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Taiji Data Challenge II Manual

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(Taiji Data Challenge Working Group)

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4 CONTENTS

5	I. Introduction	2
6	A. Taiji project for space-based gravitational wave detection	2
7	B. A brief introduction to Taiji Data Challenge II and Triangle	3
8	II. Sources & waveforms	5
9	A. Massive black hole binaries	5
10	B. Extreme mass-ratio inspirals	6
11	C. Galactic binaries	6
12	D. Stochastic gravitational wave background	7
13	III. Mock Data Generation	8
14	A. Laser interferometric measurements	8
15	B. Gravitational wave response	14
16	C. Data anomalies	15
17	D. Time-delay interferometry	15
18	References	16

19 I. INTRODUCTION

20 A. Taiji project for space-based gravitational wave detection

21 Taiji is a Chinese space mission proposed to detect gravitational waves (GWs) in the 0.1
22 mHz - 1 Hz frequency band [1, 2], which is expected to be launched in the 2030s. Similar
23 to the European mission Laser Interferometer Space Antenna (LISA), the Taiji detector
24 consists of three spacecrafts (SCs), and each SC follows a heliocentric orbit, forming a giant
25 equilateral triangle with nominal arm lengths of approximately 3 million kilometers. The
26 center of mass of the constellation leads the Earth by about 20 degrees, and is about 1 AU
27 away from the Sun.

28 The science operation of Taiji will last for at least 5 years, during which it will be observing
29 burst, continuous and stochastic GW signals. Taiji's target GW sources include $\mathcal{O}(10^7)$
30 Galactic and extra-Galactic binaries (GBs) ($\mathcal{O}(10^4)$ resolvable, others forming a confusion

31 foreground), $\mathcal{O}(10) - \mathcal{O}(10^2)$ massive black hole binaries (MBHBs), $\mathcal{O}(1) - \mathcal{O}(10^3)$ extreme
 32 mass-ratio inspirals (EMRIs), $\mathcal{O}(1) - \mathcal{O}(10)$ stellar-mass black hole binaries (sBHBs), as well
 33 as the astrophysical and/or cosmological stochastic GW backgrounds (SGWBs), *etc.*



FIG. 1. Taiji mission concept (Credit: Ref. [1]).

34 B. A brief introduction to Taiji Data Challenge II and Triangle

35 Compared to the current observations of LIGO-Virgo-KAGRA, the data of Taiji is pre-
 36 dicted to exhibit several distinct features: long duration, source overlapping in the time and
 37 frequency domains (especially a considerable fraction of signals with high signal-to-noise ra-
 38 tios (SNRs) up to $\mathcal{O}(10^2) - \mathcal{O}(10^3)$), as well as inevitable glitches, gaps, and non-stationary
 39 noises during the observation period of signals, *etc.* Consequently, “global fit”, namely si-
 40 multaneously fitting all the parameters of GW sources and detector instruments, has been
 41 regarded as the primary challenge for space-based GW data analysis, necessitating both
 42 high speed and high accuracy of the algorithms. To provide testbeds for these algorithms,
 43 both LISA and Taiji have released their simulation datasets, namely the “Data Challenges”,
 44 such as the mock LISA data challenge (MLDC) [3], LISA data challenge (LDC) [4], and the
 45 1st Taiji data challenge (TDC I) [5].

As more than one group has published their prototype global fit analyses [6–8], LDC has basically fulfilled its purpose as a simulation dataset based on idealized orbit configurations, instrumental noises and GW waveforms, and we believe it is now necessary to take a further step to introduce more realities and complexities to the mock data. The purpose of Taiji data challenge II (TDC II) is to discover and address the “new” challenges [TDC paper].

TDC II includes 5 groups of datasets, each designed to manifest specific challenge topics. All the datasets are stored in HDF5 (.h5) files, whose download link can be found in TDC II website [9]. Within the HDF5 files, all the data are organized under the attribute “eta” (for dataset groups 1 and 2) or attributes “interspacecraft_interferometer_carrier”, *etc* (for dataset groups 3 and 4), with the corresponding sampling times stored under “time”.

