

# Rotating Magnetic Fields

## 3 ways to generate voltage

- rotate windings through a magnetic field (DC machines)
- rotate magnetic field past windings (Synchronous machines)
- make the reluctance varying with rotation of the rotor (Synchronous reluctance machines)

## armature windings: which carries ac currents

## Synchronous machines

- keyword: Faraday's law:  $E_a = d\lambda/dt$
- the number of coil poles is equal to the number of rotor poles
- salient-pole vs cylindrical-rotor
  - salient
    - low speed (because it need large number of poles  $w = 120f_e/P$ ) example: hydroelectric
    - concentrated windings
    - reluctance is sinusoidal ( $\text{flux} = N_i/R_m$ )
  - cylindrical
    - high speed (low number of poles) example: steam/ gas turbines
    - distributed windings
    - $N_i$  is designed to be sinusoidal

## Induction machines

- keyword: transformer action
- IM vs SM
  - rotating speed of rotor is different
  - armature windings of IM are on the rotor, for SM on stator
  - IM are usually used as motor while SM are mostly generator — exceptions: 1. use SMs as motor if need high power 2. wind turbine power plant is IM

## DC machines

- keyword:  $F = BIL \sin \alpha$
- armature windings are on rotor- alternating voltage is rectified by commutators and brushes
- electromagnetic torque: due to amature reaction, fixed (in space) rotor flux interacts with field flux — generating mode:  $T_{em}$  opposes rotation; motoring mode:  $T_{em}$  in the dirction of rotation

## MMF of concentrated windings

- shape: rectangular — how to get it: Ampere's law and Guass's law (average value is 0)
- problem: using Fourier series to get fundamental harmonic will introduce high order harmonics

## MMF of distributed windings

- shape: stair with a flat top — introduce a winding factor in mmf function
- advantage: minimize high order harmonics — in rotor windings, the number of turns per slot is independent from other slots, so they are varied to control high order harmonics
- for DC machines
  - shape: sawtooth waveform (without flat tops)
  - current density is rectangular waveform

## MMF of a single-phase winding on stator

- shape: fixed in space but its amplitude varies sinusoidally in time
  - fixed in space: winding function
  - varied amplitude:  $i_a = \cos \omega t$
- it can be divided into a positive travelling wave and a negative travelling wave — problem: negative wave introduces negative torque and losses

## MMF of stator windings of 3-phase machines

- shape: rotates at synchronous speed with a constant amplitude  $3^{1/2} \text{MMF}_{\max}$
- the sum of negative travelling waves of 3 phases is 0

## Calculate induced voltage

- flux  $\phi$ -flux linkage  $\lambda$ -Farady's law
- $L_{ss}, L_{sr}, L_{rr}, \lambda_s, \lambda_r$ , transformer voltage, speed voltage
  - when the airgap is uniform,  $L_{ss}$  and  $L_{rr}$  are constant
    - Torque results only from mutual inductance
    - For three phase case, if the rotor speed is sychronous, torque is constant, depending on torque angle  $\delta$
  - when the rotor is salient,  $L_{ss}$  also depends on the rotor position

## Calculate torque

- $T = -f(\text{ploes}, 1/g) * F_s * F_r \sin \delta_{sr}$  — EM torque is proportional to the peak values of the stator- and rotor-mmf and to the electrical space-phase angle  $\delta_{sr}$
- if  $F_s$  is perpendicular to  $F_r$ , one can produce maximum  $T_{em}$
- when  $F_r$  leads  $F_s$  ( $\delta_{sr} > 0$ ),  $T_{em} < 0$ , generating mode