



Shigley's Mechanical Engineering Design | (10th Edition)

Chapter 14, Problem 22P

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Problem

A spur gearset has 17 teeth on the pinion and 51 teeth on the gear. The pressure angle is 20 and the overload factor $k_0 = 1$. The diametral pitch is 6 teeth/in and the face width is 2 in. The pinion speed is 1120 rev/min and its cycle life is to be 10^8 revolutions at a reliability $R = 0.99$. The quality number is 5. The material is a through-hardened steel, grade 1, with Brinell hardnesses of 232 core and case of both gears. For a design factor of 2, rate the gearset for these conditions using the AGMA method.

Step-by-step solution

Step 1 of 17

Obtain the following properties for pinion from the figure 14-6 "spur gear geometry factors J".

$$N_p = 17T, J_p = 0.292$$

Obtain the following properties for gear from the figure 14-6 "spur gear geometry factors J".

$$N_G = 51T, J_G = 0.396$$

[Comment](#)

Step 2 of 17

Find the diameter of pinion using the equation.

$$d_p = \frac{N_p}{P_d}$$

Here, N_p is the pinion tooth and P_d is the diametral pitch.

Substitute 6 teeth/in for P_d and 17 for N_p .

$$\begin{aligned} d_p &= \frac{17}{6} \\ &= 2.833 \text{ in} \end{aligned}$$

Find the diameter of gear using the equation.

$$d_G = \frac{N_G}{P_d}$$

Here, N_G is the gear tooth and P_d is the diametral pitch.

Substitute 6 teeth/in for P_d and 51 for N_G .

$$\begin{aligned} d_G &= \frac{51}{6} \\ &= 8.5 \text{ in} \end{aligned}$$

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Step 3 of 17

Find the velocity using the equation.

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Substitute 1120 rev/min for n and 2.833 in for d_p .

$$\begin{aligned} V &= \pi \times 2.833 \times 1120 \\ &= 9968.147 \text{ in/min} \\ &= 830.7 \text{ ft/min} \end{aligned}$$

[Comment](#)

Step 4 of 17

Assume constant thickness of the gears.

$$K_B = 1$$

Assume uniform loading.

$$k_o = 1$$

Find the value of B using the equation.

$$\begin{aligned} B &= 0.25(12 - Q_v)^{\frac{2}{3}} \\ &= 0.25(12 - 5)^{2/3} \\ &= 0.9148 \end{aligned}$$

Here, Q_v is quality number.

Find the value of A using the equation.

$$\begin{aligned} A &= 50 + 56(1 - B) \\ &= 50 + 56(1 - 0.9148) \\ &= 54.77 \end{aligned}$$

[Comment](#)

Step 5 of 17

Find the dynamic factor using the equation.

$$K_v = \left(\frac{A + \sqrt{V}}{A} \right)^B \text{ when } V \text{ in ft/min}$$

Substitute 0.9148 for B and 54.77 for A .

$$\begin{aligned} K_v &= \left(\frac{54.77 + \sqrt{830.7}}{54.77} \right)^{0.9148} \\ &= 1.472 \end{aligned}$$

From elastic coefficient C_p

$$C_p = 2300\sqrt{\text{psi}}$$

[Comment](#)

Step 6 of 17

Consider pinion bending

Obtain SI equation from figure of 14-3 "allowable bending stresses number through hardened steels" for grade-1.

The SI equations is

$$\begin{aligned} S_f &= 77.3H_B + 12800 \\ &= 77.3(232) + 12800 \\ &= 30734 \text{ psi} \end{aligned}$$



Stress-cycle factor for bending,

$$\begin{aligned}
 Y_N &= 1.6831(N)^{-0.0323} \\
 &= 1.6831(10^8)^{-0.0323} \\
 &= 0.928
 \end{aligned}$$

[Comment](#)

Step 7 of 17

Find the allowable stress

$$\sigma_{all} = \frac{S_t Y_N}{S_F K_T K_R}$$

Here, S_F is the AGMA factor of safety, K_T is temperature factor and K_R is the reliability factor.