Accompanying TDC II, an open-source toolkit “Triangle” is also released, which offers the instructions for accessing TDC II data, and enables the injection of customized GW signals and noises, therefore users may have the opportunity to uncover other potential challenges and scientific prospects for Taiji. The whole Triangle toolkit consists 3 code repositories:

- **Triangle-Simulator**: time-domain prototype simulator for the data of space-based GW detectors, which is the code utilized for the creation of TDC II. **Triangle-Simulator** encapsulates the simulation of GW responses, noises, instrumental effects (*e.g.* clock deviations), TDI and other pre-processing steps in a unified pipeline. Tutorials are included to introduce the related concepts, models, as well as how to access TDC II data.
- **Triangle-GB**: frequency-domain 2nd-generation TDI response calculator for GBs, adapted from the GBGPU [10–12] (the GPU version of **FastGB** [13]) to support the numerical orbit interface of **Triangle-Simulator** and 2nd-generation TDI. Examples are provided showcasing simple Bayesian analysis on the TDC II verification dataset 0.1.
- **Triangle-BBH**: frequency-domain 2nd-generation TDI response calculator for MB-HBs. The responses are modeled based on the same numerical orbit interface as **Triangle-Simulator**. Current supported waveform approximants are IMRPhe-nomD/HM implemented in **WF4PY** [14–16] (CPU) and **BBHx** [17–19] (GPU). Examples based on verification dataset 0.2 is offered.

77 With the main features, targets and data components (signals, noises, artifacts) of TDC
78 II data introduced in Ref. [TDC paper], in the following we provide detailed descriptions
79 on the models and mathematical formalism for these components, as well as their code
80 implementations in `Triangle-Simulator`. More ready-to-use instructions can be found in
81 the tutorials of the code.

82 II. SOURCES & WAVEFORMS

83 A. Massive black hole binaries

84 The parametrization of MBHB is shown in TABLE I. Note that this is the parametriza-
85 tion of IMRPhenomD and IMRPhenomT, while for SEOBNRv5EHM, φ_c should be replaced
86 by the reference phase φ_{ref} [rad], and there are 2 additional parameters: reference frequency
87 f_{ref} [Hz] and eccentricity e [1]. For time-domain simulation, we employed the IMRPhe-
88 nomD and IMRPhenomT approximants implemented in `PyCBC` [20] and SEOBNRv5EHM
89 in `pySEOBNR` [21].

TABLE I. The parametrization of MBHB.

parameter	description	unit
$\mathcal{M}_{c,z}$	chirp mass (redshifted)	M_{\odot}
q	mass ratio	1
χ_{z1}	spin of black hole 1	1
χ_{z2}	spin of black hole 2	1
t_c	time of coalescence	day
φ_c	phase at coalescence	rad
D_L	luminosity distance	Mpc
ι	inclination angle	rad
λ	Ecliptic longitude	rad
β	Ecliptic latitude	rad
ψ	polarization angle	rad

B. Extreme mass-ratio inspirals

The parametrization of EMRI (AK model) is shown in TABLE II. The sky location parameters are related to spherical coordinates $\{\theta_S, \phi_S\}$ as $\lambda = \phi_S$ and $\beta = \pi/2 - \theta_S$. The parametrizations of other EMRI waveforms differ from those of AK and can all be found in the data files.

TABLE II. The parametrization of EMRI (AK model).

parameter	description	unit
μ	mass of compact object	M_\odot
M	mass of MBH	M_\odot
Λ	lambda angle	rad
S	spin of the MBH	1
e_0	initial eccentricity	1
ν_0	initial azimuthal orbital frequency	Hz
β	Ecliptic latitude of source	rad
λ	Ecliptic longitude of source	rad
θ_K	polar angle of spin	rad
ϕ_K	azimuthal angle of spin	rad
Φ_0	initial azimuthal orbital phase	rad
$\tilde{\gamma}_0$	initial tidal gamma	rad
α_0	initial alpha angle	rad
D	distance	Gpc

C. Galactic binaries

The parametrization of GB is shown in TABLE III.

In TDC II, the amplitude of GB is defined as

$$A = \frac{2(G\mathcal{M}_c)^{5/3}(\pi f_0)^{2/3}}{c^4 D}, \quad (1)$$

TABLE III. The parametrization of GB.

parameter	description	unit
A	amplitude	1
f_0	initial GW frequency	Hz
\dot{f}_0	initial derivative of GW frequency	Hz/s
φ_0	initial GW phase	rad
ι	inclination angle	rad
λ	Ecliptic longitude	rad
β	Ecliptic latitude	rad
ψ	polarization angle	rad

and our convention for the the source-frame (denoted by superscript “ S ”) polarizations are

$$h_+^S(t) = A(1 + \cos^2 \iota) \cos[\varphi(t)], \quad h_\times^S(t) = 2A \cos \iota \sin[\varphi(t)], \quad (2)$$

where the phase of GW takes a Taylor expansion form:

$$\varphi(t) = 2\pi \left(f_0 t + \frac{1}{2} \dot{f}_0 t^2 + \frac{1}{6} \ddot{f}_0 t^3 \right) + \varphi_0, \quad (3)$$

