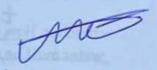
Unit operation I

Diffusion

Sheet No. (1)



Q1) A gas is being transferred a cross a stagnant air film at total pressure of 100 kPa. The partial pressure of the gas is 40 kPa at one boundary of the film and 10 kPa at the other. If the partial pressure remains constant, calculate the total pressure to double the transfer rate of the gas.

Answer: PT = 64 kPa

Q2) In a packed column operating at <u>atmospheric pressure</u> and 295 K, 10% ammonia – air mixture is scrubbed with water and the concentration is reduced to 0.1%. If the whole of the resistance to mass transfer may be regarded as lying within a thin laminar film on the gas side of the gas liquids interface, drive from the first principle an expression for the rate of absorption at any position in the column. At some intermediate point where the ammonia's concentration in the gas phase has been reduced to 5%, the partial pressure of ammonia is in equilibrium with the aqueous solution is 660 N/m², and the transfer flux is 10⁻³ kgmol/m².s. What is the thickness of the hypothetical gas film if the diffusivity of ammonia in air is 0.24 cm²/s?

Answer: Z= 0.043 mm.

column, the value of KG was found to be 2.75×10⁻⁶ kmol/m² s-kPa. At one point in the column, the composition of the gas and liquid phases were 8.0 and 0.115 mole % NH₃, respectively. The temperature was 300 K and the total pressure was 1 atm. Eighty-five percent of the total resistance to mass transfer was found to be in the gas phase. At 300 K, ammonia-water solution follow Henry's law up to 5 mole % ammonia in the liquid, with H = 1.64 when the total pressure is 1 atm. Calculate the individual film coefficients and the interfacial concentrations.

 $YA_1 \Rightarrow XA_1$ Answers: $K_g = 3.28 \times 10^{-4} \text{ kmol/m}^2 \cdot \text{s}$, $K_L = 3.05 \times 10^{-3} \text{ kmol/m}^2 \cdot \text{s}$, $V_A = 1.886 \times 10^{-3}$

 $N_A = 2.18 \times 10^{-5} \text{ kmol/m}^2 \cdot \text{s}, \quad y_{Ai} = 0.01362, \quad x_{Ai} = 8.305 \times 10^{-3}$

Q4) A chamber, of volume 1 m³, contains air at a temperature of 293 K and a pressure of 101.3 kN/m², with a partial pressure of water vapour of 0.8 kN/m². A bowl of liquid with a free surface of 0.01 m² and maintained at a temperature of 303 K is introduced into the

chamber. How long will it take for the air to become 90% saturated at 293 K and how much water must be evaporated?

The diffusivity of water vapour in air is 2.4 * 10⁻⁵ m²/s and the mass transfer resistance is equivalent to that of a stagnant gas film of thickness 0.25 mm. Neglect the effects of but flow. Saturation vapour pressure of water is 4.3 kN/m² at 303 K and 2.3 kN/m² at 293 K

Answers: mass_{H20} = 9.38 * 10⁻³ kg,

= 604 s

Stagnant layer PTI=100KPa

PAI = 40 KPa Constant in second PTZ=? If NAZ=2 NAZ

PAZ = 10 KPZ Condition

For NAI!-

for NA2 !-

NA2 = 2 NA1

divide eq.1 in eq.2 !-

$$\frac{AAI}{2NAI} = \frac{PTz * PABZ}{2RT} * In \frac{PT_1 - PAZ}{PT_1 - PAI}$$

$$\frac{1}{2} = \frac{DABZ * PTZ}{DABZ * PTZ} * In \frac{PT_2 - PAZ}{PT_1 - PAZ}$$

$$\frac{1}{2} = \frac{DABZ * PTZ}{DABZ * PTZ} * In \frac{PT_2 - PAZ}{PT_2 - PAZ}$$

