

Emitter Source Geolocation from Imparted Rotor Blade Modulation

by

Thomas Schucker

A Thesis Submitted to the Faculty of the

ELECTRICAL AND COMPUTER ENGINEERING

In Partial Fulfilment of the Requirements

For the Degree of

MASTER OF SCIENCE

In the Graduate College

THE UNIVERSITY OF ARIZONA

October 2016

STATEMENT BY AUTHOR

This thesis has been submitted in partial fulfillment of requirements for an advanced degree at the University of Arizona and is deposited in the University Library to be made available to borrowers under rules of the Library.

Brief quotations from this thesis are allowable without special permission, provided that an accurate acknowledgement of the source is made. Requests for permission for extended quotation from or reproduction of this manuscript in whole or in part may be granted by the head of the major department or the Dean of the Graduate College when in his or her judgment the proposed use of the material is in the interests of scholarship. In all other instances, however, permission must be obtained from the author.

SIGNED: Thomas Schucker

APPROVAL BY THESIS DIRECTOR

This thesis has been approved on the date shown below:

Tamal Bose	Date
Professor of	.
Electrical and Computer Engineering	.

Acknowledgements

I would like to thank my thesis advisor Dr. Tamal Bose for the opportunity to work in his lab and for the guidance through graduate school. I would also like to thank Matt Kruse and Charlie Cooper for coming up the research topic and support through the process. I would also like to thank the Broadband Wireless Access & Applications Center and Rincon Research Corporation for supporting this research.

*To my Mother and Father,
my brother Danny,
and my lovely girlfriend Clarice,
all with love,
thank you for your unconditional support.*

Contents

Statement By Author	1
Acknowledgements	2
List of Figures	7
List of Tables	9
Abbreviations	10
Symbols	11
Abstract	13
1 Introduction	14
1.1 Motivation	14
1.2 Contribution	14
1.3 Organization	15
2 Literature Review and Geometric Models	16
2.1 Introduction	16
2.2 Literature Review	16
2.3 Thesis Scope	17
2.4 Geometric Models	18
2.4.1 2D Geometric Model	18
2.4.2 3D Geometric Model	19
2.4.2.1 Transmitter in-line with Receiver and Rotor Blade	20
2.4.2.2 Approaching Model	24
2.4.2.3 Receding Model	25
3 Radio Propagation Simulation	29
3.1 Introduction	29

3.2 Radio Propagation Model	29
3.2.1 Free-Space Path Loss	30
3.2.2 Reflection	30
3.2.2.1 Specular Reflection	30
3.2.2.2 Reflection Loss	30
3.2.2.3 Diffuse Reflection	31
3.2.3 Fading	31
3.2.4 Doppler Effect	32
3.3 Scene Model	33
3.3.1 Rotor Blade	33
3.3.2 Transmitter	35
3.3.3 Receiver	35
3.4 Ray Tracing	36
3.4.1 Computation	37
3.4.2 Output	38
4 Received Signal Simulations	40
4.1 Introduction	40
4.2 Analysis Techniques	40
4.3 Receiver Position	42
4.4 Rotor Pitch	45
4.5 Transmitter Azimuth Angle	48
4.6 Transmitter Elevation Angle	52
5 Results	56
5.1 Introduction	56
5.2 Transmitter Azimuth Angle Estimation	56
5.3 Transmitter Elevation Angle Estimation	62
6 Conclusion and Future Work	70
6.1 Summary	70
6.2 Future Work	70
A Ray Tracing Software	72
B Class Documentation	75
B.1 Blade_surface Class Reference	76
B.2 Bounding_box Class Reference	78
B.3 Point3D Class Reference	80
B.4 Ray3D Class Reference	82
B.5 Receiver Class Reference	84
B.6 Rib Class Reference	86
B.7 Rotor Class Reference	87

B.8 Scene Class Reference	89
B.9 Sphere Class Reference	91
B.10 Transmitter Class Reference	93
B.11 Triangle Class Reference	95
B.12 Vector3D Class Reference	97

Bibliography	99
---------------------	-----------

List of Figures

2.1	2D Geometric model with Rx at the Axis of Rotation	18
2.2	Doppler Frequency vs. Rotor Position with varying Elevation Angle	20
2.3	3D Geometric model with Tx at Azimuth angle of 90°	21
2.4	Doppler profile of Tx at Azimuth angle of 90°	22
2.5	3D Geometric model with Tx at Azimuth angle of 270°	23
2.6	Doppler profile of Tx at Azimuth angle of 270°	24
2.7	3D Geometric model with Tx at Azimuth angle of 180°	25
2.8	Doppler profile of Tx at Azimuth angle of 180°	26
2.9	3D Geometric model with Tx at Azimuth angle of 0°	27
2.10	Doppler profile of Tx at Azimuth angle of 0°	28
3.1	Airfoil Cross-Section	33
3.2	Blade Surface Tessellation	34
3.3	Transmitter Rays	36
3.4	Disk Sampling Method	38
4.1	Example Spectrum for one Blade revolution with transmitter at Azimuth of 45° and Elevation of 35°	41
4.2	Example Spectrum with Doppler Profile for one Blade revolution with transmitter at Azimuth of 45° and Elevation of 35°	42
4.3	Position of the Receiver in Relation to the Rotor Blades	43
4.4	Max and Min Doppler vs. Receiver Position with Tx Azimuth at 135° and Elevation at 54°	43
4.5	Doppler Envelope with receiver at 0m	44
4.6	Doppler Envelope with receiver at 7m	44
4.7	Rotor Pitch	45
4.8	Max and Min Envelope Frequencies vs Rotor Pitch with Tx Azimuth at 135° and Elevation at 54°	46
4.9	Max and Min Envelope Frequencies vs Rotor Pitch Transmitter Underneath the Helicopter	46
4.10	Max Envelope Frequencies vs Transmitter Elevation Angle	47
4.11	Frequency Difference vs Transmitter Elevation Angle	48
4.12	Transmitter Azimuth Angle Relationship	49
4.13	Max and Min Envelope Frequencies vs Transmitter Azimuth Angle with Tx Elevation at 45°	49

4.14	Max and Min Envelope Frequencies vs Transmitter Azimuth Angle with Tx Elevation at 76°	50
4.15	Max and Min Envelope Frequencies vs Transmitter Azimuth Angle with Tx Elevation at 26.5°	50
4.16	Max and Min Envelope Frequencies vs Transmitter Azimuth Angle with Rx at Axis of Rotation	51
4.17	Max and Min Envelope Frequencies vs Transmitter Elevation Angle with 7.5deg Pitch	52
4.18	Transmitter Elevation Angle	52
4.19	Transmitter Range vs Elevation Angle at an Altitude of 200m	53
4.20	Max and Min Envelope Frequencies vs Transmitter Elevation Angle with Tx Azimuth of 135deg	54
4.21	Doppler Profile vs. Transmitter Elevation angle for various Azimuth angles.	55
5.1	Max and Absolute value of Min Envelope Frequencies vs Transmitter Azimuth Angle at an Elevation Angle of 45°	57
5.2	Difference between Max and Min Envelope Calculations vs Transmitter Azimuth Angle at an Elevation Angle of 45°	58
5.3	Correct Doppler Frequencies vs Transmitter Azimuth Angle at an Elevation Angle of 45°	58
5.4	Correct Doppler Frequencies with Minimum vs Transmitter Azimuth Angle at an Elevation Angle of 45°	59
5.5	Peaks of inverted Correct Doppler vs Transmitter Azimuth Angle at an Elevation Angle of 45°	60
5.6	Average Power vs Transmitter Azimuth Angle at an Elevation Angle of 45°	61
5.7	Estimated Reflection Radius at an Elevation Angle of 45°	63
5.8	Actual Elevation Angle and Estimated Elevation Angle vs Azimuth Angle	64
5.9	Elevation Angle Percent Error vs Transmitter Azimuth Angle	65
5.10	Max and Min Envelope Frequencies vs Elevation Angle with Transmitter Azimuth Angle of 180°	66
5.11	Elevation Estimate and Actual Angle with Transmitter Azimuth Angle of 180°	66
5.12	Elevation Angle Percent Error with Transmitter Azimuth Angle of 180°	67
5.13	Uncorrected Envelope Difference vs. Transmitter Azimuth and Elevation angle of 45°with Blade pitch of 7.5°	68
5.14	Uncorrected Doppler vs. Transmitter Azimuth and Elevation angle of 45°with Blade pitch of 7.5°	68

List of Tables

5.1	Azimuth Error and Azimuth Percent Error of Different Elevation Angles During Azimuth Estimation	61
5.2	Percent Peak, Power, and Frequency Difference of Different Elevation Angles During Azimuth Estimation	62
5.3	Average Elevation Error and Average Elevation Percent Error of Different Elevation Angles During Azimuth Estimation	64
A.1	Simulation parameters	73
A.2	Output file header with simulation parameter order	74

Abbreviations

2D	2-Dimensional
3D	3-Dimensional
BER	Bit Error Rate
BRDF	Bi-directional Reflection Distribution Function
CSV	Comma Separated Value
DSP	Digital Signal Processing
GPS	Global Positioning System
GPU	Graphics Processing Unit
GUI	Graphical User Interface
IQ	In-phase and Quadrature
JEM	Jet Engine Modulation
LOS	Line Of Sight
RBM	Rotor Blade Modulation
RF	Radio Frequency
RPM	Rotations Per Minute
Rx	Receiver
STFT	Short Time Fourier Transform
Tx	Transmitter

Symbols

Symbol	Name	Units
θ_{El}	Transmitter Elevation angle	degrees
θ_r	Ray Reflection angle	degrees
θ_{Az}	Transmitter Azimuth angle	degrees
f_d	Doppler Frequency shift	Hz
θ_b	Rotor Blade angle	degrees
Rx_x	Receiver position in X axis	meters
Rx_y	Receiver position in Y axis	meters
Rx_z	Receiver position in Z axis	meters
G_r	Receiver antenna gain	
G_t	Transmitter antenna gain	
R	Distance	meters
\vec{n}	Surface normal vector	
\vec{d}_i	Direction vector of incident ray	
Γ	Reflection loss coefficient	
θ_i	Angle of incidence with an objects normal	radians
r	A radius along the length of the blade	meters
ω_r	Rotational velocity of the blade	rad/second
F	Fading coefficient	

λ	Wavelength	meters
c	Speed of Light	meters/seconds
f	frequency	Hz
f_0	initial frequency	Hz
f_s	sampling frequency	samples/seconds
$ProfileDifference$	Difference between two Doppler profiles	Hz
$MaxDopplerProfile$	Array of values corresponding to the maximum of each azimuth or elevation doppler profile calculation	Hz
$MinDopplerProfile$	Array of values corresponding to the minimum of each azimuth or elevation doppler profile calculation	Hz
r_b	Length of single rotor blade (radius of rotor)	meters
f_c	Center Frequency	Hz
$R_{Estimate}$	Estimated reflection radius	meters
$f_{DopplerMax}$	The maximum amount of doppler for a particular blade length and RPM	Hz
$f_{DopplerCorrect}$	The corrected doppler per θ_{Az} to be processed	Hz
A_{shift}	The amount of shift needed to correct for Blade pitch	Hz

Abstract

In RF communications with a rotorcraft such as a helicopter, the rotor blades can impart a modulation onto the received signal called Rotor Blade Modulation (RBM). This modulation is caused by the reflection of a signal off the rotating blades. The reflected signal is Doppler shifted based on where the signal is reflected along the length of the blade as well as the angle between the axis of rotation and the emitter. RBM is known to degrade the performance of RF communications on rotorcraft and can be used in radar applications to detect and classify aircraft, but there is little on its usefulness in other areas. This thesis looks at the ability to utilize the RBM phenomenon on the rotorcraft itself to geo-locate and track a signal emitter on the ground.

To do this a 3D RF ray tracing program was developed in C++ to produce simulations of RBM signals. The developed program is based on optical ray tracing algorithms with modified physical propagation effects for RF signals, and swapping lights and cameras for RF transmitters and receivers respectively. The ray tracer was then run over a realistic set of physical parameters to determine their effects on the received signal; this includes transmitter azimuth and elevation angle, receiver position, blade pitch, etc. along with their combinations. The simulations of the azimuth and elevation angle produce predictable modulations on the received signal. Based on the trends in the signal's modulation, a DSP algorithm was distilled down that accurately determines the azimuth and elevation angle of the transmitter from simulated signal data.

Chapter 1

Introduction

1.1 Motivation

In RF communications with a rotorcraft, such as a helicopter, the rotor blades can impart a modulation onto the received signal called Rotor Blade Modulation (RBM). This modulation is caused by the reflection of a signal off the rotating blades. The reflected signal is Doppler shifted based on where the signal is reflected along the length of the blade as well as the elevation angle between the axis of rotation and the emitter. RBM can be used in radar to detect and classify aircraft based on a specific signature and can degrade communication system located on the rotorcraft itself. The motivation behind this work is to use the RBM effect to locate uncooperative emitters on the ground. This is done through the use of specific knowledge of the craft itself and measuring the RBM in the received signal.

1.2 Contribution

The main contributions of this thesis are as follows. A 3-Dimensional (3D) ray tracing software is provided to simulate the Radio Frequency (RF) propagation in the presence of a helicopter rotor blade. The software provides insight into the complex interaction between the rotor blade shape and the placement of the receiver and transmitters. The

second contribution is an in depth analysis of how several different variables affect the modulation on the received signal. And lastly, techniques to use the imparted rotor blade modulation to estimate the azimuth and elevation angles with respect to the location of the rotating blades.

1.3 Organization

In Chapter 2 we present the background and theory behind rotor blade modulation. We then formulate the basic geometry behind the RBM effect.

In Chapter 3 we introduce the radio propagation simulation in several sections. First is the RF propagation model which defines the physical effects that are simulated within the software. Next the objects of the scene model, as well as the dimensionality, are defined in software to be representative of their physical dimensions and functionality. Lastly, we describe the core ray tracing engine that traces the scene in successive frames to build the receiver output.

In Chapter 4 we present the result of the parameter swept simulations of the ray tracing software. Next the received signals from the simulation are analyzed using several Digital Signal Processing (DSP) techniques to define the signal characteristics that will be used in the next chapter for estimation.

In Chapter 5 those characteristics from chapter 4 are then used to estimate the azimuth and elevation angle of the transmitter based on the given rotor and receiver parameters. Those estimates are then compared with the original position of the transmitter to determine the methods accuracy.

In Chapter 6 the results are detailed along with the current limitations. Lastly, future improvements on the work will be discussed.

Chapter 2

Literature Review and Geometric Models

2.1 Introduction

This section details the basic phenomenon behind rotor blade modulation along with its significance in other applications, and the defining characteristics that allow its use in this application. The second part of this section describes the geometric models for the 2-Dimensional (2D) case and several 3D cases. These models will form the basis for verification of the simulations.

2.2 Literature Review

The rotating blades of the helicopter modulate signals that hit the blades by reflecting them. The reflected signal, through the Doppler effect, become shifted in frequency in relationship to the velocity of the reflection point [1]. The RBM has a complex form and is influenced by several object parameters. These parameters range from the positioning of a signal source to the physical dimensions of the rotor blades.

The resulting modulated signal has been used in several radar applications. One radar application of RBM was to determine the specific characteristics of a noncooperative helicopter using time frequency analysis by Bullard and Dowdy in [2]. Where they define specific signatures for physical parameters of a helicopter. The ability to detect a hovering helicopter based on the blade flashes caused by reflected radar pulses off the blades is examined by Misiurewicz, Kulpa, and Czekala in [3], where they used information the time domain to determine if a helicopter was hovering. The micro-Doppler produced by the radar reflection was used by Thayaparan et. al. in [4] to determine the rotation rate of both the main and tail rotor blades using the Wavelet transform. Other types of aircraft produce modulations on a returned radar pulse; one type known as Jet Engine Modulation (JEM) is the product of a radar pulse reflecting off the jet engine blades [5]. The information can similarly be used to quantify physical aspects of the aircraft when present in order to perform classification.

The Doppler shifted signal, caused by RBM, is shown by Barbiero, Vincent, and Deloues in [6] to effect the performance of common adaptive Global Positioning System (GPS) anti-jamming algorithms located on helicopter platforms. They were able to mitigate the effects by estimating the covariance within a few milliseconds but this comes at an extreme computation overhead. And for iterative based anti-jamming approaches the non-stationary signal characteristics cause degradation as well. The affect of RBM on the Bit Error Rate (BER) of communications is examined by Zhang, Amin, and Mancuso in [1], where effects of multipath and Doppler cause large BER values at small elevation angles and large scattering coefficients described in the model.

The role of RBM in this thesis is based on specific Doppler shifts associated with where a dominant reflection occurs along the length of the blade, and the associated elevation angle of the transmitter. The received signal is then used to create a mapping between the amount of Doppler present and the position of the transmitter on the ground.

2.3 Thesis Scope

ADD WHAT THIS THESIS IS AND POINT OUT WHAT IT IS NOT!

2.4 Geometric Models

The geometric model will begin with a 2D scene that will describe the geometry between the rotor blade, the transmitter, and the receiver. Then the model will evolve into a selection of 3D models that will form the foundation for the results of the ray tracer.

2.4.1 2D Geometric Model

The 2D geometric mode is based on a few assumptions, first that the receiver is placed as close as possible to the center of rotation, and second that all the physical objects are located within a single 2D plane. This model is represented in Figure 2.1.

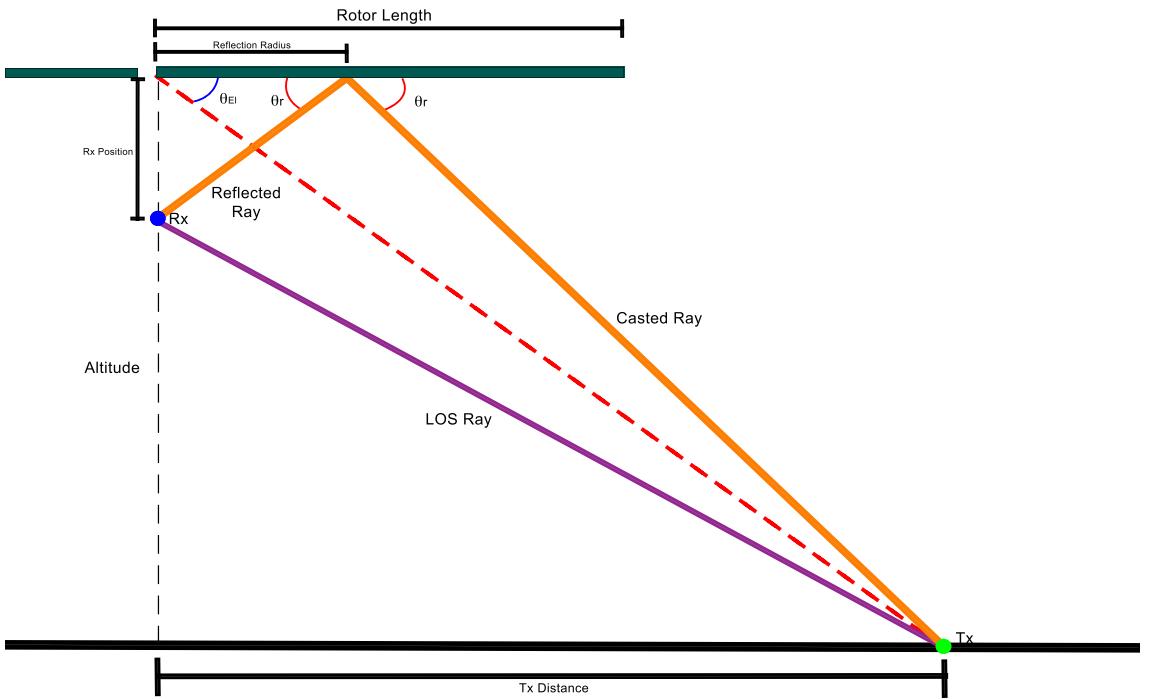


FIGURE 2.1: 2D Geometric model with Rx at the Axis of Rotation

There are three physical objects within this scene. The first being the rotor blade, which is the dark green bar depicted in the figure. Next is the transmitter Tx , in green, and the receiver Rx in blue. The measurements, depicted as black bars with denoted start and stop points, reference the various distances used in the following equations. The dashed

green line shows at which altitude the helicopter is hovering at, and the red dashed line transverses the transmitter and the center of rotation for the blades. θ_{El} is the elevation angle of the transmitter with respect to the rotor blades and θ_b denotes the specular reflection of the casted and reflected rays in orange. Lastly the line of sight (LOS) ray shows that the transmitter and receiver are in visual line of sight of each other.

The resulting Doppler equation is described by

$$f_d = -f_{DopplerMax} \cos(\theta_{El}) \cos(\theta_b) \quad (2.1)$$

where f_d is the Doppler frequency shift, $f_{DopplerMax}$ is defined later by equation 5.8 as the maximum amount of Doppler shift possible, θ_{El} is the elevation angle of the transmitter with respect to the rotor blades, and θ_b is the current angle of the rotor blade.

