

## Active Target Defense Differential Game

Meir Pachter, Eloy Garcia, and David W. Casbeer

**Abstract**—A pursuit-evasion differential game involving three agents is discussed. This scenario considers an Attacker missile pursuing a Target aircraft. The Target is however aided by a Defender missile launched by, say, its wingman, to intercept the Attacker before it reaches the Target aircraft. Thus, a team is formed by the Target and the Defender which cooperate to maximize the distance between the Target aircraft and the point where the Attacker missile is intercepted by the Defender missile, and the Attacker which tries to minimize said distance. The solution to this differential game provides optimal heading angles for the Target and the Defender team to maximize the terminal separation between Target and Attacker and it also provides the optimal heading angle for the Attacker to minimize the said distance.

### I. INTRODUCTION

Multi-agent pursuit-evasion scenarios represent important and challenging types of problems in aerospace, control, and robotics. In these types of problems one or more pursuers try to maneuver and reach a relatively small distance with respect to one or more evaders, which strive to escape the pursuers. Several types of pursuit-evasion scenarios involving many agents have been studied. This problem is usually posed as a dynamic game [1], [2], [3]. A dynamic Voronoi diagram has been used in problems with several pursuers in order to capture an evader within a bounded domain [2], [4]. Cooperation between two agents with the goal of evading a single pursuer has been addressed in [5]. Scott and Leonard [6] presented a scenario where two evaders employ coordinated strategies to evade a single pursuer, but also to keep them close to each other.

In this paper we consider a zero-sum three-agent pursuit-evasion differential game. The two-agent team consists of a Target ( $T$ ) and a Defender ( $D$ ) who cooperate; the Attacker ( $A$ ) is the opposition. The goal of the Attacker is to capture the Target while the Target tries to evade the Attacker and avoid capture. The Target cooperates with the Defender which pursues and tries to intercept the Attacker before the latter captures the Target. Cooperation between the Target and the Defender is such that the Defender will capture the Attacker before the latter reaches the Target. Such a scenario of active target defense has been analyzed in the context of cooperative optimal control [7], [8]. Indeed, sensing

capabilities of missiles and aircraft allow for implementation of complex pursuit and evasion strategies [9], [10], and recent work has proposed different guidance laws for the agents  $A$  and  $D$ . Thus, in [11] the authors addressed the case where the Defender implements Command to the Line of Sight (CLOS) guidance to pursue the Attacker which requires the Defender to have at least the same speed as the Attacker. A different guidance law for the Target-Attacker-Defender (TAD) scenario was given by Yamasaki *et.al.* [12], [13]. These authors investigated an interception method called Triangle Guidance (TG), where the objective is to command the defending missile to be on the line-of-sight between the attacking missile and the aircraft for all time while the aircraft follows some predetermined trajectory. The authors show, through simulations, that TG provides better performance in terms of Defender control effort than a number of variants of Proportional Navigation (PN) guidance laws, that is, when the Defender uses PN to pursue the Attacker instead of TG. These approaches constrain and limit the level of cooperation between the Target and the Defender by implementing Defender guidance laws without regard to the Target's trajectory.

Rubinsky and Gutman [14], [15] presented an analysis of the end-game TAD scenario based on the Attacker/Target miss distance for a *non-cooperative* Target/Defender. The authors develop linearization-based Attacker maneuvers in order to evade the Defender and continue pursuing the Target.

Different types of cooperation have been recently proposed in [16], [17], [18], [19], [20], [21], [22] for the TAD scenario. In these papers the Target represents an aircraft trying to evade a missile homing on it. The Defender represents another missile launched by the aircraft (or a wingman) in order to intercept and destroy the Attacker in order to guarantee the survival of the aircraft. Thus, in [18] optimal policies (lateral acceleration for each agent including the Attacker) are provided for the case of an aggressive Defender, that is, the Defender has a definite maneuverability advantage. A linear quadratic optimization problem is posed where the Defender's control effort weight is driven to zero to increase its aggressiveness. The work [19] provided a game theoretical analysis of the TAD problem using different guidance laws for both the Attacker and the Defender. The cooperative strategies in [20] allow for a maneuverability disadvantage for the Defender with respect to the Attacker and the results show that the optimal Target maneuver is either constant or arbitrary. Shaferman and Shima [21] implemented a Multiple Model Adaptive Estimator (MMAE) to identify the guidance law and parameters of the incoming missile and optimize a Defender strategy to minimize its control effort. In the recent

M. Pachter is with the Department of Electrical Engineering, Air Force Institute of Technology, Wright-Patterson AFB, OH 45433. meir.pachter@afit.edu

E. Garcia is a contractor (Infoscitex Corp.) with the Control Science Center of Excellence, Air Force Research Laboratory, Wright-Patterson AFB, OH 45433. elgarcia@infoscitex.com

D. Casbeer is with the Control Science Center of Excellence, Air Force Research Laboratory, Wright-Patterson AFB, OH 45433. david.casbeer@us.af.mil



reduced state space provides a compact representation of the dynamics of this three-agent differential game.

The dynamics in the reduced state space are

$$\dot{R} = \alpha \cos \phi - \cos(\theta - \chi), \quad R(t_0) = R_0 \quad (4)$$

$$\dot{r} = -\cos \chi - \cos \psi, \quad r(t_0) = r_0 \quad (5)$$

$$\begin{aligned} \dot{\theta} &= -\frac{\alpha}{R} \sin \phi + \frac{1}{R} \sin(\theta - \chi) \\ &\quad - \frac{1}{r} \sin \psi + \frac{1}{r} \sin \chi, \quad \theta(t_0) = \theta_0 \end{aligned} \quad (6)$$

for  $0 \leq t \leq t_f$ .

