

Analysis of the Nonlinear Stochastic Dynamics of an Elastic Bar with an Attached End Mass

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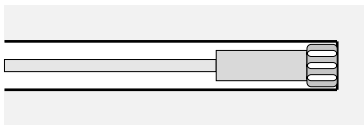
Outline

- 1 Introduction
- 2 Deterministic Approach
- 3 Stochastic Approach
- 4 Numerical Experiments
- 5 Conclusion

Motivation: structures with small devices

Some **engineering structures** have **small parts** (negligible dimensions), which induce **significant effects** on their **global behavior**.

- drill-bit on a drillstring;
- stabilizers on a column;
- buckyball on a carbon nanotube;
- etc.



Modeling and uncertainties

Typical modeling:

- continuous system coupled with discrete elements.

But these models are subjected uncertainties due to:

- variability in the system parameters;
- inaccuracies in model conception.

Research objectives

This work intends to:

- Illustrates a consistent methodology to analyze the stochastic nonlinear dynamics of a continuous system attached to discrete elements.
- Investigate the effects of a coupled discrete elements in the dynamic response of this nonlinear stochastic system.

Physical system: fixed-mass-spring bar

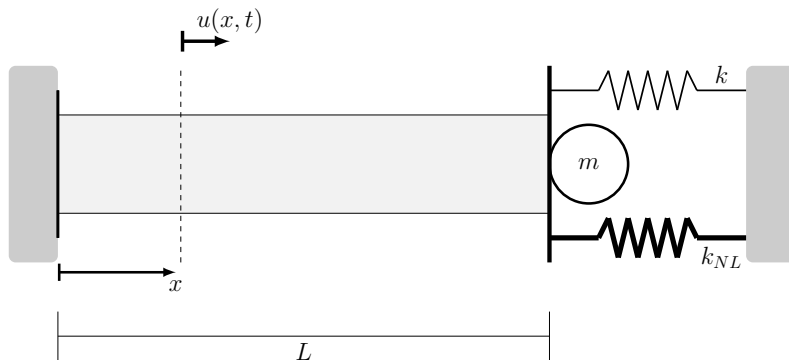


Figure: Sketch of a bar fixed at one and attached to two springs and a lumped mass on the other extreme, i.e. a **fixed-mass-spring bar**.

Strong formulation

Find a *suitable displacement field* that satisfies

$$\rho A \frac{\partial^2 u}{\partial t^2} + c \frac{\partial u}{\partial t} - \frac{\partial}{\partial x} \left(EA \frac{\partial u}{\partial x} \right) + \left(ku + k_{NL} u^3 + m \frac{\partial^2 u}{\partial t^2} \right) \delta(x - L) = f(x, t)$$

as well as the *boundary conditions*

$$u(0, t) = 0, \quad \text{and} \quad EA \frac{\partial u}{\partial x}(L, t) = 0,$$

and the *initial conditions*

$$u(x, 0) = u_0(x), \quad \text{and} \quad \frac{\partial u}{\partial t}(x, 0) = v_0(x).$$

Weak formulation

Find *suitable* $u \in \mathcal{U}_t$ that satisfies the **weak equation of motion**

$$\mathcal{M}(\ddot{u}, w) + \mathcal{C}(\dot{u}, w) + \mathcal{K}(u, w) = \mathcal{F}(w) + \mathcal{F}_{NL}(u, w),$$

for all weight $w \in \mathcal{W}$, as well as the **weak form of initial conditions**

$$\widetilde{\mathcal{M}}(u(\cdot, 0), w) = \widetilde{\mathcal{M}}(u_0, w),$$

and

$$\widetilde{\mathcal{M}}(\dot{u}(\cdot, 0), w) = \widetilde{\mathcal{M}}(v_0, w).$$

Model equation discretization

The model equation is discretized by the **Galerkin method**

$$u(x, t) \approx \sum_{n=1}^N u_n(t) \phi_n(x),$$

where ϕ_n are orthogonal modes and u_n are time-dependent functions.