However

$$DAB_{2} \propto \frac{1}{PT_{1}} = DAB_{2} \propto \frac{1}{PT_{2}}$$
 $DAB_{2} = \frac{B}{PT_{2}} = DAB_{2} = \frac{B}{PT_{2}}$

$$\frac{D_{AB2}}{D_{AB2}} = \frac{B'/PT_2}{B'/PT_2} \longrightarrow \frac{D_{AB2}}{D_{AB2}} = \frac{PT_2}{PT_2}$$



sub eq.4 in eq.3 for DAB2;-

$$\frac{1}{2} = \frac{DAB_{1}*P_{1}}{DAB_{1}*P_{1}*P_{2}} * \frac{\left|h\right| \frac{Pr_{1}-PA_{2}}{Pr_{1}-PA_{1}}}{\left|h\right| \frac{Pr_{2}-PA_{2}}{Pr_{2}-PA_{1}}}$$

$$\frac{1}{2} = \frac{\ln \frac{P_{12} - P_{A2}}{P_{12} - P_{A2}}}{\ln \frac{P_{12} - P_{A2}}{P_{12} - P_{A2}}} \rightarrow \frac{1}{2} = \frac{\ln \frac{200 - 20}{200 - 40}}{\ln \frac{P_{12} - 20}{P_{12} - 40}}$$

$$0.5 = \frac{0.4054651081}{\ln \frac{Pr_2 - 10}{Pr_2 - 40}} \rightarrow \ln \frac{Pr_2 - 10}{Pr_2 - 40} = \frac{0.4054651081}{0.5}$$

$$n \frac{PT_2 - 10}{PT_2 - 40} = 0.8209302162$$



$$V_{A1}=0.05$$
 $T=295k$ $P_{T}=2013kPa$
 $P_{A2}=660N_{m}^{6}*\frac{1.P_{E}}{1.N_{m}^{2}}*\frac{1kPa}{1000Pa}=0.66kPa$
 $V_{A}=10^{-3}kgmol/m^{2}s$ V

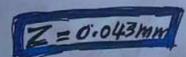
plug eq.(2) in eq.(2) for Vi-

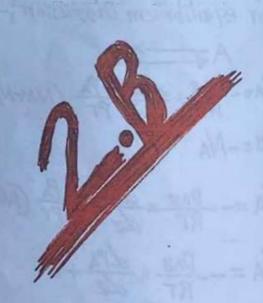
derivative for CA = PA/RT

for equilibrium Dissusion |-

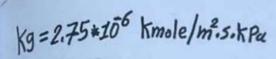


$$Z = \frac{0.24 \times 20^{-4}}{10^{3} \times 8.314 \times 295} * (5.0665 - 0.66)$$





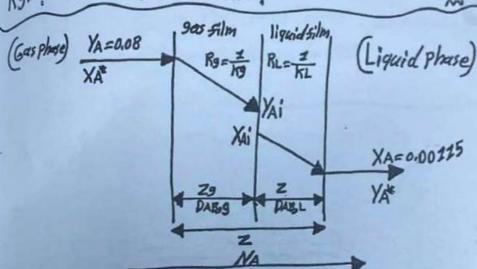
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1 = 0.08 NH3 T=300K

XA=0.00115 NH3 PT=Iatm + 10137 KPa = 101.33 KPa

kg=0.85k06 so KL=0.25k06 H=1.64



KOG=K9*PT- KOG=2.75*10 * 101.33 = 2.786575 * 20 4 Kmole/mis

$$\frac{1}{k9} = 0.85 \frac{1}{k06} \rightarrow \frac{1}{k9} = 0.85 \times \frac{1}{2.78657545} \rightarrow k9 = \frac{2.78657545}{0.85} \rightarrow k9 = \frac{3.28457545}{0.85}$$

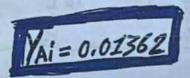
NA=KOG (YA-YA)

NA = 2786575 * 10 4 (0.08-1.886 * 103)

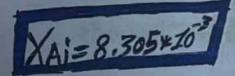
NA= 2,176705196*105 Kmal/mis



$$V_{A}=k_{9}*(Y_{A}-Y_{Ai})$$
 $V_{A}-Y_{Ai}=\frac{N_{A}}{k_{9}} \rightarrow (-Y_{Ai}=\frac{N_{A}}{k_{9}}-Y_{A})*-1 \rightarrow Y_{Ai}=Y_{A}-\frac{N_{A}}{k_{9}}$
 $V_{Ai}=0.08-\frac{2.176705196*20^{5}}{3.28*10^{4}}$



$$X_{Ai} = \frac{Y_{Ai}}{H}$$



chamber $V=1m^{3}$ I=293K $P1=101.3 \text{ KN/m}^{2} * \frac{1 \text{ KR}_{2}}{1 \text{ KN/m}^{2}} = 101.3 \text{ KR}_{2}$ $PA1=0.8 \text{ KN/m}^{2} * \frac{2 \text{ KR}_{2}}{1 \text{ KN/m}^{2}} = 0.8 \text{ KR}_{2}$