with

$$\ddot{f}_0 = \frac{11}{3} \frac{\dot{f}_0^2}{f_0}. \quad (4)$$

D. Stochastic gravitational wave background

The parametrization of SGWB varies for different models. For astrophysical SGWB, we adopt a power law model:

$$\Omega_{\text{GW}}(f) = A_{\text{astro}} \left(\frac{f}{f_{\text{astro}}} \right)^{\gamma_{\text{astro}}}, \quad (5)$$

where we fix f_{astro} at 1 mHz, so that the parameter space is 2-D: $\{A_{\text{astro}}, \gamma_{\text{astro}}\}$. While for cosmological SGWB, a double broken power law model is adopted:

$$\Omega_{\text{GW}}(f) = A_{\text{pt}} s^9 \left(\frac{1 + r_b^4}{r_b^4 + s^4} \right)^{(9-b)/4} \left(\frac{b+4}{b+4-m+ms^2} \right)^{(b+4)/2}, \quad (6)$$

where

$$m = \frac{9r_b^4 + b}{r_b^4 + 1}, \quad s = \frac{f}{f_{\text{pt}}}. \quad (7)$$

Therefore it has a 4-D parameter space: $\{A_{\text{pt}}, f_{\text{pt}}, r_b, b\}$.

108 III. MOCK DATA GENERATION

109 Taiji’s data flow incorporates sophisticated in-orbit measurements and on-ground pro-
 110 cessing steps. In order to simulate the performances of instruments and the characteristics
 111 of data within a reasonable timescale, we currently focus on the key information propagated
 112 through the system, rather than implementing a full physical simulation. Given that Taiji’s
 113 scientific data mainly originate from laser interferometric measurements, a brief workflow
 114 for the simulation of TDC II data is presented in FIG. 2.

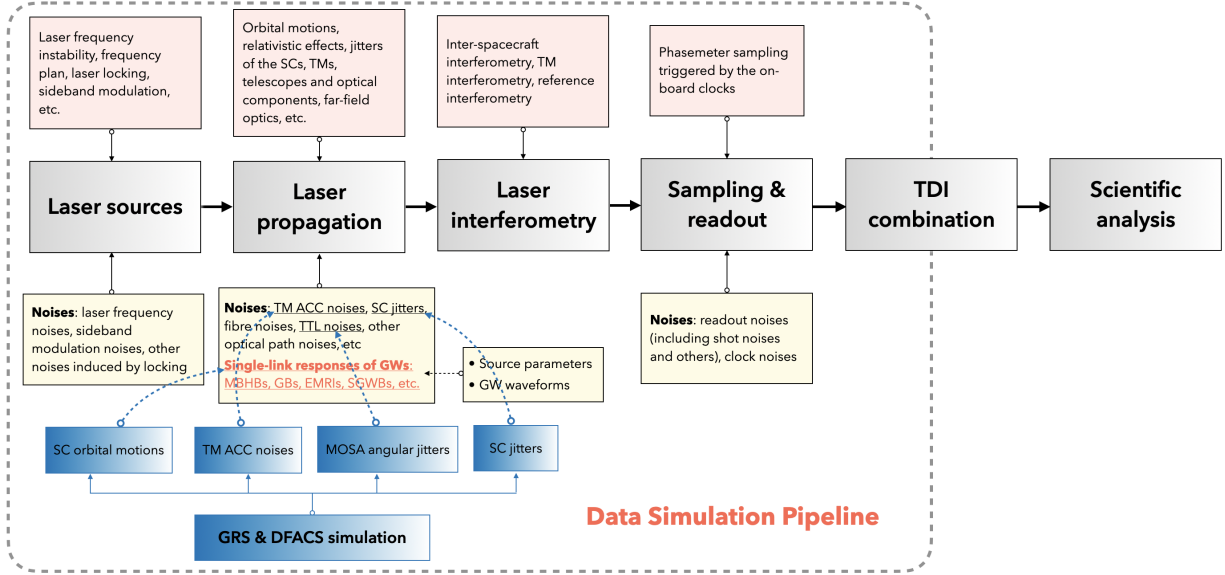


FIG. 2. A brief workflow for the simulation of TDC II data.