The objective of the Target-Defender team is to maximize the separation between the Target and the Attacker at the interception time  $R(t_f)$ , where the terminal time  $t_f$  is free, such that  $r(t_f) = r_c$ . The objective of the Attacker is to minimize the same distance  $R(t_f)$ . This can be expressed as

$$\max_{\phi, \psi} \min_{\chi} J = \int_{t_0}^{t_f} \dot{R} dt. \quad (7)$$

Then, the Hamiltonian is given by

$$\begin{aligned} H &= \cos(\theta - \chi) - \alpha \cos \phi \\ &\quad + (\alpha \cos \phi - \cos(\theta - \chi)) \lambda_R \\ &\quad - (\cos \chi + \cos \psi) \lambda_r \\ &\quad + \left(-\frac{\alpha}{R} \sin \phi + \frac{1}{R} \sin(\theta - \chi) - \frac{1}{r} \sin \psi + \frac{1}{r} \sin \chi\right) \lambda_\theta \end{aligned} \quad (8)$$

and the co-state dynamics are given by:

$$\dot{\lambda}_R = \frac{\lambda_\theta}{R^2} (\sin(\theta - \chi) - \alpha \sin \phi) \quad (9)$$

$$\dot{\lambda}_r = \frac{\lambda_\theta}{r^2} (\sin \chi - \sin \psi) \quad (10)$$

$$\dot{\lambda}_\theta = (1 - \lambda_R) \sin(\theta - \chi) - \frac{\lambda_\theta}{R} \cos(\theta - \chi). \quad (11)$$

The terminal conditions for this free terminal time problem are as follows. The terminal state  $r(t_f)$  is fixed and equal to  $r_c$ . Because the terminal states  $R(t_f)$ , and  $\theta(t_f)$  are free, we have  $\lambda_R(t_f) = \lambda_\theta(t_f) = 0$ . The final terminal condition for optimality for this problem requires that  $H(x^*(t_f), u^*(t_f), \lambda^*(t_f), t_f) = 0$ . In summary, the terminal conditions are:

$$\begin{aligned} r(t_f) &= r_c \\ \lambda_R(t_f) &= 0 \\ \lambda_\theta(t_f) &= 0 \\ \alpha^2 + 2(\alpha + \cos \theta(t_f)) \lambda_r(t_f) - 1 &= 0. \end{aligned} \quad (12)$$

*Proposition 1:* The Target and Defender optimal control headings that maximize the separation between the Target and the Attacker and achieve  $r(t_f) = r_c$  are given by

$$\sin \psi^* = \frac{\lambda_\theta}{r \sqrt{\lambda_r^2 + \lambda_\theta^2 / r^2}} \quad (13)$$

$$\cos \psi^* = \frac{\lambda_r}{\sqrt{\lambda_r^2 + \lambda_\theta^2 / r^2}} \quad (14)$$

$$\sin \phi^* = \frac{\lambda_\theta}{R \sqrt{(1 - \lambda_R)^2 + \lambda_\theta^2 / R^2}} \quad (15)$$

$$\cos \phi^* = \frac{1 - \lambda_R}{\sqrt{(1 - \lambda_R)^2 + \lambda_\theta^2 / R^2}}. \quad (16)$$

The Attacker optimal control heading that minimizes the separation between itself and the Target at  $t = t_f$  is given by

$$\sin \chi^* = \frac{\chi_s}{\sqrt{\chi_s^2 + \chi_c^2}} \quad (17)$$

$$\cos \chi^* = \frac{\chi_c}{\sqrt{\chi_s^2 + \chi_c^2}} \quad (18)$$

where  $\chi_s = (1 - \lambda_R) \sin \theta - \frac{\lambda_\theta}{R} \cos \theta + \frac{\lambda_\theta}{r}$  and  $\chi_c = (1 - \lambda_R) \cos \theta + \frac{\lambda_\theta}{R} \sin \theta - \lambda_r$ .

The optimal heading angles expressions (13)-(18) are used to numerically solve the Two-Point Boundary Value Problem (TPBVP) (4)-(7), (9)-(18). The numerical solution is found by substituting the optimal control headings into the state equations (4)-(6), and the co-state equations (9)-(11), with the terminal conditions given by (12).

#### IV. DIFFERENTIAL GAME WITH POINT CAPTURE

##### A. Target Defense Differential Game

We now undertake analysis of the Target Defense differential game. In this section we confine our attention to point capture, that is, we assume  $r_c \rightarrow 0$ . The Target ( $T$ ), the Attacker ( $A$ ), and the Defender ( $D$ ) have “simple motion” a la Isaacs. We emphasize that  $T$ ,  $A$ , and  $D$  have constant speeds of  $V_T$ ,  $V_A$ , and  $V_D$ , respectively. We assume that  $V_A = V_D$  and the speed ratio  $\alpha = \frac{V_T}{V_A} < 1$ .  $T$  and  $D$  form a team to defend from  $A$ . Thus,  $A$  strives to close in on  $T$  while  $T$  and  $D$  maneuver such that  $D$  intercepts  $A$  before the latter reaches  $T$  and the distance at interception time is maximized, while  $A$  strives to minimize the separation between  $T$  and  $A$  at the instant of interception.