Figure 2.2 shows the varying Doppler frequency caused by the RBM at various elevation angles of the transmitter. The results of this is a sinusoidal Doppler profile in which the amplitude increases as the elevation angle decreases.

Since this model has the receiver located at the axis of rotation this model can be seen as a special case of the next 3D models, because it is symmetric around the axis of rotation. Therefore, any placement of the transmitter in 3D space can be distilled down to a 2D profile as such. This symmetry should then be mirrored in the ray tracing simulation as verification.

2.4.2 3D Geometric Model

The 3D geometric model is categorized by the position of the rotor blade and the position of the signal source. Since the rotor blade has a specific airfoil shape, the models will take that into account through an approximation of that surface. The first model will be representative of having the transmitter in-line with both the receiver and the blade, with the transmitter in both fore and aft positions. The next model will have the rotor approaching both the receiver and transmitter, and lastly the rotor will be receding from

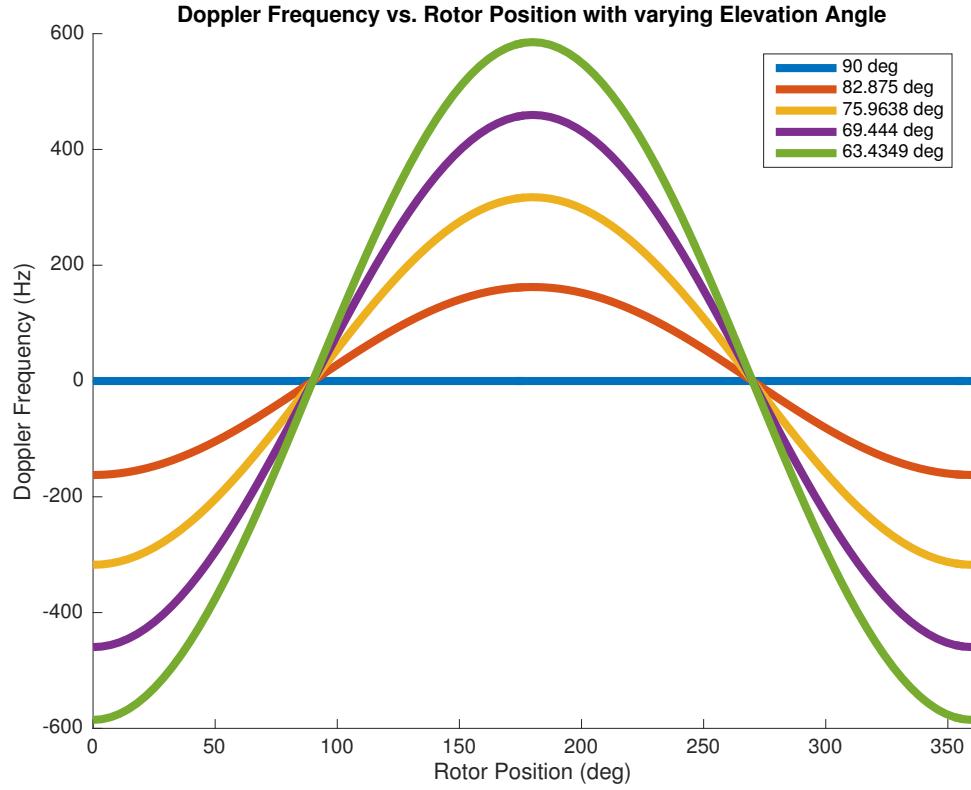


FIGURE 2.2: Doppler Frequency vs. Rotor Position with varying Elevation Angle

both the receiver and transmitter. All of the 3D models will have the receiver positioned offset from the axis of rotation.

2.4.2.1 Transmitter in-line with Receiver and Rotor Blade

The first two models as mentioned above fall under the criteria of the transmitter being in-line with both the rotor blade and the offset receiver.

Figure 2.3 depicts the transmitter at a 90° azimuth angle, which places it in-line with the position of the receiver and the current location of the rotating blades.

The objects in 2.3 are similar to the ones previously stated in the 2D case. The X and Y axis are specifically drawn in blue and red respectfully, with the Z axis now the green dashed line and altitude is now denoted with a measurement bar. The receiver offset in

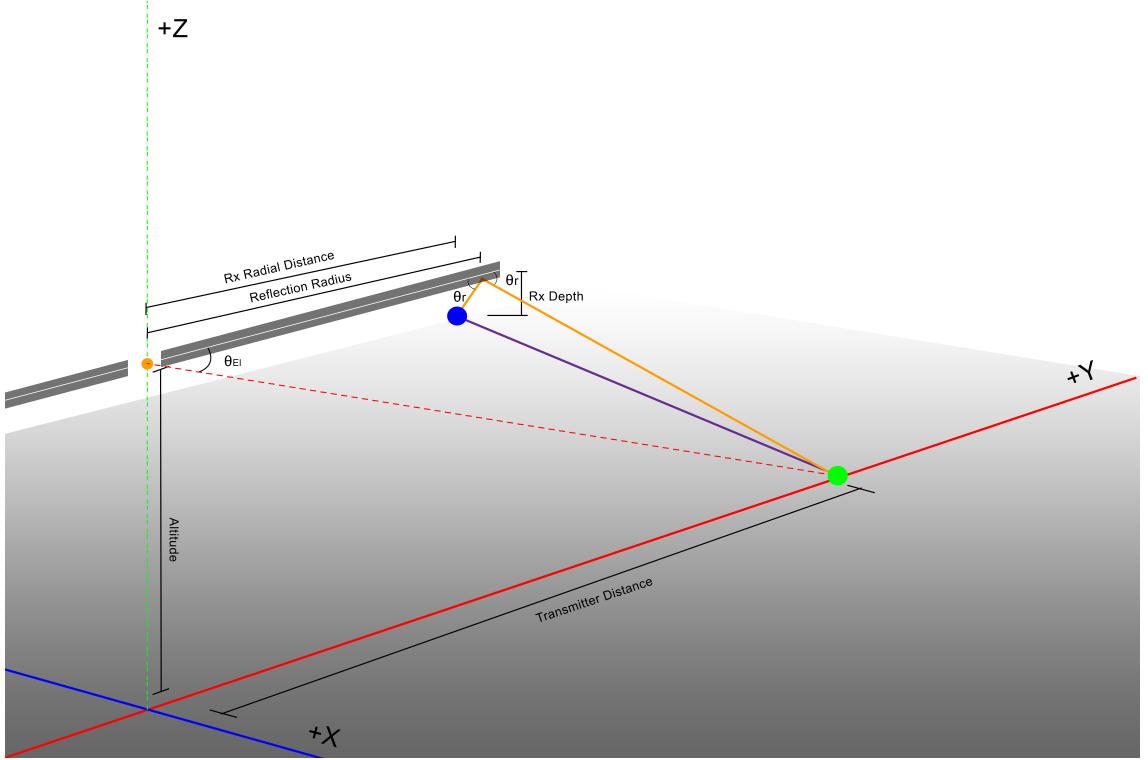


FIGURE 2.3: 3D Geometric model with Tx at Azimuth angle of 90°

the +Y direction is now stated and the blades are now colored gray. All other variables and colors denote their objects as previously stated in the 2D case.

The equation for modeling the scenario for a transmitter located at 90° azimuth is

$$\text{MaxDopplerProfile} = f_{\text{DopplerMax}} \cos(\theta_{\text{Limited}}) \quad (2.2)$$

and

$$\text{MinDopplerProfile} = -f_{\text{DopplerMax}} \cos(\theta_{\text{Limited}}) \quad (2.3)$$

where *MaxDopplerProfile* is an array of the maximum upper envelope values for each elevation sample, *MinDopplerProfile* is an array of minimum lower envelope values for each elevation sample, and θ_{Limited} is the limited elevation angle range

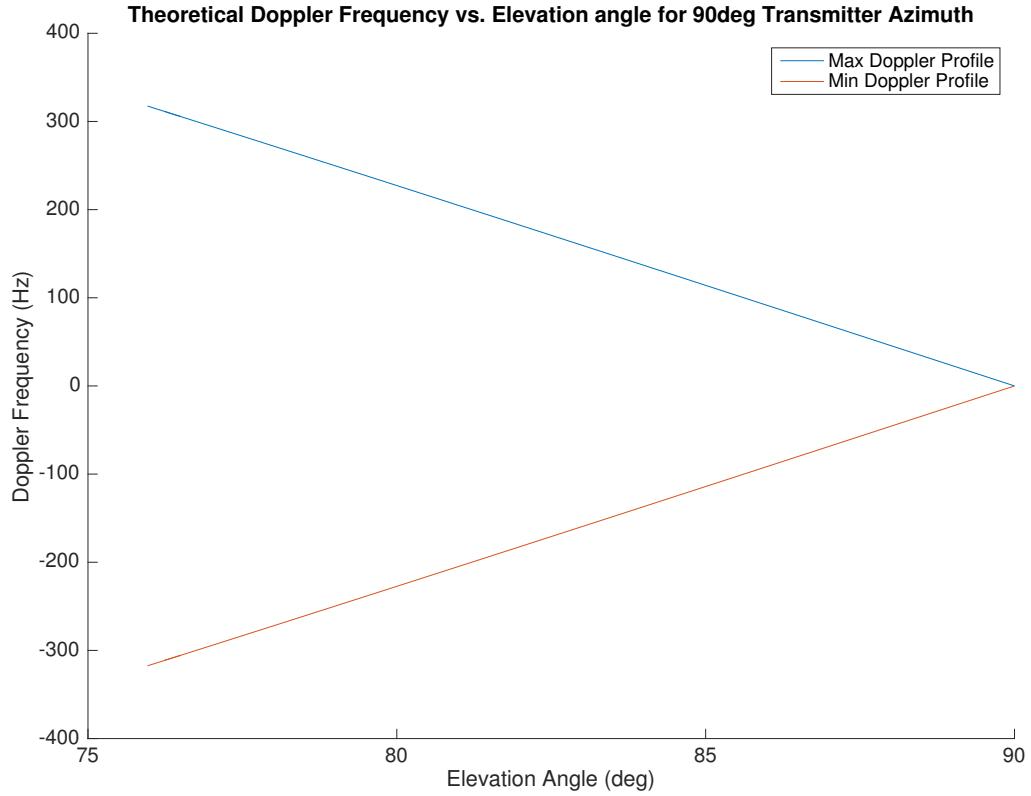


FIGURE 2.4: Doppler profile of Tx at Azimuth angle of 90°

$$\theta_{Limited} = \text{atan} \left(\frac{Rx_z}{[0, \dots, (r_b - Rx_y)]} \right) \quad (2.4)$$

where Rx_z is the receivers position below the rotor head, r_b is the length of the rotor blade, and Rx_y is the receivers position on the Y axis.

Figure 2.4 shows the maximum and minimum Doppler values versus elevation angle for a transmitter at an azimuth angle of 90°. The elevation angle is limited by the reflection angle, caused by the limited distance between the tip of the blade and the location of the receiver. This limitation constrains the Doppler profile causing inaccurate transmitter elevation estimation at this transmitter azimuth position.

Figure 2.5 depicts the transmitter at a 270° azimuth angle, which places it in-line with the position of the receiver and the current location of the rotating blades. This placement

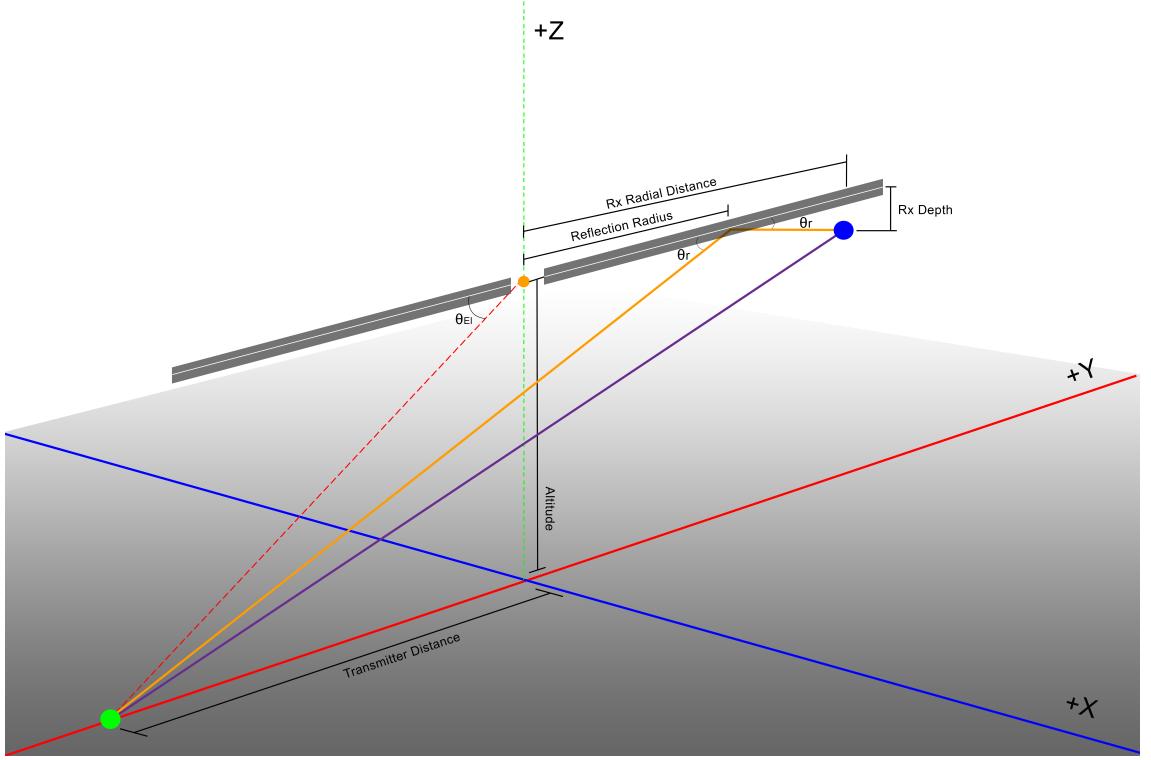


FIGURE 2.5: 3D Geometric model with Tx at Azimuth angle of 270°

of the transmitter behind the helicopter is different from the situation in Figure 2.3 because the value of θ_r is now limited by the rotor hub and maximum reflection radius.

The equation for modeling the scenario for a transmitter located at 270° azimuth is similar to the equations for calculating the 90° scenario where $f_{DopplerMax}$ is now calculated with a smaller reflection radius of 2m and $\theta_{Limited}$ is now calculated by

$$\theta_{Limited} = \text{atan} \left(\frac{Rx_z}{[0, \dots, Rx_y]} \right) \quad (2.5)$$

Figure 2.6 shows the maximum and minimum Doppler values versus elevation angle for a transmitter at an azimuth angle of 270°. The data from the figure is similar to the data from the previous Figure 2.3 and even though it is not limited on elevation angle the consequence is a limited reflection radius.

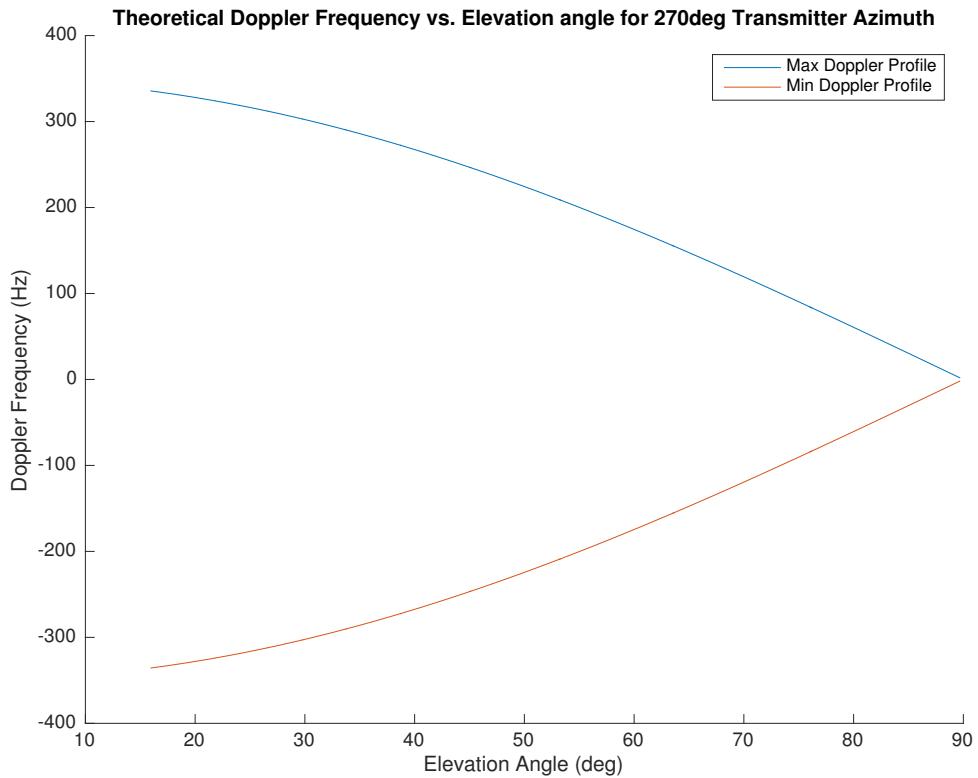


FIGURE 2.6: Doppler profile of Tx at Azimuth angle of 270°

2.4.2.2 Approaching Model

The approaching model shown in Figure 2.7 depicts the transmitter at an azimuth of 180° and the axis of X has now been rotated to be -X. The direction of the rotor blades is depicted, in green, to follow the previous assumptions.

This case of the 3D model places the transmitter at 180° so that the oncoming blades move toward both the receiver and the transmitter at the same time. This particular placement will cause a positive Doppler profile because the blades will be moving in the direction of both objects, compressing the reflected wave accordingly.

The equation for modeling the scenario for a transmitter located at 180° azimuth is

$$\text{MaxDopplerProfile} = f_{\text{DopplerMax}} \cos(\theta_{El}) \quad (2.6)$$

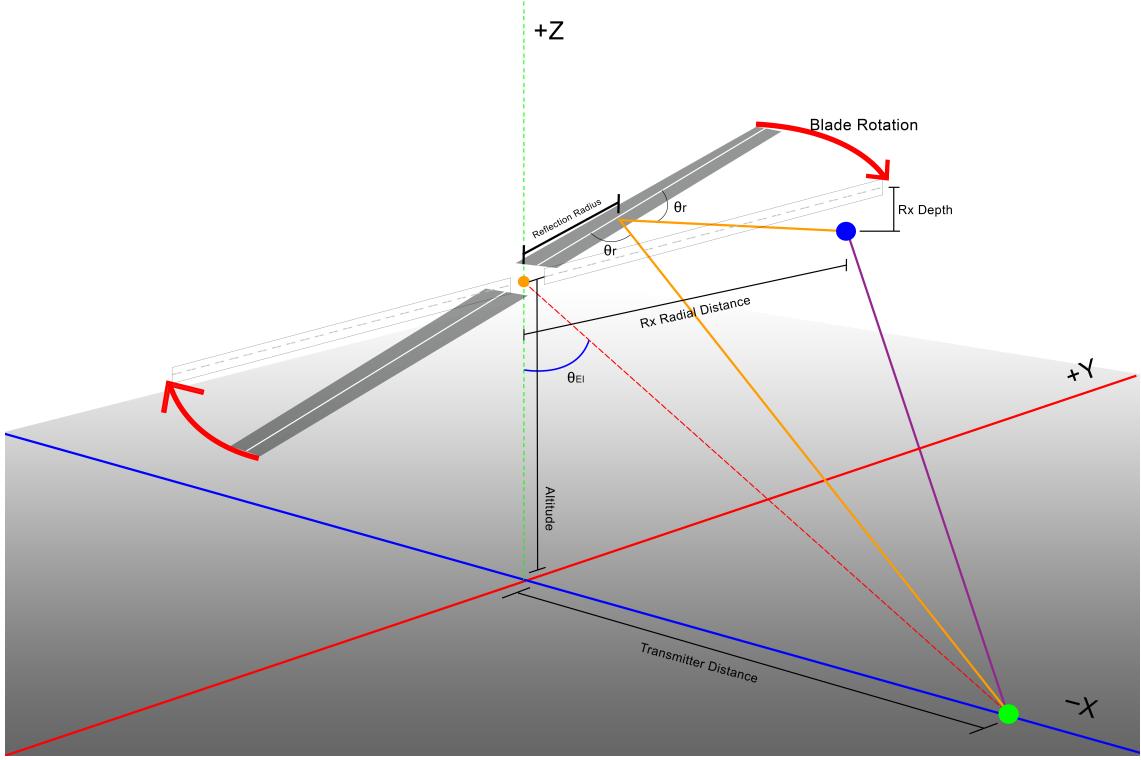


FIGURE 2.7: 3D Geometric model with Tx at Azimuth angle of 180°

and the *MinDopplerProfile* is set to 0 for the range.