The result is a $N \times N$ set of **nonlinear ordinary differential equations**

$$[M] \ddot{\mathbf{u}}(t) + [C] \dot{\mathbf{u}}(t) + [K] \mathbf{u}(t) = \mathbf{f}(t) + \mathbf{f}_{NL}(\mathbf{u}(t)),$$

supplemented by a pair of initial conditions

$$\mathbf{u}(0) = \mathbf{u}_0 \quad \text{and} \quad \dot{\mathbf{u}}(0) = \mathbf{v}_0.$$

Nonlinear ODE system solution

The **Newmark method** is used for temporal integration

$$\mathbf{v}_{n+1} = \mathbf{v}_n + (1 - \gamma)\Delta t \mathbf{a}_n + \gamma\Delta t \mathbf{a}_{n+1},$$

$$\mathbf{d}_{n+1} = \mathbf{d}_n + \Delta t \mathbf{v}_n + \left(\frac{1}{2} - \beta\right) \Delta t^2 \mathbf{a}_n + \beta \Delta t^2 \mathbf{a}_{n+1}.$$

where \mathbf{d}_n , \mathbf{v}_n and \mathbf{a}_n are approximations to $\mathbf{u}(t_n)$, $\dot{\mathbf{u}}(t_n)$ and $\ddot{\mathbf{u}}(t_n)$.

The result is a **nonlinear system of algebraic equations** with unknowns \mathbf{d}_n , \mathbf{v}_n and \mathbf{a}_n , solved by **Newton-Rapson method**.

Stochastic initial-boundary value problem

Given a probability space $(\Omega, \mathbb{A}, \mathbb{P})$, and considering that E and $f(x, t)$ are stochastic, find a *suitable* random displacement field

$$U : \Omega \times [0, L] \times [0, T] \rightarrow \mathbb{R},$$

which satisfies

$$\begin{aligned} \rho A \frac{\partial^2 U}{\partial t^2} + c \frac{\partial U}{\partial t} - \frac{\partial}{\partial x} \left(\mathbf{E} A \frac{\partial U}{\partial x} \right) \\ + \left(kU + k_{NL} U^3 + m \frac{\partial^2 U}{\partial t^2} \right) \delta(x - L) = F(\omega, x, t) \end{aligned}$$

as well as *appropriate* boundary and initial conditions.

Random external force

The external force is modeled as the **random field** such that

$$F(\omega, x, t) = \sigma \sin \left(\lambda_1 \frac{x}{L} \right) N(\omega, t),$$

where the $N(\omega, t)$ is a normalized **Gaussian white noise**.

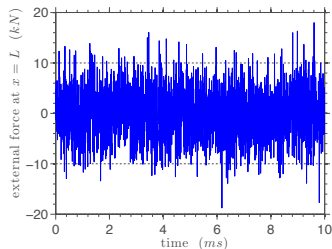


Figure: This figure illustrates a Gaussian white noise realization.

Random elastic modulus

The elastic modulus is modeled as a **random variable**.

According to the **maximum entropy principle**, the probability density function of \mathbf{E} maximizes the entropy

$$\mathbb{S}(p_{\mathbf{E}}) = - \int_0^{\infty} p_{\mathbf{E}}(\xi) \ln(p_{\mathbf{E}}(\xi)) d\xi,$$

subjected to the constraints:

- $\int_0^{\infty} p_{\mathbf{E}}(\xi) d\xi = 1,$
- $\mathbb{E}[\mathbf{E}] = \mu_{\mathbf{E}},$
- $\mathbb{E}[\ln(\mathbf{E})] < \infty \quad \implies \quad \mathbb{E}[\mathbf{E}^2] < \infty.$

Random elastic modulus

The maximum entropy PDF corresponds to a **gamma distribution**

$$p_{\mathbf{E}}(\xi) = \mathbb{1}_{(0,\infty)} \frac{1}{\mu_{\mathbf{E}}} \left(\frac{1}{\delta_{\mathbf{E}}^2} \right)^{\left(\frac{1}{\delta_{\mathbf{E}}^2} \right)} \frac{1}{\Gamma(1/\delta_{\mathbf{E}}^2)} \left(\frac{\xi}{\mu_{\mathbf{E}}} \right)^{\left(\frac{1}{\delta_{\mathbf{E}}^2} - 1 \right)} \exp \left(-\frac{\xi}{\delta_{\mathbf{E}}^2 \mu_{\mathbf{E}}} \right).$$

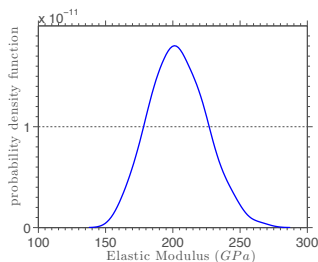


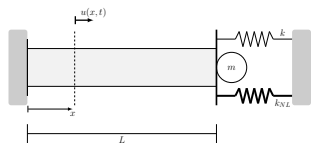
Figure: This figure illustrates the elastic modulus PDF.