In Fig. 2 the points  $A$  and  $D$  represent the positions of the Attacker and the Defender, respectively. A Cartesian frame is attached to the points  $A$  and  $D$  in such a way that the extension to infinity of  $\overline{AD}$  in both directions represents the  $X$ -axis and the orthogonal bisector line of  $\overline{AD}$  represents the  $Y$ -axis.

With respect to Fig. 2 we note that the Attacker aims at minimizing the distance between the Target at the time instant when the Defender intercepts the Attacker, point  $T'$ , and the point  $I$  on the orthogonal bisector of  $\overline{AD}$  where the Defender intercepts the Attacker. The points  $T$  and  $T'$  represent the initial and terminal positions of the Target, respectively.

##### B. Critical Speed Ratio for Target Survival

Assume that the speed ratio  $0 < \alpha < 1$  and  $x_T > 0$ . The Target needs to be able to break into the Left Half Plane (LHP) before being intercepted by the Attacker for the Defender to be able to assist the Target to escape, by intercepting the Attacker who is on route to the Target. Thus, a solution to the differential game exists if and only if the Apollonius circle, which is based on the segment  $\overline{AT}$  and the speed ratio  $\alpha$ , intersects the orthogonal bisector of  $\overline{AD}$ . This imposes a lower limit  $\bar{\alpha}$  on the speed ratio, that is, we need  $\bar{\alpha} < \alpha < 1$ . The critical speed ratio  $\bar{\alpha}$  corresponds to the case where the Apollonius circle is tangent to the orthogonal

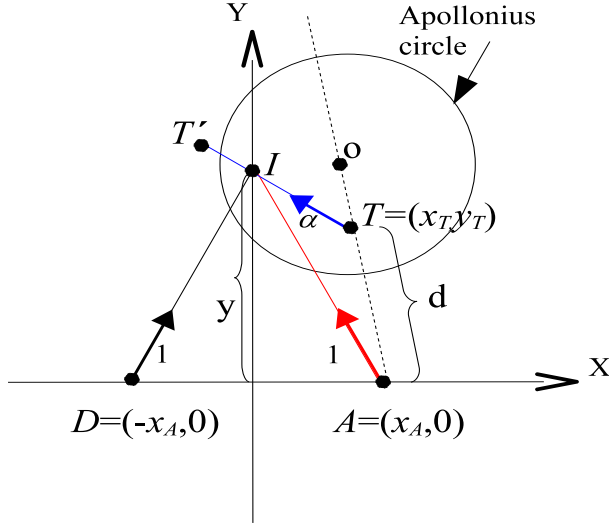


Fig. 2. Target Defense Differential Game

bisector of  $\overline{AD}$ . Note that if the speed ratio  $\alpha \geq 1$  the Target always escapes and there is no need for a Defender missile, that is, there is no Target Defense Differential Game.

The Attacker's initial position, the Target's initial position, and the center  $O$  of the Apollonius circle are collinear and lie on the dotted line in Fig. 2 which can be represented as

$$y = -\frac{y_T}{x_A - x_T}x + \frac{x_A y_T}{x_A - x_T}$$

The geometry of the Apollonius circle is as follows: The center of the circle, denoted by  $O$ , is at a distance of  $\frac{\alpha^2}{1-\alpha^2}d$  from  $T$  and its radius is  $\frac{\alpha}{1-\alpha^2}d$ , where  $d$  is the distance between  $A$  and  $T$  and is given by

$$d = \sqrt{(x_A - x_T)^2 + y_T^2}. \quad (19)$$

Hence, the following holds

$$\begin{aligned} & \left( \frac{x_T y_T}{x_A - x_T} - \frac{y_T}{x_A - x_T} x_0 \right)^2 + (x_0 - x_T)^2 \\ &= \frac{\alpha^4}{(1 - \alpha^2)^2} [(x_A - x_T)^2 + y_T^2] \end{aligned} \quad (20)$$

and we calculate the coordinates of the center of the Apollonius circle

$$\begin{aligned} x_O &= \frac{1}{1-\alpha^2}x_T - \frac{\alpha^2}{1-\alpha^2}x_A \\ y_O &= \frac{1}{1-\alpha^2}y_T. \end{aligned} \quad (21)$$

Consequently, the critical speed ratio  $\bar{\alpha}$  is the positive solution of the quadratic equation

$$x_T - \alpha^2 x_A = \alpha \sqrt{(x_A - x_T)^2 + y_T^2} \quad (22)$$

and is given by

$$\bar{\alpha} = \frac{\sqrt{(x_A + x_T)^2 + y_T^2} - \sqrt{(x_A - x_T)^2 + y_T^2}}{2x_A}. \quad (23)$$

In the special case where  $x_T = x_A$ , the critical speed ratio

$$\bar{\alpha} = \frac{\sqrt{4x_A^2 + y_T^2} - y_T}{2x_A},$$

as expected. Since  $y_T > 0$  we have  $\bar{\alpha} < 1$ .

In the special case when  $y_T = 0$ , we have that  $\bar{\alpha} = x_T/x_A < 1$  if  $x_A > x_T$ , and  $\bar{\alpha} = 1$  if  $x_A \leq x_T$ . Also note that when  $x_T = 0$ ,  $\bar{\alpha} = 0$ , as expected.

In general, it can be seen from Fig. 2 that if  $x_T < 0$  then  $\bar{\alpha} = 0$  as well. The case when  $x_T < 0$ , that is, when the Target is on the Defender's side of the orthogonal bisector of  $\overline{AD}$  is also of interest but will not be addressed here because of space constraints.