Figure 2.8 shows the maximum and minimum Doppler profile values versus elevation angle for a transmitter at an azimuth angle of 180°. The data from the figure shows the maximum, of the Doppler profile, decrease as the elevation angle gets larger.

2.4.2.3 Receding Model

The receding model shown in Figure 2.9 depicts the transmitter at an azimuth of 0° where the axis positions are back to their original places and the direction of the rotor blade is now depicted in red.

This case of the 3D model places the transmitter at 0° so that the receding blades move away from both the receiver and the transmitter at the same time. This particular placement should provide a negative Doppler profile because the blades will be moving in the opposite direction of both objects, stretching the reflected wave accordingly.

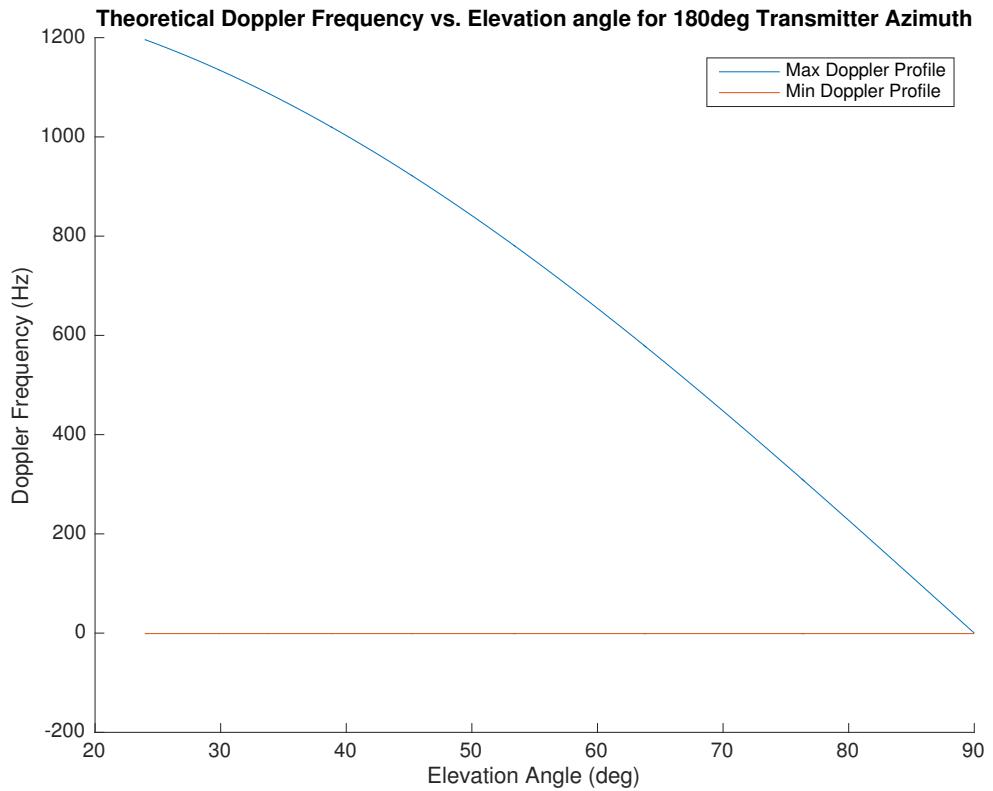


FIGURE 2.8: Doppler profile of Tx at Azimuth angle of 180°

The equation for modeling the scenario for a transmitter located at 0° azimuth is

$$\text{MinDopplerProfile} = -f_{\text{DopplerMax}} \cos(\theta_{\text{El}}) \quad (2.7)$$

and the *MaxDopplerProfile* is set to 0 for the range.

Figure 2.10 shows the maximum and minimum Doppler profile values versus elevation angle for a transmitter at an azimuth angle of 0°. The data from the figure shows the minimum of the Doppler profile increase as the elevation angle gets larger.

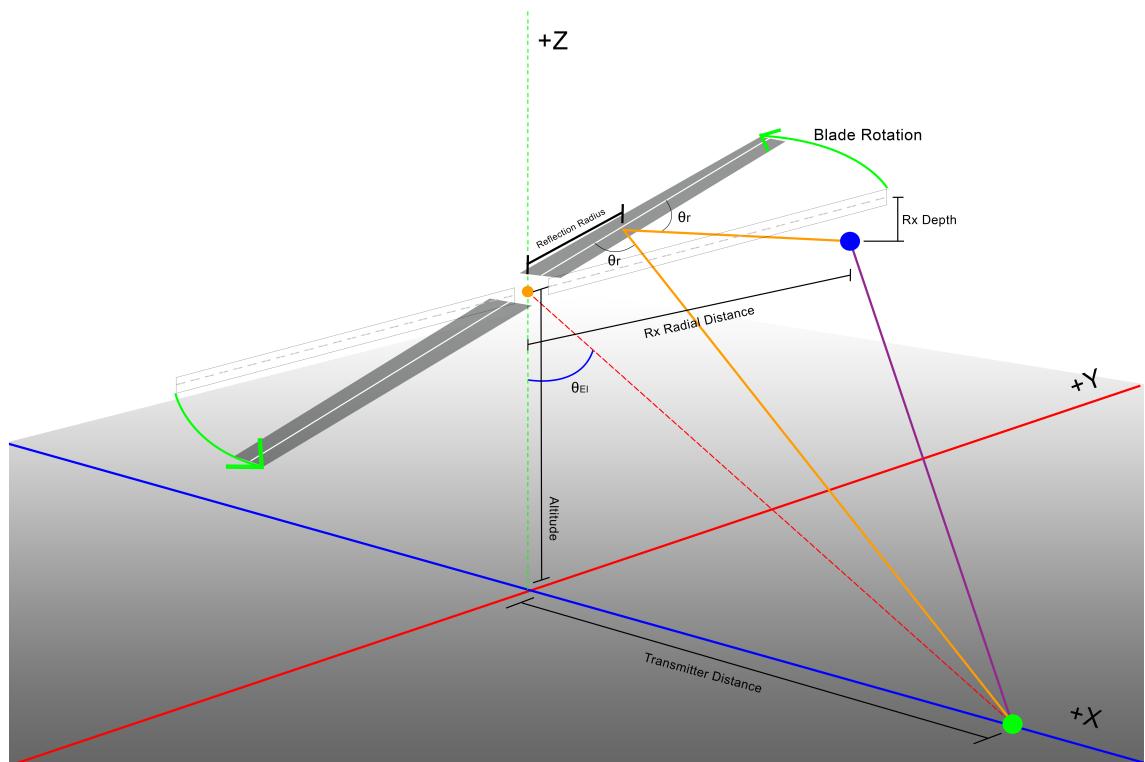


FIGURE 2.9: 3D Geometric model with Tx at Azimuth angle of 0°

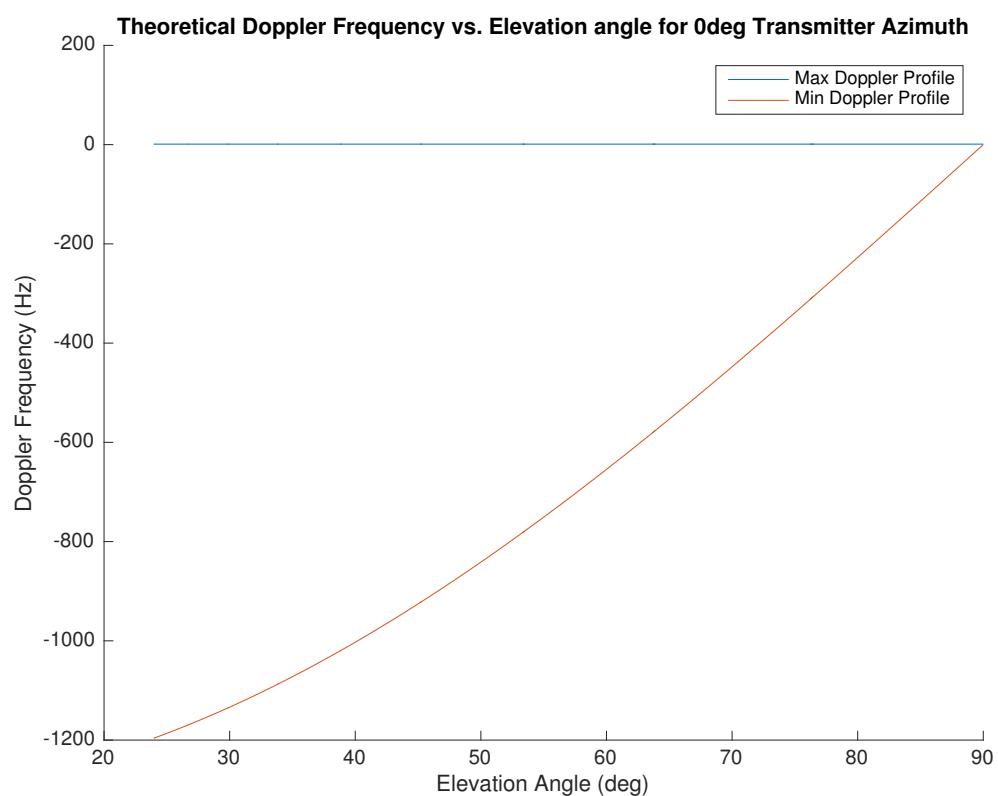


FIGURE 2.10: Doppler profile of Tx at Azimuth angle of 0°

Chapter 3

Radio Propagation Simulation

3.1 Introduction

The simulation software is broken down into three main components; the radio wave propagation model, the scene model, and the ray tracing engine. The wave propagation model is a collection of equations that describe the physical phenomena that affect the propagation when represented by rays. The model used is based upon classical geometric optics to work with the ray tracing engine. The scene model is comprised of a 3D environment in order to define the physical rotor blade surface. The receiver and transmitter will also be defined in the same environment with simulated characteristics to match real life conditions. The ray tracing engine uses recursive execution described by Whitted in [7], replacing cameras and lights for receivers and transmitters respectively in a three dimensional environment.

3.2 Radio Propagation Model

The propagation model defined in this project is based on the following physical phenomena; free-space path loss, reflection, fading, and the doppler effect. Which are all formally established models described in [8–10]. Although several effects are described within the model several were left out to simplify the computation due to the overhead

of implementation in 3D space and because of the assumptions made about the scene model.

3.2.1 Free-Space Path Loss

Free-Space Path Loss is calculated using the Friis transmission and is incorporated into the model by keeping track of the distance a ray travels and adjusting its power by

$$P_r = G_r G_t P_t \left(\frac{\lambda}{4\pi R} \right)^2 \quad (3.1)$$

where P_r is the power at the receiver, P_t is the power at the transmitter, G_r and G_t are the antenna gains, λ is the wavelength, and R is the distance between the receiver and transmitter antennas. In the simulations described in this paper, G_r and G_t are assumed to have a value of 1.

3.2.2 Reflection

3.2.2.1 Specular Reflection

In the case of a perfect reflection the angle of the reflection is calculated by

$$\theta_r = \cos^{-1}(\vec{n} \bullet (-\vec{d}_i)) \quad (3.2)$$

where θ_r is the angle of the reflected ray, \vec{n} is the normal vector to the surface, and \vec{d}_i is the direction vector of the incident ray.

3.2.2.2 Reflection Loss

Power loss due to surface reflection is described through the following coefficient

$$\Gamma = \frac{\cos(\theta_i) - \sqrt{\varepsilon} \cos(\theta_t)}{\cos(\theta_i) + \sqrt{\varepsilon} \cos(\theta_t)} \quad (3.3)$$

where θ_i is the angle of incidence with the object's surface normal, ε is the dielectric constant for that surface, and θ_t is the angle of refraction as described by Snell's law

$$\theta_t = \sin^{-1} \left(\frac{\sin(\theta_i)}{\sqrt{\varepsilon}} \right) \quad (3.4)$$

The final reflected power is then

$$P_{reflected} = P_i |\Gamma| \quad (3.5)$$

where P_i is the incident power before reflection loss.

3.2.2.3 Diffuse Reflection

A perfect diffuse reflection, also known as Lambertian reflection, will reflect rays in all directions in a uniform hemisphere [11]. The hemisphere is centered at the point the ray hits, producing rays away from the surface. To approximate a particular type of surface the rays power is attenuated by the surface's bi-directional reflectance distribution function (BRDF) [12–14]. There are several ways of calculating the BRDF, but the simplest is the Phong BRDF which will be used in this ray tracing implementation [15]. This method for the BRDF is regularly used in the rendering of computer graphics to simulate the reflection of light off surfaces and combines the diffuse and specular components. Since this was not designed for the longer wavelengths used in RF communications, an assumption is made about surface features. Where surface features, relevant to light waves, produce a reflectance distribution similar for this application.

3.2.3 Fading

The transmitted signal power experiences fading described by

FIGURE OUT WHAT TO PUT HERE FOR FADING COEFFICIENT?

The power can then be calculated using

FADING POWER?

The superposition of each ray's faded power becomes the received signal.

3.2.4 Doppler Effect

It is assumed that both the receiver and the transmitter are not moving therefore, the only Doppler imparted on the signal will be from the rotation of the blades. The associated Doppler is calculated using

$$f = f_0 + \frac{v_t + v_r}{\lambda} \quad (3.6)$$

where f_0 is the initial transmitted frequency, λ is the wavelength, v_t is the velocity in the direction of the transmitter, and v_r is the velocity in the direction of the reflection. This is similar to the Bi-static radar equation for Doppler, but since the reflection is not guaranteed to be toward the receiver we calculate the Doppler as it makes contact with the surface and as it is re-radiated according the blades direction of travel.

$$\lambda = \frac{c}{f_0} \quad (3.7)$$

where λ is the wavelength of the transmitted signal based off of the speed of light c and its initial frequency f_0 . The velocity in the direction of the transmitter is given by

$$v_t = r\omega_r(\vec{d}_p \bullet \vec{d}_t) \quad (3.8)$$

where r is the radius along the length of the blade where the reflection occurs. ω_r is the angular velocity of the rotor. \vec{d}_p is the normalized vector that is perpendicular to the rotor in its direction of travel and \vec{d}_t is the normalized vector that is in the direction of the transmitted ray. The velocity in the direction of the reflection is given by

$$v_r = r\omega_r(\vec{d}_p \bullet \vec{d}_r) \quad (3.9)$$

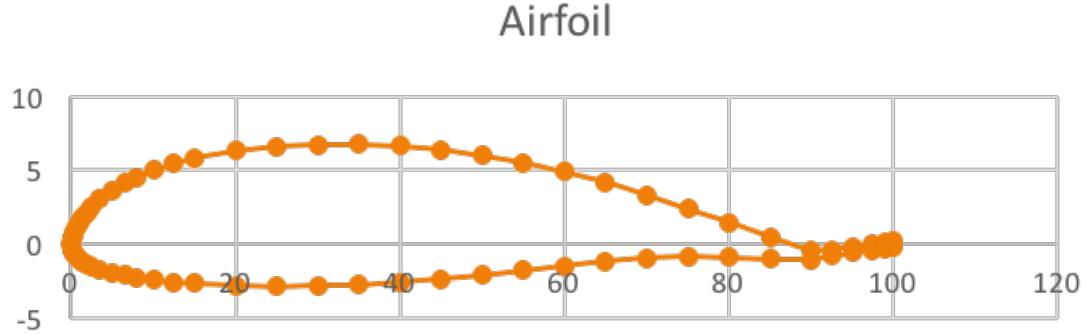


FIGURE 3.1: Airfoil Cross-Section

where \vec{d}_r is the normalized vector that is in the direction of the reflected ray.

3.3 Scene Model

The scene model is the 3D environment in which the physical objects are placed. The model is comprised of three types of objects; the rotor blades, transmitter and receiver. The rotor blade is the most complex object due to its airfoil shape. The transmitter is a point source that projects the rays into the scene, and the receiver is described in a similar fashion with a surrounding boundary layer. There are no other objects within the scene. This is because the effect of the rotor on the received signal is analyzed for defining characteristics without outside variables.

3.3.1 Rotor Blade

The airfoil shape is designed to produce lift for the helicopter, and designing one is outside the scope of this project. Fortunately, there are databases that provide real helicopter airfoil designs in x,y coordinates. This data forms a 2D cross-section of the airfoil shape that will be extruded into the length of the rotor blade. Figure 3.1 shows the airfoil cross-section that will be used to create the rotor surface.

The 2D airfoil sections will form the ribs of the rotor blade but the surface of the blade will be made up of primitive surfaces to approximate the curved airfoil shape. The

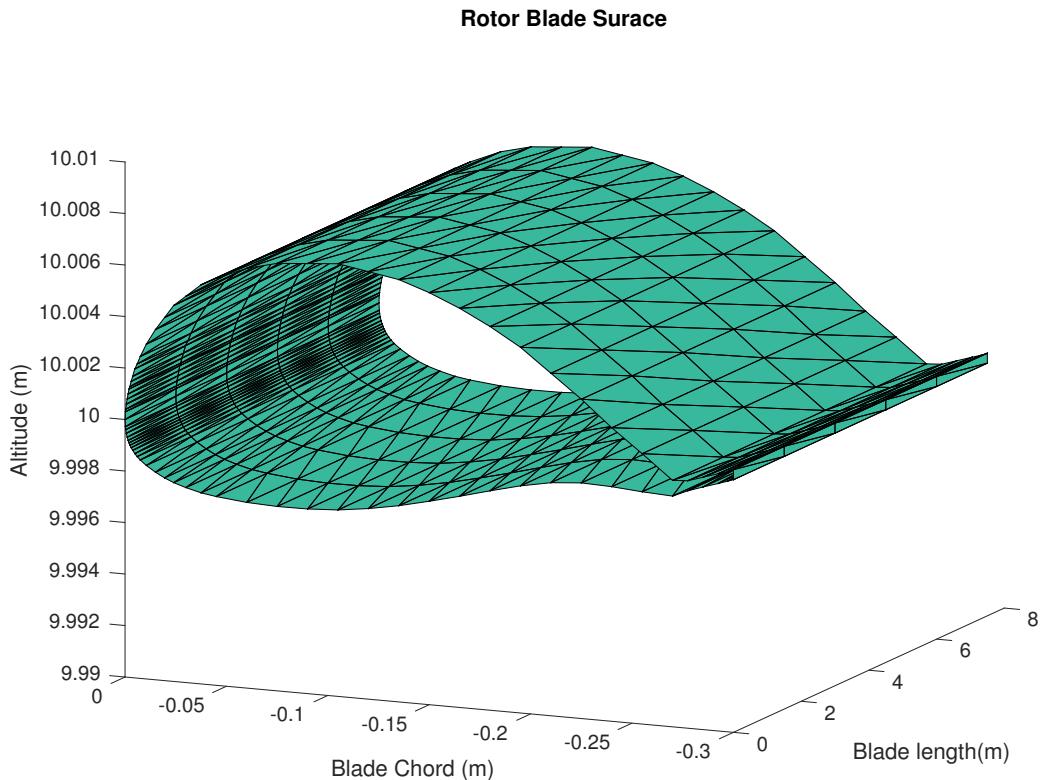


FIGURE 3.2: Blade Surface Tessellation

primitive shapes are triangles that span between the ribs and go around to cover the surface. This was done using a lightweight mesh generation method using knowledge of the blade’s finished shape. The designed algorithm, located in [B.1 *create_surface\(\)*](#) method, takes advantage of the object’s uniform structure in 2D. The surface normals are then adjusted to match the correct directionality. Figure 3.2 shows the created surface for the rotor blade that will be used in the scene.

All aspects of the rotor blade are parameterized. Starting with the airfoil shape, which is defined by a set of 2D coordinates. The length and the number of rib sections can be configured along with the number of blades and corresponding altitude, as well as the RPM. This allows the scene to replicate any type of rotor configuration and position it at a specific altitude.

3.3.2 Transmitter

The transmitter is modeled as a point source, this means that all the radio waves are projected from this point into the scene. It is assumed that the transmitter is located on the ground within the x,y plane in relation to the rotor blades. The transmitter is configured with a center frequency and is assumed to produce a tone at that frequency. Therefor, the signal produced has no inherent modulation applied to it. Being that the transmitter is emitting radio waves into a 3D space, it is assumed to be transmitting in an omnidirectional fashion. The rotor and the receiver are the only two other objects within the scene, radio waves will only be propagated in their direction. This limitation allows for a higher concentration of rays to be casted, resulting in a higher resolution picture that eliminates computational overhead for the tracing engine. Figure 3.3 shows the rays, in blue, casted only in the vicinity of the rotor blade and receiver.