Stochastic simulation

Monte Carlo method, with 4096 realizations of \mathbf{E} and F , is used to compute the uncertainty propagation.

deterministic parameters:

- $\rho = 7900 \text{ kg/m}^3$
- $L = 1 \text{ m}$
- $A = 625\pi \text{ mm}^2$
- $c = 5 \text{ kNs/m}$
- $k = 650 \text{ N/m}$
- $k_{NL} = 650 \times 10^{13} \text{ N/m}^3$
- $\sigma = 5 \text{ kN/m}$
- $\alpha_1 = 0.1 \text{ mm}$
- $\alpha_2 = 0.5 \times 10^{-3}$



initial conditions:

- $u_0(x) = \alpha_1 \sin\left(\lambda_3 \frac{x}{L}\right) + \alpha_2 x$
- $v_0(x) = 0$

parametric study:

- $\frac{m}{\rho AL} = 0.1, 1, 10, \text{ and } 50$

Mean value and interval of confidence for $U(\cdot, L, \cdot)$

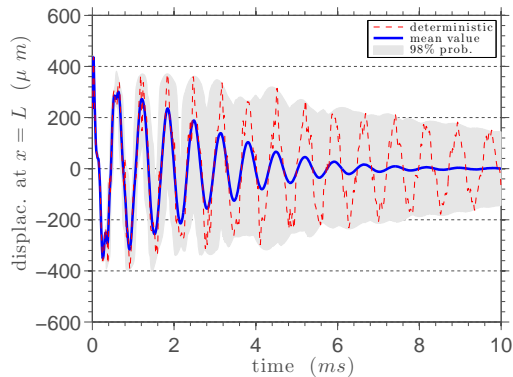


Figure: This figure illustrates the mean value (blue line) and an interval of confidence (grey shadow) for the random process $U(\cdot, L, \cdot)$, with $\frac{m}{\rho AL} = 0.1$.

Mean value and interval of confidence for $U(\cdot, L, \cdot)$

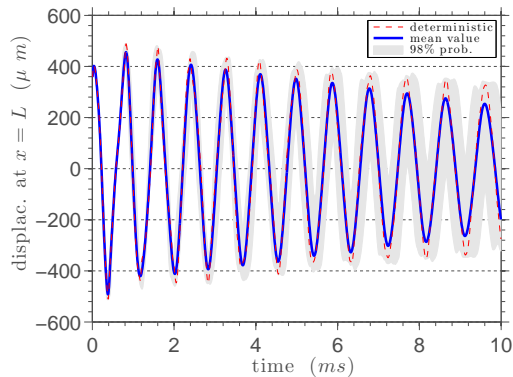


Figure: This figure illustrates the mean value (blue line) and an interval of confidence (grey shadow) for the random process $U(\cdot, L, \cdot)$, with $\frac{m}{\rho AL} = 1$.

Mean value and interval of confidence for $U(\cdot, L, \cdot)$

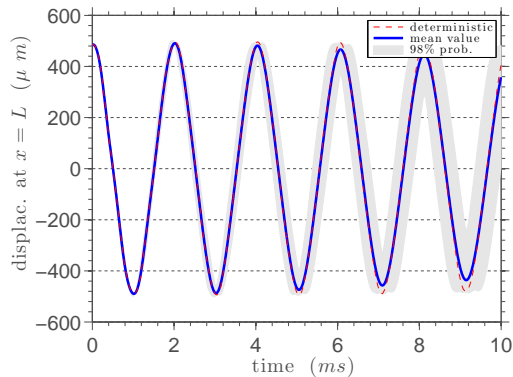


Figure: This figure illustrates the mean value (blue line) and an interval of confidence (grey shadow) for the random process $U(\cdot, L, \cdot)$, with $\frac{m}{\rho AL} = 10$.