We will assume  $\bar{\alpha} < \alpha < 1$ , so that a solution to the Target Defense Differential Game exists; otherwise, if  $\alpha \leq \bar{\alpha}$ , the Defender will not be able to help the Target by intercepting the Attacker before the latter inevitably captures the Target. And if  $\alpha \geq 1$  then the Target cannot be intercepted by the Attacker and there is no need for the Defender.

### C. Optimal Strategies

The Attacker will be intercepted by the Defender on the orthogonal bisector of  $\overline{AD}$ . Thus, the Attacker chooses his aimpoint, denoted by  $I$ , on the orthogonal bisector of  $\overline{AD}$  in order to minimize the cost function

$$J(y) = \alpha \sqrt{x_A^2 + y^2} - \sqrt{(y - y_T)^2 + x_T^2} \quad (24)$$

which represents the final separation between Target and Attacker, and where  $y$  represents the coordinate of the aimpoint  $I$  on the orthogonal bisector of  $\overline{AD}$ . This is so because the Target will head away from  $I$ .

In order to find the minimum of (24) we differentiate eq. (24) in  $y$

$$\frac{dJ(y)}{dy} = \frac{\alpha y}{\sqrt{x_A^2 + y^2}} - \frac{y - y_T}{\sqrt{(y - y_T)^2 + x_T^2}} = 0 \quad (25)$$

which can also be written as follows

$$\frac{\alpha^2 y^2}{x_A^2 + y^2} = \frac{(y - y_T)^2}{(y - y_T)^2 + x_T^2} \quad (26)$$

and we obtain the quartic equation in  $y \geq 0$

$$\begin{aligned} & (1 - \alpha^2)y^4 - 2(1 - \alpha^2)y_T y^3 \\ & + ((1 - \alpha^2)y_T^2 + x_A^2 - \alpha^2 x_T^2)y^2 \\ & - 2x_A^2 y_T y + x_A^2 y_T^2 = 0 \end{aligned} \quad (27)$$

When  $\alpha = 1$ , (27) can be reduced to the following quadratic equation

$$\left(1 - \frac{x_T^2}{x_A^2}\right)y^2 - 2y_T y + y_T^2 = 0 \quad (28)$$

and the solutions, when  $|x_T| \neq x_A$ , are given by

$$y = \frac{x_A y_T}{x_A + x_T}, \quad y = \frac{x_A y_T}{x_A - x_T}. \quad (29)$$

However, the case  $\alpha = 1$  is outside the scope of the Target defense differential game. Nevertheless, if  $\alpha = 1$  and  $x_T = x_A$  then the solution  $y^* = \frac{1}{2}y_T$  makes no good sense, as pictured in Fig. 3. In this case the Target is better off to run



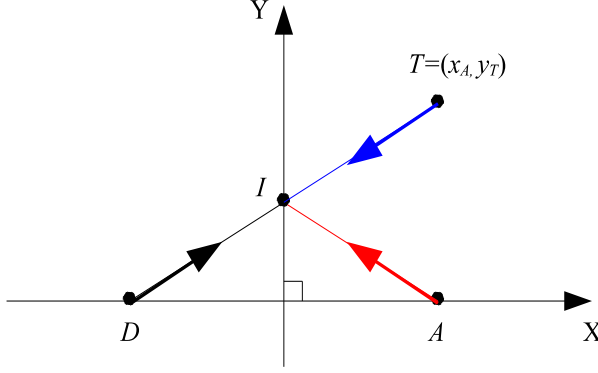


Fig. 3. “Solution” when  $\alpha = 1$  and  $x_T = x_A$  - Incorrect

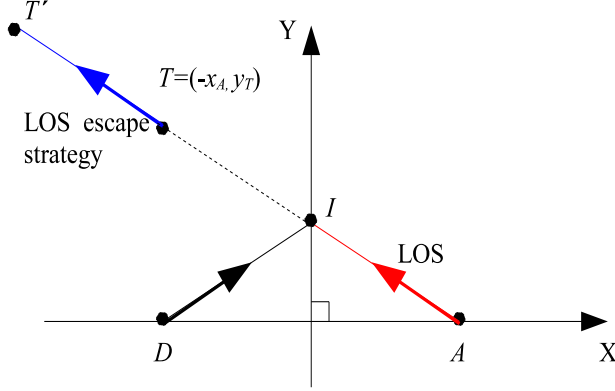


Fig. 4. Solution when  $\alpha = 1$  and  $x_T = -x_A$

North. Now, if  $\alpha = 1$  and  $x_T = -x_A = x_D$  then the solution  $y^* = \frac{1}{2}y_T$  makes sense: the initial separation between Target and Attacker,  $J^* = 2\sqrt{x_A^2 + y_T^2}/4$ , is maintained, as expected. This situation is shown in Fig. 4 where it can be seen that the Target runs away from the Attacker and there is no need for a Defender missile since the Target will not be captured. Therefore, there is no Target defense differential game in this particular situation.

*Remark.* Writing eq. (27) as  $f(y) = 0$  we can see that  $f(0) = x_A^2 y_T^2 > 0$ ,  $f(y_T) = -\alpha^2 x_T^2 y_T^2 < 0$ , and  $f(\infty) = +\infty$ . Therefore, equation (27) has two real solutions. Equation (27) has a real solution  $0 < y < y_T$  and an additional real solution  $y_T < y$ , provided that  $x_T \neq 0$ . If  $x_T = 0$ , then  $y_T$  is a repeated solution of (27) because this equation can then be written as follows

$$\begin{aligned} 0 &= (1 - \alpha^2)(y^4 - 2y_T y^3 + y_T^2 y^2) \\ &\quad + x_A^2(y^2 - 2y_T y + y_T^2) \\ &= (y^2 - 2y_T y + y_T^2)((1 - \alpha^2)y^2 + x_A^2) \\ &= (y - y_T)^2((1 - \alpha^2)y^2 + x_A^2). \end{aligned} \quad (30)$$

Hence,  $y_T$  is a repeated root of (27). In addition, there are

two complex roots:  $y = \pm i \frac{1}{\sqrt{1 - \alpha^2}} x_A$ .