3.3.3 Receiver

The receiver object is modeled as a point in 3D space with a surrounding boundary layer in the shape of a sphere. This is because the receiver is assumed to have an omnidirectional antenna which will receive radio waves from all directions uniformly. The receiver will record any ray that hits the boundary layer within each frame of the simulation to create a sample of data at that instance in time. The sample is produced using superposition of all the rays that are acting on the receiver at that instance, which are then extrapolated to produce a clear result. The receiver is configurable which allows the user to set a desired center frequency along with the sampling rate of the simulated hardware. The sampling rate will determine several simulation parameters in the ray tracer due to the need to associate this rate with the change in the rotor position for the next frame. The consequence of this is that increasing the sample rate will produce higher resolution results but, will increase the computational overhead of the simulation.

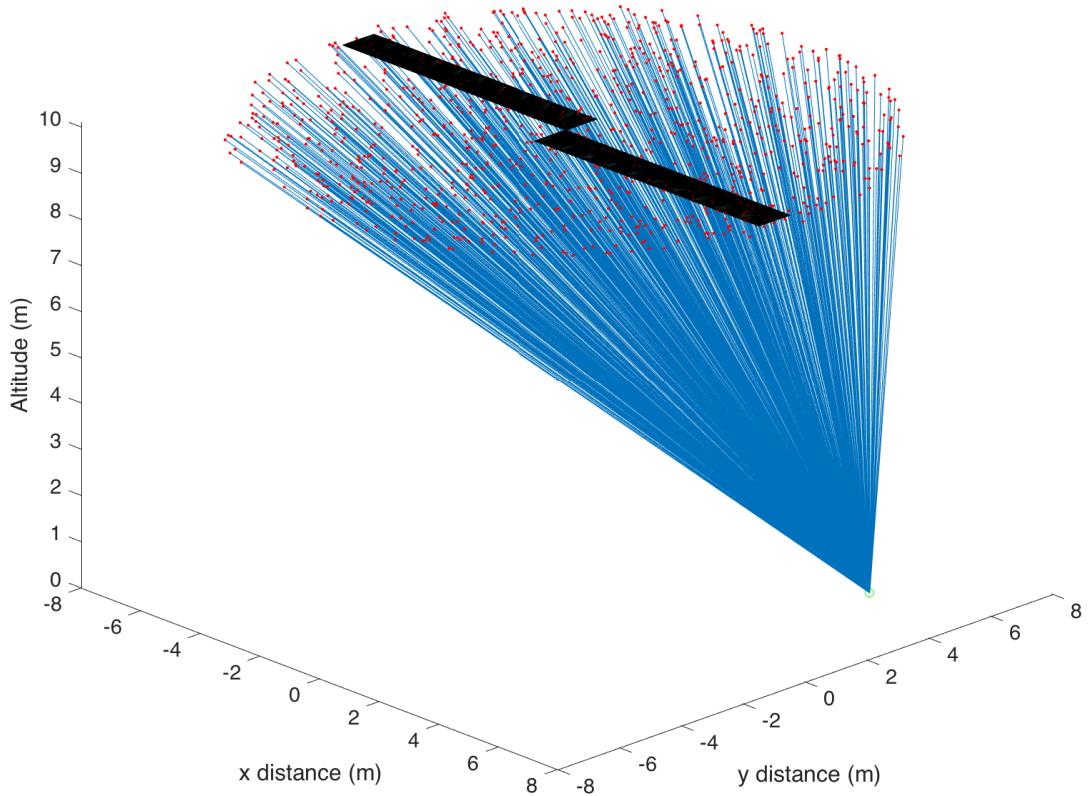


FIGURE 3.3: Transmitter Rays

3.4 Ray Tracing

The ray tracing simulation is conducted in the Monte Carlo fashion acting on the scene and propagation models. This method of raytracing is established for creating realistic images in [12], [13]. The simulation is performed over successive iterations. Each iteration is a discrete element called a frame and each frame will be updated to represent the change in the position of the rotor blade.

ADD MORE ABOUT RAY TRACING

3.4.1 Computation

The ray tracing engine first sets up the environment, creating the surfaces and placing the objects in the scene, then the number of frames that will be computed. The number of frames is determined by the number of rotations that the rotor makes within the simulation, the speed of the rotor in RPM and the sampling frequency of the receiver defined before the beginning of the simulation. This is described by

$$Frames = \frac{60f_s}{RPM} Rev \quad (3.10)$$

where $Frames$ is the number of frames that will be computed in the simulation, f_s is the sampling frequency of the receiver, RPM is the revolutions per minuet of the rotor, and Rev is the number of revolutions that the rotor makes in the simulation.

In each frame a set number of rays are casted into the scene in a uniformly distributed circle in the direction of the rotor and receiver using

$$v_{ray} = \begin{bmatrix} x \\ y \\ z \end{bmatrix} = \begin{pmatrix} \sqrt{r_u} \cos \theta_u + d_x \\ \sqrt{r_u} \sin \theta_u + d_y \\ d_z \end{pmatrix} \quad (3.11)$$

where r_u and θ_u are uniformly distributed random variables from $0 \leq r_u \leq BladeLength^2$ and $0 \leq \theta_u \leq 2\pi$ respectively.

The casting technique reduces the computation overhead by limiting the search space. It also creates a higher resolution result by focusing the limited number of rays in the direction of the other objects shown in Figure 3.4.

When a ray is casted into the scene it has an origin point, a direction vector, a frequency, and an initial power level. The ray then travels through the scene till it encounters another object. If there is a collision with the receiver it is recorded. If the ray collides with a rotor blade a new ray is calculated based on the normal of the geometric surface. The new ray's power is then updated as well as an updated frequency since the blade is

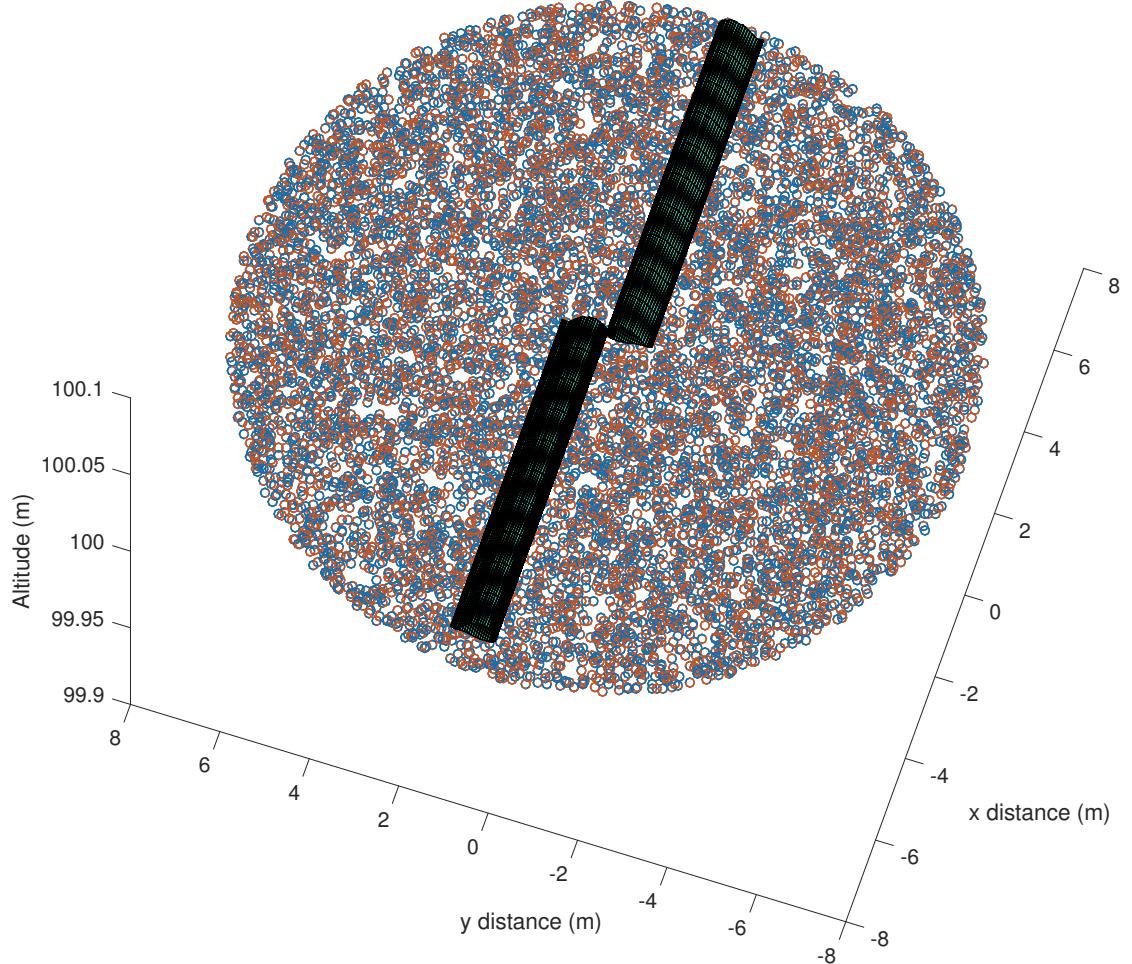


FIGURE 3.4: Disk Sampling Method

moving. The power level is adjusted based on the BRDF of the specific material. Due to only the rotor and receiver being in the scene, rays that are found to hit the rotor are reflected accordingly. Then a dedicated ray, in the direction of the receiver, is also calculated with a decayed power and adjusted frequency respective to the reflection.

3.4.2 Output

The superposition of these receiver contributions during each frame creates the received signal data. The received signal data will then be visualized in spectrograms over the length of the simulated time. The simulation does not render in real time but instead

creates a Comma Separated Value (CSV) file of In-phase and Quadrature (IQ) data that can then be loaded into MATLAB for signal processing.

Chapter 4

Received Signal Simulations

4.1 Introduction

The following simulations performed will define the search space on the effect of rotor blade modulation. Since the software developed allows for full parameterization of the objects within the scene, the simulations will focus on a few that effect the different object's positions in 3D space and the resulting received signal. The parameters that will be changed are the position of the receiver, pitch of the rotor blade, and transmitter position. The effect of each parameter will be analyzed to determine what information can be derived for localization.

4.2 Analysis Techniques

The data from the CSV files generated by the raytracing program are loaded into MATLAB scripts to process the data. The processing technique used is the spectrogram function that computes the short time Fourier transform. This allows for computations to be done in the time frequency domain and provides an accurate picture of how the signal is changing with time. Figure 4.1 shows an example of the computed spectrograms.

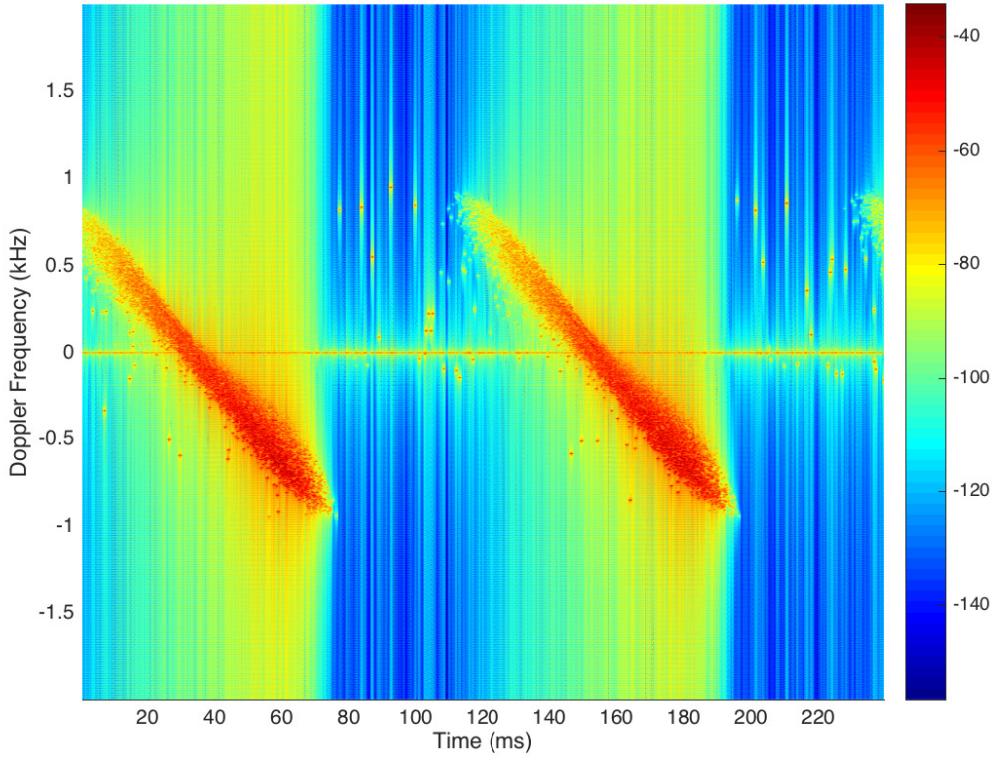


FIGURE 4.1: Example Spectrum for one Blade revolution with transmitter at Azimuth of 45° and Elevation of 35°

After the computation of the short time Fourier transform; the Doppler envelope is calculated by performing a threshold on the power, in both the positive and negative Doppler, at each time slice. The envelope value for that time slice is found by approaching zero frequency and stopping as the power reaches a predetermined level from both the negative and positive values. The power level to set the threshold is calculated differently based on whether the elevation or the azimuth parameter is being swept. For the azimuth angle sweep, which will be shown later in section 4.5, the maximum power is found in each time slice then those values are averaged. Then for each successive angle the same average is taken and averaged with all the others.

This technique is used because the elevation angle is remaining constant, so the distance with the helicopter platform should be constant as well. When varying the elevation angle in section 4.6, the same method cannot be used because the distance is changing so

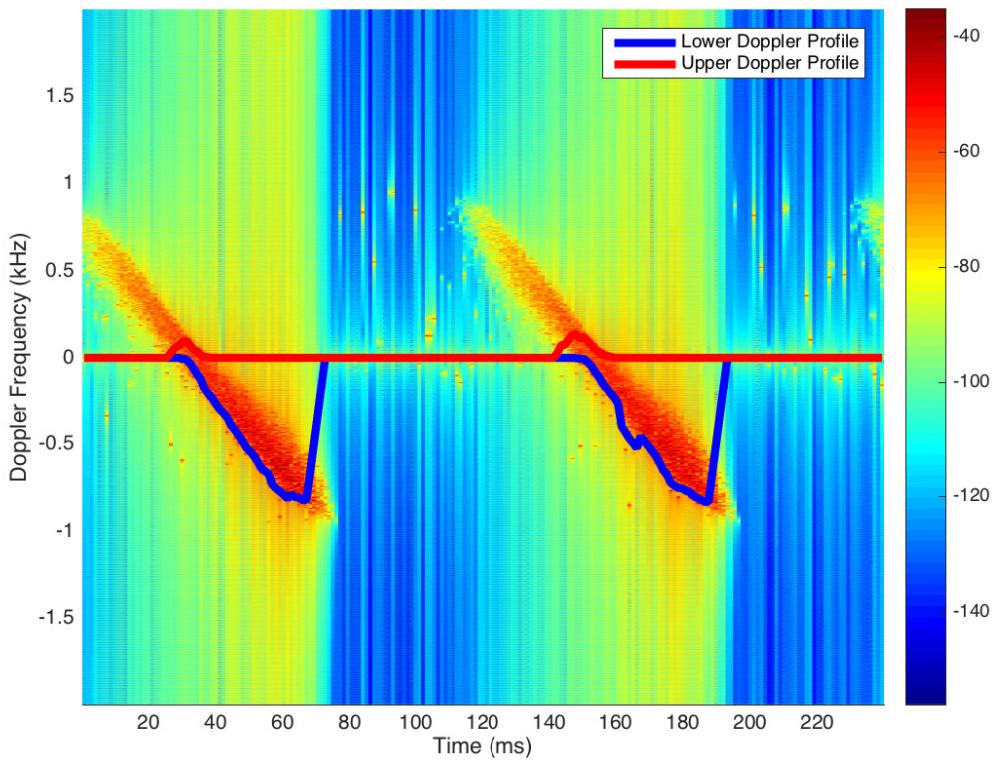


FIGURE 4.2: Example Spectrum with Doppler Profile for one Blade revolution with transmitter at Azimuth of 45° and Elevation of 35°

only the maximum power is found in each time slice. Then all those values are averaged without any successive averaging.

The Doppler envelopes are displayed in Figure 4.2, the lower in blue and the upper in red. The minimum is calculated from the lower envelope, and the maximum from the upper envelope. Those values are then used to characterize that Doppler profile and analyze signal trends as different variables change.

4.3 Receiver Position

The position of the receiver is determined ultimately by its location on the physical aircraft. The position can be anywhere along the length of the body of the helicopter,

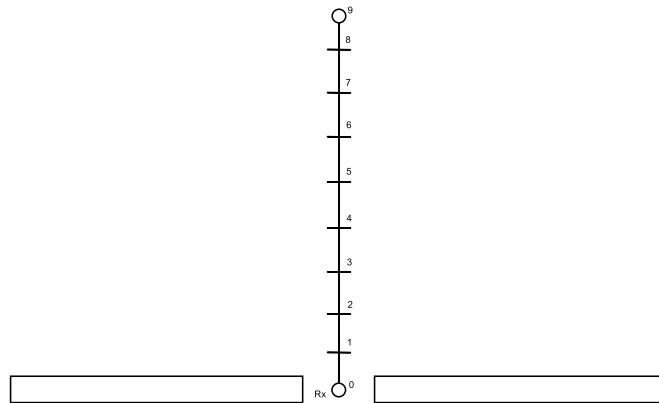


FIGURE 4.3: Position of the Receiver in Relation to the Rotor Blades

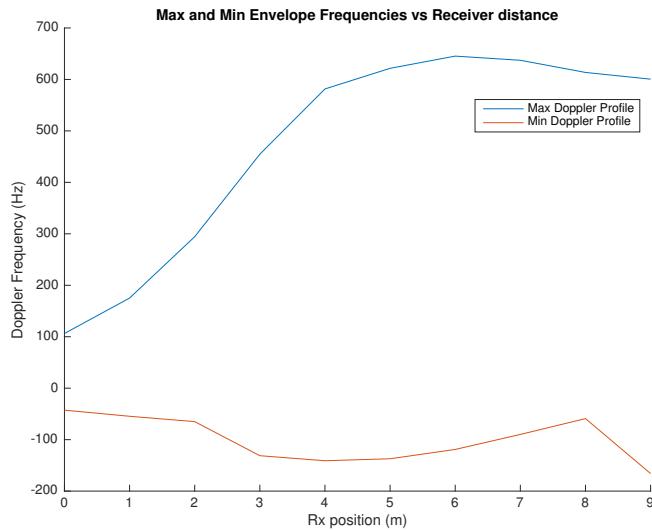


FIGURE 4.4: Max and Min Doppler vs. Receiver Position with Tx Azimuth at 135° and Elevation at 54°

but for the purpose of the simulation the receiver position will be varied from directly underneath the rotor to just past the tip.

The rotor blade length from Figure 4.3 is 7.5 m so the receiver will be varied from 0 m to 9 m in 1 m increments. The resulting signal is analyzed by calculating its Doppler envelope. Then the maximum and minimum of that envelope will then be used to determine the overall effect of the position of the receiver.

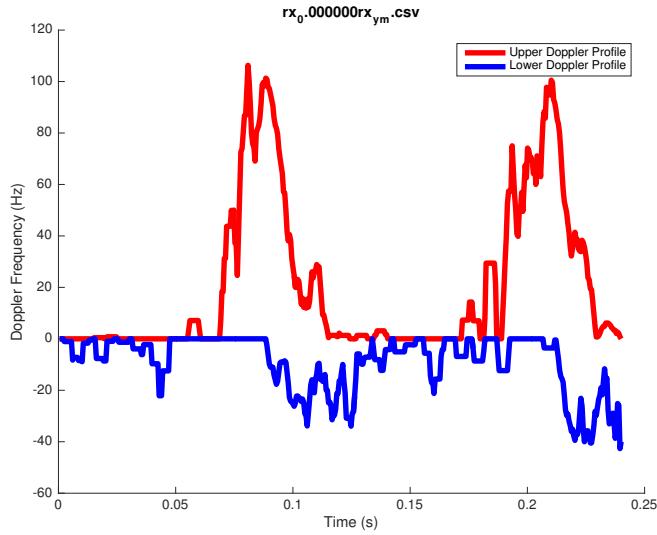


FIGURE 4.5: Doppler Envelope with receiver at 0m

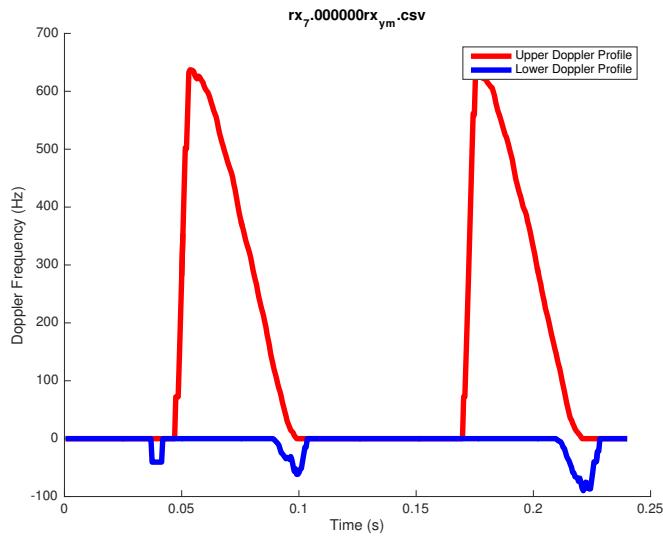


FIGURE 4.6: Doppler Envelope with receiver at 7m

Figure 4.4 shows maximum Doppler versus the position of the receiver. From this graph, the maximum Doppler frequency changes significantly as the receiver is moved from directly underneath the rotor to past the tip of the rotor at 9 m. The position of the receiver also effects the resulting signal envelope shapes shown in Figures 4.5 and 4.6.