Substitute 0.928 for Y_N , 30734 psi for S_t , 2 for S_F , 1 for K_T and 1 for K_R .

$$\begin{aligned}
 \sigma_{all} &= \frac{30734(0.928)}{2(1)(1)} \\
 &= 14261 \text{ psi}
 \end{aligned}$$

[Comment](#)

Step 8 of 17

Obtain the Lewis form factor for pinion from the table of 14-2 "values of the Lewis Form Factor Y (These values are for a normal pressure Angle of 20° , Full depth Teeth and a diametral Pitch of unity in the Plane of Rotation)" at number of teeth of pinion is 17.

Lewis form factor for pinion, $Y_p = 0.303$

Obtain the Lewis form factor for gear from the table of 14-2 "values of the Lewis form factor Y (These values are for a normal pressure Angle of 20° , Full depth Teeth and a diametral Pitch of unity in the Plane of Rotation)" at number of teeth of gear is 51.

Lewis form factor for gear, $Y_G = 0.4103$

[Comment](#)

Step 9 of 17

Find the size factor for pinion using the equation.

$$(K_s)_p = 1.192 \left(\frac{F \sqrt{Y_p}}{p} \right)^{0.0535}$$

Here, F is the face width.

Substitute 2 in for F and 0.303 for Y_p .

$$\begin{aligned}
 (K_s)_p &= 1.192 \left(\frac{2\sqrt{0.296}}{6} \right)^{0.0535} \\
 &= 1.088
 \end{aligned}$$

Find the size factor for gear using the equation.

$$\begin{aligned}
 (K_s)_G &= 1.192 \left(\frac{F \sqrt{Y_G}}{p} \right)^{0.0535} \\
 &= 1.192 \left(\frac{2\sqrt{0.4103}}{6} \right)^{0.0535} \\
 &= 1.097
 \end{aligned}$$



Step 10 of 17

Find the load distribution factor using the equation.

$$K_m = C_{mf} \\ = 1 + C_{mc} (C_{pf} C_{pm} + C_{ma} C_e)$$

Here,

C_{mf} is load distribution factor

$$C_{mc} = \begin{cases} 1 & \text{for uncrowned teeth} \\ 0.8 & \text{for crowned teeth} \end{cases}$$

$$C_{pf} = \begin{cases} \frac{F}{10d} - 0.025 & F \leq 1 \text{ in} \\ \frac{F}{10d} - 0.0375 + 0.0125F & 1 \leq F \leq 17 \text{ in} \\ \frac{F}{10d} - 0.1109 + 0.0207F - 0.000228F^2 & 17 \leq F \leq 40 \text{ in} \end{cases}$$

$$C_{pm} = \begin{cases} 1 & \text{for straddle mounted pinion with } S1/S < 0.175 \\ 1.1 & \text{for straddle mounted pinion with } S1/S \geq 0.175 \end{cases}$$

$C_{ma} = A + BF + CF^2$ Where A, B, C are Empirical constants

$$C_e = \begin{cases} 0.8 & \text{for gearing adjusted assembly} \\ 1 & \text{for all other conditions} \end{cases}$$

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Step 11 of 17

Find the following values.

$$C_{pf} = \frac{F}{10d} - 0.0375 + 0.0125F \\ = \frac{2}{10(2.833)} - 0.0375 + 0.0125(2) \\ = 0.0581$$

$$C_{mc} = 1$$

$$C_{pm} = 1$$

$$C_{ma} = A + BF + CF^2 \\ = 0.127 + 0.0158(2) - 0.093(10^{-4})(2^2) \\ = 0.1586$$

$$C_e = 1$$

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Step 12 of 17

Substitute 0.1586 for C_{ma} , 1 for C_{pm} , 1 for C_{mc} , and 1 for C_e in equation (1).