Note that (27) is parameterized by  $x_T^2$ , so whether  $x_T > 0$  or  $x_T < 0$  makes no difference in terms of the solutions to the quartic equation (27).

When  $x_T > 0$ , by choosing his heading, the Target (and the Defender) thus determine the coordinate  $y$  to maximize  $J(y)$ ; that is,  $y$  is the Target's (and Defender's) choice. Then the payoff is given by eq. (24) and the expression for  $\frac{dJ(y)}{dy}$  was shown in (25). We also have that

$$\frac{d^2 J(y)}{dy^2} = \frac{\alpha x_A^2}{(x_A^2 + y^2)^{3/2}} - \frac{x_T^2}{((y - y_T)^2 + x_T^2)^{3/2}}. \quad (31)$$

Since the Target is choosing  $y$  to maximize the cost  $J(y)$ , then the optimal coordinate  $y^*$  is the solution of (27) such that  $\frac{d^2 J(y)}{dy^2} < 0$ . In view of (25) we know that

$$\frac{1}{\sqrt{(y - y_T)^2 + x_T^2}} = \alpha \frac{y}{y - y_T} \frac{1}{\sqrt{x_A^2 + y^2}}. \quad (32)$$

Then, inserting (32) into (31) yields

$$\frac{d^2 J(y)}{dy^2} = \frac{\alpha}{(x_A^2 + y^2)^{3/2}} \left( x_A^2 - \alpha^2 \left( \frac{y}{y - y_T} \right)^3 x_T^2 \right) \quad (33)$$

and we have that  $\frac{d^2 J(y)}{dy^2} < 0$  if and only if

$$\frac{1}{\alpha^2} \left( \frac{x_A}{x_T} \right)^2 < \left( \frac{y}{y - y_T} \right)^3. \quad (34)$$

Hence, the solution  $y < y_T$  of (27) does not fulfill the role of yielding a maximum and the second solution  $y > y_T$  of (27) is the optimal solution.

Inserting (32) into (24) yields the Target and Defender payoff

$$\begin{aligned} J^*(y) &= \alpha \sqrt{x_A^2 + y^2} - \frac{1}{\alpha} \frac{y - y_T}{y} \sqrt{x_A^2 + y^2} \\ &= \frac{1}{\alpha} \sqrt{x_A^2 + y^2} \left( \frac{y_T}{y} - (1 - \alpha^2) \right). \end{aligned} \quad (35)$$

When  $\alpha > \bar{\alpha}$  we have that  $J^*(y) > 0$ . Hence, the solution  $y > y_T$  of (27) must satisfy

$$y_T < y < \frac{1}{1 - \alpha^2} y_T. \quad (36)$$

This situation is shown in Fig. 5 where the three points  $T$ ,  $I$ , and  $T'$  are collinear. Concerning expression (34), we also need the solution of the quartic equation to satisfy

$$y < \frac{1}{1 - \alpha^{2/3} \left( \frac{x_T}{x_A} \right)^{2/3}} y_T. \quad (37)$$

#### D. Discussion

When  $x_T > 0$  the Attacker and the Target are faced with a maxmin optimization problem: the Target chooses  $y_1$  and the Attacker chooses  $y_2$ , see Fig. 6.

The decision variables  $y_1$  and  $y_2$  jointly determine the distance  $d(A', T')$ , that is, the function

$$\tilde{J}(y_1, y_2) = d(A', T'). \quad (38)$$

Thus, the Attacker and the Target solve the following problem

$$\max_{y_1} \min_{y_2} \tilde{J}(y_1, y_2). \quad (39)$$

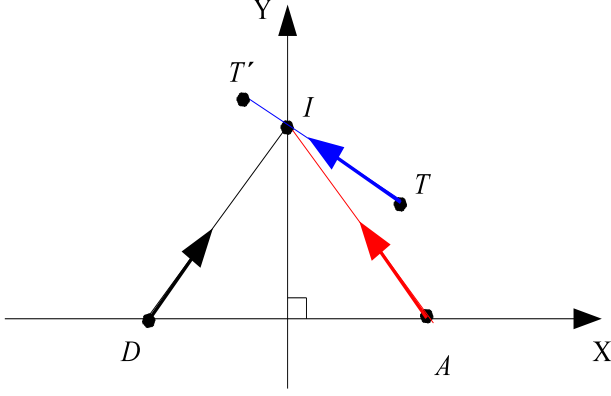


Fig. 5. Optimal solution when  $x_T > 0$

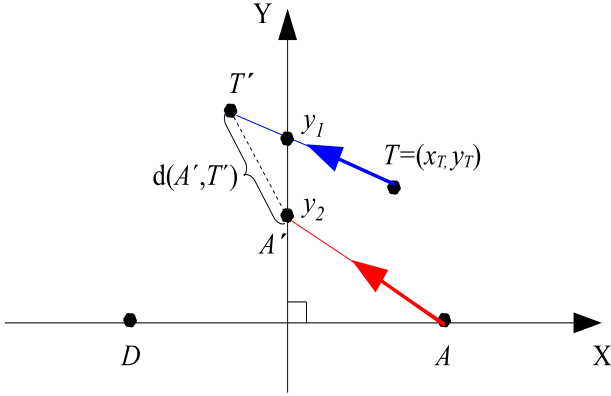


Fig. 6. Maxmin optimization problem

Should the Target choose  $y_1$ , the Attacker would respond with

$$y_2^* = f^*(y_1) = \arg \min_{y_2} \tilde{J}(y_1, y_2) \quad (40)$$

and knowing this, the Target chooses

$$y_1^* = \arg \max_{y_1} \tilde{J}(y_1, f^*(y_1)) \quad (41)$$

which yields the payoff  $\tilde{J}(y_1^*, f^*(y_1^*))$ .