115 A. Laser interferometric measurements

116 The models of interferometric measurements basically follows Ref. [22], and we make
 117 adaptations according to the conventions of TDC II. To begin with, we introduce the notations
 118 for two operators, namely the “delay” operator and the “Doppler delay” operator:

$$\mathbf{D}_{ij}f(t) \equiv f[t - d_{ij}(t)], \quad \dot{\mathbf{D}}_{ij}f(t) \equiv [1 - \dot{d}_{ij}(t)] \times f[t - d_{ij}(t)], \quad (8)$$

119 where $d_{ij}(t)$ stands for the light travel time (LTT) from SC_j to SC_i at the reception time
 120 t . The delay operator \mathbf{D}_{ij} is commonly present in the expressions of interferometric mea-
 121 surements and TDI in the early literature. While it was found by Ref. [23] that when

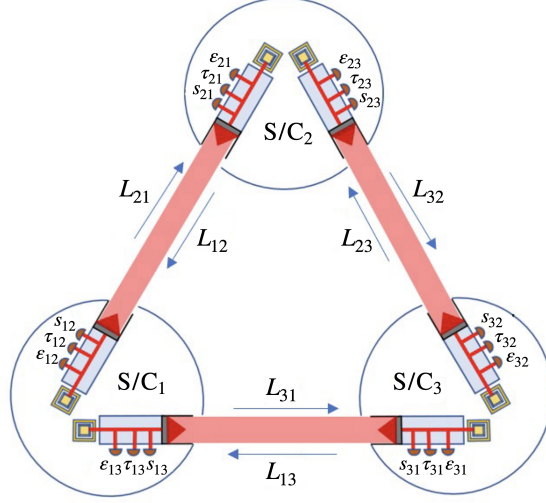


FIG. 3. A schematic of Taiji's detector constellation. Credit: Ref. [26].

interferometric measurements are expressed in units of frequency, the delay operators \mathbf{D}_{ij} should be replaced by their “Doppler” version $\dot{\mathbf{D}}_{ij}$. Note that the difference between \mathbf{D}_{ij} and $\dot{\mathbf{D}}_{ij}$ is only considerable when acted on laser frequency noises, and in the modeling of GW signals and secondary noises, one may safely replace $\dot{\mathbf{D}}_{ij}$ by the original \mathbf{D}_{ij} . For brevity we also define the multiple delay operator $\mathbf{D}_{i_1 i_2 \dots i_{n-1} i_n} f(t)$ as $f(t)$ acted upon by $\mathbf{D}_{i_{n-1} i_n}$, $\mathbf{D}_{i_{n-2} i_{n-1}}$... successively.

In our simulation the LTTs are calculated to the 1st post-Newtonian (PN) order, which takes into consideration the motions of SCs as well as the relativistic corrections due to the gravity of the Sun [24]:

$$d_{ij}(t) = d_{ij}^{0\text{PN}}(t) + d_{ij}^{0.5\text{PN}}(t) + d_{ij}^{1\text{PN}}(t). \quad (9)$$

TDI processing typically requires the LTTs to be measured to the nanosecond accuracy [25]. In above equation, $d_{ij}^{1\text{PN}}(t)$ is usually several hundreds of nanoseconds, and the PN coefficient of Sun-detector system is at the 10^{-8} order, so the next half PN correction is less than 10^{-9} s and can be safely neglected.

As is schematically shown in FIG. 3, there are two movable optical sub-assemblies (MOSAs) symmetrically installed on each SC. MOSA is a structure composed of an optical bench (OB), a laser source, a telescope, and a gravitational reference sensor hosting the test-mass (TM). Each MOSA is labeled by ij ($ij \in \{12, 23, 31, 21, 32, 13\}$), with i being the index of SC carrying this MOSA, and j the index of distant SC that transmits lasers with

140 this MOSA. All the interferometric measurements used for GW detection are taken on the
 141 OBs. Specifically, the ISI mixes the local beam with the distant beam (coming from the
 142 distant MOSA); the TMI mixes the local and adjacent beams, after it has bounced on the
 143 local TM; and the RFI mixes the local and adjacent beams without interaction with the
 144 TM. Moreover, for the purposes of clock noise reduction and inter-spacecraft ranging, *etc*,
 145 “sidebands” are created by modulating clock signals to the lasers, resulting in an additional
 146 sideband interferometric measurement for each interferometer. We label the “original” in-
 147 terferometry with subscript “c” (“c” for carrier), and the sideband interferometry with “sb”
 148 (“sb” for sideband). Note that this might only be a simplified model, and the actual designs
 149 for payloads are still under consideration.