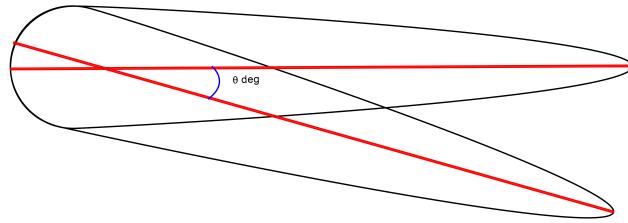


FIGURE 4.7: Rotor Pitch

Comparing the received signal envelopes Figure 4.5 and 4.6 the maximum Doppler increase reflects the information in Figure 4.4. The envelope in Figure 4.5 is also much noisier than the envelope of Figure 4.6 and the signal envelope, for the receiver is at 7 m, has a distinctive shape with less variation between its two peaks. The position of the receiver will also determine whether the azimuth angle can be derived from the resulting signal shown later in section 4.5. Therefore, the receiver will be offset from the center of rotation by 7 m for the subsequent simulations.

4.4 Rotor Pitch

The pitch of the rotor blades determines the amount of lift the rotors create. The pitch range is determined by the shape of the airfoil and the angle at which it will stall and no longer produce lift. For the purpose of the simulations, and the selected airfoil, the pitch range will be from 0° to 15° .

The resulting signal is analyzed by calculating its Doppler envelope. Then the maximum and minimum of that envelope will then be used to determine the overall effect of pitching the rotor blade.

From Figure 4.8 the effect of pitch on the maximum Doppler frequency is a linear increase between a pitch from 0° to 15° . Due to the linear increase, the pitch of the rotor blade can be accounted for when making measurements on subsequent simulation analysis. One issue does arise in when the transmitter is located underneath the helicopter which is shown in Figure 4.9.

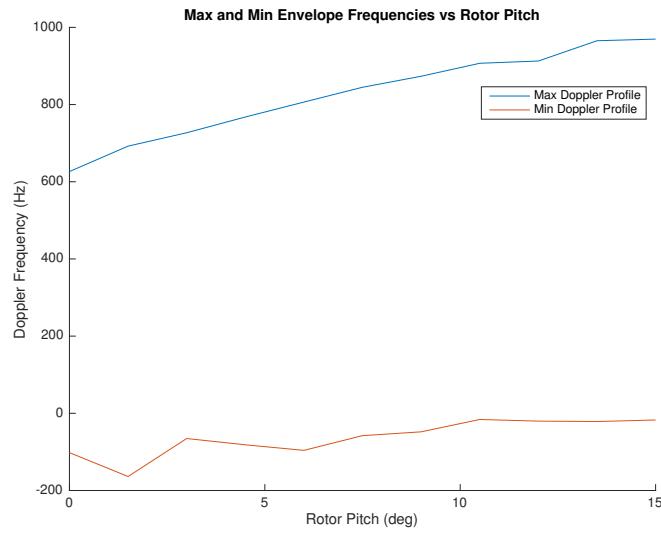


FIGURE 4.8: Max and Min Envelope Frequencies vs Rotor Pitch with Tx Azimuth at 135° and Elevation at 54°

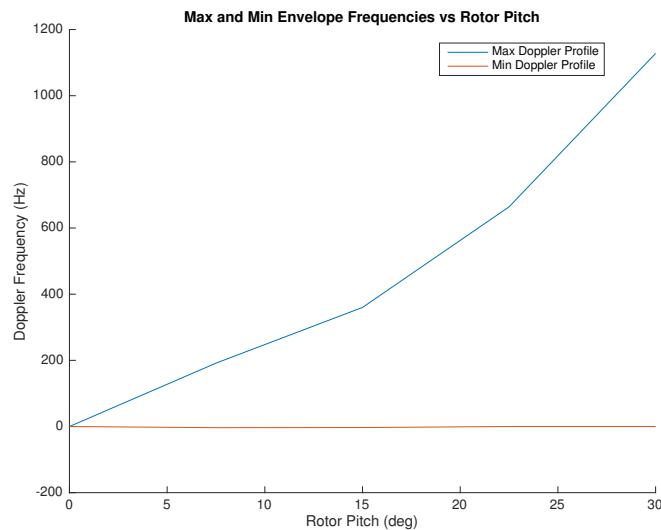


FIGURE 4.9: Max and Min Envelope Frequencies vs Rotor Pitch Transmitter Underneath the Helicopter

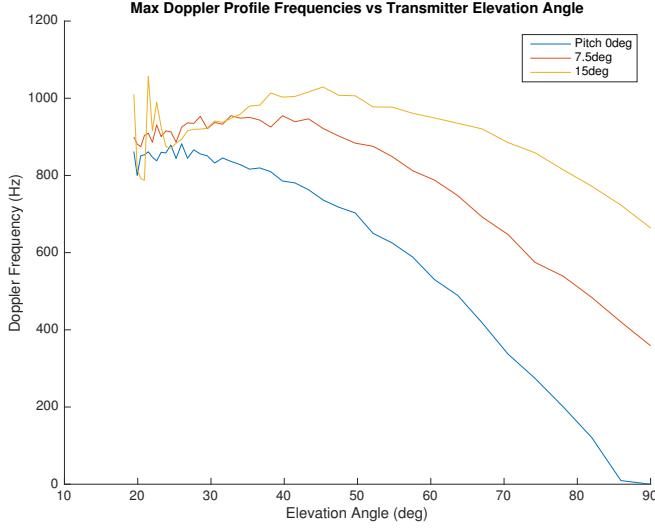


FIGURE 4.10: Max Envelope Frequencies vs Transmitter Elevation Angle

The pitch increases linearly at first then climbs at a much faster rate. This offset is caused by the pitch of the blade reflecting rays into the receiver which would be reflected back at the ground if the pitch was 0° . If the assumption is that the helicopter is hovering when these measurements take place, the pitch of the rotor will be much less than the maximum pitch available. This assumption will adjust the maximum pitch to 15° which will allow for the linear assumption to be fulfilled even when the transmitter is directly underneath the helicopter.

In Figure 4.10 the maximum Doppler versus elevation angles are initially shifted up in frequency from a pitch of 0° and, consequently, have changed in slope. This is because the rays hitting the blades from below are reflecting into the receiver at an angle that is closer to the direction of blade travel. The interesting thing about this plot is that the pitch envelopes actually become closer to the 0° envelope as the elevation angle becomes smaller. Figure 4.11 shows the difference plotted over elevation angle.

From Figure 4.11 we can see that the difference in frequency changes linearly as the elevation angle decreases, the slope of which is based on the pitch angle. This slope would have to be characterized on the physical craft and can be accounted for due to its predictable nature.

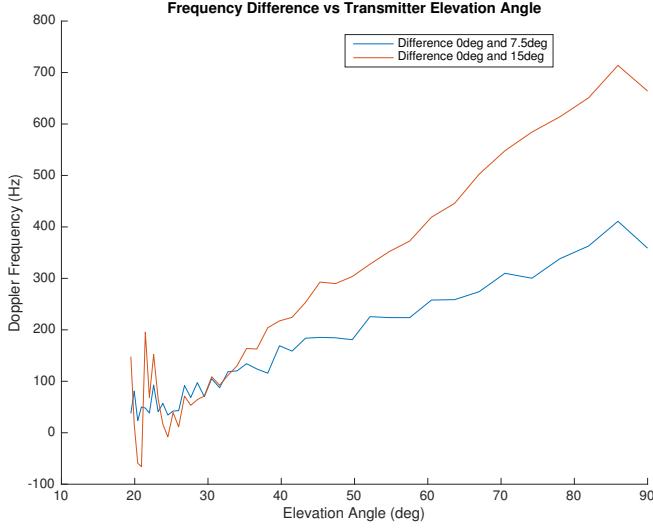


FIGURE 4.11: Frequency Difference vs Transmitter Elevation Angle

4.5 Transmitter Azimuth Angle

The transmitter azimuth angle corresponds to the cardinal direction of the transmitter with respect to the front of the helicopter.

Where θ_{Az} is the azimuth angle. The azimuth angle of the transmitter in the simulation will effect the amount of Doppler added to the signal. This is due to the direction of the rotor blade rotation as it approaches both the receiver and the transmitter and how the rays reflect off the blade as it moves. From the model we see the amount of Doppler form a sinusoidal pattern as the azimuth angle goes from 0° to 360° . This is mirrored in the simulation shown in Figure 4.13.

The graph in Figure 4.13 shows both the maximum and the minimum measured Doppler as the azimuth angle completes a full rotation. The Doppler frequency follows the azimuth angle in a sinusoidal fashion. The sinusoidal pattern is held as the elevation angle changes shown in Figures 4.14 and 4.15.

The sinusoidal pattern of minimum and maximum Doppler frequencies are only present when the receiver is located away from the axis of rotation. This is shown in Figure

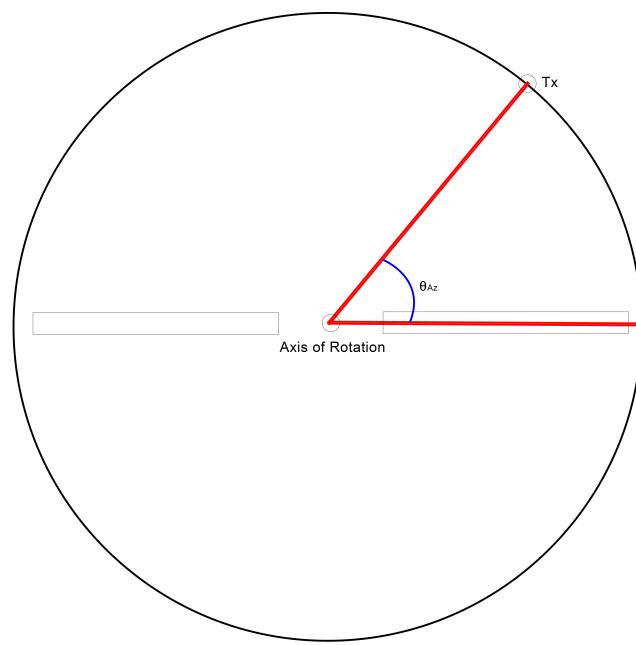


FIGURE 4.12: Transmitter Azimuth Angle Relationship

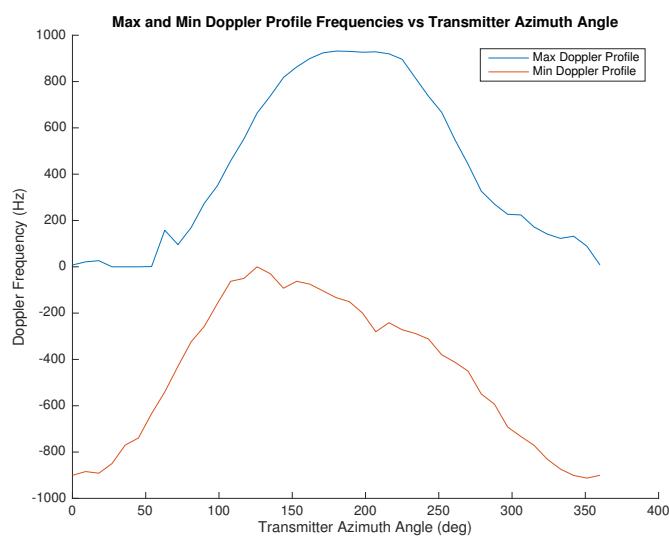


FIGURE 4.13: Max and Min Doppler Profile Frequencies vs Transmitter Azimuth Angle with Tx Elevation at 45°

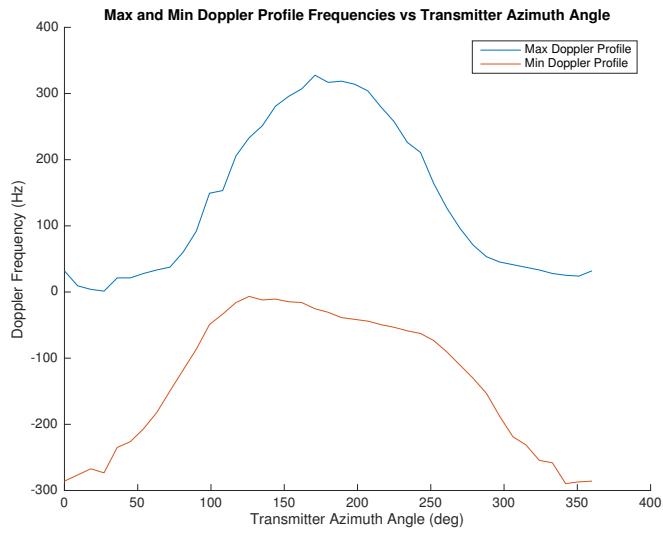


FIGURE 4.14: Max and Min Doppler Profile Frequencies vs Transmitter Azimuth Angle with Tx Elevation at 76°

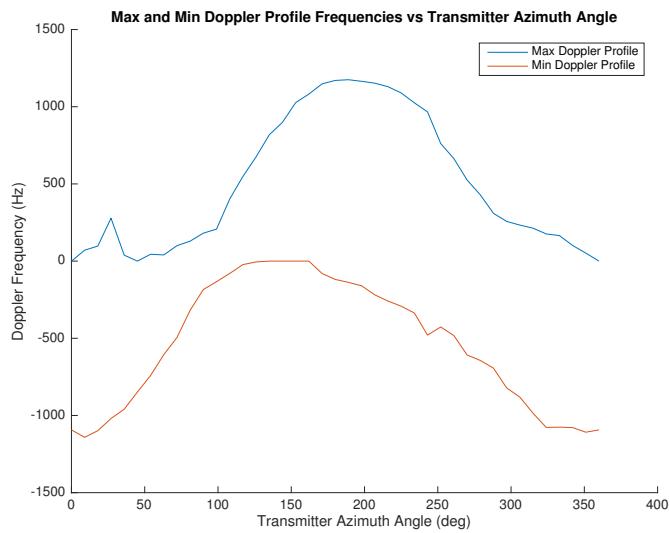


FIGURE 4.15: Max and Min Doppler Profile Frequencies vs Transmitter Azimuth Angle with Tx Elevation at 26.5°

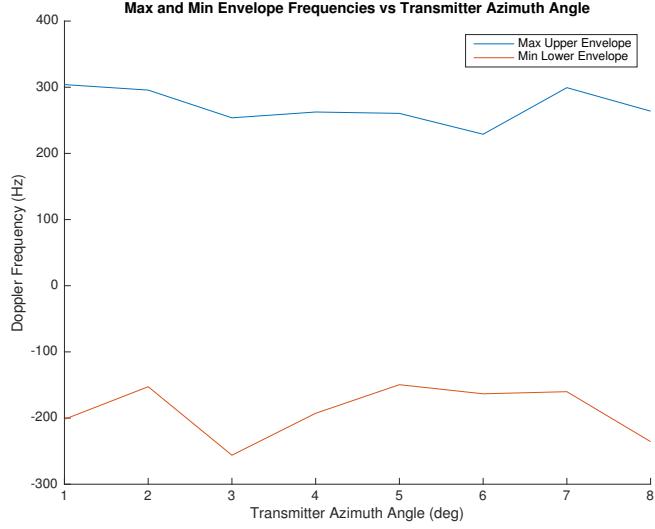


FIGURE 4.16: Max and Min Envelope Frequencies vs Transmitter Azimuth Angle with Rx at Axis of Rotation

4.16 which is devoid of any sinusoidal pattern and remains constant as the transmitter azimuth angle is changed.

Therefore all future simulations will set the receiver near the tip of the rotor which would simulate the receiver being in the nose of the helicopter.

Pitching the blade modifies the results of the azimuth sweep when compared to Figure 4.13. The resulting minimum and maximum envelope frequencies versus azimuth angle for pitch are shown in Figure 4.17. This occurs because the pitch of the blade angles RF reflections differently according to transmitter azimuth. When the transmitter is located between 90° and 270° pitch causes an increase in Doppler but elsewhere it decreases the amount of Doppler shift. The decrease is caused by the blade surface top reflecting receding Doppler away from the receiver at those angles.

The effect of the azimuth angle on the maximum measured Doppler is characterized in section 5.2

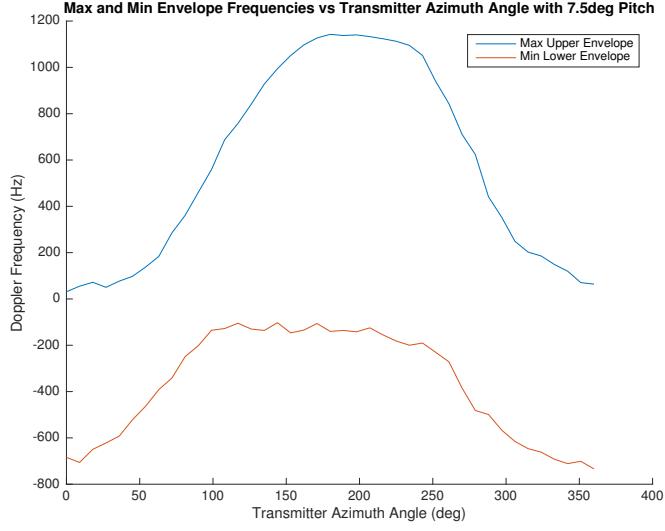


FIGURE 4.17: Max and Min Envelope Frequencies vs Transmitter Elevation Angle with 7.5deg Pitch

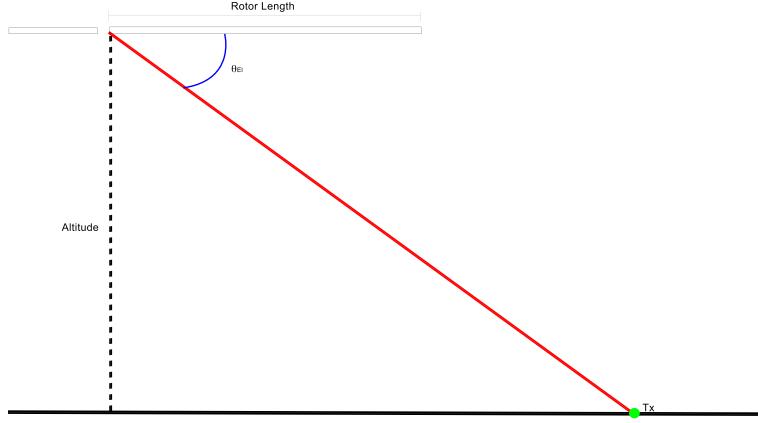


FIGURE 4.18: Transmitter Elevation Angle

4.6 Transmitter Elevation Angle

The transmitter elevation angle is the angle between the helicopter rotor and the position of the transmitter shown in Figure 4.18 where θ_{El} is the elevation angle.

The smaller elevation angles mean that the transmitter is farther away from the helicopter. The elevation angle in relation to the distance of the transmitter is shown by

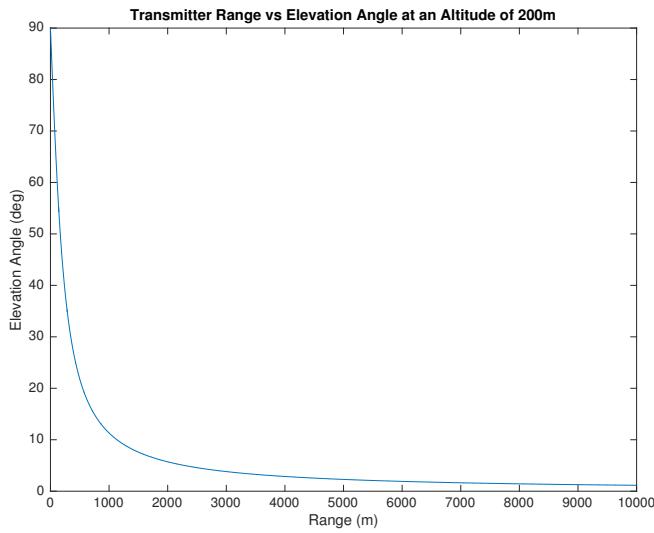


FIGURE 4.19: Transmitter Range vs Elevation Angle at an Altitude of 200m

Figure 4.19.