Thus the choices of the Target and the Attacker which solve the maxmin optimization problem at hand are  $y_1^*$  and  $y_2^* = f^*(y_1^*)$ . The Defender's choice is then determined by  $y_2^*$ .

The function  $\tilde{J}(y_1, y_2)$  is calculated as follows. The decision variable of the Target is  $y_1$  and the decision variable of the Attacker is  $y_2$ . The terminal Attacker coordinates are  $A' = (0, y_2)$ . We now calculate the coordinates of the point  $T' = (x_{T'}, y_{T'})$  as follows

$$\frac{y_1 - y_T}{x_T} = \frac{y_{T'} - y_T}{x_T - x_{T'}} \quad (42)$$

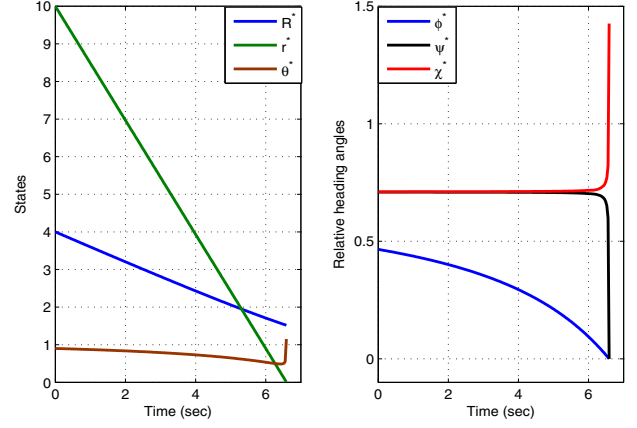


Fig. 7. Numerical solution of Example 1

and

$$(x_T - x_{T'})^2 + (y_{T'} - y_T)^2 = \alpha^2(x_A^2 + y_2^2). \quad (43)$$

Inserting (42) into (43) yields

$$\left(1 + \left(\frac{y_1 - y_T}{x_T}\right)^2\right)(x_T - x_{T'})^2 = \alpha^2(x_A^2 + y_2^2) \quad (44)$$

and we have that

$$x_{T'} = \left(1 - \alpha \sqrt{\frac{x_A^2 + y_2^2}{x_T^2 + (y_1 - y_T)^2}}\right) x_T \quad (45)$$

$$y_{T'} = y_T + \alpha(y_1 - y_T) \sqrt{\frac{x_A^2 + y_2^2}{x_T^2 + (y_1 - y_T)^2}}. \quad (46)$$

Finally, the distance between the terminal points  $A'$  and  $T'$  is given by

$$\begin{aligned} d^2(A', T') = & \left(1 - \alpha \sqrt{\frac{x_A^2 + y_2^2}{x_T^2 + (y_1 - y_T)^2}}\right)^2 x_T^2 \\ & + \left(y_T - y_2 + \alpha(y_1 - y_T) \sqrt{\frac{x_A^2 + y_2^2}{x_T^2 + (y_1 - y_T)^2}}\right)^2. \end{aligned} \quad (47)$$

*Proposition 2:* . Given the functions  $\tilde{J}(y_1, y_2)$ , the solution  $y_1^*$  and  $y_2^*$  of the optimization problem  $\max_{y_1} \min_{y_2} \tilde{J}(y_1, y_2)$  and the function  $f^*(\bullet)$ , where  $y_2^* = f^*(y_1)$  are such that the function  $f^*(\bullet)$  has a fixed point and

$$y_1^* = y_2^*. \quad (48)$$

Moreover, the function  $f^*(y_1) = y_1$  so that when  $x_T > 0$  it suffices to solve the optimization problem  $\max_y J(y)$  where