150 The results of laser interferometry are read out by the phasemeters, in terms of the in-
 151 stantaneous frequencies of interfered lasers. Therefore we simulate all the raw measurements
 152 in the frequency (Hz) unit, and each data stream is a time series uniformly spaced in time.
 153 For the sake of understanding and numerical simulation, the laser interferometric data are
 154 usually regarded as the sum of two parts [27]. One is a \sim MHz order slow-varying “offset”
 155 part, and the other is a \sim Hz order jittering “fluctuation” part. The former includes the
 156 effects of laser locking, the frequency plans, the Doppler effects due to orbital motions, *etc*,
 157 and the latter is the combination of various noises and GW signals. Note that this is only
 158 an artificial division and in realistic detection we only have access to the sum of them. The
 159 separation of these two parts is only possible after a “detrending” process. We model laser
 160 interferometry in this “two-variable decomposition” manner, denoting the “offset” parts as
 161 uppercase letters, and the “fluctuation” parts as lowercase letters. The carrier measurement
 162 of ISI reads:

$$\text{ISI}_{c,ij} = S_{c,ij} + s_{c,ij}, \quad (10)$$

163 where the “offset” part is

$$S_{c,ij} = \dot{\mathbf{D}}_{ij} O_{ji}^p - O_{ij}^p - \nu_0 \dot{d}_{ij}, \quad (11)$$

164 and the “fluctuation” part is

$$\begin{aligned} s_{c,ij} = & \dot{\mathbf{D}}_{ij} p_{ji} - p_{ij} + N_{s_{c,ij}}^{\text{ro}} + (\nu_0 + \mathbf{D}_{ij} O_{ji}^p) \left(\dot{\mathbf{D}}_{ij} \Delta_{ji} + \Delta_{ij} \right) \\ & - (\nu_0 + \mathbf{D}_{ij} O_{ji}^p) N_{s_{ij} \leftarrow ji}^{\text{op}} + (\nu_0 + O_{ij}^p) N_{s_{ij} \leftarrow ij}^{\text{op}} + (\nu_0 + \mathbf{D}_{ij} O_{ji}^p) y_{ij}. \end{aligned} \quad (12)$$

165 The sideband measurement of ISI reads

$$\text{ISI}_{sb,ij} = S_{sb,ij} + s_{sb,ij}, \quad (13)$$

166 where

$$S_{sb,ij} = S_{c,ij} + \dot{\mathbf{D}}_{ij} \left[\nu_{ji}^m \left(1 + \dot{O}_j^q \right) \right] - \nu_{ij}^m \left(1 + \dot{O}_i^q \right), \quad (14)$$

167

$$\begin{aligned} s_{sb,ij} = & \dot{\mathbf{D}}_{ij} p_{ji} - p_{ij} + N_{s_{sb,ij}}^{\text{ro}} + \left(\nu_0 + \mathbf{D}_{ij} O_{ji}^{p,sb} \right) \left(\dot{\mathbf{D}}_{ij} \Delta_{ji} + \Delta_{ij} \right) \\ & - \left(\nu_0 + \mathbf{D}_{ij} O_{ji}^{p,sb} \right) N_{s_{ij} \leftarrow ji}^{\text{op}} + \left(\nu_0 + O_{ij}^{p,sb} \right) N_{s_{ij} \leftarrow ij}^{\text{op}} + \left(\nu_0 + \mathbf{D}_{ij} O_{ji}^{p,sb} \right) y_{ij} \\ & + \nu_{ji}^m \dot{\mathbf{D}}_{ij} q_j - \nu_{ij}^m q_i + \nu_{ji}^m \dot{\mathbf{D}}_{ij} N_{ji}^m - \nu_{ij}^m N_{ij}^m. \end{aligned} \quad (15)$$

168 Similarly, for the carrier of RFI:

$$\text{RFI}_{c,ij} = T_{c,ij} + \tau_{c,ij}, \quad (16)$$

169 where

$$T_{c,ij} = O_{ik}^p - O_{ij}^p, \quad (17)$$

170

$$\tau_{c,ij} = p_{ik} - p_{ij} + N_{\tau_{c,ij}}^{\text{ro}} - (\nu_0 + O_{ik}^p) \mu_{ij} - (\nu_0 + O_{ik}^p) N_{\tau_{ij} \leftarrow ik}^{\text{op}} + (\nu_0 + O_{ij}^p) N_{\tau_{ij} \leftarrow ij}^{\text{op}}. \quad (18)$$

171 For the sideband of RFI:

$$\text{RFI}_{sb,ij} = T_{sb,ij} + \tau_{sb,ij}, \quad (19)$$

172 where

$$T_{sb,ij} = T_{c,ij} + (\nu_{ik}^m - \nu_{ij}^m) \left(1 + \dot{O}_i^q \right), \quad (20)$$

173

$$\begin{aligned} \tau_{sb,ij} = & p_{ik} - p_{ij} + N_{\tau_{sb,ij}}^{\text{ro}} - \left(\nu_0 + O_{ik}^{p,sb} \right) \mu_{ij} - \left(\nu_0 + O_{ik}^{p,sb} \right) N_{\tau_{ij} \leftarrow ik}^{\text{op}} + \left(\nu_0 + O_{ij}^{p,sb} \right) N_{\tau_{ij} \leftarrow ij}^{\text{op}} \\ & + \left(\nu_{ik}^m - \nu_{ij}^m \right) q_i + \nu_{ik}^m N_{ik}^m - \nu_{ij}^m N_{ij}^m. \end{aligned} \quad (21)$$