Mean value and interval of confidence for $U(\cdot, L, \cdot)$

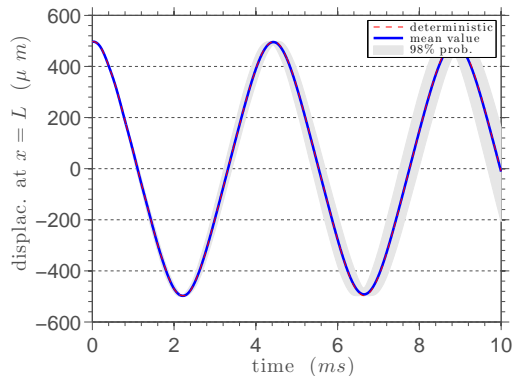
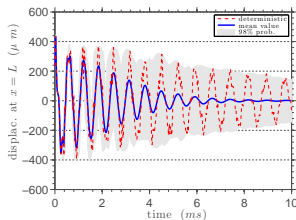
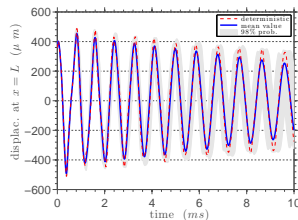


Figure: This figure illustrates the mean value (blue line) and an interval of confidence (grey shadow) for the random process $U(\cdot, L, \cdot)$, with $\frac{m}{\rho AL} = 50$.

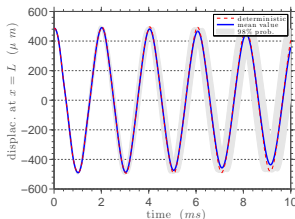
Mean value and interval of confidence for $U(\cdot, L, \cdot)$



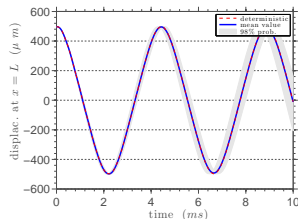
(a) $\frac{m}{\rho AL} = 0.1$



(b) $\frac{m}{\rho AL} = 1$



(c) $\frac{m}{\rho AL} = 10$



(d) $\frac{m}{\rho AL} = 50$

Mean phase space of fixed-mass-spring bar at $x = L$

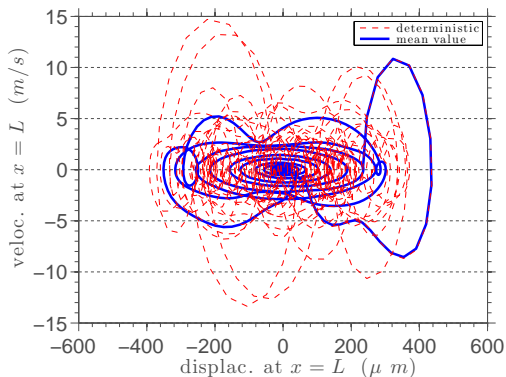


Figure: This figure illustrates the mean phase space of fixed-mass-spring bar at $x = L$, with $\frac{m}{\rho AL} = 0.1$.

Mean phase space of fixed-mass-spring bar at $x = L$

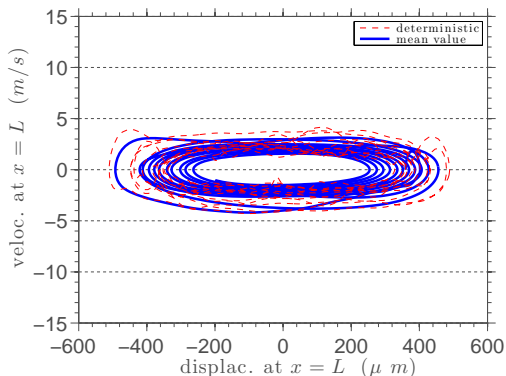


Figure: This figure illustrates the mean phase space of fixed-mass-spring bar at $x = L$, with $\frac{m}{\rho AL} = 1$.