Neglet the effect of bulk slow $PA^{\dagger}_{A} = 4.3 \text{ KN/m}^{2} \times \frac{2kPu}{2kN/m^{2}} = 4.3 \text{ KPu at } T = 303 \text{ K}$ $PA^{\dagger}_{A2} = 2.3 \text{ KN/m}^{2} \times \frac{1kPu}{2kN/m^{2}} = 2.3 \text{ KPu at } T = 293 \text{ K}$

Bowl

#

A = 0.07 m2 T=303 K

t=? massH20=? Is %90 saturated

DAB=2.4×20 m²/s

Z=0.25 mm 10000 mm = 0,00025m

NA=JA+CAV

NA = - DAB dCA + CAV

Neglet the effect of bulk slow 50

HA = - DAB dca + CAV

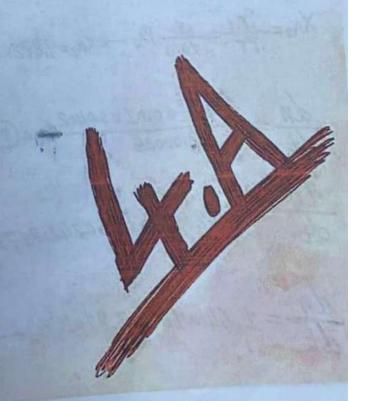
NA = - DAB dea

NA dz = -DAB dCA

NASdz = - DABS dCA

NA Sdz = DAB SdCA

NA*Z = DAB (CAI-CAZ)



$$N_{A} = \frac{D_{AB}}{Z} \quad (C_{A1} - C_{A2})$$

$$X_{A7} = \frac{C_{A1}}{C_{T}} \rightarrow C_{A1} = X_{A1} * C_{T}$$

$$PV=NRT \rightarrow P = \frac{n}{V}RT \rightarrow PT=CTRT \rightarrow CT = \frac{PT}{RT} \rightarrow GT = \frac{1013}{8.3448303}$$

CT=0.0402 Kmol/m3 at 303 K

$$X_{A1} = \frac{P_{A1}^2}{P_T} = \frac{4.3}{2023} = 0.04244817374$$

$$\frac{dn}{dt} = \frac{2.4 \times 70^{5} \pm 0.01 \times 0.0402}{0.00025} \times (0.04244817374 - 9.872408^{3} PA2)$$

for the room !-PIVI = Ps Vs NIRTI = Ps Vs Ts Ps * Vs Ts let Pi=PAz NI= PAZKVI*H5*T5 - NI = PAZ* I* 1*273

NI = PAZ* V5*TI - NI = PAZ* I* 1*273

ZOI.3* 22:4*293 11=4.10676026*10*PA2 Derivation over dt dn = 4,10676026*10 + dPA sub eq. 2 in eq. 3 4.10676026*10 4 dPA2=1.64*10-3.81*10 PA2 +3.81*107 1077.889832 dPAZ= (4.3-PAZ) (43-PA2) = 1 (43-PA2) = 1077.889832 dt Phy 1 413-Phz dA #-1 = 9.277385966*1045dt -5 -1 dPA = 9.277389166*20 4 3 dt -[n(4,3-PA2)-|n(4,3-PA)] = 9,277385966 \$10 \$t - [In (4.3-2.3) - In (4.3-0.8)] = 9.27-73859664564 $t = -\ln \frac{4.3 - 2.3}{4.3 - 0.8}$ 9.277385966*16*

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For the room !
PT*VT=NTRT->NT= PT*VT -> NT = 101.381 -> NT=0.04.16 kmole

VI = PAI -> VI = 0.8 -> VI = 7.9 * 103

Y1= N1H20 -> 11, H20= YI*NT->N1H20=7.9*10 *0.0416 -> 17, H20=3.2864*10 Karole

 $Y_2 = \frac{P_{AE}^*}{P_T} = \frac{2.3}{101.3} = 0.0227$

Y2= N2H20=Y2*NT*5 -> N2H20=0.0227*0.0416*0.9

(n2 H20 = 8.5 * 10 4 kmole)

h Water evaporate = niHzo-hzHzo

NWater evaporate = 8.5 × 10 4= 3,2864 × 10 4 = 5,2136 × 10 4 Kgmole

Masswater exaporate = MiWitto x Mwater exaporate

Mass water evaporate = 18 x 5,2136 x 10 4

Mass water experience 9,38 = 10 kg