174 For TMIs:

$$\text{TMI}_{c,ij} = E_{c,ij} + \varepsilon_{c,ij}, \quad (22)$$

175 where

$$E_{c,ij} = O_{ik}^p - O_{ij}^p, \quad (23)$$

$$\begin{aligned} \varepsilon_{c,ij} = & p_{ik} - p_{ij} + N_{\varepsilon_{c,ij}}^{\text{ro}} - 2(\nu_0 + O_{ij}^p) \delta_{ij} + 2(\nu_0 + O_{ij}^p) \Delta_{ij} - (\nu_0 + O_{ik}^p) \mu_{ij} \\ & - (\nu_0 + O_{ik}^p) N_{\varepsilon_{ij} \leftarrow ik}^{\text{op}} + (\nu_0 + O_{ij}^p) N_{\varepsilon_{ij} \leftarrow ij}^{\text{op}}. \end{aligned} \quad (24)$$

We do not simulate the sideband of TMI since it's information is duplicated with that of RFI (in the sense of sideband - carrier) In above equations $\nu_0 = 281.6$ THz is the central frequency of lasers, and $\nu_{ij}^m = 2.4/2.401$ GHz for left ($ij \in \{12, 23, 31\}$) /right ($ij \in \{21, 32, 13\}$) MOSAs is the modulation frequency of sidebands. Most importantly, y_{ij} stands for the fractional frequency difference caused by incident GWs. The meanings of other terms can be found in TABLE IV and TABLE V. Notice that above equations are implicitly expressed in a global time frame (Barycenter Coordinate Time of the Solar system, or TCB in short), and the conversion among different time frames (due to clock deviations and relativistic corrections) is not explicitly incorporated. Regarding this part, our treatments are in alignment with Ref. [22].

See Ref. [TDC paper] for the specific noise types injected into each dataset of TDC II. In TDC II, the TM acceleration noises, OB displacement noises (also termed ‘‘SC jitters’’ in Ref. [TDC paper]), and the angular jitters of MOSAs are generated based on a 60-degree-of-freedom numerical simulation of the drag-free & altitude control system (DFACS). The MOSAs’ angular jitters are further used to simulate the inter-spacecraft tilt-to-length (TTL) noises via a simple linear coupling model [28]. Other noises are generated as Gaussian stationary noises according to their corresponding designed power spectral density (PSD) models. For these PSDs, both the amplitudes and spectral shapes can be found in the source codes of **Triangle-Simulator** (**Constants.py** and **Noise.py**). Therefore, it seems that we are not so ‘‘blind’’ about these noises. However, we highly recommend the users to stay agnostic about these noise models, since this is the situation we are very likely to encounter in the future. Meanwhile, the knowledge we might possess is the transfer function of each instrumental noise, which could be crucial for the data-driven characterizations of noise spectra and correlations.

Models in this subsection are implemented via the **Triangle-Simulator.Interferometer.Interferometers** class. Notice that for dataset groups 0, 1 and 2 (*i.e.* the ‘‘scientific’’ datasets), we assume that all the data are perfectly detrended and synchronized to TCB. Therefore, in the simulation outputs, the offset terms (the upper case T , S , E) are elimi-

TABLE IV. The “offset” terms.

offset type	symbol	unit
clock drift	O_i^q	time [s]
carrier laser frequency offset	O_{ij}^p	frequency [Hz]
sideband laser frequency offset	$O_{ij}^{p, sb} = O_{ij}^p + \nu_{ij}^m \left(1 + \dot{O}_i^q\right)$	frequency [Hz]

205 nated, leaving only the fluctuation terms (the lower case s , τ , ε), and the clock drifts along
 206 with clock noises should be neglected. In this case the sideband measurements also become
 207 unnecessary.