Mean phase space of fixed-mass-spring bar at $x = L$

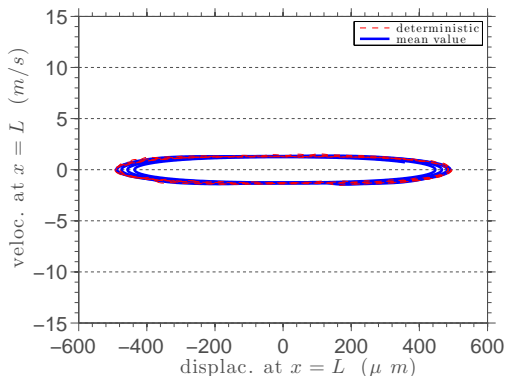


Figure: This figure illustrates the mean phase space of fixed-mass-spring bar at $x = L$, with $\frac{m}{\rho AL} = 10$.

Mean phase space of fixed-mass-spring bar at $x = L$

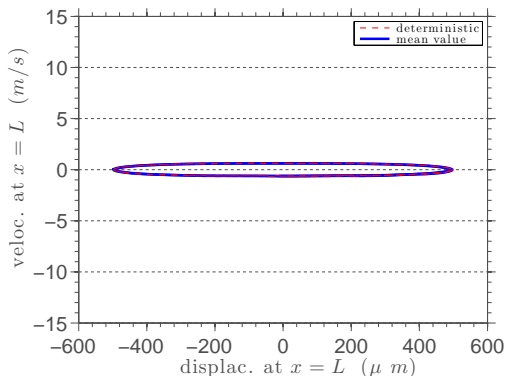
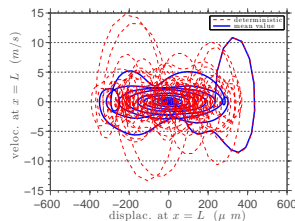
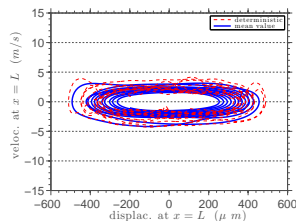


Figure: This figure illustrates the mean phase space of fixed-mass-spring bar at $x = L$, with $\frac{m}{\rho AL} = 50$.

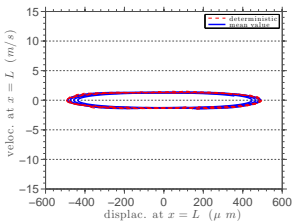
Mean phase space of fixed-mass-spring bar at $x = L$



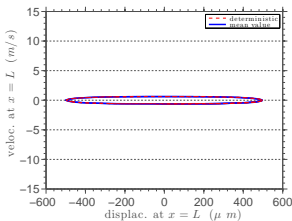
(a) $\frac{m}{\rho AL} = 0.1$



(b) $\frac{m}{\rho AL} = 1$



(c) $\frac{m}{\rho AL} = 10$



(d) $\frac{m}{\rho AL} = 50$

Power spectral density of $\dot{U}(\cdot, L, \cdot)$

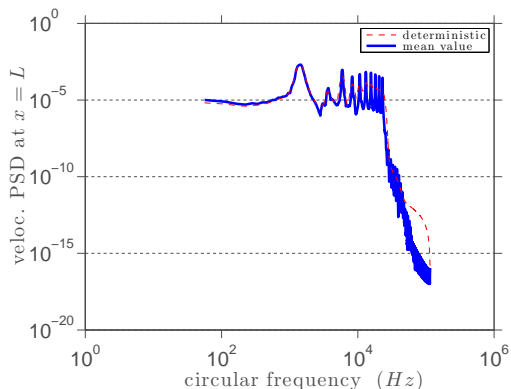


Figure: This figure illustrates the power spectral density for the random process $\dot{U}(\cdot, L, \cdot)$, with $\frac{m}{\rho AL} = 0.1$.

Power spectral density of $\dot{U}(\cdot, L, \cdot)$

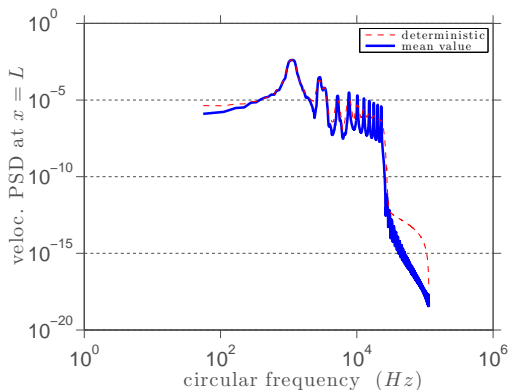


Figure: This figure illustrates the power spectral density for the random process $\dot{U}(\cdot, L, \cdot)$, with $\frac{m}{\rho AL} = 1$.

