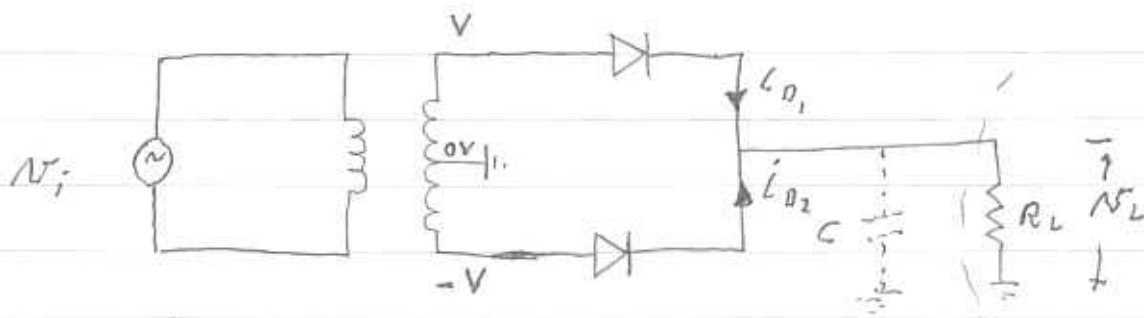


$V_{RIP} \equiv$ Peak to peak ripple

$$V_{RIP} \approx \frac{V_i (t_2 - t_1)}{R_L C} \quad \text{for } V_{RIP} \ll V_i$$

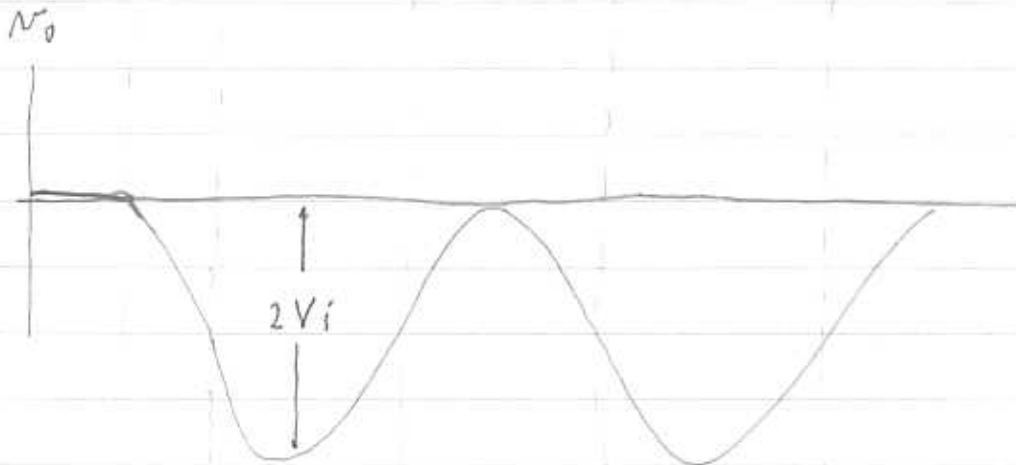
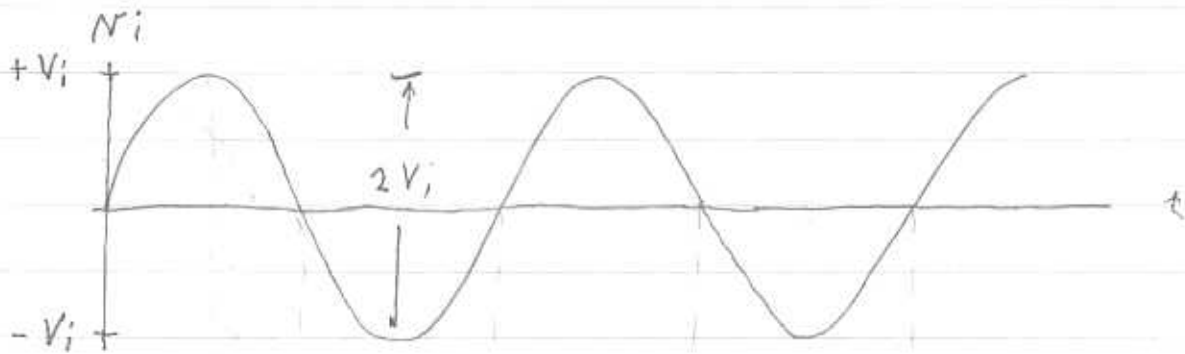
$$\approx \frac{V_i}{R_L C f}, \quad t_2 - t_1 \approx \frac{1}{f}$$

Full-wave rectifier



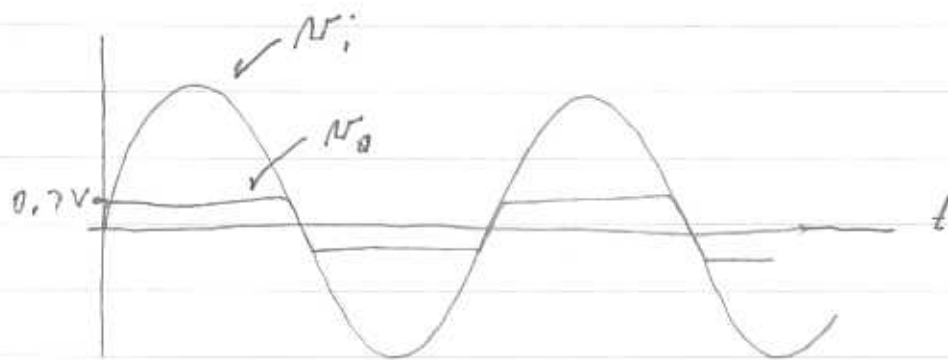
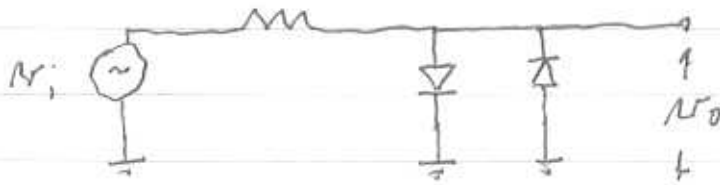
$t_2 - t_1$ is less

Clamping Circuit



output is shifted "down" by V_i volts

limiter



ERRATA



Temperature Effects

V_D is a function of temperature mainly because I_S is a function of temperature

$$V_D(T_2) - V_D(T_1) \approx -k(T_2 - T_1) \text{ for } I_D \text{ constant}$$

for silicon diode biased at $V_D \approx 0.7V$ $k = 2mV/^\circ C$

$$\Delta V_D = -k \Delta T$$