TABLE V. Symbols and alias (in **Triangle**) for the noise terms. The instrumental noises are classified into different types mainly based on the form in which they enter the interferometric measurements, rather than their physical origins.

noise type	symbol	alias	unit
laser noise	p_{ij}	laser_noise	frequency [Hz]
readout noise of IFO	$N_{\text{IFO}_{ij}}^{\text{ro}}$	ro_ifo_noise	frequency [Hz]
fibre back link noise	μ_{ij}	bl_noise	optical path derivative [s/s]
optical path noise	$N_{\text{IFO}_{ij \leftarrow kl}}^{\text{op}}$	op_ifo_noise	optical path derivative [s/s]
TM acceleration noise	δ_{ij}	acc_noise	optical path derivative [s/s]
OB displacement noise	Δ_{ij}	ob_noise	optical path derivative [s/s]
clock noise	q_i	clock_noise	time derivative [s/s]
sideband modulation noise	N_{ij}^{m}	modulation_noise	time derivative [s/s]
pseudo ranging noise	N_{ij}^{R}	ranging_noise	time [s]

208 B. Gravitational wave response

209 The single-link response of GW signal is derived under the usual conventions adopted in
 210 the literature [29–31], which is also in consistency with the response model of TDC I [5]:

$$y_{ij}(t) \equiv \frac{\nu_{\text{receive}} - \nu_{\text{send}}}{\nu_{\text{send}}} \approx \frac{1}{2(1 - \hat{\mathbf{k}} \cdot \hat{\mathbf{n}}_{ij}(t_i))} \left[H_{ij} \left(t - \frac{d_{ij}(t)}{c} - \frac{\hat{\mathbf{k}} \cdot \mathbf{R}_j(t)}{c} \right) - H_{ij} \left(t - \frac{\hat{\mathbf{k}} \cdot \mathbf{R}_i(t)}{c} \right) \right], \quad (25)$$

211 where the projection of GW on arm ij is defined as

$$H_{ij} \equiv \mathbf{h} : \hat{\mathbf{n}}_{ij} \otimes \hat{\mathbf{n}}_{ij}, \quad (26)$$

212 with $\hat{\mathbf{k}}$, \mathbf{R}_i , $\hat{\mathbf{n}}_{ij}$ being the wave vector, the position of SC_i in the Solar system barycenter
 213 (SSB) frame, and the arm vector. In terms of Ecliptic longitude and latitude, the coordinate
 214 of $\hat{\mathbf{k}}$ is

$$\hat{\mathbf{k}} = [-\cos \beta \cos \lambda, -\cos \beta \sin \lambda, -\sin \beta]. \quad (27)$$

215 The GW tensor \mathbf{h} reads

$$\mathbf{h} = h_+ \mathbf{e}_+ + h_\times \mathbf{e}_\times. \quad (28)$$

216 We transform the GW waveform from the source frame (denoted with superscript “ S ”) to
 217 the SSB frame via

$$h_+ = \cos 2\psi h_+^S - \sin 2\psi h_\times^S, \quad h_\times = \sin 2\psi h_+^S + \cos 2\psi h_\times^S, \quad (29)$$

218 where

$$\mathbf{e}_+ = \mathbf{u} \otimes \mathbf{u} - \mathbf{v} \otimes \mathbf{v}, \quad \mathbf{e}_\times = \mathbf{u} \otimes \mathbf{v} + \mathbf{v} \otimes \mathbf{u} \quad (30)$$

219 are the polarization basis tensors, which are associated to vectors \mathbf{u} , \mathbf{v} :

$$\mathbf{u} = [\sin \lambda, -\cos \lambda, 0], \quad \mathbf{v} = [-\sin \beta \cos \lambda, -\sin \beta \sin \lambda, \cos \beta]. \quad (31)$$

220 **Triangle-Simulator** provides multiple (equivalent) implementations for the GW re-
 221 sponse function. For dataset groups 0, 1 and 2 (scientific datasets), due to the large number
 222 of GW signals to be calculated, we utilize the **Triangle-Simulator.GW.GeneralTDIResponse**
 223 class (setting `return_eta=True` and `Pstrings=eta_string` since single-link responses are
 224 desired). While for dataset groups 3 and 4 (raw datasets), the **SimulateGW** function inte-
 225 grated to the **Interferometers** class is adopted, since it accounts for the realistic scenarios
 226 such as signal sampling error due to clock deviations.

227 C. Data anomalies

228 Glitches and gaps are two typical data anomalies that may be present in realistic Taiji
 229 data. LISA Pathfinder and Taiji-1 demonstrated that the TMs could be affected by unex-
 230 pected transient disturbances. Thus it is conservative to expect that these glitches would
 231 take place during the science operations of Taiji. According to the observations of LISA
 232 Pathfinder and Taiji-1, we model the glitches with a double decaying exponential form in
 233 terms of TM acceleration [32, 33]:

$$\delta_{\text{acceleration}}^{\text{glitch}}(t) = \frac{\Delta v}{\tau_1 - \tau_2} \left(e^{-\frac{t-t_0}{\tau_1}} - e^{-\frac{t-t_0}{\tau_2}} \right) \Theta(t - t_0), \quad (32)$$

234 where t_0 is the time of injection, Δv is the velocity gain caused by the glitch, $\tau_{1,2}$ are the
 235 time scales of the exponentials, and $\Theta(t)$ stands for the Heaviside function. In Datasets 4,
 236 glitches of this form are injected at random times and random TMs. On the other hand, we
 237 model data gaps originating from scheduled maintenances (e.g. re-pointing of the antennas,
 238 switching of frequency plans, and in-orbit maneuvers, *etc*) as a 7-hour duration with no data
 239 collection (set to `numpy.nan`) starting at the 15th day of Datasets 4.