$$J(y) = \alpha \sqrt{x_A^2 + y^2} - \sqrt{(y - y_T)^2 + x_T^2}.$$

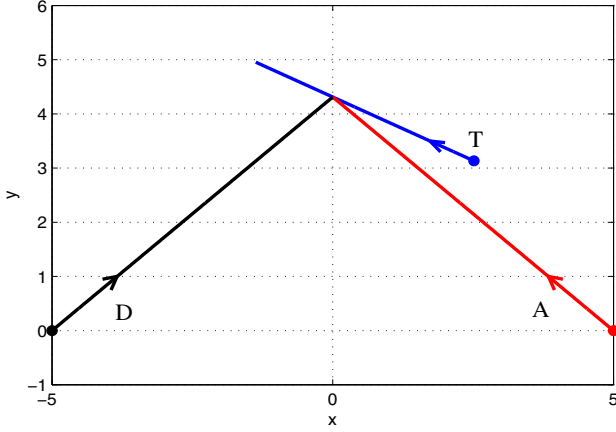


Fig. 8. Optimal trajectories for Example 1

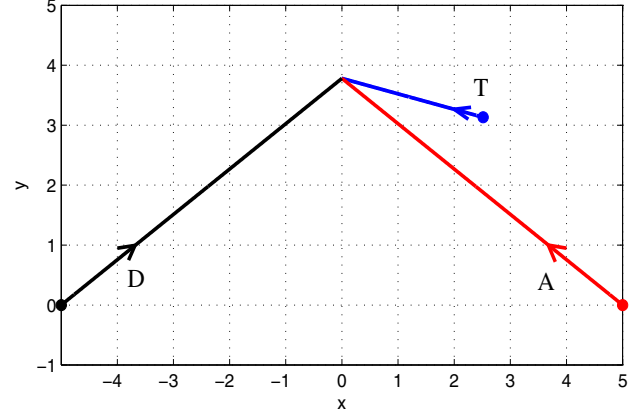


Fig. 9. Optimal trajectories for Example 2

## V. EXAMPLES

*Example 1.* We use analytical and numerical methods to solve the Target Defense Differential Game. We consider an Attacker and a Defender missile with unit speed and with initial positions given by  $A = [5, 0]$  and  $D = [-5, 0]$ , respectively. The Target has a speed  $\alpha = 0.65$  and it is initially located at  $T = [2.514, 3.133]$ . In terms of the variables used in Section III we have the following initial conditions:  $R_0 = 4$ ,  $r_0 = 10$ ,  $\theta_0 = 0.9$  rad. The numerical solution of the differential game described in Section III (when  $r_c \rightarrow 0$ ) is shown in Fig. 7; the left plot of this figure shows the optimal states and the right plot shows the optimal relative heading angles. The relative heading angles can be transformed to absolute angles with respect to a fixed frame which were denoted by  $\hat{\phi}$ ,  $\hat{\psi}$ , and  $\hat{\chi}$ . For the Target Defense Differential Game the absolute optimal angles are always constant. For this example, we have that:  $\hat{\phi} = 2.7033$  rad,  $\hat{\psi} = 0.7115$  rad, and  $\hat{\chi} = 2.4301$  rad. The interception point's coordinate is  $y = 4.311$  which was corroborated by solving the quartic equation (27) which was derived in Section IV. Both methods provide the same solutions, as expected, and we have that  $t_f = 6.6$  sec and the final separation is  $R(t_f) = 1.515$ . An important additional piece of information is the minimum relative speed to guarantee Target survival which, for this example, is given by  $\bar{\alpha} = 0.4141$ . Obviously, the numerical and the analytical solutions provide the same trajectories and here it suffices to show one set of trajectories. Analytically derived optimal trajectories are shown in Fig. 8.

*Example 2. Limit  $\alpha \rightarrow \bar{\alpha}$ .* Consider the same initial positions for the Target, Attacker, and Defender as in Example 1. The difference in this example is that the speed of the Target is  $\alpha = 0.415$  which is greater than the critical speed but very close to that critical value  $\bar{\alpha} = 0.4141$ . In this case the interception point is  $y = 3.783$ , the interception time is  $t_f = 6.34$  sec, and the final separation is  $R(t_f) = 0.0058$ . The final separation is positive but very close to zero. This

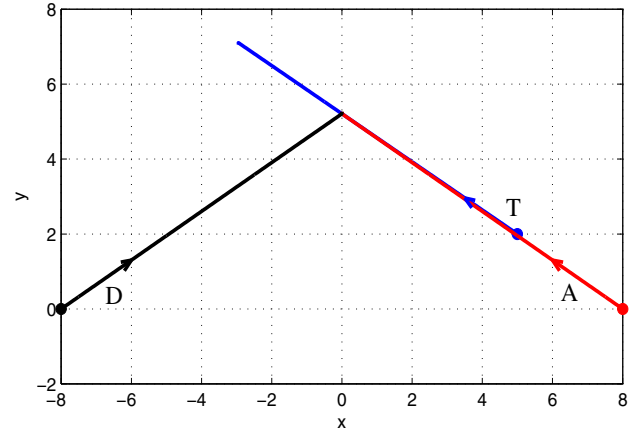


Fig. 10. Optimal trajectories for Example 3

is expected since the value of  $\alpha$  is almost equal to  $\bar{\alpha}$ . The trajectories for this example are shown in Fig. 9.

*Example 3. Limit  $\alpha \rightarrow 1$ .* Consider an Attacker and a Defender missile with unit speed and with initial positions given by  $A = [8, 0]$  and  $D = [-8, 0]$ , respectively. The Target has a speed  $\alpha = 0.99$  and it is initially located at  $T = [5, 2]$ . This value of  $\alpha$  is very close to 1; recall that when  $\alpha = 1$  we expect a LOS pursuit and escape strategy. The interception point is calculated for this example and it is found to be  $y = 5.21$ , the interception time is  $t_f = 9.55$  sec, and the final separation is  $R(t_f) = 3.51$ . The trajectories for this example are shown in Fig. 10. Note that the Target's escape trajectory and the Attacker's pursuit trajectory are similar (but not exactly) to LOS trajectories, as expected. The absolute heading angles of the Target and the Attacker are close, but not the same, and they are given by  $\hat{\phi} = 2.5709$  rad and  $\hat{\chi} = 2.5643$  rad, which show that the Target and the Attacker do not exactly follow a LOS escape and pursuit strategy.