Power spectral density of $\dot{U}(\cdot, L, \cdot)$

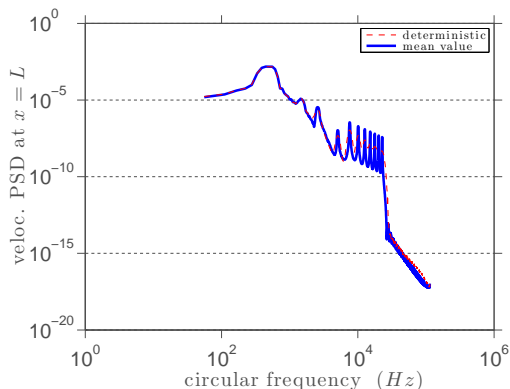


Figure: This figure illustrates the power spectral density for the random process $\dot{U}(\cdot, L, \cdot)$, with $\frac{m}{\rho AL} = 10$.

Power spectral density of $\dot{U}(\cdot, L, \cdot)$

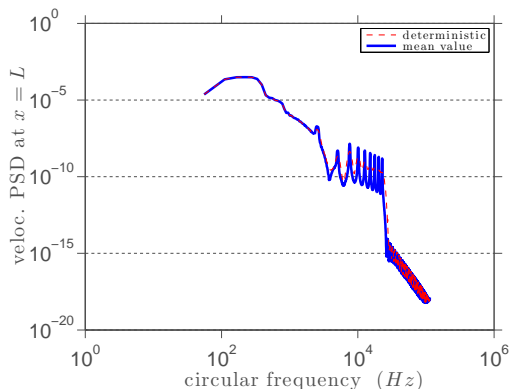
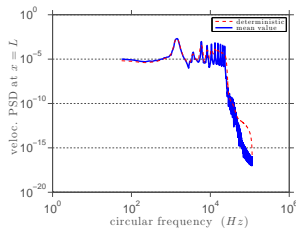
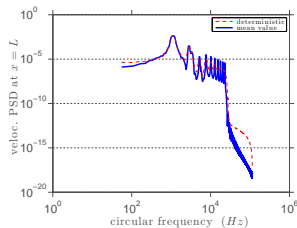


Figure: This figure illustrates the power spectral density for the random process $\dot{U}(\cdot, L, \cdot)$, with $\frac{m}{\rho AL} = 50$.

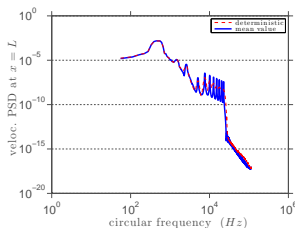
Power spectral density of $\dot{U}(\cdot, L, \cdot)$



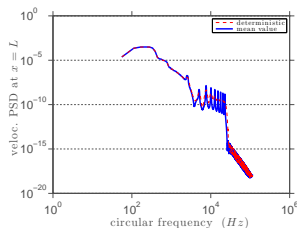
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(b) $\frac{m}{\rho AL} = 1$



(c) $\frac{m}{\rho AL} = 10$



(d) $\frac{m}{\rho AL} = 50$

Probability density function of $U(\cdot, L, T)$

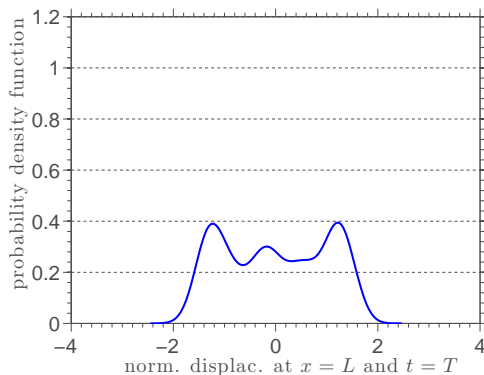


Figure: This figure illustrates an estimation to the PDF of the (normalized) random variable $U(\cdot, L, T)$, with $\frac{m}{\rho AL} = 0.1$.