The elevation angle of the transmitter in the simulation will effect the amount of Doppler added to the signal. This is due to the rays having a vector component in the direction of the travel of the rotor. When the transmitter is directly underneath the rotor and receiver, there is no vector component in the direction of rotor travel so the reflected signal is not Doppler shifted. From the model we see the amount of Doppler increase as the elevation angle decreases. This is mirrored in the simulation shown in Figure 4.20 where the maximum measured Doppler as the elevation angle increases.

Looking back at the geometric models for transmitter azimuth angles of 0° 2.10, 90° 2.4, 180° 2.8, and 270° 2.6 and their simulated counterparts shown in Figure 4.21. We see that the ray traced results match their projections on the maximum and minimum envelope Doppler as transmitter elevation angle changes. The Doppler values do not match exactly but the trends are very similar.

The effect of elevation angle on the maximum measured Doppler will be characterized in section 5.3.

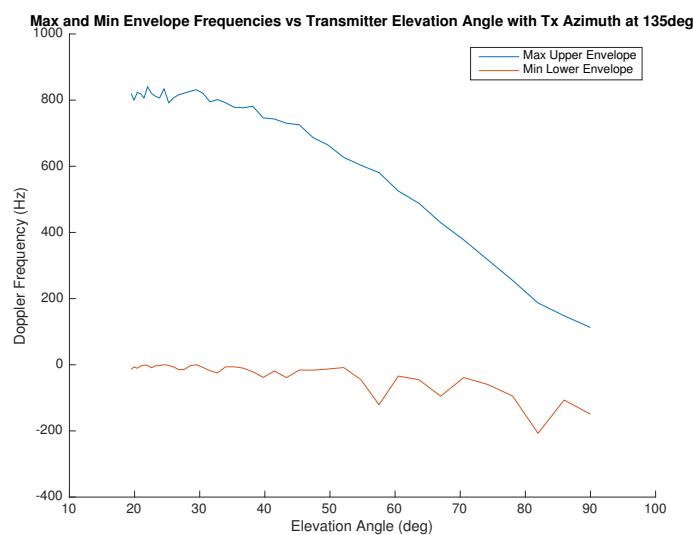


FIGURE 4.20: Max and Min Envelope Frequencies vs Transmitter Elevation Angle with Tx Azimuth of 135deg

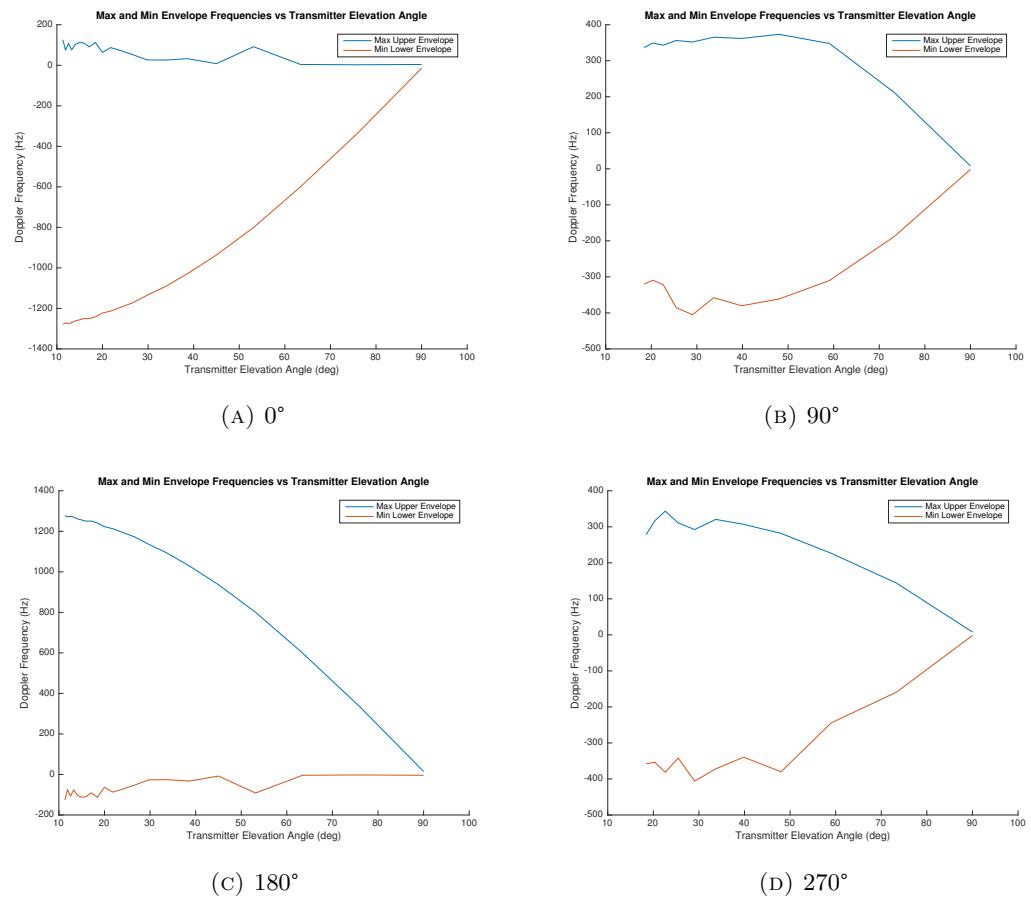


FIGURE 4.21: Doppler Profile vs. Transmitter Elevation angle for various Azimuth angles.

Chapter 5

Results

5.1 Introduction

The information gathered from the previous section is used to estimate the azimuth and elevation angles of the transmitter. First the azimuth angle will be estimated which will provide the information necessary for also calculating the elevation angle. The results of the estimation techniques are then analyzed to determine their accuracy.

5.2 Transmitter Azimuth Angle Estimation

The azimuth angle estimation technique is based on the data collected by rotating the helicopter platform in a clockwise manner, during which a Doppler envelope and subsequent maximum and minimum values are calculated. After a complete rotation the Doppler maximum and minimum values produce a sinusoidal pattern as shown in Figure 4.13 without knowing the starting azimuth angle. With this data we find an unambiguous angle that will set the coordinate space and provide an estimate of current azimuth angle. To do this the absolute value of the minimum envelope data is superimposed onto the maximum envelope data as shown in Figure 5.1.

From Figure 5.1 there are two points at which the maximums and the absolute value of the minimums cross. We then take the difference

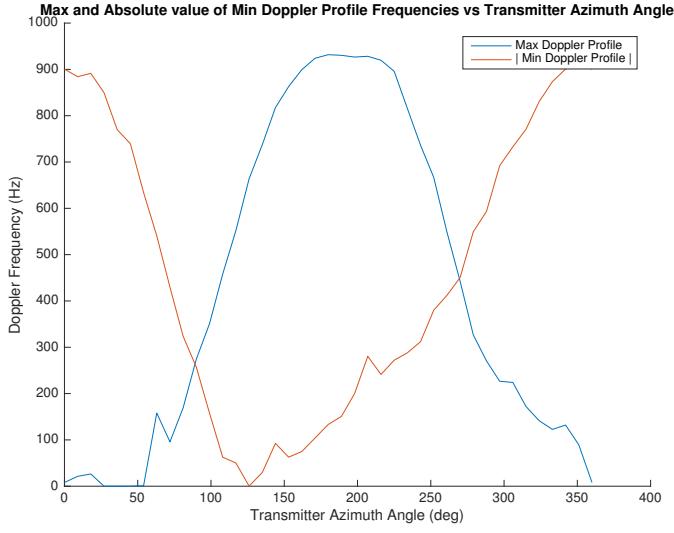


FIGURE 5.1: Max and Absolute value of Min Envelope Frequencies vs Transmitter Azimuth Angle at an Elevation Angle of 45°

$$\text{EnvelopeDifference} = \text{MaxUpperEnvelope} - |\text{MinLowerEnvelope}| \quad (5.1)$$

where *MaxUpperEnvelope* is an array of the maximum value of each upper envelope calculation, and *MinLowerEnvelope* is an array of the minimum value of each lower envelope calculation. The result is an almost exact sinusoid centered around zero, shown in Figure 5.2.

While Figure 5.2 provides information about the angle of the transmitter it does not contain enough to locate an unambiguous azimuth angle in itself. Therefore by finding the correct Doppler for each azimuth, from the *MaxUpperEnvelope* and the $|\text{MinLowerEnvelope}|$, we can determine an unambiguous reference. This is done by evaluating the difference at each angle, and if the difference is negative the $|\text{MinLowerEnvelope}|$ is used and if positive the *MaxUpperEnvelope*.

```

1 %corrected Doppler frequency for processing
2 for i = 1:length(upper)
3     if(difference(i) < 0)
4         correct_fd(i) = abs(lower(i));

```

```
5      else
6          correct_fd(i) = upper(i);
7      end
8 end
```

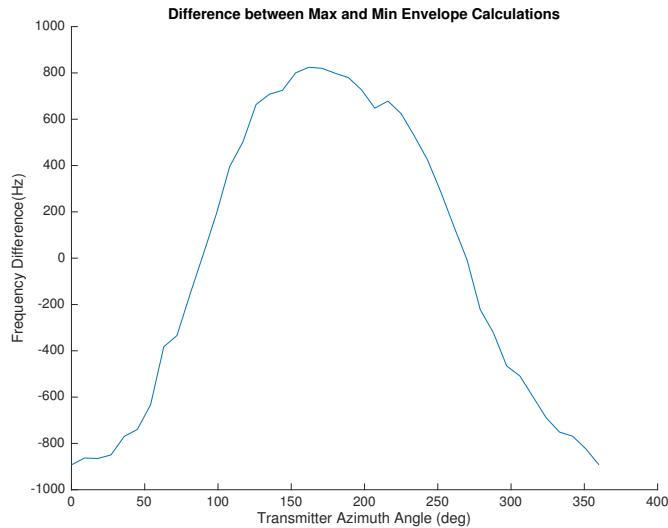


FIGURE 5.2: Difference between Max and Min Envelope Calculations vs Transmitter Azimuth Angle at an Elevation Angle of 45°

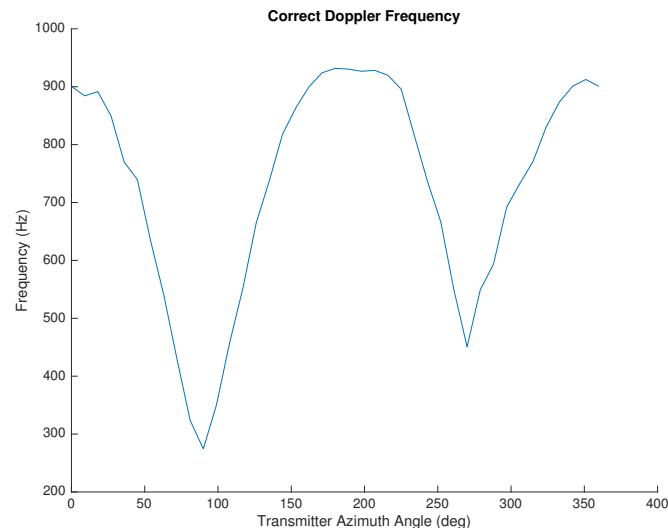


FIGURE 5.3: Correct Doppler Frequencies vs Transmitter Azimuth Angle at an Elevation Angle of 45°

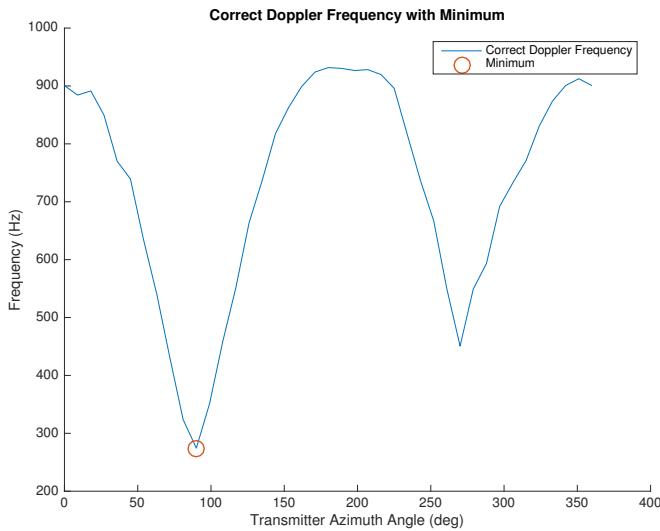


FIGURE 5.4: Correct Doppler Frequencies with Minimum vs Transmitter Azimuth Angle at an Elevation Angle of 45°

The correct Doppler is shown in Figure 5.3 which displays the amount of Doppler that is currently acting on the signal for that specific azimuth angle. The data gathered contains a global minimum at 90° and a second local minimum at 270° . The 90° can be found easily by taking the minimum of the correct Doppler signal.

```

1 %Minimum of corrected Doppler
2 [Min, I_min] = min(correct_fd);
```

In order to find the local minimum at 270° we need to use a different method. We can do this through the peak detection function within MATLAB to locate both the 90° and 270° point. By taking the inverse of the correct Doppler and tuning the peak detection function with the maximum and minimum values to determine accurate prominence.

```

1 %peak detection with prominence calculation
2 min_peak_prominence = (1/(Max - Min))*5;
3 [pk,lc] = findpeaks(1./correct_fd, 'NPeaks', 2, 'MinPeakProminence', ...
    min_peak_prominence);
```

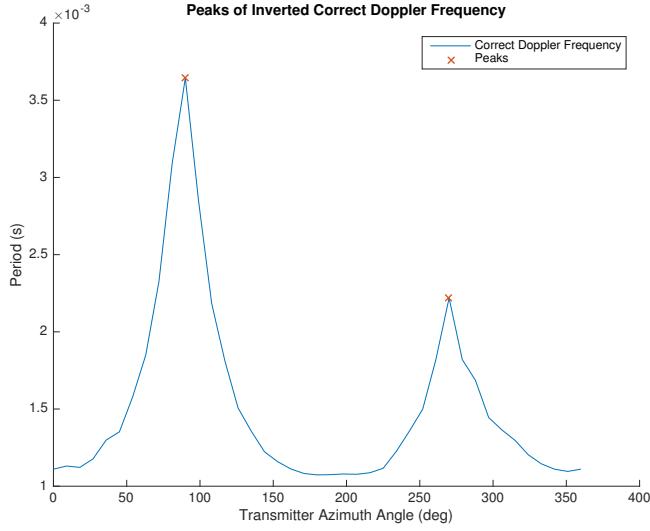


FIGURE 5.5: Peaks of inverted Correct Doppler vs Transmitter Azimuth Angle at an Elevation Angle of 45°

From Figure 5.5 we see the two peaks denoted by the red x's, one at 90° and the other at 270°. Now we have a minimum value that should denote the 90° location and the two peak locations that denote the 90° and 270° locations. Since it is possible that the minimum could find the wrong peak for the 90° location we can compare the peak locations on the average power data, that was used to find the successive average during data collection, to determine which location is actually 90°.

Figure 5.6 shows the average power at each angle sample with the angles 90° and 270° denoted as red x's. From the plot we can see that the average power at 90° is much smaller than at 270°, so this inequality will be used to resolve ambiguity in the azimuth angle.

From there the minimum method and the peak method can be compared to see if they agree on the 90° location. If this is not the case one will be chosen and the helicopter can fly in that direction. The resulting Doppler can then be measured, based on the physical movement of the helicopter or if the resulting envelope, to confirm the correct 90° location.

From Table 5.1 we can see that there is no error in the estimation of the 90° point over

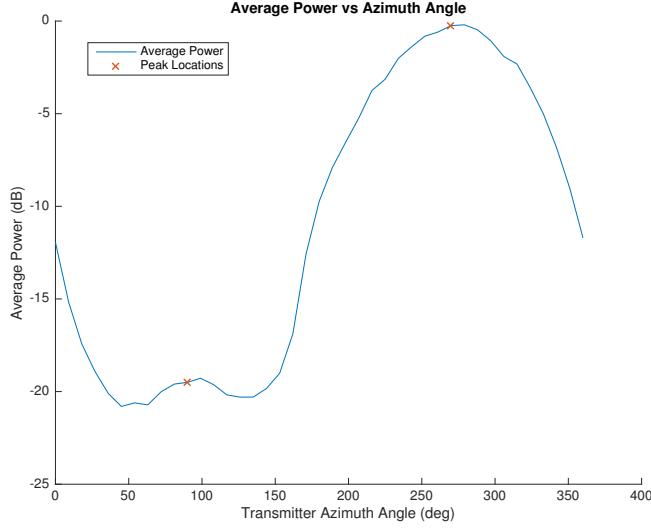


FIGURE 5.6: Average Power vs Transmitter Azimuth Angle at an Elevation Angle of 45°

Altitude	Elevation Angle	Azimuth Error in (deg)	Percent Error
200	76°	0	0
200	45°	0	0
200	26.5°	0	0
500	78.7°	0	0
500	51.34°	0	0
500	35.5°	0	0

TABLE 5.1: Azimuth Error and Azimuth Percent Error of Different Elevation Angles During Azimuth Estimation

a variety of altitude and elevation angles that were tested. But because the algorithm could potentially pick the 270° we will analyze the difference in peak heights and the power difference to evaluate the estimation further.

From Table 5.2 we can see that at the larger elevation angles the peak percent difference are significant to determine which is correctly the 90° value. Although from the frequency difference, at the large elevation angles, it is possible to confuse the estimation by just taking the minimum frequency. Therefore other values need to play a role such as the received power.

Altitude	Elevation Angle	Percent Peak Difference	Power Difference in dB	Peak Frequency Difference Hz
200	76°	-16.8675%	-14.0914	18.67
200	45°	-39.1124%	-19.7476	176.267
200	26.5°	-69.7368%	-13.3443	424.0
500	78.7°	-21.6667%	-11.4508	17.33
500	51.34°	-38.1875%	-22.4610	162.93
500	35.5°	-53.4303%	-18.6043	313.6

TABLE 5.2: Percent Peak, Power, and Frequency Difference of Different Elevation Angles During Azimuth Estimation

5.3 Transmitter Elevation Angle Estimation

Using the information gathered from the azimuth estimation procedure, we can compute the elevation angle of the transmitter. In the process of gathering azimuth information, the maximum and minimum envelopes follow a sinusoidal pattern that contains a maximum Doppler information at approximately 180° and 0° azimuth angles. Using that maximum value, along with the correct Doppler and the assumption that the maximum will occur near the tip of the rotor blade, we can approximate the respected reflection radii off the blade as the azimuth angle changes. This is done through

$$R_{Estimate} = BladeLength \left(\frac{f_{DopplerCorrect}(\theta_{Az})}{Max(f_{DopplerCorrect})} \right) \quad (5.2)$$

where $R_{Estimate}$ is the estimated reflection radius at a particular azimuth, $BladeLength$ is the length of a single blade or radius of the rotor, and $f_{DopplerCorrect}$ is the correct Doppler frequency for each azimuth angle θ_{Az} .

Figure 5.7 shows the estimated reflection radius for each azimuth angle.