## VI. CONCLUSIONS

A differential game for the cooperative aircraft defense scenario was formulated and analyzed. In this differential game of perfect information the Attacker is aware of the Defender's position and of the cooperation between Target and Defender. The Attacker computes and implements the optimal heading angle that minimizes the final Target-Attacker separation at the time instant when the Defender intercepts the Attacker. The Target strives to maximize said distance. For the case of point capture, an analytical solution of the Target Defense Differential Game is provided. For completeness, critical Target speeds were also examined in order to determine a lower bound on the speed of the Target that guarantees, with the help of the Defender, its escape from the Attacker.

## REFERENCES

- [1] S. A. Ganebny, S. S. Kumkov, S. Le Ménéec, and V. S. Patsko, "Model problem in a line with two pursuers and one evader," *Dynamic Games and Applications*, vol. 2, no. 2, pp. 228–257, 2012.
- [2] H. Huang, W. Zhang, J. Ding, D. M. Stipanovic, and C. J. Tomlin, "Guaranteed decentralized pursuit-evasion in the plane with multiple pursuers," in *50th IEEE Conference on Decision and Control and European Control Conference*, 2011, pp. 4835–4840.
- [3] K. Pham, "Risk-averse based paradigms for uncertainty forecast and management in differential games of persistent disruptions and denials," in *American Control Conference*, 2010, pp. 842–849.
- [4] E. Bakolas and P. Tsiotras, "Optimal pursuit of moving targets using dynamic voronoi diagrams," in *49th IEEE Conference on Decision and Control*, 2010, pp. 7431–7436.
- [5] Z. E. Fuchs, P. P. Khargonekar, and J. Evers, "Cooperative defense within a single-pursuer, two-evader pursuit evasion differential game," in *49th IEEE Conference on Decision and Control*, 2010, pp. 3091–3097.
- [6] W. Scott and N. E. Leonard, "Pursuit, herding and evasion: A three-agent model of caribou predation," in *American Control Conference*, 2013, pp. 2978–2983.
- [7] R. L. Boyell, "Defending a moving target against missile or torpedo attack," *IEEE Transactions on Aerospace and Electronic Systems*, vol. AES-12, no. 4, pp. 522–526, 1976.
- [8] —, "Counterweapon aiming for defence of a moving target," *IEEE Transactions on Aerospace and Electronic Systems*, vol. AES-16, no. 3, pp. 402–408, 1980.
- [9] P. Zarchan, *Tactical and strategic missile guidance*. AIAA Progress in Aeronautics and Astronautics, Reston, VA, 1997, vol. 176.
- [10] G. Siouris, *Missile guidance and control systems*. New York, Springer, 2004.
- [11] A. Ratnoo and T. Shima, "Line-of-sight interceptor guidance for defending an aircraft," *Journal of Guidance, Control, and Dynamics*, vol. 34, no. 2, pp. 522–532, 2011.
- [12] T. Yamasaki and S. N. Balakrishnan, "Triangle intercept guidance for aerial defense," in *AIAA Guidance, Navigation, and Control Conference*. American Institute of Aeronautics and Astronautics, 2010.
- [13] T. Yamasaki, S. N. Balakrishnan, and H. Takano, "Modified command to line-of-sight intercept guidance for aircraft defense," *Journal of Guidance, Control, and Dynamics*, vol. 36, no. 3, pp. 898–902, 2013.
- [14] S. Rubinsky and S. Gutman, "Three body guaranteed pursuit and evasion," in *AIAA Guidance, Navigation, and Control Conference*, 2012, pp. 1–24.
- [15] —, "Three-player pursuit and evasion conflict," *Journal of Guidance, Control, and Dynamics*, vol. 37, no. 1, pp. 98–110, 2014.
- [16] A. Perelman, T. Shima, and I. Rusnak, "Cooperative differential games strategies for active aircraft protection from a homing missile," *Journal of Guidance, Control, and Dynamics*, vol. 34, no. 3, pp. 761–773, 2011.
- [17] I. Rusnak, "The lady, the bandits, and the bodyguards—a two team dynamic game," in *Proceedings of the 16th World IFAC Congress*, 2005.
- [18] I. Rusnak, H. Weiss, and G. Hexner, "Guidance laws in target-missile-defender scenario with an aggressive defender," in *Proceedings of the 18th IFAC World Congress*, vol. 18, no. Pt 1, 2011, pp. 9349–9354.
- [19] A. Ratnoo and T. Shima, "Guidance strategies against defended aerial targets," *Journal of Guidance, Control, and Dynamics*, vol. 35, no. 4, pp. 1059–1068, 2012.
- [20] T. Shima, "Optimal cooperative pursuit and evasion strategies against a homing missile," *Journal of Guidance, Control, and Dynamics*, vol. 34, no. 2, pp. 414–425, 2011.
- [21] V. Shaferman and T. Shima, "Cooperative multiple-model adaptive guidance for an aircraft defending missile," *Journal of Guidance, Control, and Dynamics*, vol. 33, no. 6, pp. 1801–1813, 2010.
- [22] O. Prokopov and T. Shima, "Linear quadratic optimal cooperative strategies for active aircraft protection," *Journal of Guidance, Control, and Dynamics*, vol. 36, no. 3, pp. 753–764, 2013.
- [23] E. Garcia, D. W. Casbeer, K. Pham, and M. Pachter, "Cooperative aircraft defense from an attacking missile," in *53rd IEEE Conference on Decision and Control*, 2014.
- [24] E. Garcia, D. W. Casbeer, K. Pham, and M. Pachter, "Cooperative aircraft defense from an attacking missile using proportional navigation," in *submitted to the 2015 AIAA Guidance, Navigation, and Control Conference*, 2014.