Probability density function of $U(\cdot, L, T)$

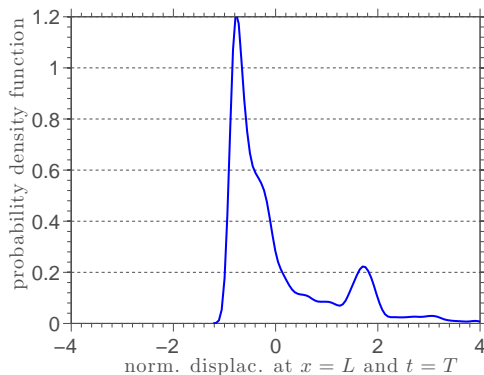


Figure: This figure illustrates an estimation to the PDF of the (normalized) random variable $U(\cdot, L, T)$, with $\frac{m}{\rho AL} = 1$.

Probability density function of $U(\cdot, L, T)$

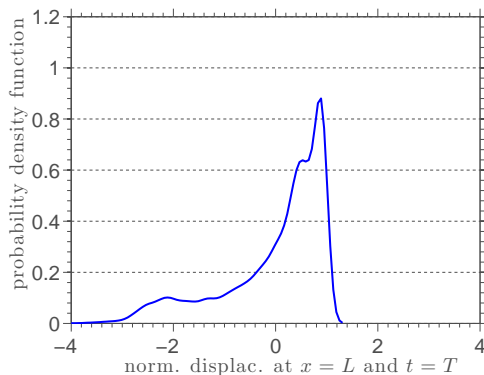


Figure: This figure illustrates an estimation to the PDF of the (normalized) random variable $U(\cdot, L, T)$, with $\frac{m}{\rho AL} = 10$.

Probability density function of $U(\cdot, L, T)$

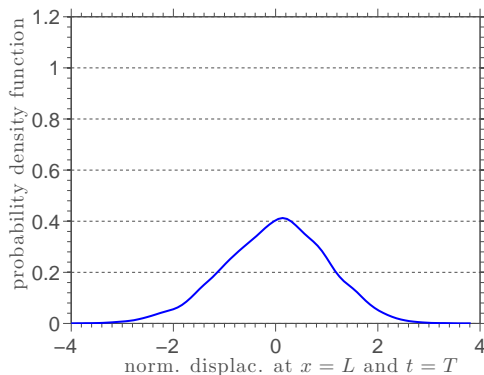
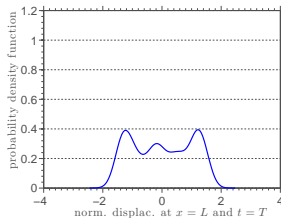
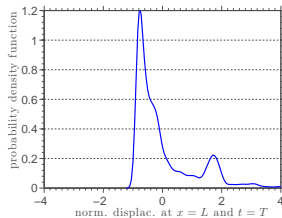


Figure: This figure illustrates an estimation to the PDF of the (normalized) random variable $U(\cdot, L, T)$, with $\frac{m}{\rho AL} = 50$.

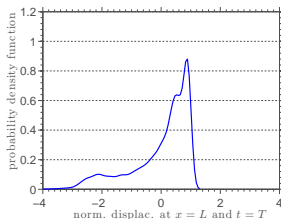
Probability density function of $U(\cdot, L, T)$



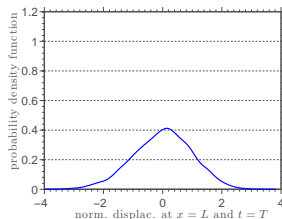
(a) $\frac{m}{\rho AL} = 0.1$



(b) $\frac{m}{\rho AL} = 1$



(c) $\frac{m}{\rho AL} = 10$



(d) $\frac{m}{\rho AL} = 50$

Concluding remarks




- This work illustrates a consistent methodology to analyze the stochastic dynamics of a continuous/discrete system;
- Large values of the lumped mass makes the behavior of the continuous system like a mass-spring oscillator;
- A reduction of uncertainty in the system response is observed when the lumped mass increases;
- An irregular energy distribution through the spectrum occurs maybe due to the spring cubic nonlinearity;
- The system response presents multimodal distributions.

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References

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