Now we find the maximum amount of Doppler that could be induced at that reflection radius location through

$$f_{Doppler_{REstimateMax}} = 2 \frac{v_r f_c}{c} \quad (5.3)$$

where $f_{Doppler_{REstimateMax}}$ is the maximum amount of Doppler that could happen at that location if the signal was reflected parallel to the direction of motion. f_c is the center

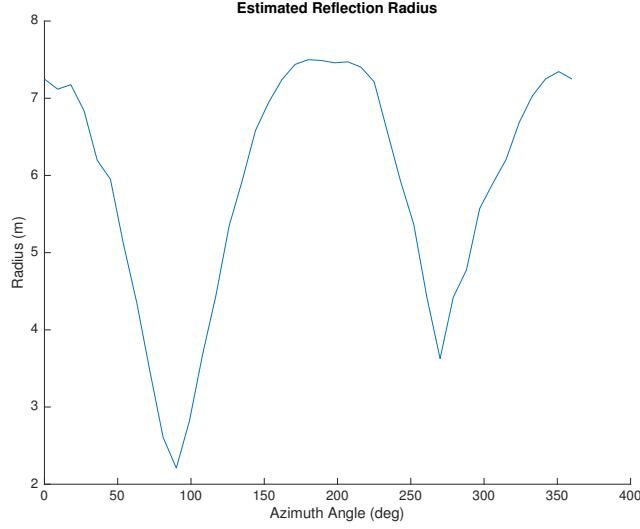


FIGURE 5.7: Estimated Reflection Radius at an Elevation Angle of 45°

frequency of the signal, c is the speed of light and v_r is the radial velocity based of the *RPM* defined by

$$v_r = \frac{2\pi}{60} RPM R_{Estimate} \quad (5.4)$$

Then to find the elevation angle we look back at equation 2.6 swapping *MaxUpperEnvelope* with $f_{DopplerCorrect}(\theta_{Az})$ because this is now over the azimuth range and swap $f_{DopplerMax}$ for $f_{DopplerREstimateMax}$ because we need the maximum doppler for the current reflection estimate. We then solve for the elevation angle

$$\theta_{El} = \arccos \left(\frac{f_{DopplerCorrect}(\theta_{Az})}{f_{DopplerREstimateMax}} \right) \quad (5.5)$$

where θ_{El} is the elevation angle of the transmitter. If the elevation angle is all the information needed equation 5.5 distills down to

$$\theta_{El} = \arccos \left(\frac{\text{Max}(f_{DopplerCorrect})}{f_{DopplerMax}} \right) \quad (5.6)$$

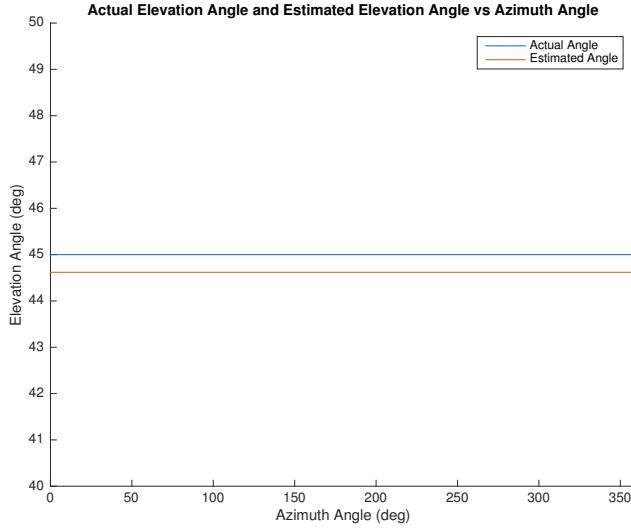


FIGURE 5.8: Actual Elevation Angle and Estimated Elevation Angle vs Azimuth Angle

Altitude	Elevation Angle	Average Elevation Error in (deg)	Average Percent Error
200	76°	-0.4632°	-0.6097%
200	45°	-0.3809°	-0.8464%
200	26.5°	-0.4072°	-1.5329%
500	78.7°	0.0914°	0.1162%
500	51.34°	-0.6236°	-1.2146%
500	35.5°	-0.6803°	-1.9143%

TABLE 5.3: Average Elevation Error and Average Elevation Percent Error of Different Elevation Angles During Azimuth Estimation

where $f_{DopplerMax}$ is defined in equation 5.8.

Figure 5.8 shows the estimation of the elevation angle θ_{El} with respect to the azimuth angle. What it shows is that the elevation angle remains constant with respect to azimuth angle. Which means that the estimation in the reflection radius is correctly compensating for the azimuth angle. The percent error off the actual elevation angle is shown in Figure 5.9 which is very small but consistent over the azimuth range.

From Table 5.3 we can see elevation estimation error is extremely small for the given elevation angles. There is a trend that is evident in the data that as the elevation angle decreases the amount of error is increasing.

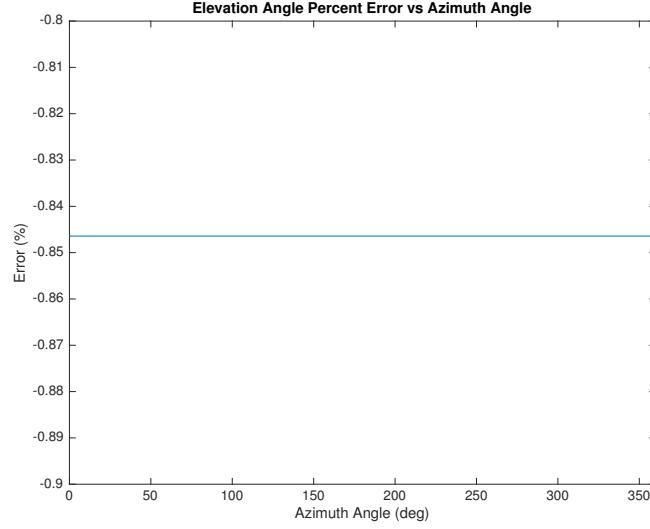


FIGURE 5.9: Elevation Angle Percent Error vsTransmitter Azimuth Angle

The error in elevation is caused by a limitation on the estimation. Where the Doppler shift is limited by the maximum amount Doppler that the blade rotation can produce shown in equation 5.4 by replacing v_r with v_rMax which is calculated by

$$v_{rMax} = \frac{2\pi}{60} RPM BladeLength \quad (5.7)$$

then using that to find the maximum available Doppler through

$$f_{DopplerMax} = 2 \frac{v_{rMax} f_c}{c} \quad (5.8)$$

This limitation is shown by varying the elevation angle at the azimuth angle that provides the maximum Doppler shift, which is 180° . The maximum and minimum envelope data is shown in Figure 5.10

Using the estimation method described above, Figure 5.11 shows the elevation angle estimated versus the actual angle. The estimation method is accurate till elevation angles of 18° or 20° , where it becomes noisy. This is due to the inability of the envelope estimation to resolve the correct maximum Doppler for that range. By going back

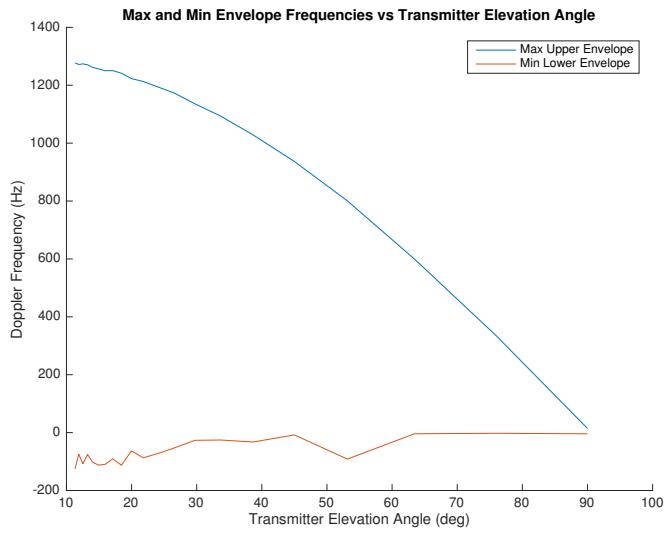


FIGURE 5.10: Max and Min Envelope Frequencies vs Elevation Angle with Transmitter Azimuth Angle of 180°

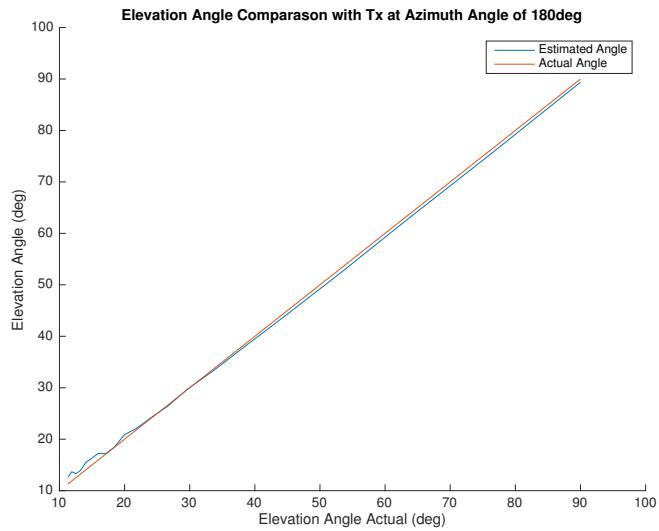


FIGURE 5.11: Elevation Estimate and Actual Angle with Transmitter Azimuth Angle of 180°

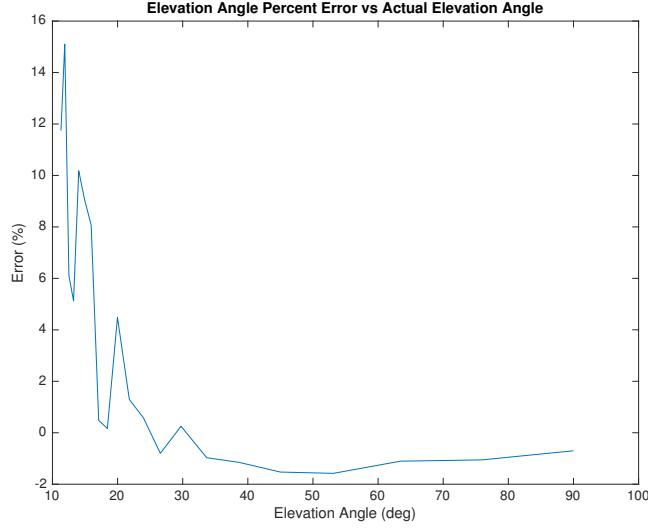


FIGURE 5.12: Elevation Angle Percent Error with Transmitter Azimuth Angle of 180°

to Figure 4.19 we can see that as the transmitter moves farther and farther away the elevation angle is still decreasing but at a much smaller and smaller rate. So the difference between elevation angles closer to zero are more difficult to resolve.

Figure 5.12 shows the percent error with respect to the elevation angle. The estimation starts to become unusable around 18° or 20° where the percent error starts to shoot past acceptable ranges.

If we now consider a pitched blade the above method for estimating azimuth and elevation becomes inaccurate due to the increased Doppler between 90° and 270° and the decreased Doppler on the other side. To correct this error we need to correct both the difference calculation and the correct Doppler data accordingly. The uncorrected data is shown in Figure 5.13 and 5.14 with percent azimuth error of 20% and percent elevation error of 35%.

Comparing the envelope difference of no pitch and pitched blade, in Figures 5.2 and 5.13 respectively, we can see that the difference calculation of the pitch is a shifted up version of the one with no pitch. Therefore we can first correct this by re-centering the pitch difference according to

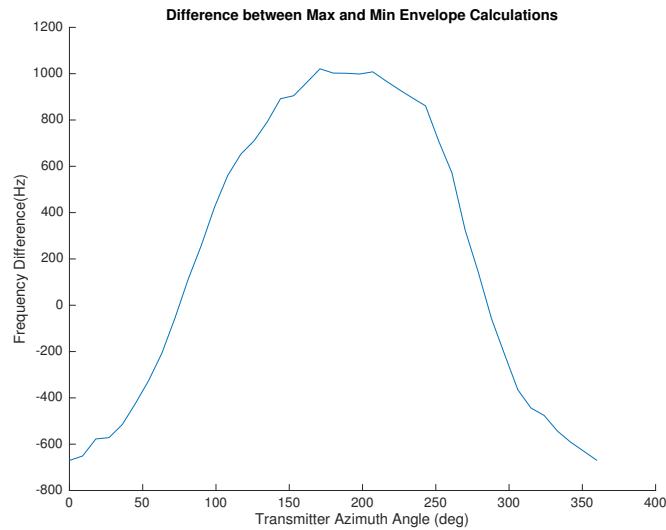


FIGURE 5.13: Uncorrected Envelope Difference vs. Transmitter Azimuth and Elevation angle of 45°with Blade pitch of 7.5°

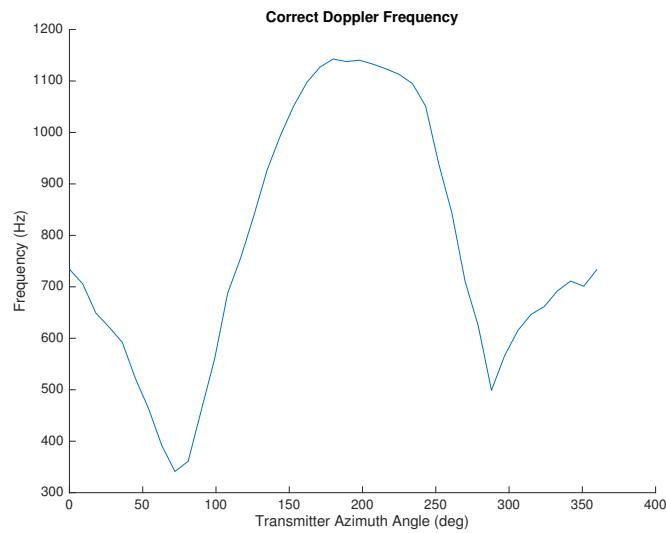


FIGURE 5.14: Uncorrected Doppler vs. Transmitter Azimuth and Elevation angle of 45°with Blade pitch of 7.5°

$$A_{shift} = \frac{Max(MaxUpperEnvelope) - |Min(MinLowerEnvelope)|}{2} \quad (5.9)$$

where A_{shift} is the amount that the difference calculation will be shifted down

$$EnvelopeDifference = EnvelopeDifference - A_{shift} \quad (5.10)$$

Then with this knowledge $f_{DopplerCorrect}$ is recalculated and then is adjusted to the correct frequencies with

$$f_{DopplerCorrect} = f_{DopplerCorrect} + A_{shift}\cos(\theta_{Az}) \quad (5.11)$$

Since θ_{Az} is unknown during the calculation of equation 5.11 the correct starting phase can be determined by matching it to the *EnvelopeDifference* and that the cosine should be one period in length. These corrections result in the percent azimuth error of 0% and 7% elevation angle error. The elevation angle percent error is within a useable range but could be decreased with further tuning to the preliminary pitch adjustment algorithm. When the pitch corrections are applied to a transmitter elevation angle of 26.56° the correction achieves better performance than the unpitched calculation with percent azimuth error of 0% and percent elevation error of 0.114%. This is still a preliminary correction method that requires more in depth analysis but from the initial results shows merit. The increased accuracy as the elevation angle decreases relates back to Figure 4.10 where as the elevation angle decreases the effect of pitch on the signal converges back to the unpitched results.

Chapter 6

Conclusion and Future Work

6.1 Summary

Over the course of this thesis a three dimensional ray tracer application was built in C++ to produce a RBM signal according to a variety of physical parameters. The physical parameters associated with a helicopter blade and the positioning of transmitter and receiver hardware were swept independently to build knowledge on how they affect the resulting signal. That data was then processed using time frequency analysis to produce a Doppler envelope. An envelope of each parameter step was used to determine an overall trend. Then with those trends an algorithm was derived to find the azimuth and elevation angle of the transmitter with relationship to the helicopter platform. The algorithm accurately finds the azimuth angle and elevation using the data collected in the simulation environment with almost no error in the azimuth estimation and less than 2% error in elevation angle when blade pitch in 0°.

6.2 Future Work

The first thing that needs to be done in continuing this research is to perform a real world experiment to officially evaluate the ray tracing application. To do this appropriate hardware needs to be defined in the form of a software defined radio for both the receiver

and transmitter along with a software workflow such as GNU Radio. Next a small scale environment would need to be set up, with some form of rotating metal blade or thin plate rotating at a sufficient rate to produce a Doppler spread similar to those defined in the simulation. After that data is collected and analyzed a full scale experiment would need to be conducted including a real helicopter platform and an environment with large expanses of flat ground.

Once the real world experiments have been conducted, and are shown to be similar to the signal produced by the simulation, the estimation techniques defined in this thesis can be evaluated on the real signal to determine if they are sufficient in practice.

After the physical validation the ray tracing application can be modified to include more physical phenomenon. The other improvement would be to introduce more objects into the scene model which would require modification to the tracing algorithm to include ray casting distributions in their particular direction.

Another improvement on the simulation would be to increase the speed of computation. This could be done by implementing multi-threading or, since raytracing is heavily parallelizable, a Graphics Processing Unit (GPU) based architecture. The multi-threading option would require minor code modifications but realizing the simulation on a GPU would require a full rewrite of the software to take advantage of the GPU's abilities.

The current estimation does not take into account the physical pitch value when correcting for pitch and might not cover all the cases that pitch can effect. Therefore further investigation is needed into how the pitch affects the received signal for improved azimuth and elevation estimation.

The estimation methods described in this thesis rely only on the maximum and minimum values of the Doppler envelopes calculated but their shape could also be of particular interest as well. When varying the parameters of azimuth and elevation the shape of the envelope changes in a distinctive manner, by using a training algorithm the position of the transmitter might be able to be tracked in time by evaluating the change in shape. Under the defined estimation methods a full revolution of the helicopter platform is needed to resolve position ambiguity.

Appendix A

Ray Tracing Software

The ray tracing software developed during the course of the thesis is written in C++ in an XCode environment, but a generic implementation is provided to run on other operating systems. This code is loosely based on the work Eric Degroot developed for [16] and implemented some modified base classes developed by him. It is a specific tool for analyzing the affects of rotor blade modulation on a signal tone, it does not provide generic 3D ray tracing in order to optimize the performance for this task. The software is provided without a GUI implementation and is run on different parameters by modifying the main.c file. This is due to the amount of parameters involved but could be easily extended to provide command line arguments in future iterations.

To use the software for performing RBM simulations there are several key parameters that are needed. First a file containing the points that define the 2D section of the airfoil shape, one default file is included in the software package for ease of use and as a template for other airfoil shapes. The other key parameters that define the simulation are shown in Table A.1

The output file also needs to be defined with a unique name that changes, this is important because the program will just write over the old file if you do not have a unique naming scheme. This could be just an increasing number or related to one of the variable sweeps.

Name	type	Default Value	units	Description
rx_x	double	0	m	receiver position in x
rx_y	double	7	m	receiver position in y
rx_z	double	2	m	receiver position in z below rotor
Bandwidth	double	2000	Hz	Bandwidth of the receiver
rx_fc	double	1000000000	Hz	center frequency of the receiver
tx_x	double	100	m	transmitter position in x
tx_y	double	100	m	transmitter position in y
tx_fc	double	1000000000	Hz	transmitter center frequency
tx_power	double	4000		transmitter power
num_blades	int	2	none	number of blades
RPM	double	250	RPM	Blade revolutions per minuet
altitude	double	200	m	rotor altitude
blade_length	double	7.5	m	length of the one rotor blade
pitch	double	0	radians	pitch of the rotor use $-\theta_p$
num_ribs	double	10	none	number of ribs that makes up one blade
files	double	10	none	number of files to produce

TABLE A.1: Simulation parameters

To run the simulation on a Mac load into XCode the project file and configure the main file to reflect the type of simulation desired, then hit the play button.

On Linux machines the code must first be built using Make with the main file configured before hand. Then run the Raytracer3D executable.

The output file contains more than just the signal data the first few data entries are data pertaining to the simulation parameters. it is important to separate this data from the

1	2	3	4	5	6	7	8	9	10
rx_x	rx_y	rx_z	Bandwidth	rx_fc	tx_x	tx_y	tx_fc	tx_power	num_ribs
11	12	13	14	15	16	17	18		
num _blades	blade _length	pitch	RPM	altitude	tx_radius	elevation _angle	azimuth _angle		

TABLE A.2: Output file header with simulation parameter order

signal data before processing the signal. The template for this data is shown in Table A.2.

This data is all provided in a single string of comma separated values called a .CSV file. MATLAB has a built in function to read CSV data.

```
1 data = csvread('file_path/file_name')
```

After all the data is read into MATLAB the data can be split into two vectors, one pertaining to the physical simulation parameters and the other to the received signal.

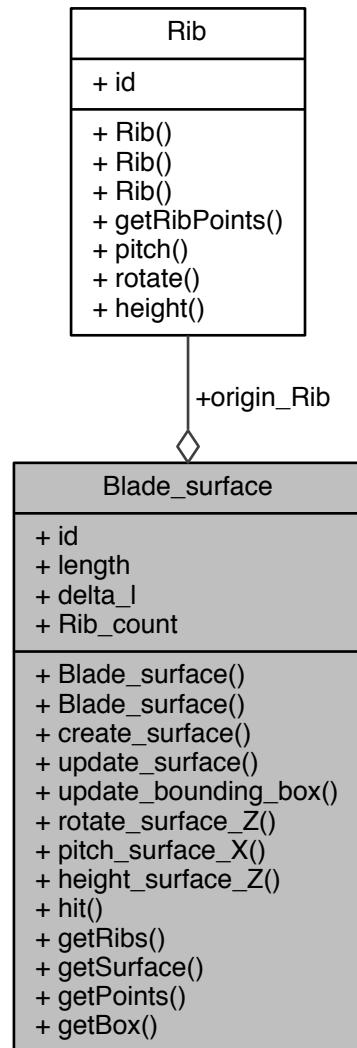
There are several templates for simulation execution in the main.c file that are commented out to help get started, depending on the execution environment the generation of a single file can take anywhere from a few minuets to several days. Under the defaults provided a single file can be generated in approximately 15min.