240 D. Time-delay interferometry

241 The complete TDI processing includes 3 steps. Firstly, the intermediate variable ξ_{ij} is
 242 constructed, which is free of OB displacement noises:

$$\xi_{ij} = s_{ij} + \frac{\tau_{ij} - \varepsilon_{ij}}{2} + \dot{\mathbf{D}}_{ij} \frac{\tau_{ji} - \varepsilon_{ji}}{2}, \quad (33)$$

243 where $ij \in \{12, 23, 31, 21, 32, 13\}$.

244 Secondly, we construct the intermediate variable η_{ij} to reduce half of the laser noises:

$$\eta_{ij} = \xi_{ij} + \dot{\mathbf{D}}_{ij} \frac{\tau_{ji} - \tau_{jk}}{2}, \quad \eta_{ik} = \xi_{ik} + \frac{\tau_{ij} - \tau_{ik}}{2}, \quad (34)$$

245 with $ijk \in \{123, 231, 312\}$. To convert to the fractional frequency difference unit, we further
 246 divide all the η_{ij} by the central frequency ν_0 . These are just the data streams that users
 247 have access to for Datasets 0, 1 and 2. For a signal-only simulation, one has $\eta_{ij} = y_{ij}$. While
 248 for the 2-component noise model usually employed in simplified investigations,

$$\eta_{ij} = y_{ij} + n_{ij}, \quad n_{ij} = N_{ij} + \delta_{ij} + \dot{\mathbf{D}}_{ij} \delta_{ji}, \quad (35)$$

with N_{ij} and δ_{ij} being the optical metrology system (OMS) noise and TM acceleration (ACC) noise, respectively.

The third step is constructing TDI variables to mitigate all the remaining laser noises. This step varies for different TDI schemes. Despite that there are hundreds of TDI schemes in the literature, they can all be abstracted into a unified form:

$$\text{TDI} = \sum_{ij} \mathbf{P}_{ij} \eta_{ij}. \quad (36)$$

Taking the second-generation Michelson channel X_2 as an example, the fiducial rule of X_2 channel used by **Triangle** is

$$X_2 = \left(1 - \dot{\mathbf{D}}_{131} - \dot{\mathbf{D}}_{13121} + \dot{\mathbf{D}}_{1213131}\right) \left(\eta_{12} + \dot{\mathbf{D}}_{12} \eta_{21}\right) - \left(1 - \dot{\mathbf{D}}_{121} - \dot{\mathbf{D}}_{12131} + \dot{\mathbf{D}}_{1312121}\right) \left(\eta_{13} + \dot{\mathbf{D}}_{13} \eta_{31}\right), \quad (37)$$

which can be expressed in terms of \mathbf{P}_{ij} operators as

$$\begin{aligned} \mathbf{P}_{12} &= 1 - \dot{\mathbf{D}}_{131} - \dot{\mathbf{D}}_{13121} + \dot{\mathbf{D}}_{1213131}, \\ \mathbf{P}_{23} &= 0, \\ \mathbf{P}_{31} &= -\dot{\mathbf{D}}_{13} + \dot{\mathbf{D}}_{1213} + \dot{\mathbf{D}}_{121313} - \dot{\mathbf{D}}_{13121213}, \\ \mathbf{P}_{21} &= \dot{\mathbf{D}}_{12} - \dot{\mathbf{D}}_{1312} - \dot{\mathbf{D}}_{131212} + \dot{\mathbf{D}}_{12131312}, \\ \mathbf{P}_{32} &= 0, \\ \mathbf{P}_{13} &= -1 + \dot{\mathbf{D}}_{121} + \dot{\mathbf{D}}_{12131} - \dot{\mathbf{D}}_{1312121}. \end{aligned} \quad (38)$$

The expressions for Y_2 and Z_2 channels can be obtained using the permutation rule $1 \rightarrow 2, 2 \rightarrow 3, 3 \rightarrow 1$. The conventions for Michelson channels might differ by a minus sign in other works. The **Triangle-Simulator.TDI.TDI** class is capable of combining any TDI variable, given the strings representing the \mathbf{P}_{ij} operators.

In the presence of clock noises, an additional step should be performed to calculate and subtract the clock noise correction term [34], which doesn't affect the signal content of data.

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