$$K_m = C_{mf} \\ = 1 + C_{mc} (C_{pf} C_{pm} + C_{ma} C_e) \\ = 1 + 1[0.0581(1) + 0.1586(1)] \\ = 1.2167$$

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Find the load acting using the equation.

$$W' = \frac{F J_p \sigma_{all}}{K_o K_v (K_s)_p P_d K_m K_B}$$

Substitute 1 for K_B , 1 for K_o , 1.2167 for K_m , 2 in for F , 0.292 for J_p , 14261 psi for σ_{all} , 1.088 for $(K_s)_p$.

$$W' = \frac{2(0.292)(14261)}{1(1.472)(1.088)(6)(1.2167)(1)} \\ = 712 \text{ lbf}$$

Find the horse power required using the equation.

$$H = \frac{W' V}{33000}$$

Substitute 712 lbf for W' and 830.7 ft/min.

$$H = \frac{775(830.7)}{33000} \\ = 17.92 \text{ hp}$$

[Comment](#)

Step 14 of 17

Consider the pinion wear

Obtain the stress cycle factor from figure of 14-15 "pitting resistance stress cycle" for 10^8 .

$$Z_N = 2.466 N^{-0.056} \\ = 2.466 (10^8)^{-0.056} \\ = 0.879$$

Find the gear ratio using the equation.

$$m_G = \frac{N_G}{N_P} \\ = \frac{51}{17} \\ = 3$$

[Comment](#)

Step 15 of 17

Find the geometry factor using the equation.

$$I = \frac{\cos \phi_t \sin \phi_t}{2 m_N} \left(\frac{m_G}{m_G + 1} \right)$$

Here, ϕ_t is the pressure angle.

Substitute 1 for m_N , and 3 for m_G .

$$I = \left[\frac{\sin 20^\circ \cos 20^\circ}{2(1)} \right] \left(\frac{3}{3 + 1} \right) \\ = 0.1205$$

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Step 16 of 17



$$\frac{H_{BG}}{H_{BG}} = C_H$$

$$= 1$$

Obtain the SI equation from figure of 14-5 "contact fatigue strength at 10^7 cycles and 0.99 reliability for steel gears" for grade 1.

$$(S_c) = 322(H_B) + 29100 \text{ psi}$$

$$= 322(232) + 29100$$

$$= 103804 \text{ psi}$$

[Comment](#)

Step 17 of 17

Find the allowable contact stress using the equation.

$$\sigma_{c,all} = \frac{S_c(Z_N)}{S_H(C_H)(I)}$$

Substitute 103804 psi for S_c , 0.879 for Z_N , 1 for C_H and $\sqrt{2}$ for S_H .

$$\sigma_{c,all} = \frac{103804(0.879)}{\sqrt{2}(1)(1)}$$

$$= 64519 \text{ psi}$$

Find the load acting using the equation.

$$W' = \left(\frac{\sigma_{c,all}}{C_p} \right)^2 \frac{F d_p I}{K_o K_v K_s K_m C_f}$$

Substitute 0.1205 for I , 64519 psi for $\sigma_{c,all}$, $2300\sqrt{\text{psi}}$ for C_p and 1 for C_f .

$$W' = \left(\frac{64519}{2300} \right)^2 \left[\frac{2(2.833)(0.1205)}{1(1.472)(1.088)(1.2167)(1)} \right]$$

$$= 275.71 \text{ lbf}$$

Find the horse power required using the equation.

$$H = \frac{W'V}{33000}$$

Substitute 275.71 lbf for W' and 830.7 ft/min.

$$H = \frac{W'V}{33000}$$

$$= \frac{275.71 \times 830.7}{33000}$$

$$= 6.94 \text{ hp}$$

From the values of rated horse power is minimum value controls the pinion.

$$H_{rated} = 6.94 \text{ hp}$$

Therefore, required rated horse power is **6.94 hp**.

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