Appendix B

Class Documentation

B.1 Blade_surface Class Reference

Collaboration diagram for Blade_surface:



Public Member Functions

- **Blade_surface** (const int id, const double length, const int Rib_count, [Rib &origin_Rib](#))
- void **create_surface** ()
- void **update_surface** ()
- void **update_bounding_box** ()
- void **rotate_surface_Z** (double angle)
- void **pitch_surface_X** (const double angle)
- void **height_surface_Z** (const double height)
- bool **hit** (const [Ray3D &ray](#), double &hitDistance, [Vector3D &hitNormal](#), [Point3D &hitPoint](#))
- std::vector< [Rib](#) > **getRibs** ()
- std::vector< [Triangle](#) > **getSurface** ()
- std::vector< [Point3D](#) > **getPoints** ()
- [Bounding_box](#) **getBox** ()

Public Attributes

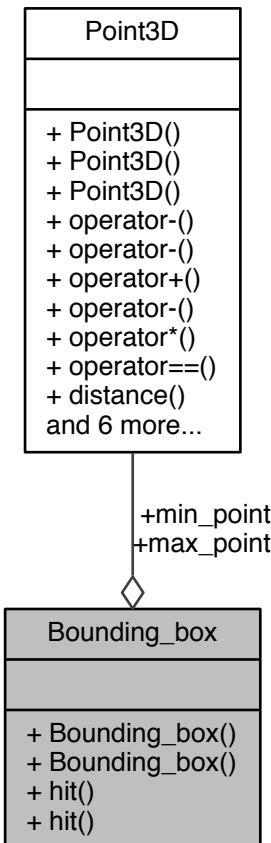
- int **id**
- double **length**
- double **delta_l**
- int **Rib_count**
- [Rib](#) **origin_Rib**

The documentation for this class was generated from the following files:

- Raytracer3D/Raytracer3D/Blade_surface.hpp
- Raytracer3D/Raytracer3D/Blade_surface.cpp

B.2 Bounding_box Class Reference

Collaboration diagram for Bounding_box:



Public Member Functions

- `Bounding_box (std::vector< Point3D > &points)`
- `bool hit (const Ray3D &ray, Point3D &hit_point) const`
- `bool hit (const Ray3D &ray) const`

Public Attributes

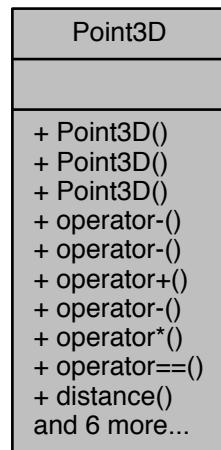
- `Point3D min_point`
- `Point3D max_point`

The documentation for this class was generated from the following files:

- Raytracer3D/Raytracer3D/Bounding_box.hpp
- Raytracer3D/Raytracer3D/Bounding_box.cpp

B.3 Point3D Class Reference

Collaboration diagram for Point3D:



Public Member Functions

- **Point3D** (const double x, const double y, const double z)
- **Point3D** (const double y, const double z)
- **Point3D operator-** () const
- **Vector3D operator-** (const [Point3D](#) &p) const
- **Point3D operator+** (const [Vector3D](#) &v) const
- **Point3D operator-** (const [Vector3D](#) &v) const
- **Point3D operator*** (const double a) const
- bool **operator==** (const [Point3D](#) &p) const
- double **distance** (const [Point3D](#) &p) const
- double **x** () const
- double **y** () const
- double **z** () const

- void **rotate_Z** (const double angle)
- void **rotate_X** (const double angle)
- void **translate_Z** (const double height)

Friends

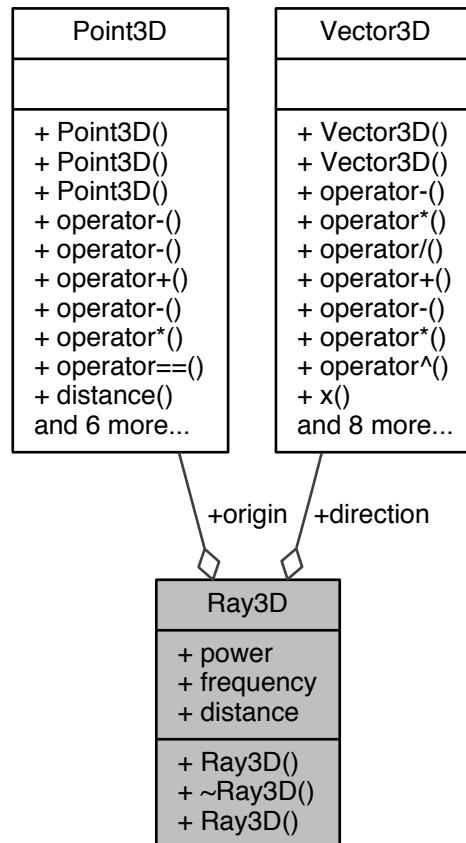
- void **swap** ([Point3D](#) &a, [Point3D](#) &b)

The documentation for this class was generated from the following files:

- Raytracer3D/Raytracer3D/Point3d.hpp
- Raytracer3D/Raytracer3D/Point3d.cpp

B.4 Ray3D Class Reference

Collaboration diagram for Ray3D:



Public Member Functions

- **Ray3D** (const [Point3D](#) &origin, const [Vector3D](#) &direction, const double power=1.0, const double frequency=0.0, const double distance=0)

Public Attributes

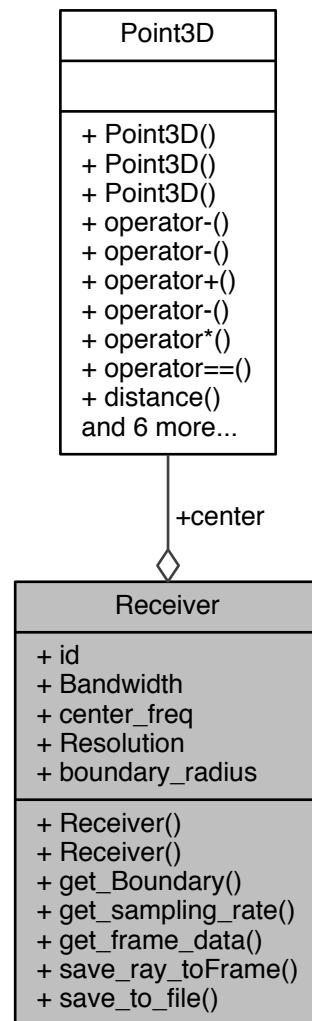
- `Point3D origin`
- `Vector3D direction`
- `double power`
- `double frequency`
- `double distance`

The documentation for this class was generated from the following files:

- Raytracer3D/Raytracer3D/Ray3d.hpp
- Raytracer3D/Raytracer3D/Ray3d.cpp

B.5 Receiver Class Reference

Collaboration diagram for Receiver:



Public Member Functions

- **Receiver** (const int id, const double Bandwidth, const double center_freq, const [Point3D](#) ¢er, const double boundary_radius, const std::string &savefile_name,

- ```
const std::string &dopplerfile_name)
```
- **Sphere get\_Boundary ()**
  - **double get\_sampling\_rate ()**
  - **std::vector< Ray3D > get\_frame\_data ()**
  - **void save\_ray\_toFrame (Ray3D &ray)**
  - **void save\_to\_file ()**

## Public Attributes

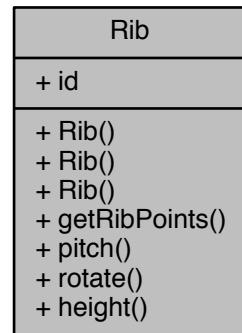
- **int id**
- **double Bandwidth**
- **double center\_freq**
- **double Resolution**
- **double boundary\_radius**
- **Point3D center**

The documentation for this class was generated from the following files:

- Raytracer3D/Raytracer3D/Receiver.hpp
- Raytracer3D/Raytracer3D/Receiver.cpp

## B.6 Rib Class Reference

Collaboration diagram for Rib:



### Public Member Functions

- **Rib** (int id, [Rib](#) &x, const double delta\_l)
- **Rib** (int id, const std::string &filename)
- std::vector< [Point3D](#) > **getRibPoints** ()
- void **pitch** (double angle)
- void **rotate** (double angle)
- void **height** (const double height)

### Public Attributes

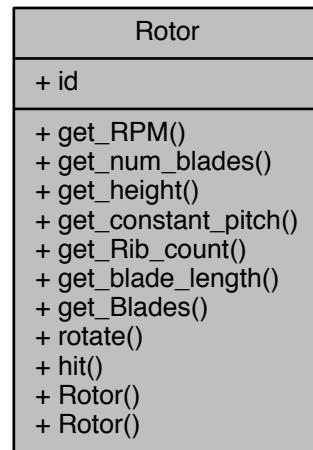
- int **id**

The documentation for this class was generated from the following files:

- Raytracer3D/Raytracer3D/Rib.hpp
- Raytracer3D/Raytracer3D/Rib.cpp

## B.7 Rotor Class Reference

Collaboration diagram for Rotor:



### Public Member Functions

- double **get\_RPM** ()
- int **get\_num\_blades** ()
- double **get\_height** ()
- double **get\_constant\_pitch** ()
- double **get\_Rib\_count** ()
- double **get\_blade\_length** ()
- std::vector< [Blade\\_surface](#) > **get\_Blades** ()
- void **rotate** (const double angle)
- bool **hit** (const [Ray3D](#) &ray, double &hitDistance, [Vector3D](#) &hitNormal, [Point3D](#) &hitPoint)
- **Rotor** (const int id, const int num\_blades, const double RPM, const double height, const double constant\_pitch, const double blade\_length, const int Rib\_count)

## Public Attributes

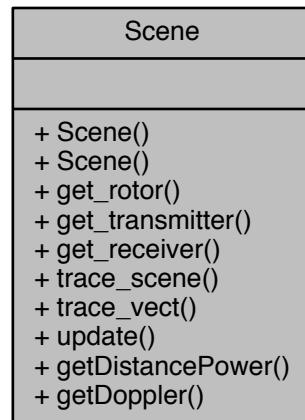
- int **id**

The documentation for this class was generated from the following files:

- Raytracer3D/Raytracer3D/Rotor.hpp
- Raytracer3D/Raytracer3D/Rotor.cpp

## B.8 Scene Class Reference

Collaboration diagram for Scene:



### Public Member Functions

- **Scene** (double rx\_x, double rx\_y, double rx\_z, double Bandwidth, double rx\_fc, double tx\_x, double tx\_y, double tx\_fc, double tx\_power, int num\_blades, double RPM, double altitude, double pitch, double blade\_length, int num\_ribs, const std::string &filename)
- **Rotor** **get\_rotor** ()
- **Transmitter** **get\_transmitter** ()
- **Receiver** **get\_receiver** ()
- void **trace\_scene** (int num\_rays)
- void **trace\_vect** ([Ray3D](#) &test\_ray, double &hitDistance, [Vector3D](#) &hitNormal, [Point3D](#) &hitPoint)
- void **update** (double angle)
- double **getDistancePower** (const double frequency, const double power, const double distance) const

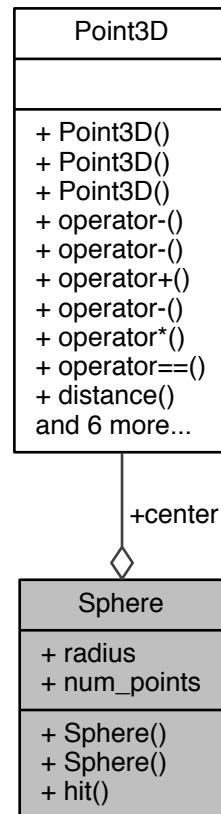
- double getDoppler (Ray3D &test\_ray, Vector3D &hitNormal, Point3D &hitPoint, double RPM) const

The documentation for this class was generated from the following files:

- Raytracer3D/Raytracer3D/Scene.hpp
- Raytracer3D/Raytracer3D/Scene.cpp

## B.9 Sphere Class Reference

Collaboration diagram for Sphere:



### Public Member Functions

- **Sphere** (const double radius, const [Point3D](#) &center)
- bool **hit** (const [Ray3D](#) &ray, double &hitDistance, [Vector3D](#) &hitNormal, [Point3D](#) &hitPoint) const

## Public Attributes

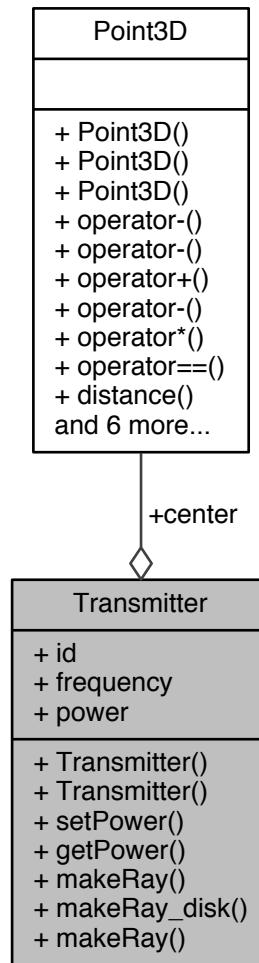
- double **radius**
- [Point3D](#) **center**
- int **num\_points**

The documentation for this class was generated from the following files:

- Raytracer3D/Raytracer3D/Sphere.hpp
- Raytracer3D/Raytracer3D/Sphere.cpp

## B.10 Transmitter Class Reference

Collaboration diagram for Transmitter:



### Public Member Functions

- **Transmitter** (const int id, const double frequency, const double power, const [Point3D](#) &center, const double l)
- void **setPower** (const double power)

- double **getPower** () const
- Ray3D **makeRay** ()
- Ray3D **makeRay\_disk** (const double height)
- Ray3D **makeRay** (const Vector3D &rayDirection)

## Public Attributes

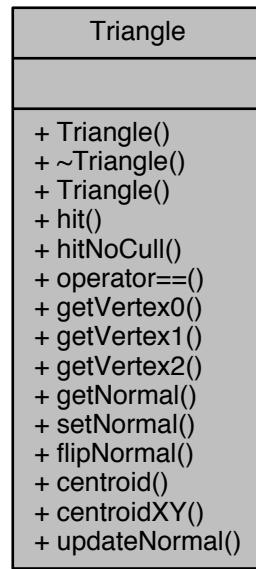
- int **id**
- double **frequency**
- Point3D **center**
- double **power**

The documentation for this class was generated from the following files:

- Raytracer3D/Raytracer3D/Transmitter.hpp
- Raytracer3D/Raytracer3D/Transmitter.cpp

## B.11 Triangle Class Reference

Collaboration diagram for Triangle:



### Public Member Functions

- **Triangle** (`Point3D &v0, Point3D &v1, Point3D &v2`)
- bool **hit** (const `Ray3D` &ray, double &hitDistance, `Vector3D` &hitNormal, `Point3D` &hitPoint) const
- bool **hitNoCull** (const `Ray3D` &ray, double &hitDistance, `Vector3D` &hitNormal, `Point3D` &hitPoint) const
- bool **operator==** (`Triangle` &Tri)
- `Point3D` **getVertex0** ()
- `Point3D` **getVertex1** ()
- `Point3D` **getVertex2** ()
- `Vector3D` **getNormal** () const

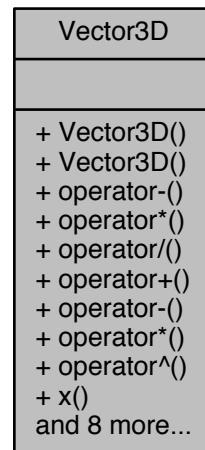
- void **setNormal** (const [Vector3D](#) &normal)
- void **flipNormal** ()
- [Point3D](#) **centroid** () const
- [Point3D](#) **centroidXY** () const
- void **updateNormal** ()

The documentation for this class was generated from the following files:

- Raytracer3D/Raytracer3D/Triangle.hpp
- Raytracer3D/Raytracer3D/Triangle.cpp

## B.12 Vector3D Class Reference

Collaboration diagram for Vector3D:



### Public Member Functions

- **Vector3D** (const double x, const double y, const double z)
- **Vector3D operator-** (void) const
- **Vector3D operator\*** (const double a) const
- **Vector3D operator/** (const double a) const
- **Vector3D operator+** (const **Vector3D** &v) const
- **Vector3D operator-** (const **Vector3D** &v) const
- double **operator\*** (const **Vector3D** &b) const
- **Vector3D operator^** (const **Vector3D** &v) const
- double **x** () const
- double **y** () const
- double **z** () const
- double **dotProduct** (const **Vector3D** &v) const

- `Vector3D crossProduct (const Vector3D &v) const`
- `double length () const`
- `Vector3D normalized () const`
- `Vector3D rotatedAboutZ (const double angle) const`
- `bool isNormal () const`

The documentation for this class was generated from the following files:

- Raytracer3D/Raytracer3D/Vector3d.hpp
- Raytracer3D/Raytracer3D/Vector3d.cpp

# Bibliography

- [1] Yimin Zhang, M. Amin, and V. Mancuso, “On the effects of rotating blades on DS/SS communication systems,” in *Proceedings of the Tenth IEEE Workshop on Statistical Signal and Array Processing (Cat. No.00TH8496)*. IEEE, 2000, pp. 682–686. [Online]. Available: <http://ieeexplore.ieee.org/lpdocs/epic03/wrapper.htm?arnumber=870213>
- [2] B. D. Bullard and P. C. Dowdy, “Pulse Doppler Signature of a Rotary-Wing Aircraft,” *IEEE Aerospace and Electronic Systems Magazine*, vol. 6, no. 5, pp. 28–30, 1991.
- [3] J. Misiurewicz, “Analysis of recorded helicopter echo,” in *Radar Systems (RADAR 97)*, vol. 1997. IEE, 1997, pp. 449–453. [Online]. Available: <http://digital-library.theiet.org/content/conferences/10.1049/cp{ }19971715>
- [4] T. Thayaparan, S. Abrol, E. Riseborough, L. Stankovic, D. Lamothe, and G. Duff, “Analysis of radar micro-Doppler signatures from experimental helicopter and human data,” *IET Radar, Sonar & Navigation*, vol. 1, no. 4, p. 289, 2007. [Online]. Available: <http://digital-library.theiet.org/content/journals/10.1049/iet-rsn{ }20060103>
- [5] Naval Air Systems Command, *Electronic Warfare and Radar Systems Engineering Handbook*, 1999, no. April 1997.

- [6] F. L. F. Barbiero, F. Vincent, T. Deloues, "Effects of Rotor Blade Modulation on GNSS Array Antenna Anti-jamming Algorithms," in *Proceedings of the 2014 International Technical Meeting of The Institute of Navigation, San Diego, California, January 2014*, 2014.
- [7] T. Whitted, "An improved illumination model for shaded display," *ACM SIGGRAPH Computer Graphics*, vol. 13, no. 2, p. 14, aug 1979. [Online]. Available: <http://portal.acm.org/citation.cfm?doid=965103.807419>
- [8] H. L. Bertoni, *Radio Propagation for Modern Wireless Systems*. Upper Saddle River, NJ.: Prentice Hall PTR, 1999.
- [9] J. D. Parsons, *The Mobile Radio Propagation Channel*. Chichester, UK: John Wiley & Sons, Ltd, 2000. [Online]. Available: <http://doi.wiley.com/10.1002/0470841524>
- [10] N. J. Willis, *Bistatic radar*. SciTech Publishing, 2005. [Online]. Available: <http://app.knovel.com/mlink/toc/id:kpBR000005/bistatic-radar/bistatic-radar>
- [11] H. Sizun, *Radio Wave Propagation for Telecommunication Applications*, ser. Signals and Communication Technology. Berlin/Heidelberg: Springer-Verlag, 2005. [Online]. Available: <http://link.springer.com/10.1007/b137896>
- [12] K. Suffern, *Ray Tracing from the Ground Up*. Wellesley, Mass: A K Peters, 2007, vol. 1.
- [13] M. Pharr and G. Humphreys, "Monte Carlo Integration I: Basic Concepts," in *Physically Based Rendering*. Elsevier, 2010, pp. 636–676. [Online]. Available: <http://linkinghub.elsevier.com/retrieve/pii/B9780123750792500135>
- [14] A. S. Glassner, "Principles of Digital Image Synthesis," p. 1377, 1995.
- [15] B. T. Phong, "Seminal graphics." New York, NY, USA: ACM, 1998, ch. Illumination for Computer Generated Pictures, pp. 95–101. [Online]. Available: <http://doi.acm.org/10.1145/280811.280980>
- [16] E. H. de Groot, "Transmitter localization by virtual multipath correlation," 2015, copyright - Database copyright ProQuest LLC; ProQuest does not claim

copyright in the individual underlying works; Last updated - 2016-06-14.  
[Online]. Available: <http://ezproxy.library.arizona.edu/login?url=http://search.proquest.com.ezproxy2.library.arizona.edu/docview/1759037361?accountid=8360>